

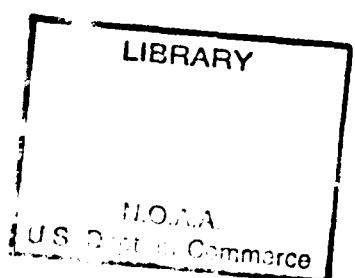
SOCIJALISTIČKA FEDERATIVNA REPUBLIKA JUGOSLAVIJA—RÉPUBLIQUE SOCIALISTE FÉDÉRATIVE DE YUGOSLAVIE
HIDROMETEOROLOŠKA SLUŽBA—SERVICE HYDROMÉTÉOROLOGIQUE

METEOROLOŠKI GODIŠNjak I

ANNUAIRE METEOROLOGIQUE I

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S A D R Ž A J

Strana

Objašnjenja

Azbučni spisak meteoroloških stanica	I
A) Dnevna osmatranja	1
B) Mesečni i godišnji pregled	99

TABLE DES MATIERES

Pages

Notice explicative

Liste alphabétique des stations météorologiques	I
A) Observations journalières	1
B) Revue mensuelle et annuelle	99

O B J A Š N J E N J A

Meteorološki godišnjak I ima dva dela: A) Dnevna osmatranja i B) Mesečni i godišnji pregled. U delu A) objavljuju se podaci 8 odabralih stanica, i to: Ljubljana-Bežigrad, Zagreb-Grič, Split-Marjan, Bjelašnica, Sarajevo, Beograd, Titograd i Skopje. U delu B) nalaze se podaci svih meteoroloških stanica osnovnih mreža.

Značenje upotrebljenih oznaka je sledeće:

φ = geografska širina, λ = geografska dužina od Griniča, ΔG vremenska razlika u odnosu na Grinič, H_s = nadmorska visina podnožja termometarskog zaklona, H_b = nadmorska visina rezervoara barometra, h_t = visina rezervoara termometra iznad tla, h_r = visina otvora kišomera iznad tla.

Oznake pojedinih elemenata su upotrebljene prema medjunarodnim konvencijama, a vrednosti su date u ovim jedinicama:

P = vazdušni pritisak u mm visine živinog stuba, reducirane na 0°C ; T = temperatura u $^{\circ}\text{C}$; e = pritisak vodene pare u mm visine živinog stuba; U = relativna vlažnost u procentima; D = pravac vetra po ruži vetra od 16 ili 8 pravaca; F = jačina vetra po Boforovoj skali (0-12); v = brzina vetra u m/sek; V = vidljivost u km; N = oblačnost (0-10); insolacija = trajanje osunčavanja u satima; R = padavine u mm; h_s = snežni pokrivač u cm; W = razvoj vremena (vrsta pojave, intenzitet i trajanje) opisan medjunarodnim simbolima.

U rubrici "razvoj vremena" su upotrebljene ove skraćenice:

n = u toku noći; rj = rano jutro; dp = do podne; pp = po podne, kv = kasno veče; i = s prekidima.

Srednje dnevne i mesečne vrednosti temperature vazduha izmerene u 7, 14, i 21 h po lokalnom vremenu računate su po formuli:

$$\frac{t_7 + t_{14} + 2 \times t_{21}}{4}$$

a za ostale elemente (P, e, U, N) srednje dnevne i mesečne vrednosti dobijene su kao proste aritmetičke sredine terminskih vrednosti.

Ekstremni termometri su očitavani i uredjivani u 21 h i vrednosti ubeležavane na dan merenja.

Dnevne vrednosti padavina se odnose na protekla 24 sata, od 7 h predhodnog dana do 7^h dana merenja u koji su zabeležene.

Visina snežnog pokrivača je merena u 7 h.

U tablicama A podvučene su vrednosti maksimuma vazdušnog pritiska, temperature vazduha, pritisaka vodene pare, jačine vetra kad ona iznosi najmanje 6 po Boforu, i padavina, kao i vrednosti minimuma vazdušnog pritiska, temperature vazduha, pritisaka vodene pare i relativne vlažnosti.

U tablicama B za srednje mesečne ekstremne temperature vazduha upotrebljene su oznake M_{ax} i M_{in} ; za rubrike broj dana sa ● ili ♀, ✕ ili ♂, i ✖ prebrojani su samo dani kad je visina naznačenih padavina iznosila najmanje 0.1 mm.

Broj stanica (kolona 2 Azbučnog spiska) je ustvari redni broj niza stanica sa podacima u tablicama dela B).

Na kraju knjige nalazi se karta SFRJ sa naznačenim klimatološkim stanicama u 1978 godini čiji brojevi odgovaraju brojevima stanicu sa podacima u tablicama B.

NOTICE EXPLICATIVE

L'Annuaire météorologique I a deux parties; A) Observations journalières et: B) Résumés mensuels et annuels. Dans la partie A) sont publiées les données de huit stations choisies, à savoir: Ljubljana-Bežigrad, Zagreb-Grič, Split-Marjan, Bjelašnica, Sarajevo, Beograd, Titograd et Skopje. Dans la partie B) figurent les données de toutes les stations météorologiques des réseaux de base.

La signification des symboles utilisés est la suivante:

φ = latitude, λ = longitude E de Greenwich, ΔG = différence entre l'heure locale et l'heure de Greenwich, H_s = altitude du pied de l'abri météorologique, H_b = altitude de la cuvette du baromètre, h_t = hauteur, au-dessus du sol, du réservoir du thermomètre, h_r = hauteur, au-dessus du sol, de l'ouverture de l'entonnoir du pluviomètre.

La désignation des éléments météorologiques particuliers sont conformes aux conventions internationales. Leur valeurs sont données en unités de mesure suivantes:

P = pression atmosphérique en mm (hauteur de la colonne de mercure réduite à 0°C); T = température en °C; e = tension de vapeur d'eau en mm de la hauteur de la colonne de mercure; U = humidité relative en %; D = direction du vent en rose des vents de 8 ou de 16 directions; F = force du vent d'après l'échelle Beaufort (0-12); v = vitesse du vent en m/s; V = visibilité en km; N = nébulosité (0-10); insolation = durée d'insolation en heures; R = = précipitations en mm; h_s = épaisseur de la couche de neige en cm; W = évolution du temps (genre du phénomène, son intensité et sa durée) décrite par des symboles internationaux.

Dans la colonne "Razvoj vremena" (évolution du temps) les abréviations suivantes sont utilisées:

n = au cours de la nuit; rj = tôt le matin; dp = avant midi; pp = après midi; kv = tard le soir; i = avec intermittence.

Les valeurs moyennes journalières et mensuelles de la température - à 7 h, 14 h et 21 h, heure locale, sont calculées d'après la formule:

$$\frac{t_7 + t_{14} + 2 \times t_{21}}{4},$$

et pour les autres éléments (P, e, U, N) on a calculé les moyennes arithmétiques simples pour obtenir les valeurs moyennes journalières et mensuelles des observations de 7h, 14 h et 21 h.

Les lectures des thermomètres à maxima et minima suivies de leur amorçage, ont été faites à 21 h et les valeurs inscrites le même jour.

Les valeurs journalières des précipitations relevées à 7 h se rapportent aux 24 heures précédentes, c'est-à-dire de 7 h à la veille à 7 h du jour de la lecture.

L'épaisseur de la couche de neige est mesurée à 7 h.

Dans les tableaux A sont soulignées les valeurs maxima de la pression atmosphérique, de la température de l'air, de la tension de vapeur d'eau, de la force du vent $F \geq 6$ (de l'échelle Beaufort) et des précipitations, ainsi que les valeurs minima de la pression atmosphérique, de la température de l'air, de la tension de vapeur d'eau et de l'humidité relative.

Dans les tableaux B pour les extrêmes moyennes mensuelles de la température de l'air, les indications M_{ax} et M_{in} ont été utilisées; dans les colonnes "Broj dana sa" (Nombre de jours avec) ● ou ♀, * ou Δ, et ⚡ sont indiqués seulement les jours avec une hauteur de précipitation en question de 0.1 mm au moins.

Le numéro de la station (colonne 2 de la Liste alphabétique) est en effet le numéro d'ordre de la série des stations dont les données figurent dans les tableaux de la partie B).

A la fin de la publication on trouvera la carte de la R.S.F. de Yougoslavie donnant les stations climatologiques de l'année 1978; les numéros de ces stations correspondent aux numéros des stations dont les données figurent dans les tableaux de la partie B.

A Z B U Č N I S P I S A K S T A N I C A
PO SOCIJALISTIČKIM REPUBLIKAMA

Znak x pokazuje da stanica raspolaže odgovarajućim podacima meteoroloških elemenata navedenih u kolonama 7-14.

A Z B U Č N I S P I S A K S T A N I C A
PO SOCIJALISTIČKIM REPUBLIKAMA

II Znak x pokazuje da stanica raspolaže odgovarajućim podacima meteoroloških elemenata navedenih u kolonama 7-14

S T A N I C A	Broj	Meteorološka	Geografska	Geografska	Red	Vlažnost	Temperatura	Vjetar	Oblakost	Insolacijia	Razdavine	Broj karak-	
	stanice	visina Hs m	širina δ 9° N	dubina Δ E Gr.	stanice	vrednost pričesak	vazduha	vazduha	vremena	radiacija	teritorijalnih dani	13	14
1	2	3	4	5	6	7	8	9	10	11	12	13	14
Crikvenica	48	2	45°10'	14°42'	ob	x	x	x	x	x	x	x	x
Čazma	61	144	45 45	16 38	ob	x	x	x	x	x	x	x	x
Daruvar	65	161	45 36	17 14	gl	x	x	x	x	x	x	x	x
Donji Miholjac	68	97	45 46	18 10	ob		x	x	x	x	x	x	x
Dubrovnik	98	49	42 39	18 06	ob		x	x	x	x	x	x	x
Djakovo	69	98	45 17	18 25	ob		x	x	x	x	x	x	x
Gospic	82	564	44 33	15 22	gl	x	x	x	x	x	x	x	x
Gračac	83	560	44 18	15 51	ob		x	x	x	x	x	x	x
Hvar	88	20	43 10	16 27	gl	x	x	x	x	x	x	x	x
Ilok	72	133	45 13	19 22	ob		x	x	x	x	x	x	x
Karlovac	52	112	45 30	15 33	ob	x	x	x	x	x	x	x	x
Knin	84	234	44 02	16 12	ob	x	x	x	x	x	x	x	x
Komiža	86	6	43 03	16 05	ob		x	x	x	x	x	x	x
Koprivnica	42	141	46 11	16 49	ob		x	x	x	x	x	x	x
Korčula	95	15	42 58	17 09	ob		x	x	x	x	x	x	x
Kostel	39	270	46 11	15 45	ob		x	x	x	x	x	x	x
Križevci	41	155	46 02	16 33	ob	x	x	x	x	x	x	x	x
Lastovo	94	186	42 46	16 54	gl	x	x	x	x	x	x	x	x
Ličko Lešće	81	463	44 48	15 19	ob		x	x	x	x	x	x	x
Lipik	64	154	45 25	17 10	ob		x	x	x	x	x	x	x
Makarska	90	9	43 18	17 01	ob		x	x	x	x	x	x	x
Mali Lošinj	75	53	44 32	14 28	gl	x	x	x	x	x	x	x	x
Ogulin	51	328	45 16	15 14	gl	x	x	x	x	x	x	x	x
Opuzen	91	2	43 01	17 34	ob		x	x	x	x	x	x	x
Orebić	96	6	42 58	17 10	ob		x	x	x	x	x	x	x
Osijek	71	89	45 32	18 44	gl	x	x	x	x	x	x	x	x
Pag	79	3	44 27	15 04	ob		x	x	x	x	x	x	x
Palagruž	92	98	42 24	16 16	ob	x	x	x	x	x	x	x	x
Parg	47	863	45 36	14 38	ob	x	x	x	x	x	x	x	x
Pazin	45	291	45 14	13 56	ob	x	x	x	x	x	x	x	x
Poreč	43	15	45 14	13 36	ob		x	x	x	x	x	x	x
Pula	73	30	44 52	13 51	ob		x	x	x	x	x	x	x
Puntijarka	54	988	45 55	15 58	gl	x	x	x	x	x	x	x	x
Rab	76	24	44 45	14 46	ob	x	x	x	x	x	x	x	x
Rijeka	46	120	45 20	14 27	ob	x	x	x	x	x	x	x	x
Rovinj	44	5	45 05	13 39	ob		x	x	x	x	x	x	x
Senj	77	26	44 59	14 54	gl	x	x	x	x	x	x	x	x
Sinj	89	308	43 43	16 40	ob		x	x	x	x	x	x	x
Sisak	60	98	45 30	16 22	ob	x	x	x	x	x	x	x	x
Skrad	50	625	45 25	14 56	ob		x	x	x	x	x	x	x
Slavonski Brod	66	152	45 20	17 41	ob		x	x	x	x	x	x	x
Slavonski Brod	62	88	45 10	18 00	gl	x	x	x	x	x	x	x	x
Split	43	348	45 03	15 34	ob		x	x	x	x	x	x	x
Split-Marijan	87	107	45 21	16 26	gl	x	x	x	x	x	x	x	x
Ston	99	0	45 50	17 42	ob		x	x	x	x	x	x	x

A Z B U Č N I S P I S A K S T A N I C A

PO SOCIJALISTIČKIM REPUBLIKAMA

Znak x pokazuje da stanica raspolaže odgovarajućim podacima meteoroloških elemenata navedenih u kolonama 7-14.

III

AZBUČNI SPISAK STANICA
PO SOCIJALISTIČKIM REPUBLIKAMA

PO SOCIALISTICKIM REPUBLIKAMA

Znak x pokazuje da stanica raspolaže odgovarajućim podacima meteoroloških elemenata navedenih u kolonama 7-14

S T A N I C A	Broj stанице	Nadzorna visina H m	Geografska širina φ ° M	Geografska dužina λ ° E Gr.	Red stанице	Vadudan pritisak	Temperatura vazduha	Vlažnost vazduha	Vetar	Oblačnost	Imanolacija	Padačine	Broj karak- terističnih danih	
	1	2	3	4	5	6	7	8	9	10	11	12	13	14
Mlinište	108	970	44°16'	16°52'	ob		x	x	x	x	x	x	x	x
Modriča	120	115	44 59	18 18	ob		x	x	x	x	x	x	x	x
Mostar	134	99	43 21	17 48	gl	x	x	x	x	x	x	x	x	x
Ponikve	121	970	44 11	18 22	ob		x	x	x	x	x	x	x	x
Prijedor	107	135	44 59	16 45	ob		x	x	x	x	x	x	x	x
Prnjavor	116	150	44 52	17 42	ob		x	x	x	x	x	x	x	x
Prozor	130	800	43 50	17 38	ob		x	x	x	x	x	x	x	x
Rakitno	128	915	43 34	17 27	ob		x	x	x	x	x	x	x	x
Sanski Most	106	158	44 46	16 42	gl		x	x	x	x	x	x	x	x
Sarajevo	139	630	43 52	18 26	gl	x	x	x	x	x	x	x	x	x
Sokolac	143	872	43 57	18 49	ob		x	x	x	x	x	x	x	x
Teslić	117	225	44 36	17 54	ob		x	x	x	x	x	x	x	x
Travnik	115	581	44 14	17 40	ob		x	x	x	x	x	x	x	x
Tuzla	123	305	44 33	18 42	gl	x	x	x	x	x	x	x	x	x
Vlasenica	125	670	44 12	18 57	ob		x	x	x	x	x	x	x	x
Zenica	118	344	44 13	17 54	gl	x	x	x	x	x	x	x	x	x
S O C I J A L I S T I Č K A R E P U B L I K A S R B I J A														
Aleksandrovac	195	360	43°27'	21°04'	ob		x			x		x	x	x
Babušnica	207	495	43 04	22 26	ob		x			x		x	x	x
Bačka Topola	152	100	45 49	19 39	ob		x			x		x	x	x
Bački Petrovac	151	85	45 22	19 34	ob		x			x		x	x	x
Bećej	157	78	45 38	20 02	ob		x			x		x	x	x
Bela Crkva	178	90	44 54	21 25	ob		x			x		x	x	x
Bele Vode-Golija	190	1500	43 25	20 17	ob		x			x		x	x	x
Beograd	169	132	44 48	20 28	gl	x	x			x		x	x	x
Bosiljgrad	228	830	42 30	22 28	ob		x			x		x	x	x
Bujanovac	221	400	42 27	21 47	ob		x			x		x	x	x
Bukovička Banja	172	265	44 18	20 33	ob		x			x		x	x	x
Čačak	191	250	43 53	20 19	ob		x			x		x	x	x
Čuprija	200	123	43 56	21 23	gl	x	x			x		x	x	x
Dimitrovgrad	210	446	43 01	22 45	gl	x	x			x		x	x	x
Dragaš	215	1060	42 04	20 39	ob		x			x		x	x	x
Flemunda	177	160	44 56	21 05	ob		x			x		x	x	x
Gladnoš	156	185	45 08	20 00	ob		x			x		x	x	x
Gornji Milanovac	170	365	44 03	20 29	ob		x			x		x	x	x
Istok	213	465	42 47	20 30	ob		x			x		x	x	x
Ivanjica	189	465	43 35	20 14	ob		x			x		x	x	x
Jaša Tomić	161	80	45 27	20 51	ob		x			x		x	x	x
Kikinda	160	81	45 51	20 28	gl	x	x			x		x	x	x
Klina	214	385	42 38	20 34	ob		x			x		x	x	x
Knjaževac	206	280	43 34	22 16	ob		x			x		x	x	x
Kos. Mitrovica	217	510	42 53	20 52	ob		x			x		x	x	x
Kragujevac	175	190	44 02	20 56	ob		x			x		x	x	x
Kraljevo	193	219	43 44	20 41	gl	x	x			x		x	x	x

A Z B U Č N I S P I S A K S T A N I C A
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Znak x pokazuje da stanica raspolaže odgovarajućim podacima meteoroloških elemenata navedenih u kolonama 7-14

V

S T A N I C A	Broj	Majorska	Nadmorska	Geografska	Geografska	Red	Vazdušni	Temperatura	Vlažnost	Vetar	Oblastnost	Indolacija	Radavine	Broj karakterističnih
	stanice	visina	h m	Širina	dužina	stanice	pritisak	vazduha	vazduha	10	11	12	13	14
1	2	3	4	5	6	7	8	9	10	11	12	13	14	
Kruševac	199	166	43°34'	21°21'	gl		x	x	x	x	x	x	x	x
Kukavica	223	1250	42 45	21 59	ob		x	x	x	x	x	x	x	x
Kuršumlija	198	380	43 08	21 16	gl	x	x	x	x	x	x	x	x	x
Leskovac	204	230	42 59	21 57	gl	x	x	x	x	x	x	x	x	x
Loznica	163	121	44 33	19 14	gl	x	x	x	x	x	x	x	x	x
Ljubovija	164	170	44 11	19 23	ob		x	x	x	x	x	x	x	x
Mitrovac-Tara	184	1080	43 55	19 26	ob		x	x		x	x	x	x	x
Negotin	183	42	44 14	22 33	gl	x	x	x	x	x	x	x	x	x
Niš	203	202	43 20	21 54	gl	x	x	x	x	x	x	x	x	x
Novi Pazar	192	545	43 08	20 31	ob		x	x		x	x	x	x	x
Novi Sad-Petrovaradin	155	132	45 15	19 52	ob	x	x	x	x	x	x	x	x	x
Novi Sad-Rimski Šančevi	154	86	45 20	19 51	gl	x	x	x	x	x	x	x	x	x
Palić	148	102	46 06	19 46	gl	x	x	x	x	x	x	x	x	x
Pančevo	173	80	44 53	20 40	ob		x	x	x	x	x	x	x	x
Peć	211	498	42 40	20 18	gl	x	x	x	x	x	x	x	x	x
Petrovac	179	120	44 23	21 25	ob		x	x		x	x	x	x	x
Pirot	208	370	43 09	22 36	ob		x	x		x	x	x	x	x
Predejane	225	318	42 50	22 08	ob		x	x	x	x	x	x	x	x
Priština	218	573	42 39	21 09	gl	x	x	x	x	x	x	x	x	x
Prizren	216	402	42 13	20 44	gl	x	x	x	x	x	x	x	x	x
Prokuplje	201	265	43 14	21 36	ob		x	x	x	x	x	x	x	x
Rekovac	196	230	43 52	21 06	ob		x	x	x	x	x	x	x	x
Rudnik	171	700	44 08	20 31	ob		x	x	x	x	x	x	x	x
Senta	158	80	45 56	20 05	ob		x	x	x	x	x	x	x	x
Sijarinska Banja	220	455	42 47	21 36	ob		x	x		x	x	x	x	x
Sjenica	187	1015	43 16	20 01	gl	x	x	x	x	x	x	x	x	x
Skivjane-Djakovica	212	415	42 26	20 21	ob		x	x		x	x	x	x	x
Smederevo	174	120	44 39	20 55	ob		x	x		x	x	x	x	x
Smed. Palanka	176	121	44 22	20 57	gl	x	x	x	x	x	x	x	x	x
Sokobanja	202	300	43 39	21 51	ob		x	x		x	x	x	x	x
Sombor	149	87	45 46	19 09	gl	x	x	x	x	x	x	x	x	x
Sr. Mitrovica	165	81	44 58	19 38	gl		x	x	x	x	x	x	x	x
Surdulica	226	500	42 41	22 11	ob		x	x		x	x	x	x	x
Svetozarevo	197	115	43 59	21 14	ob		x	x	x	x	x	x	x	x
Sabac	166	80	44 46	19 41	ob		x	x		x	x	x	x	x
Sid	150	105	45 07	19 15	ob		x	x	x	x	x	x	x	y
Tekija	182	50	44 41	22 25	ob		x	x	x	x	x	x	x	x
Titovo Užice	186	440	43 52	19 51	ob		x	x	x	x	x	x	x	x
Topli Do	209	700	43 20	22 41	ob		x	x		x	x	x	x	y
Uroševac	219	580	42 23	21 10	ob		x	x	x	x	x	x	x	x
Uđ. Požega	188	311	42 51	20 62	gl	x	x	x	x	x	x	x	x	y
Valjevo	168	174	44 17	19 56	gl	x	x	x	y	x	x	x	x	y
Veliko Gradište	180	82	44 45	21 31	gl	x	x	x	x	x	x	x	x	x
Vlastivice	171	114	44 27	19 47	ob		x	x	x	x	x	x	x	y
Vlasina	227	114	45 44	22 21	ob		x	x		x	x	x	y	x

AZBUČNI SPISAK STANICA
PO SOCIJALISTIČKIM REPUBLIKAMA

VI Znak x pokazuje da stanica raspolaže odgovarajućim podacima meteoroloških elemenata navedenih u kolonama 7-14

STANICA	Broj stanice	Majstorska visina H, m	Geografska latituda N	Geografska longituda E Gr.	Red stanice	Vazdušni pritisak	Temperatura vazduha	Vlažnost vazduha	Vetar	Oblakost	Insolacija	Padavine	Broj karakterističnih dana	
1	2	3	4	5	6	7	8	9	10	11	12	13	14	
Vlasotince	224	270	42°58'	22°08'	ob	x	x	x	x	x	x	x	x	x
Vranje	222	433	42 33	21 55	gl	x	x	x	x	x	x	x	x	x
Vrbas	153	87	45 34	19 39	ob		x	x	x	x	x	x	x	x
Vrnjačka Banja	194	235	43 37	20 54	ob		x	x	x	x	x	x	x	x
Vršac	162	83	45 09	21 19	gl	x	x	x	x	x	x	x	x	x
Zaječar	206	137	43 53	22 18	ob		x	x	x	x	x	x	x	x
Zlatibor	185	1029	43 44	19 43	gl	x	x	x	x	x	x	x	x	x
Zrenjanin	159	80	45 24	20 21	gl		x	x	x	x	x	x	x	x
Zagubica	181	314	44 12	21 47	ob		x	x	x	x	x	x	x	x
SOCIJALISTIČKA REPUBLIKA CRNA GORA														
Bar	240	1	42°06'	19°06'	gl	x	x	x	x	x	x	x	x	x
Bijelo Polje	232	560	43 02	19 45	ob		x	x	x	x	x	x	x	x
Budva	236	2	42 17	18 51	ob	x	x	x	x	x	x	x	x	x
Cetinje	237	655	42 24	18 56	ob		x	x	x	x	x	x	x	x
Grašovo	234	710	42 39	18 41	ob		x	x	x	x	x	x	x	x
Herceg Novi-Igalo	233	40	42 28	18 30	gl	x	x	x	x	x	x	x	x	x
Ivangrad	244	670	42 50	19 52	ob		x	x	x	x	x	x	x	x
Kolašin	243	944	42 50	19 32	gl	x	x	x	x	x	x	x	x	x
Krševac	229	950	43 00	18 44	ob		x	x	x	x	x	x	x	x
Nikšić	238	647	42 46	18 57	gl	x	x	x	x	x	x	x	x	x
Prijepolje	231	784	43 21	19 21	gl	x	x	x	x	x	x	x	x	x
Titograd	242	49	42 26	19 17	ob	x	x	x	x	x	x	x	x	x
Titograd-Golubovci	241	33	42 22	19 15	gl	x	x	x	x	x	x	x	x	x
Tivat	235	5	42 26	18 42	gl	x	x	x	x	x	x	x	x	x
Ulcinj	245	97	41 55	19 13	gl	x	x	x	x	x	x	x	x	x
Virpazar	239	14	42 14	19 05	ob		x	x	x	x	x	x	x	x
Zabljak	230	1450	43 09	19 08	gl	x	x	x	x	x	x	x	x	x
SOCIJALISTIČKA REPUBLIKA MAKEDONIJA														
Berovo	227	874	41°42'	22°51'	gl	x	x	x	x	x	x	x	x	x
Bitola	261	586	41 03	21 22	gl	x	x	x	x	x	x	x	x	x
Debar	251	675	41 °1	20 37	ob		x	x	x	x	x	x	x	x
Delčevo	226	630	41 °8	20 46	ob		x	x	x	x	x	x	x	x
Demir Kapija	269	126	41 25	20 15	gl	x	x	x	x	x	x	x	x	x
Entsiklo	268	253	41 10	20 07	ob		x	x	x	x	x	x	x	x
Gevgелија	222	64	41 04	20 30	ob		x	x	x	x	x	x	x	x
Gostivar	240	526	41 48	20 55	ob		x	x	x	x	x	x	x	x
Hrvatsko	267	265	41 26	20 07	ob		x	x	x	x	x	x	x	x
Jestavnica	26	676	41 °1	20 48	ob		x	x	x	x	x	x	x	x
Jub	24	74	41 °4	20 37	ob		x	x	x	x	x	x	x	x
Karpoš	244	696	41 °3	20 34	ob		x	x	x	x	x	x	x	x
Kumanovo	220	590	41 03	20 37	ob		x	x	x	x	x	x	x	x
Kruševo	245	64	41 10	20 37	ob		x	x	x	x	x	x	x	x
Lipkovski Vrh	246	65	41 10	20 37	ob		x	x	x	x	x	x	x	x
Macedonski Brod	247	66	41 10	20 37	ob		x	x	x	x	x	x	x	x
Makedonski Konjic	248	67	41 10	20 37	ob		x	x	x	x	x	x	x	x
Makedonski Tresonec	249	68	41 10	20 37	ob		x	x	x	x	x	x	x	x
Makedonski Vitosha	250	69	41 10	20 37	ob		x	x	x	x	x	x	x	x
Makedonski Žiri	251	70	41 10	20 37	ob		x	x	x	x	x	x	x	x
Makedonski Žalgir	252	71	41 10	20 37	ob		x	x	x	x	x	x	x	x
Makedonski Želenec	253	72	41 10	20 37	ob		x	x	x	x	x	x	x	x
Makedonski Žirovci	254	73	41 10	20 37	ob		x	x	x	x	x	x	x	x
Makedonski Žirovci	255	74	41 10	20 37	ob		x	x	x	x	x	x	x	x
Makedonski Žirovci	256	75	41 10	20 37	ob		x	x	x	x	x	x	x	x
Makedonski Žirovci	257	76	41 10	20 37	ob		x	x	x	x	x	x	x	x
Makedonski Žirovci	258	77	41 10	20 37	ob		x	x	x	x	x	x	x	x
Makedonski Žirovci	259	78	41 10	20 37	ob		x	x	x	x	x	x	x	x
Makedonski Žirovci	260	79	41 10	20 37	ob		x	x	x	x	x	x	x	x
Makedonski Žirovci	261	80	41 10	20 37	ob		x	x	x	x	x	x	x	x
Makedonski Žirovci	262	81	41 10	20 37	ob		x	x	x	x	x	x	x	x
Makedonski Žirovci	263	82	41 10	20 37	ob		x	x	x	x	x	x	x	x
Makedonski Žirovci	264	83	41 10	20 37	ob		x	x	x	x	x	x	x	x
Makedonski Žirovci	265	84	41 10	20 37	ob		x	x	x	x	x	x	x	x
Makedonski Žirovci	266	85	41 10	20 37	ob		x	x	x	x	x	x	x	x
Makedonski Žirovci	267	86	41 10	20 37	ob		x	x	x	x	x	x	x	x
Makedonski Žirovci	268	87	41 10	20 37	ob		x	x	x	x	x	x	x	x
Makedonski Žirovci	269	88	41 10	20 37	ob		x	x	x	x	x	x	x	x
Makedonski Žirovci	270	89	41 10	20 37	ob		x	x	x	x	x	x	x	x
Makedonski Žirovci	271	90	41 10	20 37	ob		x	x	x	x	x	x	x	x
Makedonski Žirovci	272	91	41 10	20 37	ob		x	x	x	x	x	x	x	x
Makedonski Žirovci	273	92	41 10	20 37	ob		x	x	x	x	x	x	x	x
Makedonski Žirovci	274	93	41 10	20 37	ob		x	x	x	x	x	x	x	x
Makedonski Žirovci	275	94	41 10	20 37	ob		x	x	x	x	x	x	x	x
Makedonski Žirovci	276	95	41 10	20 37	ob		x	x	x	x	x	x	x	x
Makedonski Žirovci	277	96	41 10	20 37	ob		x	x	x	x	x	x	x	x
Makedonski Žirovci	278	97	41 10	20 37	ob		x	x	x	x	x	x	x	x
Makedonski Žirovci	279	98	41 10	20 37	ob		x	x	x	x	x	x	x	x
Makedonski Žirovci	280	99	41 10	20 37	ob		x	x	x	x	x	x	x	x
Makedonski Žirovci	281	100	41 10	20 37	ob		x	x	x	x	x	x	x	x
Makedonski Žirovci	282	101	41 10	20 37	ob		x	x	x	x	x	x	x	x
Makedonski Žirovci	283	102	41 10	20 37	ob		x	x	x	x	x	x	x	x
Makedonski Žirovci	284	103	41 10	20 37	ob		x	x	x	x	x	x	x	x
Makedonski Žirovci	285	104	41 10	20 37	ob		x	x	x	x	x	x	x	x
Makedonski Žirovci	286	105	41 10	20 37	ob		x	x	x	x	x	x	x	x
Makedonski Žirovci	287	106	41 10	20 37	ob		x	x	x	x	x	x	x	x
Makedonski Žirovci	288	107	41 10	20 37	ob		x	x	x	x	x	x	x	x
Makedonski Žirovci	289	108	41 10	20 37	ob		x	x	x	x	x	x	x	x
Makedonski Žirovci	290	109	41 10	20 37	ob		x	x	x	x	x	x	x	x
Makedonski Žirovci	291	110	41 10	20 37	ob		x	x	x	x	x	x	x	x
Makedonski Žirovci	292	111	41 10	20 37	ob		x	x	x	x	x	x	x	x
Makedonski Žirovci	293	112	41 10	20 37	ob		x	x	x	x	x	x	x	x
Makedonski Žirovci	294	113	41 10	20 37	ob		x	x	x	x	x	x	x	x
Makedonski Žirovci	295	114	41 10	20 37	ob		x	x	x	x	x	x	x	x
Makedonski Žirovci	296	115	41 10	20 37	ob		x	x	x	x	x	x	x	x
M														

A Z B U Č N I S P I S A K S T A N I C A
PO SOCIJALISTIČKIM REPUBLIKAMA

Znak x pokazuje da stanica raspolaže odgovarajućim podacima meteoroloških elemenata navedenih u kolonama 7-14.

VII

A) Dnevna osmatranja

$\varphi = 46^{\circ}04' N$ $\lambda = 14^{\circ}31' E$ Gr. $\Delta G = + 58$ min.

BR. ST. 13

D S	Vzdušni pritisak P mm			Temperatura vozduha T °C								Napon vodenih parov e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0-12)					
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21			
1	734.6	738.0	741.3	01.2	08.8	-01.6	01.7	09.0	-01.6	-07.6	03.4	03.0	03.0	68	35	75	59	NNW	3	NW	2	ESE 1	
2	741.8	739.1	739.0	-05.3	08.8	05.0	03.4	09.4	-05.6	-10.3	03.0	03.9	04.1	97	46	63	69	E	1	W	3	W 2	
3	737.6	735.9	732.3	03.1	06.0	07.0	05.8	07.5	02.7	01.7	04.3	04.8	05.9	75	69	79	74	NW	2	-	0	WSW 2	
4	731.9	732.3	735.1	04.6	09.6	03.5	05.3	10.4	03.0	02.2	04.6	03.0	03.1	73	34	52	53	SW	2	S	1	W 2	
5	738.7	742.6	746.7	-01.6	01.5	-02.2	-01.1	03.5	-02.4	-08.1	03.9	02.9	01.6	95	57	41	64	SW	1	NNE	3	ESE 1	
6	748.7	747.0	745.7	-07.4	-00.7	-02.2	-03.1	00.4	-07.7	-13.0	02.2	01.8	02.5	83	41	64	63	E	1	ENE	1	N 1	
7	744.9	745.3	746.7	-06.3	04.0	01.8	00.3	04.7	-06.7	-10.5	02.5	03.0	04.9	87	49	93	76	N	1	E	2	S 2	
8	745.8	744.7	744.7	00.4	02.5	-03.0	-00.8	03.0	-03.2	00.3	04.5	03.4	03.4	95	62	92	83	E	2	ENE	1	WSW 1	
9	743.2	742.1	741.7	-04.0	-03.6	-04.2	-04.0	-02.9	-04.2	-09.6	03.1	02.8	02.7	90	78	81	83	SE	1	SSE	2	SW 1	
10	739.8	738.5	739.0	-04.7	-02.0	-04.1	-03.7	-00.5	-04.9	-09.2	03.0	03.4	J3.2	93	85	94	91	SSE	1	ENE	1	SSW 2	
11	735.7	730.1	726.5	-03.9	-02.2	-00.6	-01.8	-00.2	-05.2	-09.6	03.3	03.5	04.2	96	90	96	94	NNE	1	ENE	1	NE 1	
12	725.3	727.0	731.4	00.9	03.0	02.4	02.2	03.3	-01.2	-00.6	04.8	05.0	05.3	98	87	97	94	WSW	1	S	1	N 1	
13	735.3	738.3	739.4	02.0	03.6	03.3	03.1	04.1	01.9	00.6	05.1	05.8	05.7	97	98	98	98	W	1	WSW	1	ENE 1	
14	739.0	738.6	739.7	02.7	03.2	02.4	02.7	03.9	02.4	00.5	05.5	05.6	05.4	98	97	98	98	NNW	1	NW	1	S 2	
15	739.1	737.9	737.5	01.9	01.3	00.9	01.3	02.9	00.6	01.4	05.1	04.7	04.6	97	93	93	94	NE	1	SE	1	E 1	
16	735.3	734.8	735.1	-00.5	00.8	-00.3	-00.1	01.2	-00.7	-01.3	04.3	03.9	03.8	96	81	84	87	NNE	1	ENE	1	SE 1	
17	732.9	728.4	726.6	-01.0	-00.6	-01.2	-01.0	-00.2	-01.3	-01.6	03.7	04.0	04.0	86	92	96	91	E	1	ENE	1	SE 2	
18	727.6	729.3	730.9	-01.4	01.0	-00.2	-00.2	01.1	-01.7	-01.8	04.1	04.2	04.4	98	85	96	93	NNW	1	SE	1	ENE 1	
19	730.3	729.0	728.6	-00.3	-00.2	-00.8	-00.5	00.8	-00.9	-01.0	04.3	04.0	03.9	96	89	91	92	NW	1	SE	1	ESE 2	
20	727.9	728.1	730.0	-01.6	00.1	-01.0	-00.9	00.1	-02.0	-02.3	03.8	04.0	03.9	94	87	92	91	NNE	1	NW	1	NE 1	
21	730.0	730.5	732.1	-01.0	00.5	00.0	-00.1	00.6	-01.4	-02.6	03.9	03.9	03.6	92	82	79	84	NNW	1	SE	1	ESE 2	
22	731.7	731.2	732.5	-01.2	-01.1	-02.0	-01.6	00.1	-02.0	-02.4	03.6	03.7	03.5	87	87	89	88	SSE	1	SE	2	NE 1	
23	733.1	734.8	735.2	-02.1	01.6	00.0	-00.1	02.0	-02.4	-03.3	03.7	04.0	03.9	94	77	86	86	ENE	1	E	1	WNW 1	
24	731.0	727.2	723.6	-00.7	00.4	01.6	00.7	02.3	-01.4	-02.3	04.0	04.3	04.9	93	91	95	93	SE	1	W	1	W 2	
25	722.5	726.5	729.5	01.0	05.3	00.2	01.7	06.6	-00.3	00.0	04.8	05.4	04.6	97	80	98	92	NE	1	SW	1	NE 1	
26	730.7	731.9	732.8	-01.3	01.6	00.9	00.5	02.2	-01.4	-03.6	04.1	04.5	04.6	98	87	95	93	NE	2	ENE	1	WSW 1	
27	733.8	734.9	736.6	-02.3	04.4	-01.8	-00.4	05.4	-02.8	-02.8	03.7	04.1	03.9	96	65	98	86	N	1	SE	1	W 1	
28	734.3	729.5	724.8	-04.8	-00.1	01.4	-00.5	01.9	-05.0	-04.1	03.1	04.1	04.9	98	91	97	95	ENE	1	NW	2	N 1	
29	715.5	712.8	716.9	02.6	03.5	03.2	03.1	04.6	01.3	00.6	05.4	05.7	04.8	98	97	83	93	NNE	1	SSW	3	WNW 2	
30	720.0	721.5	724.1	01.0	02.4	01.4	01.6	03.2	00.7	-00.2	04.8	04.9	04.8	98	90	95	94	NE	1	SSW	1	SE 1	
31	727.7	729.5	732.0	-00.1	01.8	-00.4	00.2	02.7	-00.4	-00.7	04.6	04.3	04.3	90	82	96	93	ENE	1	ENE	1	NE 1	
MES.	RED.			733.7	733.5	734.1	-01.0	02.1	00.3	00.4	03.0	-01.7	-03.3	04.0	04.0	04.0	92	77	87	85	1.2	1.4	1.4

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1	732.7	730.9	729.6	-02.2	-00.4	-01.6	-01.5	00.2	-02.6	-01.8	03.7	03.5	03.9	96	78	95	90	NNW	2	W	1	WSW 1
2	724.8	725.3	727.1	-01.4	01.1	00.4	00.1	01.7	-01.8	-02.0	04.0	04.5	04.4	97	90	93	93	NE	1	ENE	1	S 1
3	729.1	731.7	734.7	00.4	02.4	-00.3	00.6	03.1	-00.3	00.0	J4.1	04.4	04.3	88	91	96	88	N	1	SE	1	NNE 1
4	736.6	737.0	738.3	-02.1	03.6	01.5	01.1	04.1	-02.3	-05.9	03.9	03.6	03.8	100	61	75	79	N	1	ENE	1	ESE 2
5	738.1	736.7	735.6	-00.2	01.7	00.6	00.7	01.9	-00.4	-01.3	J4.3	03.9	03.4	95	75	71	80	NW	1	S	1	NE 1
6	732.0	730.6	731.0	-00.6	04.3	00.6	01.2	04.6	-00.7	-02.3	03.5	03.3	03.9	80	53	81	71	NW	1	E	3	SE 1
7	729.4	728.4	728.5	-01.2	04.6	00.4	01.1	04.7	-01.3	-03.8	03.9	03.6	03.4	93	57	72	74	NNE	1	SE	2	SE 1
8	727.8	728.1	728.7	-01.6	-00.8	-02.7	-02.0	01.1	-02.8	-02.2	03.8	03.3	03.1	92	76	82	83	SE	2	SE	3	SE 2
9	729.6	730.4	731.6	-04.5	-00.8	-03.2	-02.9	-00.5	-04.5	-04.7	J2.8	03.3	02.6	85	76	71	77	SE	2	SE	1	SE 2
10	731.6	728.9	727.3	-05.0	-03.2	-03.6	-03.9	-02.8	-05.0	-08.0	J2.5	02.7	03.3	78	75	92	82	S	2	N	2	NW 1
11	721.5	720.3	721.0	-03.0	-01.4	-01.9	-02.1	-00.9	-03.6	-03.6	03.6	03.9	03.8	97	95	96	96	NW	1	NNE	1	SE 1
12	721.8	724.1	725.5	-01.5	04.5	00.3	04.9	04.6	-01.9	-04.9	04.0	04.8	04.6	99	75	98	91	NE	1	NNE	1	ENE 1
13	725.4	725.3	725.9	00.0	01.4	00.0	00.4	01.5	-00.3	-02.3	04.5	04.2	04.3	98	83	95	92	NNW	1	N	1	N 1
14	724.9	723.6	726.2	-00.2	04.8	00.5	01.4	05.2	-00.3	-01.6	J4.1	03.5	03.5	91	54	74	73	SE	1	S	2	ESE 1
15	729.1	730.1	731.3	-02.8	02.7	-02.5	-01.3	04.3	-03.7	-09.1	02.5	02.1	0									

BR. ST. 13

 $H_s = 299 \text{ m } H_b = 297.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.5 \text{ m}$

Dan	Vrijeme 0-9	Oblačnost N (0-10)					Intenziteta bojišnici	Podzemna R mm	Snežni pokrivač h cm	Razvoj vremena w	
		14	7	14	21	Sred Dnes				7	7
1	9 02	01○	00	01.0	07.3	.	.	—	—	—	—
2	8 00	01○	09	03.3	07.8	.	.	—	—	—	—
3	7 10	10	10●	10.0	00.0	00.0	.	—	—	—	—
4	8 09	04○	10	07.7	03.5	00.1	.	—	—	—	—
5	8 00	09○*	00	03.0	06.2	.	.	—	—	—	—
6	7 01	06○	07	04.7	05.6	00.0	.	—	—	—	—
7	6 04	06○	10	06.7	04.9	.	.	—	—	—	—
8	7 10	08○	00	06.0	01.4	00.0	.	—	—	—	—
9	6 10	10	10	10.0	00.0	.	.	—	—	—	—
10	5 10	09○	02	07.0	00.8	00.0	.	—	—	—	—
11	4 10	10●	10●	10.0	00.0	00.2	.	—	—	—	—
12	6 10●	10	10	10.0	00.0	06.2	01	—	—	—	—
13	3 10●	10●	10●	10.0	00.0	00.5	.	—	—	—	—
14	3 10●	10●	10●	10.0	00.0	04.7	.	—	—	—	—
15	4 10●	10●	10●	10.0	00.0	03.9	.	—	—	—	—
16	5 10	10	10	10.0	00.0	10.1	06	—	—	—	—
17	3 10	10●*	10●*	10.0	00.0	03.2	08	—	—	—	—
18	5 10	10●*	10●*	10.0	00.0	19.4	26	—	—	—	—
19	5 10	10●*	10●*	10.0	00.0	03.2	27	—	—	—	—
20	5 10●*	10●*	10●*	10.0	00.0	07.2	30	—	—	—	—
21	6 10*	10*	10	10.0	00.0	04.8	35	—	—	—	—
22	5 10	10*	10	10.0	00.0	00.3	30	—	—	—	—
23	6 10	05○	10	08.3	01.0	00.0	29	—	—	—	—
24	5 10	10	10●	10.0	00.0	00.0	27	—	—	—	—
25	5 10	10	10●	10.0	00.0	03.1	18	—	—	—	—
26	5 10●	09○	10	09.7	00.5	.	14	—	—	—	—
27	5 09●	00○	10●	06.3	05.1	.	12	—	—	—	—
28	5 10●	10●	10●	10.0	00.0	.	12	—	—	—	—
29	6 10	10●	09	09.7	00.0	14.5	10	—	—	—	—
30	5 10	10●	09	09.7	00.0	13.4	07	—	—	—	—
31	5 10●	10	10	10.0	00.0	01.5	06	—	—	—	—
MES. VRED.	08.5	08.3	08.6	08.5	48.2	93.5					

LJUBLJANA-BEŽIGRAD

1978 FEBRUAR

1	5 10	10	10	10.0	00.0	.	05	—	—	—	—
2	4 10*	10*	10	10.0	00.0	02.7	08	—	—	—	—
3	6 10	09	04	07.7	00.0	03.7	08	—	—	—	—
4	6 10●	09○	09	09.3	01.9	00.0	07	—	—	—	—
5	6 10*	10	10	10.0	00.0	00.1	16	—	—	—	—
6	7 10	05○	10	08.3	04.3	00.0	06	—	—	—	—
7	6 10	04○	07	07.0	04.3	.	05	—	—	—	—
8	6 10*	10*	10*	10.0	00.1	00.4	06	—	—	—	—
9	6 09*	09	10	09.3	02.1	00.6	06	—	—	—	—
10	6 10	10*	10*	10.0	00.0	00.0	05	—	—	—	—
11	4 10*	10*	10*	10.0	00.0	04.2	09	—	—	—	—
12	5 10	10●	10●	10.0	02.2	15.6	18	—	—	—	—
13	5 10●	10	10	10.0	00.0	00.8	11	—	—	—	—
14	6 09	01○	09	06.3	05.1	00.0	08	—	—	—	—
15	8 02	00○	00	00.7	08.5	.	08	—	—	—	—
16	4 09	10*	10*	09.7	00.0	.	08	—	—	—	—
17	6 10	10*	10	10.0	00.0	00.4	08	—	—	—	—
18	6 10*	04○	00	04.7	04.1	01.1	08	—	—	—	—
19	4 10	10*	10*	10.0	00.0	00.7	08	—	—	—	—
20	6 10	06○	09	08.3	02.5	06.5	12	—	—	—	—
21	6 00●	02○	03	01.7	05.9	00.1	11	—	—	—	—
22	6 01	00○	06	02.3	08.8	.	10	—	—	—	—
23	6 09	09	10	09.3	00.0	.	09	—	—	—	—
24	7 10	10	10	10.0	00.0	.	05	—	—	—	—
25	7 09	10●	10●	09.7	01.0	00.0	00	—	—	—	—
26	5 10●	10●	10●	10.0	00.0	09.2	.	—	—	—	—
27	6 10●	09	07	08.7	00.2	11.1	.	—	—	—	—
28	6 09	08○	10	09.0	01.0	00.0	.	—	—	—	—
MES. VRED.	08.8	07.7	08.4	08.3	52.0	57.2					

$\varphi = 46^{\circ}04' N$ $\lambda = 14^{\circ}31' E$ Gr. $\Delta G = + 58$ min.

BR. ST. 13

D S	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodenih pare e mm			Relativna vlažnost U %			Pravac i jačina vetrova D, f (0—12)				
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21		
1	729.5	730.1	731.6	06.7	10.6	08.4	08.5	11.8	06.5	06.2	07.0	07.3	06.2	95	76	75	82	NNW 1	NNW 1	SW 2		
2	731.9	730.9	731.4	07.2	15.6	09.7	10.6	15.7	07.0	03.4	06.6	06.1	06.7	87	46	74	69	NW 1	SW 3	S 2		
3	731.3	729.6	729.7	04.6	17.2	09.7	10.3	18.3	04.4	-00.4	05.9	05.7	06.3	93	39	69	67	NNW 1	NNW 2	WSW 1		
4	729.7	727.8	729.9	00.9	17.5	08.4	08.8	18.0	06.7	-03.6	04.7	06.7	06.8	96	45	82	74	NNW 1	SW 1	SW 2		
5	728.7	728.9	730.3	04.7	10.4	07.8	07.7	11.3	04.2	00.8	06.1	07.0	07.6	96	73	96	88	ENE 1	ENE 1	NNW 1		
6	732.2	732.0	732.7	07.6	10.0	07.7	08.3	10.1	07.0	06.0	06.9	06.4	06.7	88	70	84	81	NNE 1	E 2	S 2		
7	734.5	736.0	737.0	03.6	02.3	01.9	02.4	07.7	01.8	03.4	05.7	04.4	04.2	95	82	80	86	SSE 2	E 2	ESE 2		
8	737.0	735.4	735.0	-01.0	08.3	03.4	03.5	09.3	-01.2	-04.7	04.2	03.7	04.2	98	45	73	72	N 1	E 1	NNW 1		
9	733.9	732.9	737.8	01.7	12.0	08.4	07.6	14.7	01.4	-02.3	04.8	05.0	03.0	92	48	36	59	SE 1	ENE 1	NNE 2		
10	740.0	738.6	740.8	00.4	15.1	08.0	07.9	15.3	00.4	-04.6	04.1	03.5	03.6	86	27	44	52	N 1	N 3	ESE 2		
11	740.2	734.5	733.0	-10.8	15.8	09.5	08.5	16.8	-01.0	-04.9	04.1	04.6	04.5	94	34	50	59	N 1	SW 3	SW 2		
12	734.4	734.2	735.8	00.4	12.4	07.3	06.9	13.8	00.4	-04.5	04.6	04.0	03.7	98	37	48	61	NNW 1	E 1	SE 2		
13	735.6	734.0	735.8	00.7	12.2	08.0	07.2	12.7	00.0	-04.9	04.2	03.7	05.6	86	35	70	64	E 1	SW 3	SSW 3		
14	736.4	735.0	733.5	06.4	08.1	05.8	06.5	08.4	05.8	04.4	05.9	06.7	06.6	82	82	96	87	SW 1	WSW 3	ESE 1		
15	731.3	730.6	732.3	07.3	08.8	06.7	07.4	09.2	05.4	03.6	06.3	06.8	05.9	82	80	80	81	WSW 3	S 2	SW 2		
16	731.8	728.9	725.5	01.7	10.2	09.8	07.9	10.6	01.6	-01.6	05.0	06.5	06.1	97	70	67	78	NNE 1	S 3	S 4		
17	722.0	724.3	726.8	09.4	13.1	07.4	09.3	13.7	07.3	05.8	05.9	04.0	03.8	67	35	50	51	SW 4	SW 3	WSW 2		
18	728.9	732.6	735.6	02.0	01.0	00.9	01.2	07.4	00.5	-01.6	04.9	04.8	04.8	93	97	98	96	NE 1	W 1	1		
19	737.0	736.4	736.8	01.0	05.2	00.7	01.9	06.9	00.6	-01.4	04.8	04.6	04.6	97	69	95	87	NNW 1	WSW 1	1		
20	732.6	727.8	724.6	-01.6	07.6	06.6	04.8	08.8	-01.7	-05.6	04.0	04.5	04.5	98	57	62	72	NNE 2	W 3	3		
21	718.9	720.3	724.0	04.9	11.4	06.4	07.3	12.9	04.0	03.2	06.2	05.3	03.8	96	53	53	67	ENE 1	E 2	ENE 2		
22	728.9	732.3	735.7	00.4	10.6	03.6	04.6	10.8	00.3	-04.6	04.2	02.1	02.2	90	22	37	50	SE 2	NNW 4	W 1		
23	734.3	730.2	729.7	-02.6	09.1	03.1	03.2	09.9	-02.9	-07.6	03.4	04.3	05.5	90	50	95	78	NNE 1	SSW 3	NNW 1		
24	726.8	726.5	729.0	00.7	05.7	02.7	03.0	07.9	00.3	00.1	04.7	04.3	05.0	98	63	90	84	SSW 1	SE 2	S 1		
25	733.3	734.8	735.5	00.0	13.0	06.0	06.3	13.3	-00.2	-03.3	04.4	02.4	03.4	96	22	48	55	E 2	SSE 1	S 2		
26	732.3	729.7	732.1	-00.4	11.6	02.7	04.2	12.0	-00.7	-05.1	04.1	03.7	05.4	93	36	97	75	NE 1	SSW 3	S 2		
27	735.7	735.0	736.7	00.6	12.7	07.0	06.8	13.0	00.0	-13.2	04.7	03.0	03.6	98	27	48	58	NW 1	E 2	S 2		
28	738.8	738.2	738.2	02.7	16.2	09.6	09.5	17.1	02.2	-02.9	05.0	04.3	04.2	90	31	47	56	NNE 1	S 3	S 2		
29	737.5	736.3	735.9	01.4	17.0	09.8	09.5	17.8	00.6	-04.2	04.8	04.7	05.6	95	32	62	63	N 1	SW 3	S 3		
30	733.9	731.7	732.0	03.6	18.4	12.0	11.5	18.6	01.8	-02.9	05.0	04.8	05.9	85	30	56	57	NNE 1	SW 4	SW 2		
31	731.0	729.2	730.6	03.6	19.1	10.6	11.0	19.6	02.7	-00.4	05.6	04.9	06.2	94	29	65	63	ESE 1	SE 2	SW 3		
MES.	732.6			731.8	732.8	02.5	11.6	06.8	06.9	12.7	01.9	-01.2	05.1	04.8	05.0	92	50	69	70	1.3	2.2	1.9
REND.																						

1	729.8	726.9	726.6	04.3	18.0	11.3	11.2	18.7	03.8	-01.8	05.8	04.5	07.1	93	29	71	64	NNE 2	S 2	SSW 3	
2	724.6	723.5	725.3	04.0	17.2	10.4	10.5	17.8	03.6	-01.3	05.8	05.5	06.4	95	37	68	67	NE 1	SW 3	S 2	
3	726.8	725.9	726.7	04.8	15.0	10.6	10.3	15.6	04.3	04.0	06.0	06.0	06.5	93	52	68	71	N 1	NE 3	ENE 2	
4	727.1	727.4	728.8	09.0	14.6	11.3	11.6	15.4	08.9	05.6	07.1	06.4	06.3	83	51	63	66	ENE 2	ENE 3	ENE 2	
5	729.5	729.1	731.3	07.9	13.9	09.7	10.3	14.1	07.7	04.9	07.1	06.1	06.7	88	51	74	71	ENE 1	E 2	ENE 1	
6	734.2	734.9	736.8	05.4	09.6	06.2	06.9	10.1	05.4	03.8	04.2	04.2	04.2	03.5	63	47	49	53	SE 2	NE 3	E 3
7	736.1	732.4	729.9	01.8	08.1	06.6	05.8	09.4	01.8	01.5	02.8	03.0	03.0	53	36	41	43	E 2	ENE 4	E 4	
8	728.1	727.9	728.5	02.3	08.3	04.3	04.8	09.4	01.6	01.6	04.6	03.0	03.9	85	37	62	61	SSW 1	E 3	NNE 1	
9	730.1	729.0	730.1	-00.1	14.4	10.0	08.4	14.6	-01.6	-06.7	04.0	04.0	05.1	91	33	56	60	ENE 1	SE 3	ESE 1	
10	730.0	729.9	730.4	04.4	12.4	09.9	09.2	12.6	04.1	-03.3	05.3	06.2	07.1	84	57	78	73	ENE 1	S 2	SSW 2	
11	733.6	730.4	731.0	08.4	11.3	08.6	09.2	13.3	08.4	06.4	07.4	06.9	07.7	96	69	92	84	SW 2	SSW 2	SE 1	
12	726.8	730.2	732.2	07.8	09.4	03.7	06.2	10.1	03.7	06.4	07.7	07.9	04.9	97	89	82	89	E 2	WNW 2	E 2	
13	727.3	724.2	721.9	02.4	03.2	00.6	01.7	03.9	00.6	01.6	05.2	05.3	04.6	95	92	90	94	ESE 1	NNE 1	WNW 1	
14	720.8	722.2	723.1	00.6	02.7	01.4	01.5	02.8	00.2	-00.2	04.7	05.0	04.9	98	90	97	95	W 1	WSW 1	S 2	
15	722.9	723.9	727.0	02.0	05.3	01.3	02.5	05.4	00.9	00.0	05.1	04.8	04.9	97	72	97	89	NW 1	E 3	M 2	
16	728.1	729.5	731.6	01.4	09.1	04.5	04.9	10.4	00.5	00.2	04.8	04.3	04.8	95	50	77	74	ESE 1	NNE 3	SSE 1	
17	733.6	733.2	735.3	00.2	11.4	05.4	05.6	11.9	-00.3	-04.5	04.6</td										

BR. ST. 13

 $H_s = 299 \text{ m } H_b = 297.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.5 \text{ m}$

Dan	Vdrljivost 0-9	Oblačnost N (0-10)					Iznad broj saj š	Padavina R mm	Snežni pokrivač h cm	Razvoj vremena w	
		14	7	14	21	Sred Dnes				7	7
1	6	100	10	05	08.3	01.4	00.8	.	.	$\Delta^0 -0.3^0 8^0 10^0; \Delta^0 3^0 8^0, = 3^0 14^0, \infty 14^0 15^0, \Delta^0 20^0 24^0, \circlearrowleft$	
2	8	06	050	01	04.0	05.2	00.6	.	.	$\bullet 2^0 3^0, \circlearrowleft$	
3	8	03	020	01	02.0	08.7	.	.	.	$\Delta^0 0^0 5^0, \Delta^0 1^0 10^0, 20^0 24^0, = 3^0 9^0, \circlearrowleft$	
4	8	010	020	01	01.3	06.7	.	.	.	$\Delta^0 -0.4^0 20^0 24^0, = 2^0 10^0, \Delta^0 4^0 8^0, = 0^0 10^0 12^0, \circlearrowleft$	
5	6	100	090	100	09.7	01.4	01.7	.	.	$\Delta^0 0.3^0, = 0^0 13^0, 10^0 24^0, \bullet 2^0 3^0, 3^0 24^0, \infty 10^0 18^0, \circlearrowleft$	
6	7	100	10	100	10.0	00.0	11.4	.	.	$\Delta^0 -0.2^0 6^0 9^0 15^0, 20^0 24^0, = 0^0 6^0$	
7	7	100	10	10	10.0	00.0	04.3	.	.	$\bullet 0^0 8^0, \Delta^0 2^0 24^0, \Delta^0 20^0 24^0, = 2^0 4^0 8^0, 20^0 24^0, = 3^0 8^0, \infty 14^0 19^0, \circlearrowleft$	
8	6	080	010	00	03.0	07.9	00.0	.	.	$= 0^0 14^0 6^0, 20^0 24^0, \Delta^0 20^0 24^0, = 2^0 4^0 8^0, 20^0 24^0, = 3^0 8^0, \infty 14^0 19^0, \circlearrowleft$	
9	7	090	080	01	06.0	05.7	.	.	.	$\Delta^0 0.1^0, = 0^0 10^0, \infty 10^0 16^0, \circlearrowleft$	
10	8	000	020	00	00.7	10.5	.	.	.	$\Delta^0 2^0 3^0, \circlearrowleft$	
11	8	080	020	04	04.7	08.6	.	.	.	$\Delta^0 2^0 7^0, = 8^0 10^0, \Delta^0 16^0 17^0, \Delta^0 22^0 24^0, \circlearrowleft$	
12	8	000	000	01	00.3	39.8	.	.	.	$\Delta^0 -0.4^0, \Delta^0 4^0 8^0, = 4^0 9^0, \infty 9^0 19^0, \circlearrowleft$	
13	7	09	090	10	09.3	04.1	.	.	.	$\Delta^0 -1^0 10^0, \Delta^0 2^0 24^0, \Delta^0 2^0 24^0, \circlearrowleft$	
14	7	100	09	10	09.7	00.0	00.1	.	.	$\bullet 0^0 10^0, \Delta^0 2^0 24^0, \Delta^0 2^0 24^0, \circlearrowleft$	
15	7	09	09	04	07.3	01.4	05.4	.	.	$= 0^0 13^0, 23^0 24^0, \Delta^0 20^0 24^0, = 2^0 4^0 8^0, \infty 9^0 19^0, 13^0 14^0, \circlearrowleft$	
16	7	080	100	04	07.3	00.3	03.5	.	.	$= 0^0 11^0, \infty 11^0 15^0, \Delta^0 10^0 14^0, \bullet 0^0 14^0 24^0, \circlearrowleft$	
17	8	100	060	01	05.7	06.3	04.4	.	.	$\bullet 0^0 9^0, \Delta^0 9^0 15^0, \Delta^0 10^0 14^0, \bullet 0^0 14^0 24^0, \circlearrowleft$	
18	4	09	10*	10	09.7	00.0	00.1	.	.	$\Delta^0 2^0 7^0, \Delta^0 10^0 15^0, 17^0 22^0, = 9^0 24^0, 2^0 12^0 13^0, 17^0 18^0, \star 10^0 19^0, \square$	
19	8	10	070	09	05.7	02.6	16.9	00	.	$= 0^0 11^0, 23^0 24^0, \Delta^0 19^0 20^0, \Delta^0 20^0 24^0, = 2^0 4^0 8^0, \infty 23^0 24^0, \square$	
20	8	100	09	10	09.7	10.6	.	.	.	$= 0^0 0^0, 6^0 8^0, \Delta^0 0^0 9^0, = 0^0 15^0 6^0, = 0^0 11^0, \star 0^0 8^0, \Delta^0 2^0 24^0, \circlearrowleft$	
21	7	09	100	09	09.3	33.9	06.3	.	.	$\bullet 0^0 3^0, = 0^0 10^0, \bullet 0^0 10^0, \Delta^0 10^0 14^0, \bullet 0^0 14^0 24^0, \circlearrowleft$	
22	9	050	040	00	03.0	10.1	00.2	.	.	$\Delta^0 0^0 4^0 8^0, \Delta^0 10^0 16^0, \circlearrowleft$	
23	8	030	10	100	07.7	02.0	.	.	.	$\Delta^0 0^0 23^0 24^0, \Delta^0 19^0 20^0, \Delta^0 20^0 24^0, = 2^0 4^0 8^0, \infty 23^0 24^0, \square$	
24	7	10*	10	09	09.7	01.8	18.5	03	.	$= 0^0 10^0, \star 0^0 24^0, 4^0 9^0, \Delta^0 2^0 4^0, \bullet 0^0 8^0, \Delta^0 9^0, \circlearrowleft, \square$	
25	9	040	020	01	02.3	11.9	00.0	.	.	$\Delta^0 0^0 23^0 7^0, \circlearrowleft$	
26	8	090	090	10	09.3	01.3	.	.	.	$\Delta^0 3^0 7^0, \bullet 0^0 15^0 20^0, \bullet 0^0 15^0 18^0, = 19^0 24^0, \circlearrowleft$	
27	8	100	010	05	05.3	08.5	06.1	.	.	$= 0^0 5^0 8^0, \Delta^0 10^0 14^0, = 0^0 5^0 8^0, \circlearrowleft$	
28	8	050	060	00	03.7	10.0	.	.	.	$\Delta^0 -3^0 6^0, \Delta^0 10^0 14^0, \circlearrowleft$	
29	8	010	020	01	01.3	11.4	.	.	.	$\Delta^0 0.3^0, \Delta^0 3^0 7^0, \circlearrowleft$	
30	8	020	040	00	02.0	39.0	.	.	.	$\Delta^0 2^0 5^0, \Delta^0 5^0 7^0, \infty 2^0 7^0 15^0 9^0, \Delta^0 13^0 15^0, \circlearrowleft$	
31	8	040	020	01	02.3	11.1	.	.	.	$\Delta^0 0^0 10^0, \Delta^0 16^0 18^0, \circlearrowleft$	
MES. RED.					06.8	06.1	04.5	05.8	161.2	80.7	

LJUBLJANA-BEŽIGRAD

1978 APRIL

1	8	040	040	02	03.3	10.5	.	.	.	$\Delta^0 0^0 10^0, \circlearrowleft$	
2	7	050	040	01	03.3	08.4	.	.	.	$\Delta^0 0^0 8^0, 22^0 24^0, = 3^0 9^0, 23^0 24^0, \infty 9^0 13^0, \circlearrowleft$	
3	7	040	050	04	04.3	14.3	.	.	.	$= 0^0 9^0, 22^0 24^0, \Delta^0 0^0 10^0, \infty 9^0 22^0, \bullet 0^0 23^0 24^0, \circlearrowleft$	
4	7	10	09	09	09.3	03.3	00.8	.	.	$\bullet 0^0 0^0, = 0^0 8^0, \Delta^0 23^0 24^0, \circlearrowleft$	
5	6	100	10	100	10.0	30.0	00.0	.	.	$\Delta^0 0^0 6^0, = 0^0 24^0, \bullet 0^0 6^0 10^0, 9^0 10^0, 15^0 21^0, \bullet 0^0 14^0 15^0, \circlearrowleft$	
6	7	09	09	10	09.3	01.4	02.5	.	.	$= 0^0 1^0, \circlearrowleft$	
7	7	07	090	10	08.7	05.6	.	.	.	$\Delta^0 22^0 24^0, \circlearrowleft$	
8	7	10	10	05	08.3	00.0	.	.	.	$\Delta^0 0^0 3^0, = 10^0 10^0, \Delta^0 1^0 15^0, \infty 10^0 19^0, \circlearrowleft$	
9	7	010	010	09	03.7	09.8	.	.	.	$\Delta^0 0^0 1^0, = 10^0 9^0, \infty 9^0 20^0, \bullet 0^0 13^0 14^0, 16^0 16^0, \circlearrowleft$	
10	6	10	100	10	10.0	00.4	.	.	.	$\Delta^0 0^0 23^0 7^0, \circlearrowleft$	
11	7	040	100	100	J8.3	02.6	00.2	.	.	$\bullet 0^0 6^0, 10^0 17^0, 20^0 24^0, \bullet 0^0 10^0 15^0, \Delta^0 15^0 15^0, = 23^0 24^0, \circlearrowleft$	
12	6	100	100	11	10.0	19.0	18.3	.	.	$= 0^0 24^0, \bullet 0^0 24^0, \circlearrowleft$	
13	5	100	100	10*	10.0	30.0	50.0	00	.	$= 0^0 3^0, 24^0 24^0, \bullet 0^0 10^0 15^0, 15^0 15^0, \bullet 0^0 14^0 22^0, \star 20^0 24^0, \square$	
14	5	10*	10*	10*	10.0	10.0	26.9	05	.	$= 0^0 24^0, \star 0^0 10^0 15^0, \bullet 0^0 10^0 16^0, \bullet 0^0 14^0 19^0, 22^0 24^0, \square$	
15	7	100	100	100	10.0	30.0	20.8	08	.	$= 0^0 8^0, 17^0 24^0, \bullet 0^0 10^0 15^0, \bullet 0^0 21^0 24^0, \circlearrowleft$	
16	7	10	070	08	J8.3	03.2	16.2	01	.	$\bullet 0^0 2^0 20^0, = 0^0 10^0, 23^0 24^0, \bullet 0^0 23^0 30^0, \bullet 0^0 16^0 16^0, \Delta^0 21^0 24^0, \circlearrowleft$	
17	7	100	050	05	06.7	06.6	00.0	.	.	$= 0^0 2^0 7^0, \Delta^0 10^0 14^0, \Delta^0 0^0 30^0, 20^0 24^0, = 0^0 2^0 10^0 8^0, \bullet 0^0 10^0 20^0, \bullet 0^0 10^0 20^0, \circlearrowleft$	
18	7	020	060	04	04.0	19.2	00.0	.	.	$= 0^0 8^0, \Delta^0 0^0 10^0, 20^0 24^0, \circlearrowleft$	
19	8	010	080	09	06.0	05.3	.	.	.	$\Delta^0 0^0 7^0, \Delta^0 8^0 20^0, \infty 8^0 10^0, 10^0 10^0, \circlearrowleft$	
20	7	09	09	05	17.7	32.7	.	.	.	$\Delta^0 0^0 30^0, 9^0 30^0, 14^0 18^0, = 21^0 24^0, \circlearrowleft$	
21	6	100	090	100	09.7	04.7	00.5	.	.	$= 0^0 10^0 20^0, \bullet 0^0 10^0 25^0, \bullet 0^0 20^0 30^0, \bullet 0^0 16^0 16^0, \Delta^0 21^0 24^0, \circlearrowleft$	
22	7	030	100	09	06.0	18.5	05.4	.	.	$\bullet 0^0 2^0 8^0, \Delta^0 8^0 14^0, \circlearrowleft$	
23	8	04	060	09	08.0	29.0	00.0	.	.	$\bullet 0^0 4^0 10^0, \Delta^0 20^0 24^0, \circlearrowleft$	
24	7	050	100	08	07.7	15.9	.	.	.	$\bullet 0^0 4^0 15^0, \Delta^0 0^0 10^0, 20^0 24^0, \bullet 0^0 10^0 12^0, \bullet 0^0 12^0 13^0, \bullet 0^0 14^0 15^0, \circlearrowleft$	
25	7	010	020	04	01.7	11.1	00.1	.	.	$\Delta^0 0^0 8^0, = 0^0 20^0, 20^0 24^0, \circlearrowleft$	
26	7	030	090	07	36.3	15.4	.	.	.	$\Delta^0 0^0 15^0, = 3^0 10^0, 10^0 15^0, \Delta^0 10^0 15^0, \bullet 0^0 18^0 18^0, \circlearrowleft$	
27	8	010	090	09	09.3	32.8	00.0	.	.	$\bullet 0^0 2^0 10^0, 10^0 12^0, = 3^0 10^0, \circlearrowleft$	
28	8	09	050	01	-0.5	37.7	04.1	.	.	$\bullet 0^0 5^0 5^0, \Delta^0 0^0 10^0, 12^0, \circlearrowleft$	
29	7	040	050	10	16.3	38.1	00.0	.	.	$\Delta^0 0^0 6^0, = 0^0 10^0, 10^0 10^0, \bullet 0^0 15^0 15^0, \circlearrowleft$	
30	8	09	090	10	09.3	04.0	00.0	.	.	$\bullet 0^0 10^0, 10^0 10^0, \circlearrowleft$	
MES. RED.					36.9	37.5	27.5	27.3	143.6	154.7	

$\varphi = 46^{\circ}04' N$ $\lambda = 14^{\circ}31' E$ Gr. $\Delta G = + 58$ min.

BR. ST. 13

Dan	Vzdušni pritisak P mm			Temperatura vazduha T C°								Napon vodenе pare e mm			Relativna vlažnost u %				Pravac i jačina veta D, f (0-12)				
	7	14	21	7	14	21	Sred Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dnes	7	14	21			
1	724.5	722.3	722.0	10.2	13.7	12.8	12.4	15.1	9.1	04.7	08.4	09.4	09.5	90	80	86	85	WSW 1	NNE 1	SW 2			
2	720.1	721.7	725.1	09.8	12.8	12.2	11.8	15.9	08.4	04.9	08.6	08.3	07.4	95	74	70	80	NNE 1	S 2	SW 2			
3	729.6	731.5	734.6	09.9	19.4	13.7	14.2	19.4	09.6	06.1	07.4	06.9	07.9	81	41	67	63	NNW 2	SSW 3	SSW 2			
4	736.1	736.7	737.3	11.0	17.6	13.0	13.7	19.3	08.6	03.0	08.0	06.9	06.6	82	46	59	62	SSW 1	SSW 3	SSW 1			
5	737.7	735.5	734.8	07.6	21.0	16.4	15.4	21.1	05.6	00.8	07.3	07.2	06.5	93	39	46	59	E 1	SW 3	SSW 2			
6	733.4	731.5	729.6	11.1	14.7	11.3	12.1	16.4	10.6	06.6	09.6	09.1	09.7	97	72	97	89	E 1	S 1	N 1			
7	726.8	726.3	726.8	10.1	15.6	11.6	12.2	16.9	10.1	09.1	09.2	08.6	07.5	99	65	73	79	NNW 1	SW 1	SSW 2			
8	727.6	726.0	727.8	10.0	19.0	13.4	14.0	20.4	06.2	04.5	08.2	05.8	07.4	89	35	64	63	NNE 1	W 2	W 2			
9	728.5	728.8	731.2	09.8	19.1	14.2	14.3	20.0	09.4	07.0	08.6	06.7	08.7	95	41	72	69	NNW 1	NNE 2	S 2			
10	734.2	734.8	736.7	10.9	16.3	11.1	12.4	16.7	10.6	09.4	08.8	07.1	07.5	90	51	75	72	ESE 1	E 3	NE 1			
11	736.4	738.6	738.9	07.4	05.1	03.7	05.0	12.2	02.4	01.1	06.9	05.6	04.9	89	86	82	86	E 3	SE 2	SE 3			
12	737.6	734.2	731.4	01.7	09.7	08.4	07.1	12.0	-00.4	-02.1	04.8	03.1	04.2	92	37	51	60	ENE 1	SW 2	SSW 2			
13	729.4	728.8	726.7	05.8	04.5	00.8	03.0	08.4	00.7	01.3	05.9	05.9	04.8	85	93	98	92	S 2	ESE 2	NNW 1			
14	730.6	731.5	733.5	02.0	14.5	07.7	08.0	14.9	00.8	00.2	05.1	06.0	07.1	97	48	90	78	ENE 1	SE 2	NE 1			
15	733.5	731.7	732.2	04.7	14.9	09.0	09.4	16.0	03.7	-01.1	06.2	05.6	07.0	97	44	82	74	NNW 1	SE 2	S 2			
16	733.8	733.3	735.2	05.1	18.2	10.9	11.3	19.4	03.3	-01.4	06.4	05.1	06.9	97	33	71	67	ENE 1	WSW 2	S 1			
17	736.4	736.3	735.8	06.0	12.3	10.6	09.9	14.7	03.6	-01.4	06.5	05.8	08.5	93	81	88	87	NE 1	SSW 3	SSW 2			
18	735.8	735.2	734.9	10.5	17.6	14.6	14.3	18.9	08.7	06.0	08.6	07.8	08.4	91	52	67	70	ENE 1	SW 2	MSW 2			
19	733.7	733.9	732.8	12.0	13.4	12.6	12.7	18.9	10.0	07.5	09.6	10.7	10.6	91	92	97	93	NNE 1	S 2	SE 1			
20	733.0	732.7	734.8	12.9	23.0	13.6	15.8	23.0	11.7	10.8	10.8	08.4	11.1	97	40	95	77	NW 1	SSE 2	- 0			
21	734.2	733.0	731.3	13.2	16.2	15.0	14.9	16.9	11.9	08.2	10.9	12.2	12.1	96	88	95	93	NE 1	NNE 1	NNE 1			
22	726.6	723.9	723.6	14.2	15.8	12.6	13.8	16.3	12.6	08.5	11.9	11.7	10.5	98	87	96	94	NE 1	SE 2	SE 1			
23	724.5	726.4	727.8	14.1	14.2	12.7	13.4	16.6	09.4	06.6	08.3	08.7	09.0	69	72	82	74	SSW 3	SSW 2	SW 2			
24	729.3	731.2	732.3	11.7	13.4	11.7	12.1	14.8	10.6	10.3	09.7	08.4	08.9	94	73	87	85	WSW 1	SW 1	SE 1			
25	733.5	733.7	735.0	11.2	20.8	14.2	15.1	20.8	10.3	06.0	09.1	08.7	09.7	91	47	80	73	ESE 1	ESE 2	NNE 1			
26	736.3	736.4	737.4	09.7	18.6	11.3	12.7	19.6	09.0	05.2	08.8	07.7	09.7	98	48	97	81	WWN 1	SSE 2	NE 1			
27	737.2	736.1	736.8	08.9	18.4	13.3	13.5	19.0	08.7	06.1	08.4	06.3	06.8	99	39	59	66	N 1	ENE 3	ENE 2			
28	736.9	736.9	738.0	11.4	18.8	12.4	13.8	21.7	08.6	04.6	08.1	07.5	08.9	80	46	83	70	ENE 1	N 2	W 2			
29	736.7	734.7	735.0	11.8	20.9	13.0	14.7	22.4	09.1	04.4	08.8	07.0	10.6	84	38	95	72	S 2	NNE 2	SSE 1			
30	735.2	735.4	737.4	12.8	18.7	12.5	14.1	20.8	11.0	06.0	09.3	07.5	10.5	84	47	97	76	NW 1	ENE 3	W 1			
31	738.2	737.8	738.6	11.8	21.0	15.5	16.0	21.7	10.3	06.1	10.0	09.8	11.6	97	52	88	79	NW 1	SE 2	WWN 2			
MES.	YRED.			732.5	732.2	732.8	09.6	16.1	11.8	12.4	17.7	07.9	04.8	08.3	07.7	08.4	91	58	80	76	1.2	2.1	1.5

1	740.3	739.0	739.1	13.0	24.7	16.9	17.9	25.3	10.7	06.2	10.6	09.3	10.5	95	40	73	69	W 1	SE 2	NNE 2
2	739.8	737.5	737.4	12.2	26.2	17.2	18.2	27.3	09.5	05.4	09.6	08.4	13.0	90	33	89	71	NNE 1	NNE 2	E 1
3	737.6	735.8	736.4	13.8	27.4	17.7	19.2	28.8	11.1	07.6	10.5	09.5	10.0	88	35	66	63	NNE 1	ESE 2	NNE 1
4	737.5	736.2	737.3	14.6	23.6	19.8	19.5	28.0	11.3	07.9	09.6	10.7	10.1	77	49	58	61	NE 1	S 2	S 1
5	737.8	736.4	737.1	15.6	28.0	20.4	21.1	28.0	12.0	09.2	10.7	09.0	08.7	80	32	48	53	NNE 1	SSW 3	WSW 2
6	736.9	735.1	736.1	15.4	27.2	20.0	20.7	27.3	11.8	10.4	10.7	09.2	08.1	81	34	46	54	NE 2	WSW 3	W 2
7	736.0	735.2	735.8	15.0	26.9	21.2	21.1	27.2	12.4	13.2	10.4	10.4	09.7	81	39	51	57	NNE 1	SW 4	SW 3
8	735.3	734.0	736.0	18.0	26.2	19.0	20.6	26.3	13.5	10.5	11.4	10.1	11.6	74	39	70	61	N 1	SSW 2	SSW 1
9	736.7	734.6	734.3	16.0	25.4	21.6	21.2	26.4	13.3	09.9	11.8	11.5	11.3	86	47	58	64	NE 1	S 1	S 2
10	734.1	733.1	733.8	16.6	25.8	21.2	21.2	26.0	15.1	12.5	12.3	10.9	10.9	86	44	58	63	NNE 1	WSW 3	SSW 1
11	735.7	738.4	738.8	16.2	14.4	13.6	14.5	21.2	13.6	12.6	13.2	11.8	11.3	96	96	97	96	NNE 1	NNE 2	NNW 1
12	735.3	731.7	730.0	14.0	17.2	15.2	15.4	17.2	12.7	11.0	11.4	10.8	12.3	95	73	95	88	NE 2	SE 1	ENE 1
13	731.7	732.7	733.3	12.4	11.0	09.7	10.7	15.4	08.6	12.2	10.3	08.7	08.6	96	88	95	93	NNE 2	SSE 2	E 1
14	732.3	732.4	731.9	09.6	15.6	11.8	12.2	17.2	09.0	08.7	08.5	07.8	08.5	95	58	82	78	ENE 1	S 1	ENE 1
15	732.5	729.9	727.5	09.2	20.2	13.9	14.3	20.7	08.1	08.2	08.5	07.3	08.4	98	41	70	70	ESE 1	SSE 2	SSE 1
16	727.2	726.4	726.9	10.4	21.6	16.4	16.2	21.9	07.4	05.1	08.2	07.9	11.3	87	41	81	70	ENE 1	E 2	SM 1
17	727.0	727.5	728.0	14.2	15.6	14.4	14.7	16.6	12.7	11.7	11.1</td									

BR. ST. 13

$$H_s = 299 \text{ m } H_b = 297.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.5 \text{ m}$$

Dan	Vlaknos 0-9	Oblačnost N (0-10)					Insekcija broj seni	Padavina R mm	Snežni pokrivač h cm	Razvoj vremene w
		14	7	14	21	Sred Dies				
1	7 09	10	08	09.0	00.3	00.0	.	0°-6°, 17°-18°, 1= 0°-10°, ○		
2	7 09	09	06	08.0	01.4	04.6	.	0°-10°, 13°-14°, 1= 23°-24, ○		
3	7 01○	05○	06	04.0	11.6	00.0	.	0°-10°, 8°, ○		
4	7 09○	07○	00	05.3	04.2	00.1	.	0°-10°, 1= 0°-10°, ○		
5	8 10	10	09	09.7	03.3	.	.	0°-10°, 1= 21°-22°, 12°, ○		
6	7 09	10	10	09.7	00.4	06.0	.	0°-10°, 6°, 15°-16°, 1= 0°-10°, 15°-20°, 1= 13°-24, ○		
7	7 10	07○	02	06.3	03.1	17.9	.	0°-10°, 13°-14°, 1= 0°-13°, 1= 9°-10°, ○		
8	8 07○	05○	10	07.3	08.1	01.4	.	0°-10°, 12°-13°, ○		
9	8 10○	06○	09○	08.3	03.3	00.1	.	0°-10°, 7°-9°, 15°-16°, 1= 10°-15°, 1= 20°-21°, 1= 21°-22°, 1= 22°-23°, ○		
10	8 10	02○	05	05.7	07.7	01.4	.	0°-10°, 12°-13°, 1= 10°-12°, 15°-16°, 1= 20°-21°, 1= 21°-22°, 1= 22°-23°, 1= 23°-24, ○		
11	7 10	09○	10	09.7	00.4	00.7	.	0°-10°, 1= 10°-12°, 1= 10°-15°, 1= 15°-20°, 1= 17°-20°, 1= 18°-19°, ○		
12	8 02○	06○	10	06.0	09.6	04.2	.	0°-10°, 7°, 1= 4°-5°, 5°, ○		
13	6 10○	10○	10*	10.0	00.0	00.1	.	0°-10°, 10°-11°, 1= 10°-11°, 1= 11°-12°, 1= 12°-13°, □		
14	8 10	05○	05	06.7	07.5	33.8	01	0°-10°, 1= 0°-10°, 1= 11°-12°, 1= 12°-13°, 1= 13°-14°, 1= 14°-15°, 1= 15°-16°, 1= 16°-17°, 1= 17°-18°, 1= 18°-19°, 1= 19°-20°, 1= 20°-21°, 1= 21°-22°, 1= 22°-23°, 1= 23°-24, ○, □		
15	7 10	09○	05	08.0	03.6	00.0	.	0°-10°, 1= 0°-10°, 1= 11°-12°, 1= 12°-13°, 1= 13°-14°, 1= 14°-15°, 1= 15°-16°, 1= 16°-17°, 1= 17°-18°, 1= 18°-19°, 1= 19°-20°, 1= 20°-21°, 1= 21°-22°, 1= 22°-23°, 1= 23°-24, ○		
16	8 00=○	09	01	03.3	07.7	00.0	.	0°-10°, 10°-11°, 1= 0°-8°, 1= 10°-11°, 1= 11°-12°, 1= 12°-13°, 1= 13°-14°, 1= 14°-15°, 1= 15°-16°, 1= 16°-17°, 1= 17°-18°, 1= 18°-19°, 1= 19°-20°, 1= 20°-21°, 1= 21°-22°, 1= 22°-23°, 1= 23°-24, ○		
17	7 07○	10	09	08.7	01.0	00.2	.	0°-10°, 1= 4°-5°, 1= 9°-10°, 1= 9°-10°, 1= 10°-11°, 1= 11°-12°, 1= 12°-13°, 1= 13°-14°, 1= 14°-15°, 1= 15°-16°, 1= 16°-17°, 1= 17°-18°, 1= 18°-19°, 1= 19°-20°, 1= 20°-21°, 1= 21°-22°, 1= 22°-23°, 1= 23°-24, ○		
18	7 08	09	09	08.7	05.0	00.7	.	0°-10°, 1= 4°-5°, 1= 9°-10°, 1= 9°-10°, 1= 10°-11°, 1= 11°-12°, 1= 12°-13°, 1= 13°-14°, 1= 14°-15°, 1= 15°-16°, 1= 16°-17°, 1= 17°-18°, 1= 18°-19°, 1= 19°-20°, 1= 20°-21°, 1= 21°-22°, 1= 22°-23°, 1= 23°-24, ○		
19	6 09	10	10*	09.7	00.8	.	.	0°-10°, 1= 0°-10°, 1= 11°-12°, 1= 12°-13°, 1= 13°-14°, 1= 14°-15°, 1= 15°-16°, 1= 16°-17°, 1= 17°-18°, 1= 18°-19°, 1= 19°-20°, 1= 20°-21°, 1= 21°-22°, 1= 22°-23°, 1= 23°-24, ○		
20	7 10	05○	10	08.3	07.1	12.6	.	0°-10°, 1= 0°-10°, 1= 11°-12°, 1= 12°-13°, 1= 13°-14°, 1= 14°-15°, 1= 15°-16°, 1= 16°-17°, 1= 17°-18°, 1= 18°-19°, 1= 19°-20°, 1= 20°-21°, 1= 21°-22°, 1= 22°-23°, 1= 23°-24, ○		
21	7 10	10	10	10.0	00.0	04.6	.	0°-10°, 1= 2°-10°, 1= 11°-12°, 1= 12°-13°, 1= 13°-14°, 1= 14°-15°, 1= 15°-16°, 1= 16°-17°, 1= 17°-18°, 1= 18°-19°, 1= 19°-20°, 1= 20°-21°, 1= 21°-22°, 1= 22°-23°, 1= 23°-24, ○		
22	7 10*	10	07	09.0	00.1	07.3	.	0°-10°, 1= 0°-10°, 1= 11°-12°, 1= 12°-13°, 1= 13°-14°, 1= 14°-15°, 1= 15°-16°, 1= 16°-17°, 1= 17°-18°, 1= 18°-19°, 1= 19°-20°, 1= 20°-21°, 1= 21°-22°, 1= 22°-23°, 1= 23°-24, ○		
23	7 09	10	10	09.7	02.8	04.4	.	0°-10°, 1= 0°-10°, 1= 11°-12°, 1= 12°-13°, 1= 13°-14°, 1= 14°-15°, 1= 15°-16°, 1= 16°-17°, 1= 17°-18°, 1= 18°-19°, 1= 19°-20°, 1= 20°-21°, 1= 21°-22°, 1= 22°-23°, 1= 23°-24, ○		
24	6 10*	10	02	07.3	00.0	03.4	.	0°-10°, 1= 0°-10°, 1= 11°-12°, 1= 12°-13°, 1= 13°-14°, 1= 14°-15°, 1= 15°-16°, 1= 16°-17°, 1= 17°-18°, 1= 18°-19°, 1= 19°-20°, 1= 20°-21°, 1= 21°-22°, 1= 22°-23°, 1= 23°-24, ○		
25	7 10	05○	08	07.7	06.3	00.8	.	0°-10°, 1= 0°-10°, 1= 11°-12°, 1= 12°-13°, 1= 13°-14°, 1= 14°-15°, 1= 15°-16°, 1= 16°-17°, 1= 17°-18°, 1= 18°-19°, 1= 19°-20°, 1= 20°-21°, 1= 21°-22°, 1= 22°-23°, 1= 23°-24, ○		
26	7 10=	10	09	09.7	02.2	00.0	.	0°-10°, 1= 0°-10°, 1= 11°-12°, 1= 12°-13°, 1= 13°-14°, 1= 14°-15°, 1= 15°-16°, 1= 16°-17°, 1= 17°-18°, 1= 18°-19°, 1= 19°-20°, 1= 20°-21°, 1= 21°-22°, 1= 22°-23°, 1= 23°-24, ○		
27	7 09	09○	07	08.3	07.4	05.4	.	0°-10°, 1= 0°-10°, 1= 11°-12°, 1= 12°-13°, 1= 13°-14°, 1= 14°-15°, 1= 15°-16°, 1= 16°-17°, 1= 17°-18°, 1= 18°-19°, 1= 19°-20°, 1= 20°-21°, 1= 21°-22°, 1= 22°-23°, 1= 23°-24, ○		
28	8 02○	05○	09	05.3	09.2	00.0	.	0°-10°, 1= 0°-10°, 1= 11°-12°, 1= 12°-13°, 1= 13°-14°, 1= 14°-15°, 1= 15°-16°, 1= 16°-17°, 1= 17°-18°, 1= 18°-19°, 1= 19°-20°, 1= 20°-21°, 1= 21°-22°, 1= 22°-23°, 1= 23°-24, ○		
29	8 02○	09	09	06.7	08.4	00.3	.	0°-10°, 1= 0°-10°, 1= 11°-12°, 1= 12°-13°, 1= 13°-14°, 1= 14°-15°, 1= 15°-16°, 1= 16°-17°, 1= 17°-18°, 1= 18°-19°, 1= 19°-20°, 1= 20°-21°, 1= 21°-22°, 1= 22°-23°, 1= 23°-24, ○		
30	8 04○	09○	10○	07.7	06.7	03.6	.	0°-10°, 1= 0°-10°, 1= 11°-12°, 1= 12°-13°, 1= 13°-14°, 1= 14°-15°, 1= 15°-16°, 1= 16°-17°, 1= 17°-18°, 1= 18°-19°, 1= 19°-20°, 1= 20°-21°, 1= 21°-22°, 1= 22°-23°, 1= 23°-24, ○		
31	7 08○	09○R	02	06.3	05.7	14.7	.	0°-10°, 1= 0°-10°, 1= 11°-12°, 1= 12°-13°, 1= 13°-14°, 1= 14°-15°, 1= 15°-16°, 1= 16°-17°, 1= 17°-18°, 1= 18°-19°, 1= 19°-20°, 1= 20°-21°, 1= 21°-22°, 1= 22°-23°, 1= 23°-24, ○		
MES. RED.		07.9	08.0	07.3	07.7	134.9	128.3			

LJUBLJANA-BEZIGRAD

1978 JUN

1	7	070	030	01	03.7	11.1	02.7	.	= 14.8, ∇° 4-5°, 1° 4°-4°, 18.4°-5°, Δ 23°-24°, ○
2	8	040	020	00	02.0	11.4	.	.	Δ 0-8°, ∇° 5° 16°, Δ^{+4} 16°-16°, ∇° 8°-8°, Δ^{+4} 20°-24°, ○
3	7	000	010	02	01.0	13.1	00.5	.	Δ^{-1} 0.5°, 19.9°-24°, ○
4	7	010	060	09	05.3	08.2	.	.	Δ^{+2} 0-8°, 23°-24°, = 20-5°, 00 8°-19°, ∇ 13°-13°, ○
5	8	010	020	00	01.0	10.4	.	.	Δ^{+2} 0-8°, ○
6	7	040	050	02	03.7	10.4	.	.	Δ° 2-8°, = 20-9°, 00 9°-12°, \oplus 11°-14°, ○
7	8	020	020	03	02.3	10.4	.	.	Δ° 13°-8°, ∇° 4°-11°, ∇° 13°-17°, ○
8	8	310	060	02	03.0	09.7	00.0	.	Δ° 4-7°, 00 10°-19°, ○
9	7	020	090	00	03.7	08.2	.	.	Δ^{+1} 0.5°, = 4°-9°, 00 9°-12°, ○
10	8	010	10	05	05.3	05.3	.	.	00 7°-9°, ○
11	7	10	100	09	09.7	00.0	01.8	.	Δ 2°-4°, = 20-9°, 00 9°-24°, \oplus° 4-20°, i
12	7	09	100	10	09.7	00.1	49.2	.	= 0-9°, 13°-24°, \oplus° 4-20°, 00 20°-24°, 0-1-19°-19°, ○
13	7	100	100	100	10.0	00.0	31.2	.	= 0-9°, 23°-24°, \oplus° 4-24°, ∇ 4-5°, 5°
14	7	100	090	02	07.0	04.1	16.8	.	\bullet 0-7°, = 0-8°, Δ 20°-24°, ○
15	8	10	050	01	05.3	10.6	00.0	.	Δ^{+4} 0-10°, 20°-24°, = 10-3°, 7°-10°, = 0-13°, 7°-30°, ○
16	8	010	060	09	05.3	09.9	.	.	Δ° 0-10°, = 10-10°, 00 10°-12°, \oplus° 4-16°, 17°, \oplus° 24°-21°, ○
17	6	09	100	100	09.7	00.0	00.9	.	\bullet 0-15°, 12°, i = 9°-24°, ○
18	8	030	010	01	01.7	12.4	27.6	.	= 0-3°, 6°-7°, = 0-3-4°, 6°-7°, ∇ 14°-14°, Δ 0-1-21°-24°, ○
19	8	020	030	09	04.7	13.8	.	.	Δ° 0-9°, 21°-22°, \oplus° 24°-24°, ∇ 21°-24°, ○
20	8	080	030	01	04.0	08.8	28.3	.	Δ^{+2} 0-0°, 17°-18°, 18°-18°, 0-0°, 17°-18°, \oplus° 4-13°, = 0-10°, ○
21	7	090	09	06	08.0	02.3	01.6	.	= 0-9°, Δ° 6°-7°, 00 9°-13°, \oplus° 19°-20°, ○
22	8	070	040	00	03.7	00.0	00.0	.	= 0-10°, Δ° 8°-11°, Δ 0-1-21°-24°, ○
23	7	010	090	09	06.3	10.2	00.1	.	Δ° 0-9°, 00 7°-12°, 12°-15°, \oplus° 11°-15°, Δ 0-1-22°-23°, ○
24	8	090	070	090K	08.3	06.0	00.6	.	\bullet 0-5°, 5°-8°, 20°-21°, ∇ 14°-14°, \oplus° 18-20°, T 10°-21°, Δ 22°-23°, ○
25	7	020	080	100	06.7	05.3	00.2	.	\bullet 0-10°, 11°-12°, ∇ 10°-12°, \oplus° 12°-13°, 19°-24°, ∇ 20°-23°, ○
26	9	040	040	02	03.3	11.3	10.2	.	Δ^{+2} 0-0°, 5°-5°, 15°-15°, Δ 14°-14°, T 0°-14°, 18°-18°, Δ 20°-24°, ○
27	8	10	090	09	09.3	04.6	00.9	.	Δ^{+1} 0-10°, Δ° 4°-10°, ∇ 7°-17°, 12°-16°, 19°-19°, ∇ 13°-13°, ○
28	9	340	040	02	03.3	11.9	03.4	.	= 3°-6°, Δ 21°-24°, ○
29	8	310	050	03	03.0	12.3	.	.	Δ^{+2} 0-9°, 21°-24°, = 22-24°, ○
30	7	000	020	07	03.0	12.4	.	.	Δ° 0-8°, 23°-24°, = 0-6°, ○

$\varphi = 46^{\circ}04' N$ $\lambda = 14^{\circ}31' E$ Gr. $\Delta G = + 58$ min.

BR. ST. 13

D S	Vzdušni pritisak P mm			Temperatura vazduha T °C								Napon vodenе pare e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0-12)			
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21	
1	736.0	735.3	735.6	15.3	24.6	18.9	19.4	26.2	12.1	0.9.2	10.2	0.9.8	11.0	78	42	67	62	ENE 1	W 3	NNW 1	
2	735.7	736.7	736.2	15.4	16.5	14.4	15.2	19.7	14.4	11.8	11.7	11.5	11.4	89	82	93	88	SSE 1	SE 1	NNE 1	
3	735.2	732.9	732.4	12.5	25.7	18.7	18.9	26.6	11.5	0.8.8	10.3	0.8.7	0.9.6	94	35	60	63	SSW 1	S 3	S 2	
4	731.7	730.9	729.6	16.9	22.1	19.6	19.6	24.0	13.3	10.3	11.3	11.6	11.4	78	58	67	68	E 1	SW 3	SSW 1	
5	728.2	728.1	731.8	16.4	19.6	10.7	14.4	20.0	10.7	14.6	13.4	11.3	0.9.2	96	66	95	86	ENE 1	W 2	ESE 1	
6	734.7	732.8	732.6	09.3	16.4	14.4	13.6	20.0	08.6	0.5.4	08.5	11.4	11.8	96	82	96	91	NE 1	W 2	NNW 1	
7	732.6	734.0	735.2	11.6	13.6	12.8	12.7	16.8	10.8	0.9.3	09.8	10.1	0.9.4	95	86	85	89	NNW 2	NNE 1	W 1	
8	736.9	735.9	736.4	10.4	18.9	13.7	14.2	20.2	10.0	0.7.7	0.9.0	0.6.5	10.3	95	40	87	74	WSW 1	NNE 1	W 2	
9	734.9	731.3	730.4	09.7	21.2	16.3	15.9	21.7	09.6	0.5.1	08.8	0.8.0	10.0	98	42	72	71	S 1	SW 4	NNW 1	
10	731.3	731.7	732.4	13.2	17.0	17.3	16.2	19.9	12.8	12.0	10.8	11.4	13.3	95	78	90	88	NW 2	SE 1	ESE 1	
11	733.7	734.4	734.2	14.4	20.7	19.2	18.4	22.6	12.0	14.4	11.8	12.1	13.4	96	66	80	81	NE 1	ESE 2	S 2	
12	735.6	734.5	735.5	16.1	27.8	20.6	21.3	26.5	13.8	11.7	13.3	10.6	0.8.7	97	38	48	61	SSE 1	SW 3	S 2	
13	738.2	736.7	738.5	17.4	28.8	17.7	20.4	29.1	13.7	10.2	11.5	11.4	13.8	77	38	91	69	W 1	ESE 2	SSW 1	
14	738.8	737.2	737.3	17.6	26.4	20.0	21.0	27.0	15.7	14.4	13.8	12.9	16.3	91	50	93	78	ENE 2	E 2	W 2	
15	734.6	735.0	736.1	17.4	19.0	17.5	17.9	25.4	15.8	14.7	13.8	13.5	13.7	92	82	91	88	ENE 2	E 2	NNW 2	
16	736.6	735.1	735.0	16.3	21.7	18.4	18.7	23.3	13.4	10.4	10.5	10.5	13.4	75	54	84	71	E 2	ENE 2	E 1	
17	737.2	736.2	735.5	16.0	24.1	20.4	20.2	26.1	14.6	11.4	12.8	13.3	15.0	94	59	84	79	NNE 1	NE 1	S 1	
18	734.1	731.2	730.0	16.3	26.8	20.5	21.0	27.8	15.0	12.9	13.6	13.8	14.2	98	52	76	76	ENE 1	SW 3	NNW 1	
19	728.8	729.6	732.1	14.0	17.1	15.2	15.4	21.4	12.5	10.5	10.9	11.9	12.4	87	66	92	82	NNW 3	-	E 1	
20	734.4	731.9	730.8	13.0	23.2	17.2	17.7	24.2	11.3	0.7.2	10.3	0.9.1	12.4	91	43	84	73	N 1	SSE 2	SW 1	
21	731.3	731.6	735.0	14.8	15.7	10.4	12.8	17.4	10.4	10.0	11.2	12.7	0.9.2	89	95	98	94	-	0	ENE 1	
22	737.5	737.6	738.8	10.1	20.0	16.1	15.6	22.0	0.9.3	0.5.0	09.2	0.7.6	10.7	99	43	78	73	NNW 2	E 3	E 1	
23	739.1	737.8	738.0	10.9	21.4	15.0	15.6	22.0	0.8.5	0.4.9	09.3	0.7.5	10.1	95	39	79	71	NE 1	SE 2	NE 3	
24	738.3	736.6	737.0	11.4	23.0	18.0	17.6	23.7	0.9.0	0.5.3	09.4	0.9.5	10.5	93	45	68	69	NE 1	SE 2	E 1	
25	737.7	736.0	736.7	13.2	25.0	19.4	19.3	25.1	11.1	0.7.2	10.6	0.9.7	10.2	94	41	60	65	E 1	ENE 1		
MES.	RED.	735.5	734.6	735.1	14.2	22.4	17.3	17.8	23.9	12.2	0.9.8	11.1	10.6	11.8	91	54	80	75	1.2	1.9	1.3

1978 AVGUST

LJUBLJANA-BEŽIGRAD

1	736.2	735.3	735.2	14.9	27.3	21.3	21.2	28.5	13.7	11.8	12.2	13.0	16.9	96	48	89	78	SW 1	S 2	ENE 1
2	736.0	734.7	735.5	17.8	29.4	22.0	22.8	29.5	16.3	13.0	14.6	12.7	14.7	95	41	74	70	W 1	SW 2	NNE 1
3	735.7	733.8	734.9	16.7	29.2	23.6	23.3	29.5	15.5	11.8	13.6	13.9	13.6	95	46	62	68	NE 1	SW 1	S 1
4	736.1	734.8	735.5	17.0	16.9	16.6	16.8	24.2	15.8	11.8	13.6	13.7	13.2	93	95	93	94	SSE 1	WNW 2	SW 1
5	736.8	735.1	735.6	15.6	26.9	21.2	21.2	27.6	14.0	12.2	12.9	12.1	14.9	97	45	79	74	SSW 1	SE 2	W 1
6	735.3	733.2	732.5	17.1	28.3	22.4	22.6	29.0	15.4	12.6	12.3	13.6	15.9	84	47	78	70	SE 1	E 1	S 1
7	731.0	728.6	724.6	17.7	27.1	23.4	22.9	29.6	16.4	13.8	14.2	14.6	14.3	93	54	66	71	NE 1	SSW 2	NW 1
8	722.7	725.9	730.1	19.1	17.5	13.3	15.8	24.7	12.8	14.2	11.3	11.3	10.6	68	75	92	78	SSW 2	WSW 3	WSW 1
9	733.3	732.0	733.2	10.6	24.6	17.6	17.6	24.8	10.0	0.7.4	0.9.4	0.9.5	0.9.8	98	41	65	68	WNW 1	SSW 2	WSW 1
10	735.0	735.0	735.7	13.6	17.2	12.8	14.1	20.0	12.8	12.6	11.2	10.8	10.1	96	73	91	87	NNE 2	ENE 1	NNE 1
11	736.9	736.0	736.3	10.3	22.2	14.0	15.1	22.2	0.9.3	0.7.0	0.9.2	0.9.9	10.7	98	49	90	79	S 1	NNE 2	NE 1
12	736.0	736.7	737.5	10.9	22.4	15.3	16.0	22.7	10.0	0.7.0	0.9.3	0.7.8	10.8	95	38	83	72	N 1	E 2	N 1
13	737.7	736.2	735.6	12.2	14.7	14.0	13.7	16.6	10.6	0.7.1	10.1	10.9	11.5	94	87	96	92	NE 1	I S 1	- 0
14	736.6	737.3	737.5	13.3	18.8	13.7	14.9	20.6	13.0	11.6	11.1	10.8	10.9	97	60	93	83	WNW 1	E 1	NNE 1
15	737.8	736.2	736.4	11.1	23.2	18.0	17.6	25.5	10.3	0.7.0	0.9.6	11.2	11.7	97	52	76	75	SE 1	NE 2	S 3
16	737.4	736.3	736.7	11.6	26.4	18.8	18.9	26.8	10.8	0.7.6	10.0	12.3	12.2	98	48	75	74	ENE 1	WSW 2	SSW 1
17	737.7	737.2	736.0	13.7	22.7	17.0	17.6	24.2	12.9	0.9.6	11.5	12.4	14.3	98	60	98	85	ENE 1	SE 2	NNE 3
18	738.4	738.1	739.9	14.6	22.7	17.6	18.1	23.4	14.0	13.0	11.8	10.3	11.6	95	50	77	74	WNW 1	E 2	ENE 2
19	740.8	739.1	738.9	13.5	21.2	15.4	16.4	22.8	11.7	0.7.6	0.9.8	0.9.6	10.7	84	51	81	72	N 1	SE 2	NE 1
20	738.7	737.0	738.0	10.9	23.1	15.4	16.2	24.9	0.9.8	0.6.0	0.9.6	10.6	11.5	98	50	88	79	SSE 1	SE 1	WNW 1
21	739.0	738.2	739.2	11.1	25.0	17.1	17.6	25.4	10.5	0.6.4	0.9.8	10.1	11.6	99	43	79	74	ENE 1	SE 2	NE 1
22	739.9	738.9	738.6	14.6	24.6	18.7	19.2	25.2	12.0	0.9.4	11.2	11.6	12.3	90	50	76	72	SSE 1	SE 2	NE 1
23	737.9	736.8	737.2	13.9	25.5	19.0	19.4	26.6	13.3	0.9.4	11.2									

BR. ST. 13

$$H_s = 299 \text{ m } H_b = 297.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.5 \text{ m}$$

LJUBLJANA-BEŽIGRAD

1978 AUGUST

1978 SEPTEMBAR

LJUBLJANA-BEŽIGRAD

φ = 46°04' N λ = 14°31' E Gr. ΔG = + 58 min.

BR. ST. 13

Dn	Vazdušni pritisak P mm			Temperatura vazduha T °C								Napon vodenih pare e mm			Relativna vlažnost u %				Pravac i jačina veta D, 1 (0—12)					
	7	14	21	7	14	21	Sred. Dies	Max	Min	Mn 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21				
1	730.7	729.5	730.2	04.6	14.8	11.3	10.5	18.7	03.6	00.5	06.1	06.1	08.7	96	49	86	77	S	1	SSW	4	W	1	
2	731.3	730.2	732.1	07.6	17.8	12.8	12.8	20.8	05.9	02.6	07.6	06.9	09.3	97	45	84	75	ESE	1	N	1	W	3	
3	733.3	732.2	732.4	07.5	20.0	13.7	13.7	21.2	06.4	02.6	07.7	08.9	10.3	99	51	87	79	E	1	SSW	3	SE	1	
4	732.5	731.4	731.1	11.2	21.2	17.2	16.7	21.8	09.4	06.3	09.3	11.6	10.6	93	61	72	75	NNE	1	NNE	2	SSW	1	
5	729.5	728.3	729.1	12.2	23.9	17.3	17.7	24.2	11.9	08.0	09.6	11.2	12.2	90	50	82	74	NNE	1	S	2	SW	2	
6	728.4	727.4	728.4	13.6	22.4	16.1	17.1	22.5	12.7	09.2	11.4	13.1	12.9	98	65	94	86	N	1	NE	4	W	1	
7	727.9	726.4	730.3	14.6	17.8	14.3	15.3	21.7	14.0	11.9	12.1	12.2	11.5	97	80	94	90	W	1	NE	2	SW	1	
8	731.9	732.7	735.0	12.8	18.6	16.2	16.0	20.7	12.5	12.7	10.6	10.2	11.1	96	63	81	80	S	1	ENE	1	SE	2	
9	736.2	735.8	736.9	13.6	22.7	16.4	17.3	24.0	13.4	12.6	11.1	10.8	11.8	95	52	85	77	S	1	SSE	1	S	1	
10	737.2	735.7	735.3	13.9	23.6	18.7	18.7	23.9	12.6	09.5	11.2	14.0	11.7	94	64	73	77	W	1	NE	2	SW	3	
11	734.5	732.1	731.1	12.3	27.6	19.3	19.6	27.1	11.9	08.9	10.6	11.7	13.4	99	42	80	74	NE	1	SSW	2	SW	1	
12	730.5	733.2	734.9	11.6	16.6	11.4	12.8	19.6	10.8	11.3	09.5	08.2	08.8	93	58	88	80	WW	2	SE	2	S	1	
13	738.5	738.5	741.0	06.9	20.8	12.1	13.0	21.4	06.0	02.9	06.5	06.0	06.8	87	31	65	62	WW	1	ENE	1	SE	2	
14	760.6	737.7	736.7	07.3	18.7	10.9	12.0	19.5	05.5	02.4	06.8	07.7	08.6	88	47	88	74	NE	1	E	2	ENE	1	
15	737.3	736.8	737.0	07.7	22.0	13.4	14.1	22.8	06.4	03.5	07.8	10.1	10.7	99	51	92	81	E	1	SE	2	N	1	
16	736.7	739.2	740.0	11.0	19.3	14.7	14.9	22.4	10.6	06.7	09.6	11.4	11.9	98	68	95	87	N	1	SE	1	NE	1	
17	741.5	738.6	738.6	11.4	23.4	16.8	17.1	25.2	10.9	07.1	09.9	11.6	10.1	98	54	70	74	SE	1	E	2	S	1	
18	737.7	736.4	736.7	10.1	24.3	17.4	17.3	24.7	08.8	05.4	09.2	12.5	13.1	99	55	88	81	NE	1	NE	1	NE	1	
19	736.1	735.0	734.0	15.4	18.2	13.4	15.1	18.9	13.3	12.8	12.1	08.5	11.2	92	54	97	81	E	1	SE	2	W	2	
20	737.1	738.2	741.3	11.4	16.8	08.0	11.1	17.7	08.0	07.3	09.9	06.7	05.9	98	47	74	73	E	1	SE	3	E	1	
21	742.6	741.4	741.5	02.6	15.7	08.6	08.9	16.3	02.4	-01.6	05.4	05.3	07.3	98	39	87	75	NE	1	NW	2	W	1	
22	741.6	738.6	737.4	05.8	18.6	12.6	12.4	20.4	05.2	00.8	06.7	08.6	10.3	97	53	94	81	N	1	NE	1	SE	1	
23	734.8	734.3	736.3	10.8	19.9	13.7	14.5	21.6	10.0	09.0	09.6	11.1	93	55	95	61	NE	1	SSW	2	ENE	1		
24	738.5	737.9	739.1	10.4	23.1	17.6	17.2	24.0	10.0	06.6	09.2	12.5	11.1	98	59	73	77	SW	1	SSE	3	SSW	3	
25	740.3	739.5	740.0	10.6	23.1	16.6	16.7	23.7	09.4	05.0	09.4	11.2	11.2	98	53	79	77	ENE	1	SW	3	SW	2	
26	740.0	737.5	736.1	10.3	24.4	16.9	17.1	25.5	10.2	05.6	09.3	12.7	12.4	99	56	86	80	NE	1	ENE	1	NN	2	
27	734.6	734.9	733.8	12.9	12.0	09.4	10.9	17.3	09.4	08.1	10.8	10.0	08.5	97	95	96	96	ENE	1	NE	2	SE	2	
28	731.5	731.9	732.9	07.4	11.7	07.0	08.3	14.0	06.9	06.7	07.3	07.7	07.1	95	75	95	88	ENE	1	W	1	ENE	1	
29	732.6	731.3	732.5	07.0	13.6	10.4	10.4	17.3	06.6	00.8	07.2	08.1	08.3	96	69	88	84	NE	1	SW	2	NW	2	
30	731.5	729.5	728.0	10.8	13.8	13.2	12.8	15.1	09.8	01.4	09.4	11.3	10.5	96	96	92	95	NW	1	W	2	E	1	
MES.	VRED.	735.3	734.5	735.0	10.2	19.5	13.9	14.4	21.2	09.2	06.1	09.1	09.9	10.3	96	58	85	80	1.0	2.0	1.5			

1978 OKTOBAR

LJUBLJANA-BEŽIGRAD

1	730.1	730.6	732.3	06.9	07.3	05.3	06.2	13.6	04.8	06.4	07.1	07.3	06.4	95	95	96	95	ENE	2	NNW	2	NE	2
2	733.9	735.8	736.0	06.6	08.6	08.6	08.1	09.2	04.9	04.7	07.0	07.7	08.0	96	92	95	94	NW	1	NNW	1	NW	1
3	733.9	733.2	732.1	08.6	12.3	11.4	10.9	12.5	08.3	08.2	08.1	09.8	09.9	96	91	98	95	ESE	1	N	1	NNE	1
4	730.2	730.4	732.3	11.0	17.4	12.2	13.2	17.6	10.7	10.3	09.6	10.2	10.1	98	68	94	87	NE	1	SE	2	NE	1
5	736.8	738.6	740.8	10.3	12.8	08.0	09.8	13.4	08.0	08.9	08.5	06.5	07.5	91	59	94	81	SW	2	S	3	E	1
6	741.0	740.0	741.1	06.4	16.2	09.7	10.5	16.9	05.7	01.0	07.0	07.5	08.2	97	54	90	80	W	1	SW	1	NW	1
7	742.1	741.1	741.7	07.4	20.7	10.8	12.4	20.8	06.9	01.4	07.5	09.4	09.3	97	51	95	81	NE	1	W	2	NNE	1
8	741.7	741.2	741.7	09.2	18.4	11.2	12.5	19.2	08.7	03.5	08.5	09.8	09.2	98	62	92	84	ENE	1	SE	2	E	1
9	741.7	740.9	741.4	08.4	19.4	10.4	12.2	20.0	08.0	02.6	08.2	08.3	08.8	99	49	93	83	NE	1	S	2	NE	1
10	741.4	740.9	742.0	08.2	17.9	10.2	11.6	19.8	08.1	02.8	07.9	09.2	08.9	97	60	95	84	ENE	1	NNE	1	NW	1
11	743.6	743.7	744.4	08.8	17.7	10.7	12.0	16.9	08.5	02.8	08.4	10.4	09.1	99	68	94	87	NE	1	ENE	1	NE	1
12	744.1	744.1	744.7	09.2	16.5	09.7	11.3	19.1	09.1	05.5	08.6	09.1	08.6	99	65	95	86	ESE	1	SE	2	N	1
13	744.8	742.7	742.4	07.8	20.0	10.7	12.3	20.5	06.6	01.9	07.7	08.9	09.1	97	51	94	81	ENE	1	SE	1	WWN	1
14	741.4	740.3	740.4	07.9	15.6	10.6	11.2	17.4	07.7	01.8	07.9	09.3	09.1	99	70	95	88	W	1	ESE	1	E	1
15	739.2	738.2	737.8	10.0	14.4	09.3	10.8	15.8	09.3	07.0	08.8	07.8	08.5	95	63	96	85	NNW	1	WWN	1	ENE	1</td

BR. ST. 13

$$H_s = 299 \text{ m } H_b = 297.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.5 \text{ m}$$

LJUBLJANA-BEZ IGRAD

1878 OCTOBER

1	6	10	10	10	10.0	00.0	22.6	.	$\nabla^{+1} 0-3^{\circ} 6^{\circ} 15^{\circ} 0-3^{\circ} 4^{\circ} 0^{\circ} 0^{\circ}-1^{\circ}, 3^{\circ}-2^{\circ} 4^{\circ}, = 13^{\circ} 24$
2	6	10	10	10	10.0	00.0	27.3	.	$= 0-24^{\circ} 15^{\circ} 12^{\circ} 15^{\circ} 24^{\circ},$
3	6	10	10	10	10.0	00.0	33.7	.	$\bullet^{+1} 0-3^{\circ} 30^{\circ} 30^{\circ} 4^{\circ} 15^{\circ} 22^{\circ} 4^{\circ}, = 0-24^{\circ} 6^{\circ} 3^{\circ} 30^{\circ} 8^{\circ} 20^{\circ} H^{\circ}, = 0^{\circ} 8^{\circ} 10^{\circ}$
4	7	10	05	10	08.3	01.9	05.1	.	$= 0-3^{\circ} 6^{\circ} 15^{\circ} 21^{\circ} 24^{\circ}, \bullet^{+1} 3^{\circ} 15^{\circ} 11^{\circ} 15^{\circ} 24^{\circ}, = 0-3^{\circ} 5^{\circ} 5^{\circ}, = 0^{\circ} 5^{\circ} 6^{\circ}, \nabla^{+1} 12^{\circ} 5^{\circ} 4^{\circ}, \odot$
5	8	10	06	00	05.3	02.7	08.7	.	$\bullet^{+1} 0-1^{\circ} 5^{\circ} 10^{\circ}, = 0-2^{\circ} 24^{\circ}, \Delta^{+1} 13^{\circ} 24^{\circ}, \odot$
6	7	10	07	09	08.7	06.2	01.0	.	$\Delta^{+1} 0-12^{\circ} 19^{\circ} 24^{\circ}, = 0-0^{\circ} 9^{\circ} 30^{\circ} 11^{\circ} 22^{\circ} 24^{\circ}, = 0-0^{\circ} 9^{\circ} 24^{\circ},$
7	8	10	01	00	03.7	07.7	.	.	$= 0-5^{\circ} 9^{\circ} 20^{\circ} 15^{\circ} 23^{\circ} 25^{\circ}, = 0-1^{\circ} 2^{\circ} 9^{\circ} 23^{\circ} 24^{\circ}, 00^{\circ} 11^{\circ} 13^{\circ}, \odot$
8	7	10	04	04	06.0	05.7	.	.	$\Delta^{+1} 0-1^{\circ} 10^{\circ} 18^{\circ} 24^{\circ}, = 0-2^{\circ} 1^{\circ} 10^{\circ} 20^{\circ}, = 0-4^{\circ} 4^{\circ} 9^{\circ} 11^{\circ} 20^{\circ} 24^{\circ}, 00^{\circ} 11^{\circ} 20^{\circ}, \odot$
9	6	10	01	00	03.7	05.9	.	.	$\Delta^{+1} 0-10^{\circ} 18^{\circ} 24^{\circ}, = 0-0^{\circ} 9^{\circ} 24^{\circ}, = 0-0^{\circ} 1^{\circ} 1^{\circ} 1^{\circ}, = 0-0^{\circ} 9^{\circ} 24^{\circ},$
10	6	10	00	00	03.3	06.5	.	.	$\Delta^{+1} 0-1^{\circ} 10^{\circ} 17^{\circ} 24^{\circ}, = 0-0^{\circ} 9^{\circ} 11^{\circ} 17^{\circ} 24^{\circ}, = 0-0^{\circ} 9^{\circ} 11^{\circ} 22^{\circ} 24^{\circ}, 00^{\circ} 11^{\circ} 17^{\circ} 20^{\circ}, = 0-1^{\circ} 2^{\circ} 12^{\circ} 22^{\circ}, \odot$
11	6	10	00	06	35.3	35.5	.	.	$\Delta^{+1} 0-13^{\circ} 19^{\circ} 24^{\circ}, = 0-0^{\circ} 1^{\circ} 1^{\circ} 1^{\circ}, = 0-0^{\circ} 1^{\circ} 1^{\circ} 1^{\circ}, 17^{\circ} 24^{\circ}, = 0-1^{\circ} 2^{\circ} 22^{\circ} 24^{\circ}, \odot$
12	6	10	00	00	03.3	04.9	00.3	.	$\Delta^{+1} 0-6^{\circ} 10^{\circ} 24^{\circ}, = 0-0^{\circ} 11^{\circ} 20^{\circ} 13^{\circ} 24^{\circ}, = 0-1^{\circ} 2^{\circ} 13^{\circ} 24^{\circ}, 00^{\circ} 13^{\circ} 19^{\circ}, = 0-1^{\circ} 2^{\circ} 44^{\circ}, \odot$
13	7	10	01	00	03.7	37.3	00.0	.	$\Delta^{+1} 0-2^{\circ} 9^{\circ} 17^{\circ} 24^{\circ}, = 0-0^{\circ} 1^{\circ} 1^{\circ} 1^{\circ}, = 0-0^{\circ} 1^{\circ} 1^{\circ} 1^{\circ}, 17^{\circ} 24^{\circ}, = 0-1^{\circ} 2^{\circ} 24^{\circ}, 00^{\circ} 11^{\circ} 20^{\circ}, \odot$
14	5	10	00	10	36.7	04.6	.	.	$\Delta^{+1} 0-13^{\circ} 17^{\circ} 24^{\circ}, = 0-0^{\circ} 9^{\circ} 13^{\circ} 24^{\circ}, = 0-0^{\circ} 9^{\circ} 13^{\circ} 24^{\circ}, 00^{\circ} 13^{\circ} 17^{\circ} 24^{\circ}, \odot$
15	6	10	06	10	08.7	32.6	.	.	$\Delta^{+1} 0-13^{\circ} 17^{\circ} 24^{\circ}, = 0-1^{\circ} 10^{\circ} 17^{\circ} 24^{\circ}, 00^{\circ} 13^{\circ} 17^{\circ} 24^{\circ}, \odot$
16	7	10	00	00	33.3	04.5	.	.	$\Delta^{+1} 0-11^{\circ} 18^{\circ} 24^{\circ}, = 0-1^{\circ} 10^{\circ} 18^{\circ} 24^{\circ}, 00^{\circ} 11^{\circ} 18^{\circ}, \odot$
17	6	10	01	09	06.7	33.6	.	.	$\Delta^{+1} 0-11^{\circ} 18^{\circ} 24^{\circ}, = 0-0^{\circ} 1^{\circ} 1^{\circ} 1^{\circ}, = 0-0^{\circ} 1^{\circ} 1^{\circ} 1^{\circ}, 18^{\circ} 24^{\circ}, = 0-1^{\circ} 2^{\circ} 44^{\circ}, \odot$
18	6	10	10	10	10.0	02.7	00.0	.	$\Delta^{+1} 0-2^{\circ} 10^{\circ} 18^{\circ} 24^{\circ}, = 0-0^{\circ} 1^{\circ} 1^{\circ} 1^{\circ}, 18^{\circ} 24^{\circ}, = 0-0^{\circ} 1^{\circ} 1^{\circ} 1^{\circ}, 00^{\circ} 10^{\circ} 20^{\circ}, \odot$
19	6	10	10	10	13.0	00.6	01.3	.	$\Delta^{+1} 0-12^{\circ} 18^{\circ} 24^{\circ}, = 0-0^{\circ} 9^{\circ} 13^{\circ} 24^{\circ}, = 0-0^{\circ} 9^{\circ} 13^{\circ} 24^{\circ}, 00^{\circ} 12^{\circ} 18^{\circ}, \odot$
20	7	10	10	10	10.0	00.7	.	.	$\Delta^{+1} 0-7^{\circ}, = 0-7^{\circ},$
21	7	10	02	00	04.0	07.1	.	.	$= 0^{\circ} 12^{\circ} 2^{\circ}, \Delta^{+1} 6^{\circ} 3^{\circ} 20^{\circ} 24^{\circ}, = 0^{\circ} 16^{\circ} 8^{\circ} 2^{\circ}, = 0^{\circ} 16^{\circ} 2^{\circ} 30^{\circ}, 00^{\circ} 12^{\circ} 19^{\circ}, \nabla^{+1} 22^{\circ} 24^{\circ}, \odot$
22	8	06	08	09	07.7	07.3	.	.	$\Delta^{+1} 0-10^{\circ} 2^{\circ} 24^{\circ}, 00^{\circ} 6^{\circ}, \Delta^{+1} 7^{\circ} 7^{\circ}, = 0^{\circ} 16^{\circ} 24^{\circ}, \odot$
23	7	09	01	09	03.3	07.0	.	.	$\Delta^{+1} 0-2^{\circ} 17^{\circ} 24^{\circ}, = 0-10^{\circ} 1^{\circ} 2^{\circ} 7^{\circ}, 00^{\circ} 10^{\circ} 24^{\circ}, \odot$
24	7	04	01	00	01.7	36.5	.	.	$\Delta^{+1} 0-4^{\circ} 17^{\circ} 24^{\circ}, = 0^{\circ} 2^{\circ} 10^{\circ} 20^{\circ} 24^{\circ}, \Delta^{+1} 4^{\circ} 7^{\circ} 2^{\circ}, \odot$
25	6	10	06	09	08.3	34.8	.	.	$\Delta^{+1} 0-0^{\circ} 17^{\circ} 24^{\circ}, = 0-3^{\circ} 10^{\circ} 20^{\circ}, \Delta^{+1} 0^{\circ} 8^{\circ}, = 0^{\circ} 3^{\circ} 5^{\circ}, 10^{\circ} H^{\circ}, = 0^{\circ} 5^{\circ} 10^{\circ}, \odot$
26	7	10	10	10	10.0	00.0	00.0	.	$\Delta^{+1} 0-4^{\circ} 10^{\circ} 20^{\circ} 24^{\circ}, = 0^{\circ} 4^{\circ} 10^{\circ} 20^{\circ} 24^{\circ}, \Delta^{+1} 0^{\circ} 10^{\circ}, = 0^{\circ} 10^{\circ} H^{\circ}$
27	8	03	03	03	33.3	39.0	00.0	.	$\bullet^{+1} 3^{\circ} 3^{\circ} 10^{\circ} H^{\circ}, \Delta^{+1} 10^{\circ} 10^{\circ}, \Delta^{+1} 20^{\circ} 24^{\circ}, \odot$
28	7	06	09	09	08.0	04.5	.	.	$\Delta^{+1} 0-8^{\circ}, \odot$
29	7	03	00	01	01.3	08.9	.	.	$\Delta^{+1} 0-7^{\circ} 7^{\circ}, \Delta^{+1} 19^{\circ} 24^{\circ}, \odot$
30	6	10	00	00	03.3	06.4	.	.	$\Delta^{+1} 0-0^{\circ} 17^{\circ} 24^{\circ}, \Delta^{+1} 0^{\circ} 8^{\circ}, = 0^{\circ} 3^{\circ} 10^{\circ} 10^{\circ} H^{\circ}, = 0^{\circ} 1^{\circ} 10^{\circ} H^{\circ}, 00^{\circ} H^{\circ} H^{\circ}, \odot$
31	6	10	10	00	06.7	30.3	.	.	$\Delta^{+1} 0-12^{\circ} 20^{\circ} 24^{\circ}, = 0-0^{\circ} 8^{\circ} 20^{\circ} 24^{\circ}, 00^{\circ} H^{\circ} 20^{\circ}, \odot$

$\varphi = 46^{\circ}04' N \lambda = 14^{\circ}31' E$ Gr. $\Delta G = + 58$ min.

BR. ST. 13

D	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodenе pare e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0-12)				
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21	
1	745.7	745.6	747.5	01.6	12.4	04.1	05.6	13.3	00.6	-04.2	05.1	06.4	05.9	98	59	95	84	-	0	ENE 1	N 1
2	747.4	745.9	745.8	04.6	10.8	03.3	05.5	11.0	02.4	-03.4	06.0	06.1	05.4	94	63	94	84	ENE 1	SE 2	NNW 1	
3	744.9	744.2	745.2	03.5	10.0	06.2	06.5	11.0	01.4	-04.3	05.5	06.2	06.3	94	68	89	84	NNE 1	SSE 2	NNW 1	
4	745.1	744.7	745.2	05.8	09.4	05.3	06.5	09.5	05.3	04.6	05.8	05.4	05.5	83	61	82	75	NW 1	E 1	ENE 2	
5	745.3	746.0	747.0	00.7	08.8	05.3	05.0	09.0	00.0	-06.0	04.7	04.5	05.2	98	54	77	76	N 1	SE 2	NNW 2	
6	747.2	746.8	747.2	04.6	05.8	04.7	05.0	06.3	04.6	03.7	04.5	04.7	04.6	71	69	71	70	SSE 1	SSE 1	E 2	
7	747.4	746.8	748.0	02.9	06.4	03.2	03.9	07.3	02.4	02.6	04.2	04.4	04.7	75	62	81	73	NNE 2	NE 2	ENE 1	
8	747.4	746.7	747.2	02.8	05.3	01.4	02.7	06.3	01.3	02.1	04.3	04.1	04.4	76	61	87	75	ESE 2	NNW 2	NNW 1	
9	746.8	746.1	746.8	01.7	03.4	02.5	02.5	03.7	01.5	00.4	04.5	04.8	04.7	87	82	86	85	ENE 2	NNE 1	N 1	
10	745.9	744.6	744.8	01.3	01.8	01.0	01.3	03.2	00.9	01.1	04.5	04.4	04.4	90	85	90	88	SSE 1	S 1	N 2	
11	744.7	744.4	745.1	-00.4	00.7	00.6	00.4	01.4	-00.4	-00.3	04.3	04.2	04.4	96	88	91	92	NNE 2	ENE 1	SSE 1	
12	744.5	743.9	744.0	-01.0	00.5	-00.1	-00.2	00.8	-01.0	-00.6	04.2	04.0	03.9	98	84	86	89	NNW 1	NNW 1	SSW 1	
13	744.7	745.3	747.0	-01.6	-00.4	-00.7	-00.9	00.2	-01.7	-01.5	03.8	03.9	03.9	92	87	89	89	NNW 2	ENE 1	NNW 1	
14	749.0	749.4	750.5	-02.0	03.2	-00.6	00.0	04.6	-02.0	-02.0	03.7	04.0	04.1	94	69	93	85	N 1	-	0	
15	749.1	747.4	746.7	-02.4	02.8	-02.0	-00.9	03.8	-03.2	-07.4	03.8	04.7	03.9	100	84	98	94	E 1	ENE 1	-	
16	744.6	742.8	743.1	-02.8	01.5	-02.1	-01.4	02.1	-03.1	-03.0	03.7	04.4	03.8	98	87	98	94	NW 1	ENE 1	ENE 1	
17	747.4	747.3	748.4	-01.2	06.6	-00.8	01.0	07.4	-03.3	-03.4	04.1	04.8	04.1	97	66	96	86	NNE 1	NE 1	NNW 2	
18	747.6	746.5	746.6	-02.1	02.4	-01.3	-00.6	03.4	-02.1	-08.1	03.9	04.4	04.1	100	81	98	93	NE 2	SSE 1	SSE 1	
19	745.6	743.8	742.8	-02.7	00.0	-02.0	-01.7	00.3	-02.8	-02.5	03.7	04.4	04.0	97	96	100	98	E 1	ENE 1	-	
20	741.2	740.6	742.7	-03.0	03.8	-01.6	-00.6	05.6	-03.1	-02.6	03.6	04.4	03.9	99	73	97	90	NE 1	E 1	ENE 1	
21	744.4	744.7	747.6	-02.3	01.2	-01.3	-00.9	01.3	-02.8	-03.0	03.9	04.5	04.0	98	90	96	95	SSW 2	ESE 1	SSE 1	
22	749.7	750.1	750.8	-02.2	01.0	-00.8	-00.7	01.2	-02.2	-01.8	03.9	04.4	04.2	100	90	96	95	S 1	-	0	
23	749.9	748.5	749.2	-02.3	00.2	-01.0	-01.0	00.6	-02.6	-02.3	J3.8	04.4	J4.1	98	95	96	96	W 1	ENE 1	S 1	
24	747.5	744.6	743.2	-02.2	-00.4	-01.0	-01.2	00.1	-02.5	-02.0	03.8	04.4	04.2	98	98	98	98	N 1	NE 1	NNW 1	
25	740.1	736.4	735.6	-03.8	01.8	01.5	00.3	02.9	-04.4	-03.1	03.4	04.4	04.7	98	85	92	92	NNM 1	ESE 1	E 1	
MES.	VRED.	742.9	742.2	742.7	-00.3	03.4	00.4	01.0	04.1	-01.0	-02.4	04.2	04.5	04.4	93	78	91	88	1.2	1.2	1.1

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1	733.1	734.0	735.1	-07.0	-04.8	-04.4	-05.2	-03.7	-08.2	-11.1	02.6	03.1	J3.1	96	95	94	95	S 1	-	0	-	0
2	736.2	737.0	738.3	-05.0	01.0	-05.5	-03.8	01.3	-05.7	-08.2	02.9	04.0	03.0	91	81	97	90	NNE 1	NE 1	ENE 1		
3	737.9	735.2	733.9	-06.8	-04.2	-07.4	-06.4	-06.5	-03.5	-08.0	02.6	03.0	02.4	94	90	93	92	S 1	ENE 1	-	0	
4	733.4	733.1	733.6	-08.6	-05.4	-04.6	-05.6	-05.8	-04.5	-08.9	02.2	02.9	J3.0	92	95	91	93	-	0	ENE 1	NNW 1	
5	735.9	736.9	741.7	-01.0	-00.1	-04.0	-02.3	00.6	-04.6	-05.4	03.7	03.9	03.1	86	86	92	88	ENE 3	E 3	E 1		
6	742.5	741.9	742.7	-05.6	-05.1	-06.1	-06.7	-03.3	-08.1	-17.4	02.5	02.5	02.1	81	80	82	81	ESE 1	SSE 2	ENE 2		
7	740.6	738.6	739.2	-08.9	-05.8	-06.9	-07.1	-05.3	-09.1	-12.5	02.1	02.0	02.0	89	68	72	76	NNE 2	E 2	NE 2		
8	738.5	737.4	735.8	-08.1	-06.4	-06.4	-06.8	-05.6	-08.2	-11.5	J1.8	J1.9	J2.6	72	66	92	77	NNW 1	NE 5	ENE 1		
9	732.7	733.6	736.5	-04.9	02.4	-01.2	-01.2	02.9	-06.6	-08.7	J2.9	04.4	J4.1	91	81	97	90	SE 1	SSW 1	NNE 1		
10	737.1	737.3	737.5	-01.2	-00.9	-01.2	-01.1	-03.6	-02.3	-01.3	04.1	04.2	J4.1	97	97	97	97	ENE 1	-	0	W 1	
11	735.7	733.8	732.3	-03.3	01.2	01.8	00.4	03.4	-03.4	-J4.0	J3.5	04.7	04.9	97	95	93	95	ENE 1	NE 1	W 1		
12	728.2	726.6	724.5	05.9	04.4	03.4	04.3	06.7	01.8	00.6	06.7	06.0	05.7	96	96	97	96	NNW 3	-	0	NNW 1	
13	722.5	723.1	721.5	02.9	05.1	03.0	03.5	05.8	02.2	00.6	05.5	06.1	05.4	97	93	95	95	NW 1	NE 1	NNW 1		
14	715.9	718.4	719.3	04.0	04.9	03.2	02.8	06.4	03.0	01.0	05.7	05.8	J5.4	94	90	94	93	NNW 2	NW 1	-	0	
15	721.8	724.0	726.3	01.0	01.7	-00.7	00.3	03.6	-01.0	-03.0	04.8	05.1	04.2	98	96	97	97	ENE 1	NE 1	NNW 1		
16	725.0	723.5	720.5	01.2	05.2	02.8	03.0	05.7	-01.7	-03.7	04.7	06.1	05.3	93	91	95	93	NNE 1	E 1	NNW 2		
17	725.4	728.8	731.3	01.6	07.4	04.0	04.3	07.7	04.6	-03.4	05.0	05.9	05.7	97	77	94	89	NNW 1	NNW 1	-		
18	734.8	738.0	741.0	01.8	-00.3	-07.2	-00.7	04.0	-02.2	-J1.1	04.4	03.3	02.4	83	73	62	73	ENE 2	E 3	E 3		
19	739.3	735.2	732.6	-04.8	-04.2	-05.5	-05.0	-02.2	-05.5	-J5.1	02.7	02.7	02.7	83	79	88	83	ENE 2	S 2	SSE 1		
20	731.6	733.0	734.7	-05.0	-01.8	-02.4	-02.9	-J1.2	-05.6	-15.0	02.9	03.0	03.3	91	74	86	84	ENE 1	NW 1	W 1		
21	736.0	736.2	736.1	-05.4	-01.3	-01.6	-05.2	-05.7	-J2.4	-12.4	02.8	03.7	03.8	93	88	93	91	N 1	NE 1	ENE 1		
22	736.0	734.2	732.2	-01.2	-00.9	-01.0	-01.0	-03.6	-02.0	-J3.7	J3.7	J3.9	J4.0	88	92	94	91	SSE 1	NNW 1	SSE 1		
23	731.1	731.2	732.1	-00.9	01.0	00.3	00.2	01.6	-01.1	-J1.5	04.1	04.3	04.4	96	86	93	92	NNW 1	ENE 1	NNE 1</td		

BR. ST. 13

 $H_s = 299 \text{ m } H_b = 297.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.5 \text{ m}$

Dan	Vremenska časovna sredina o. O.	Oblačnost N (0-10)					Inzidencija nebojšči ški	Padavine R mm	Snežni pokrivali h cm	Razvoj vremena w	
		14	7	14	21	Sred Dies				7	7
1	6	10≡	01○	00	03.7	05.7	.	.	.	$\square^{+1} 0-10^{\circ}, 17^{\circ} 20^{\circ}, = 10^{\circ} 13^{\circ}, 19^{\circ} 24^{\circ}, \square^{+1} 10^{\circ} 5^{\circ}, 20^{\circ} 24^{\circ}, = 1^{\circ} 3^{\circ} 4^{\circ}, = 1^{\circ} 4^{\circ} 10^{\circ}, 00^{\circ} 13^{\circ} 16^{\circ}, 0$	
2	6	10	07○	00	05.7	00.5	.	.	.	$\square^{+1} 0-2^{\circ}, 19^{\circ} 24^{\circ}, = 0-2^{\circ}, \square^{+1} 10^{\circ} 5^{\circ}, 19^{\circ} 24^{\circ}, 0$	
3	6	10	07	10	09.0	02.5	.	.	.	$\square^{+1} 0-3^{\circ}, = 0-0^{\circ}, 2^{\circ}, 10^{\circ}, 10^{\circ}, 24^{\circ}, = 0^{\circ} 10^{\circ}, 20^{\circ}, 00^{\circ} 14^{\circ} 18^{\circ}, 0$	
4	7	10	10	00	06.7	00.4	.	.	.	$= 0-11^{\circ}, 19^{\circ} 24^{\circ}, 00^{\circ} 13^{\circ} 19^{\circ}, \square^{+1} 20^{\circ} 22^{\circ}, \square^{+1} 22^{\circ} 24^{\circ}, 0$	
5	7	06	05○	09	06.7	02.6	.	.	.	$\square^{+1} 0-7^{\circ}, = 0-11^{\circ}, 0$	
6	7	10	10	09	09.7	00.0	.	.	.	$\infty 6^{\circ}, 19^{\circ} 30^{\circ}$	
7	6	10	03○	10	07.7	04.1	.	.	.	$= 8^{\circ}, 14^{\circ}, 23^{\circ}, 24^{\circ}, 00^{\circ} 11^{\circ}, 17^{\circ}, 0$	
8	6	10	00○	10	06.7	02.6	.	.	.	$= 0-13^{\circ}, 17^{\circ} 24^{\circ}, 00^{\circ} 13^{\circ} 17^{\circ}, \square^{+1} 20^{\circ} 22^{\circ}, 0$	
9	6	10	10	10	10.0	00.0	.	.	.	$= 0-24$	
10	6	10	10	10	10.0	00.0	.	.	.	$= 0-24$	
11	6	10	10	10	10.0	00.0	.	.	.	$= 0-24$	
12	5	10	10	10	10.0	00.0	.	.	.	$= 0-24$	
13	5	10	10	10	10.0	00.0	.	.	.	$= 0-24$	
14	6	10	01○	00	03.7	03.4	.	.	.	$= 0-24, \square^{+1} 19^{\circ} 24^{\circ}, 0$	
15	3	10≡	03○	19≡	07.7	02.7	.	.	.	$\square^{+1} 0-7^{\circ}, = 0-24, 14^{\circ} 16^{\circ}, = 0-24, 14^{\circ} 16^{\circ}, = 0-11^{\circ}, 18^{\circ}, 0$	
16	3	10≡	00○	10≡	06.7	03.3	00.0	.	.	$\square^{+1} 0-9^{\circ}, 19^{\circ} 24^{\circ}, = 0-10^{\circ}, 16^{\circ}, 24^{\circ}, \square^{+1} 10^{\circ}, 19^{\circ}, 0$	
17	7	10	01○	00	03.7	03.7	00.1	.	.	$\square^{+1} 0-10^{\circ}, 18^{\circ}, 24^{\circ}, = 0-3^{\circ}, 23^{\circ}, 24^{\circ}, = 3^{\circ}, 19^{\circ}, 18^{\circ}, 22^{\circ}, = 0-22^{\circ}, 23^{\circ}, 0$	
18	3	10≡	06○	10≡	08.7	02.0	00.1	.	.	$\square^{+1} 0-5^{\circ}, = 0-4^{\circ}, 16^{\circ}, 24^{\circ}, \square^{+1} 10^{\circ}, 19^{\circ}, 24^{\circ}, \square^{+1} 5^{\circ}, 9^{\circ}, = 0-11^{\circ}, 16^{\circ}, 0$	
19	3	10≡	06○	10≡	08.7	00.0	.	.	.	$= 0-11^{\circ}, 19^{\circ} 24^{\circ}, \square^{+1} 10^{\circ}, 19^{\circ}, 24^{\circ}, = 0-11^{\circ}, 18^{\circ}, 0$	
20	4	10≡	00○	10≡	06.7	03.5	.	.	.	$= 0-10^{\circ}, 19^{\circ} 24^{\circ}, \square^{+1} 10^{\circ}, 19^{\circ}, 24^{\circ}, = 0-11^{\circ}, 18^{\circ}, 0$	
21	1	10≡●	00○	10≡	06.7	00.0	00.0	.	.	$\square^{+1} 0-6^{\circ}, = 0-10^{\circ}, 15^{\circ}, 24^{\circ}, \square^{+1} 6^{\circ}, 10^{\circ}, = 0-13^{\circ}, 15^{\circ}, 0$	
22	3	10≡	09≡	10≡	09.7	00.0	00.0	.	.	$= 0-10^{\circ}, 15^{\circ}, 24^{\circ}, \square^{+1} 11^{\circ}, 15^{\circ}, 0$	
23	3	10≡	10≡	10≡	10.0	00.0	.	.	.	$= 0-14^{\circ}, 19^{\circ}, 22^{\circ}, = 11^{\circ}, 14^{\circ}, 0$	
24	2	10≡	10≡	10≡	10.0	00.0	00.5	.	.	$= 0-24, \square^{+1} 0-9^{\circ}, 15^{\circ}, 0$	
25	3	10≡	00○	09	06.3	02.4	00.3	.	.	$= 0-12^{\circ}, \square^{+1} 0-17^{\circ}, = 17^{\circ}, 24^{\circ}, \square^{+1} 23^{\circ}, 24^{\circ}, 0$	
26	4	10≡●	10*	10*	10.0	00.0	03.2	.	.	$* 0-16^{\circ}, = 0-5^{\circ}, 13^{\circ}, 24^{\circ}, = 0-5^{\circ}, 13^{\circ}, 24^{\circ}, * 14^{\circ}, 16^{\circ}, * 14^{\circ}, 16^{\circ}, 0$	
27	5	10*	10*	10*	10*	00.0	51.9	15	.	$* 0-24, = 0-24^{\circ}, = 14^{\circ}, 15^{\circ}, 0$	
28	6	10	10	09	09.7	00.0	13.7	25	.	$* 0-24^{\circ}, = 0-14^{\circ}, 17^{\circ}, 24^{\circ}, = 0-24^{\circ}, 14^{\circ}, 0$	
29	7	10	09	10≡	09.7	00.0	22	.	.	$= 0-12^{\circ}, 19^{\circ}, 20^{\circ}, * 14^{\circ}, 16^{\circ}, = 0-20^{\circ}, 24^{\circ}, 0$	
30	3	10≡	04○	10≡	08.0	02.1	00.0	21	.	$= 0-10^{\circ}, 19^{\circ}, 24^{\circ}, = 0-11^{\circ}, 15^{\circ}, = 15^{\circ}, 19^{\circ}, 0$	
MES. RED.	09.9	06.1	08.2	08.1	41.5	69.8					

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1	4	10≡	09≡	13	09.7	30.0	.	21		$\square^{+1} 0-10^{\circ}, V 6^{\circ}, 15^{\circ}, = 0-10^{\circ}, 13^{\circ}, = 13^{\circ}, 24^{\circ}, 0$	
2	4	09	00○	19≡	06.3	04.6	00.1	19		$= 0-10^{\circ}, * 0-10^{\circ}, = 10^{\circ}, 24^{\circ}, 0$	
3	3	10≡	00○	10≡	06.7	30.0	.	18		$= 0-12^{\circ}, 18^{\circ}, 24^{\circ}, = 12^{\circ}, 18^{\circ}, 0$	
4	4	10≡	10	13	10.0	00.0	.	18		$= 0-13^{\circ}, \square^{+1} 10^{\circ}, 13^{\circ}, = 13^{\circ}, 24^{\circ}, 0$	
5	7	10	03○	09	07.3	03.1	00.0	18		$= 0-11^{\circ}, 15^{\circ}, 24^{\circ}, 0$	
6	6	10	10	00	06.7	30.3	00.1	17		$= 0-24, 0$	
7	7	10*	04○	10*	08.0	00.5	00.0	17		$= 0-10^{\circ}, 18^{\circ}, 24^{\circ}, \square^{+1} 3^{\circ}, 9^{\circ}, 12^{\circ}, 13^{\circ}, 17^{\circ}, 24^{\circ}, 0$	
8	6	10	10	10*	10.0	00.0	00.1	17		$= 0-24, * 0-14^{\circ}, 17^{\circ}, 24^{\circ}, 0$	
9	4	10	09	10≡	09.7	01.3	03.5	21		$= 0-17^{\circ}, * 0-4^{\circ}, \square^{+1} 10^{\circ}, 19^{\circ}, 24^{\circ}, 0$	
10	2	10≡	10≡	10≡	10.0	30.0	05.3	18		$= 0-24^{\circ}, = 24^{\circ}, 22^{\circ}, = 22^{\circ}, 24^{\circ}, 0$	
11	4	10≡	07○	13	09.0	01.6	.	17		$\square^{+1} 0-10^{\circ}, 11^{\circ}, 12^{\circ}, = 0-10^{\circ}, 11^{\circ}, 12^{\circ}, = 1-18^{\circ}, 14^{\circ}, 0$	
12	1	10	10	10	10.0	00.0	01.0	11		$= 0-10^{\circ}, 12^{\circ}, 24^{\circ}, \square^{+1} 12^{\circ}, 13^{\circ}, 24^{\circ}, 0$	
13	3	10	10	10	10.0	30.3	14.0	36		$\square^{+1} 0-20^{\circ}, 14^{\circ}, 20^{\circ}, = 0-10^{\circ}, 19^{\circ}, 22^{\circ}, = 10^{\circ}, 13^{\circ}, 17^{\circ}, 22^{\circ}, 0$	
14	7	10	09	04	07.7	31.0	04.5	32		$= 0-12^{\circ}, 17^{\circ}, 23^{\circ}, \square^{+1} 20^{\circ}, 25^{\circ}, 24^{\circ}, 10^{\circ}, 13^{\circ}, 0$	
15	2	10≡	10≡	09≡	19.7	31.0	03.0	•		$\square^{+1} 0-20^{\circ}, = 20^{\circ}, 21^{\circ}, = 21^{\circ}, 24^{\circ}, 0$	
16	5	10	10*	13*	09.7	30.0	00.2	.		$= 0-24, \square^{+1} 10^{\circ}, 20^{\circ}, 20^{\circ}, 0$	
17	6	10	07	10	10.0	04.6	23.0	.		$= 0-22^{\circ}, \square^{+1} 10^{\circ}, 20^{\circ}, 22^{\circ}, = 0-22^{\circ}, 22^{\circ}, 0$	
18	6	10	10*	10*	10.0	30.0	03.0	.		$= 0-20^{\circ}, 20^{\circ}, 20^{\circ}, 20^{\circ}, 20^{\circ}, 20^{\circ}, 0$	
19	6	10*	10*	10*	10.0	00.0	24.1	35		$* 0-10^{\circ}, 24^{\circ}, = 0-10^{\circ}, 24^{\circ}, 0$	
20	6	10*	10	03	17.7	30.0	14.6	17		$* 0-10^{\circ}, 16^{\circ}, 16^{\circ}, 24^{\circ}, = 0-16^{\circ}, 19^{\circ}, = 0-19^{\circ}, 24^{\circ}$	
21	4	07	10	10	09.0	33.0	03.3	17		$= 0-7^{\circ}, 13^{\circ}, 24^{\circ}, = 0-7^{\circ}, 13^{\circ}, 24^{\circ}, = 0-10^{\circ}, 13^{\circ}, 0$	
22	5	10	10*	10*	10.0	00.0	00.7	16		$= 0-24, * 0-10^{\circ}, 14^{\circ}, 10^{\circ}, 19^{\circ}, 24^{\circ}, \square^{+1} 16^{\circ}, 17^{\circ}, 0$	
23	5	10*	10*	10	10.0	00.0	04.1	17		$= 0-24, * 0-10^{\circ}, 14^{\circ}, 10^{\circ}, 19^{\circ}, 24^{\circ}, \square^{+1} 16^{\circ}, 17^{\circ}, 0$	
24	5	10	10*	10	10.0	00.0	01.4	15		$= 0-24, * 0-10^{\circ}, 14^{\circ}, 10^{\circ}, 19^{\circ}, 24^{\circ}, \square^{+1} 16^{\circ}, 17^{\circ}, 0$	
25	5	10*	10*	10*	10.0	00.0	03.0	17		$= 0-16^{\circ}, * 0-6^{\circ}, 16^{\circ}, 21^{\circ}, 21^{\circ}, 0$	
26	3	10≡	10≡	10≡	10.0	10.0	03.9	15		$\square^{+1} 0-24, 9^{\circ}, 22^{\circ}, 23^{\circ}, 0$	
27	7	10≡	09	10	10.0	10.0	10.0	17		$= 0-10^{\circ}, 9^{\circ}, 10^{\circ}, 10^{\circ}, 0$	
28	4	10*	10*	09	09.0	03.0	32.0	.		$\square^{+1} 0-17^{\circ}, 6^{\circ}, = 5^{\circ}, 24^{\circ}, 0$	
29	7	09	10	10*	10.0	10.0	04.0	.		$= 0-10^{\circ}, 10^{\circ}, 10^{\circ}, 10^{\circ}, 10^{\circ}, 10^{\circ}, 0$	
30	8	10	09○	09	09.0	13.0	16.0	.		$\square^{+1} 0-15^{\circ}, 0$	
31	7	1									

$\varphi = 45^{\circ}49' N \lambda = 15^{\circ}59' E$ Gr. $\Delta G = + 1h 04 min.$

BR. ST. 56

D	Vazdušni pritisk P mm			Temperatura vazduha T C°							Napon vodené pare e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0-12)				
	7	14	21	7	14	21	Sred Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dnes	7	14	21	
1	748.3	752.4	755.8	02.7	06.4	02.8	03.7	06.6	00.0	-	03.4	04.3	03.5	61	61	63	62	NNW 3	SSE 2	ENE 2	
2	755.5	752.8	751.5	-01.1	06.3	05.0	03.8	07.2	-01.2	-	03.5	04.3	04.2	83	60	65	69	WSW 1	W 2	WSW 3	
3	750.5	749.8	745.1	07.7	08.8	07.0	07.6	09.0	04.8	-	05.4	05.8	05.9	68	68	79	72	WNW 2	WSW 1	NW 2	
4	745.0	746.7	749.1	07.6	06.6	03.0	05.1	09.0	03.0	-	03.8	05.2	03.7	49	70	66	62	N 2	SW 2	N 2	
5	752.8	756.6	761.9	00.0	00.8	-02.6	-01.1	03.0	-02.6	-	03.2	03.1	02.3	70	63	60	64	E 1	NE 4	ENE 2	
6	763.0	761.3	759.3	-04.7	-00.6	-01.2	-01.9	-00.6	-04.7	-	01.9	01.8	02.0	59	40	49	49	NNE 1	SW 2	W 2	
7	758.6	760.0	761.1	-30.6	00.2	02.2	01.0	02.2	-01.3	-	02.8	04.3	04.8	64	92	89	82	SSE 1	SSW 1	E 1	
8	760.6	760.0	759.9	-00.2	-00.3	-02.6	-01.4	02.3	-02.6	-	03.9	03.7	03.1	86	82	83	84	E 1	SSE 2	E 1	
9	758.3	756.9	756.3	-03.2	-03.7	-04.4	-03.9	-02.6	-04.4	-	03.0	02.8	02.4	83	80	74	79	E 1	SSE 2	S 1	
10	754.5	753.4	753.7	-03.4	-03.6	-03.2	-03.4	-03.1	-04.4	-	02.8	03.2	03.2	80	90	89	86	S 2	E 1	S 1	
11	750.4	744.9	741.6	-03.8	-04.4	-02.0	-03.1	-02.0	-05.1	-	03.0	03.0	03.4	88	91	86	88	SSE 2	E 2	E 1	
12	740.0	741.0	745.0	01.5	07.0	07.0	05.6	07.8	-02.0	-	04.0	04.7	05.3	78	63	70	70	ENE 2	E 2	ENE 2	
13	749.3	752.0	753.3	04.2	04.7	04.2	04.3	07.0	03.5	-	05.6	05.9	05.9	91	92	95	93	SW 1	S 1	SW 1	
14	752.8	753.1	754.1	01.4	02.6	03.2	02.6	04.2	00.5	-	04.9	05.4	05.6	97	96	96	96	SSE 1	N 1	NW 1	
15	753.6	752.8	751.9	02.3	01.0	00.8	01.2	03.2	00.8	-	05.0	04.4	04.6	92	91	95	93	ESE 2	E 2	ENE 3	
16	749.7	749.0	749.6	-00.1	01.0	01.2	00.8	01.2	-00.2	-	04.3	04.4	04.6	95	91	93	93	ENE 2	E 1	N 1	
17	746.8	742.3	740.4	00.8	00.6	-00.2	00.3	01.2	-00.2	-	04.5	04.5	04.4	93	94	98	95	ENE 1	ENE 2	ENE 3	
18	741.9	743.4	744.9	-00.5	01.1	-00.2	00.1	01.1	-00.5	-	04.1	04.4	04.3	93	89	95	92	W 1	E 1	SSW 1	
19	744.7	743.6	743.1	00.0	-00.3	-00.8	-00.5	00.0	-01.3	-	04.1	04.1	04.0	89	91	92	91	E 1	ENE 2	E 1	
20	741.8	742.7	744.4	00.1	00.0	00.1	00.1	00.1	-00.8	-	04.1	03.8	03.9	89	85	86	87	E 2	E 2	E 2	
21	744.6	745.1	746.8	-01.4	-00.1	00.6	-00.1	00.6	-02.0	-	03.7	03.5	04.1	88	78	85	84	E 3	ENE 3	ENE 2	
22	746.5	745.7	746.7	-01.5	-00.2	-00.7	-00.8	00.6	-01.9	-	03.4	03.7	03.5	83	81	80	81	E 2	E 2	E 1	
23	747.4	749.2	749.4	-01.0	01.0	00.2	00.1	01.0	-01.0	-	03.6	04.0	04.0	85	83	86	85	WSM 1	SW 2	WWN 1	
24	745.3	741.0	737.0	-00.3	02.2	03.6	02.3	03.6	-00.3	-	03.9	04.3	05.1	87	80	85	84	WSM 1	SSW 1	WWN 2	
25	736.2	740.2	743.0	03.2	05.9	03.5	04.0	06.3	03.2	-	05.2	05.5	05.3	91	80	90	87	SW 1	NW 1	WWN 1	
MES.	VRED.	747.9	747.7	748.2	00.6	02.2	01.4	01.4	03.2	-00.5	-	04.0	04.3	04.2	83	80	82	82	1.5	1.7	1.5

1	746.2	744.5	743.9	00.9	03.9	02.4	02.4	04.2	00.6	-	04.1	04.1	04.0	84	68	74	75	-	0	WSW 2	E 1
2	739.4	739.2	741.0	01.5	02.4	01.4	01.7	02.8	00.6	-	03.8	05.0	04.7	75	92	93	87	ENE 2	WNW 2	W 1	
3	743.1	745.6	748.6	00.7	03.4	03.1	02.6	04.6	-00.3	-	04.8	04.1	04.2	89	69	78	79	WNM 1	S 1	ESE 1	
4	750.6	751.3	752.6	02.3	03.6	02.4	02.7	04.0	02.3	-	04.8	04.1	04.2	89	69	78	79	E 1	ENE 2	E 2	
5	752.1	750.8	749.8	01.2	02.9	01.3	01.7	03.0	01.2	-	03.8	03.4	03.9	76	61	78	72	E 1	E 2	E 2	
6	746.1	745.0	745.0	00.9	02.2	01.7	01.6	02.3	00.8	-	04.1	04.1	04.6	83	77	88	83	ENE 2	E 1	E 1	
7	743.7	742.9	742.8	00.3	02.3	00.2	00.8	02.6	-00.2	-	03.8	03.8	03.9	81	70	84	78	NE 1	E 2	E 2	
8	742.2	742.5	743.3	-00.9	-00.1	-02.2	-01.4	00.2	-02.2	-	03.1	02.9	02.8	72	64	73	70	ENE 3	E 3	E 2	
9	743.9	744.4	745.8	-03.3	-01.0	00.9	-01.5	-00.9	-03.3	-	02.7	02.6	02.8	76	63	65	68	ENE 2	E 1	SSW 1	
10	745.5	743.0	740.9	-01.6	-00.1	-00.4	-00.6	01.0	-01.9	-	02.9	03.3	03.4	71	72	75	73	SW 1	E 2	ENE 2	
11	734.7	734.3	734.6	00.5	00.8	01.1	00.9	01.8	-01.0	-	04.0	04.5	04.7	84	92	95	90	ENE 2	W 2	E 1	
12	736.3	737.9	739.0	00.7	07.9	04.7	04.5	08.9	00.0	-	04.7	05.7	05.3	96	71	82	83	E 1	W 2	S 1	
13	739.3	739.1	739.7	-00.6	01.9	02.7	01.7	04.7	-00.8	-	04.3	05.0	04.8	98	95	86	93	NNE 1	E 1	NE 1	
14	738.5	737.7	740.4	01.9	04.3	01.4	02.3	04.7	01.2	-	03.1	03.4	03.1	60	55	61	59	ENE 3	SSE 1	E 2	
15	743.7	744.6	745.5	-01.2	02.2	-00.2	00.2	02.9	-01.3	-	02.8	02.6	02.6	66	48	57	57	E 1	S 2	WNW 2	
16	743.1	739.3	736.5	-03.4	01.6	02.6	00.9	02.6	-03.4	-	02.5	02.9	04.2	69	55	75	66	WNW 2	SW 1	W 2	
17	740.6	741.9	740.2	01.2	01.4	00.4	00.9	04.7	00.4	-	03.9	03.1	03.2	78	60	71	70	ESE 3	E 2	N 1	
18	745.7	748.5	749.7	-01.2	02.2	-00.6	-00.1	02.7	-01.4	-	03.5	02.5	02.6	83	47	58	63	ENE 3	E 2	NE 2	
19	747.7	745.5	744.5	-02.3	-02.4	-03.8	-03.1	-00.6	-03.8	-	02.7	03.4	03.0	70	87	88	82	E 1	ESE 1	ENE 2	
20	745.8	750.3	754.4	-03.4	-01.6	-04.0	-03.3	-01.3	-04.0	-	J2.8	03.0	02.4	80	74	69	74	ENE 2	E 2	ENE 1	
21	755.7	754.5	753.0	-09.8	-01.9	-04.3	-05.1	-01.9	-10.3	-	01.2	02.1	01.6	55	52	50	52	NE 1	SSE 2	ENE 1	
22	731.5	750.5	751.0	-09.2	-00.1	-00.9	-02.8	01.1	-09.4	-	01.8	02.6	03.0	80	57	70	69	E 1	S 2	ENE 1	
23	749.2	747.9	748.8	-02.8	08.2	06.3	04.5	08.9	-04.0	-	03.1	05.4	05.7	83	66	79	76	WSM 1	WSW 3	W 2	
24	748.7	748.5	747.2	08.4	10.7	10.6	10.1	11.1	05.9	-	06.2	07.0	07.0	75	73	74	74	W 3	W 3	WWN 2	
25	744.8	742.3	74																		

BR. ST. 56

 $H_s = 157 \text{ m } H_b = 162,5 \text{ m } h_t = 6.0 \text{ m } h_r = 2.0 \text{ m}$

Dan	Vrijeme	Oblačnost N (0-10)					Iseljavanje R mm	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dnes				
1	8 05	010	00	02.0	07.4	00.1	.	• n		
2	7 00	010	00	00.3	08.2	.	.	— n — n, = n — n		
3	6 10	10	09	09.7	00.6	.	.	= n — n		
4	7 10	040	09	07.7	02.9	00.8	.	= n — n, = n — n		
5	6 00	080	00	02.7	04.0	.	.	= n — n, = n — n, = n — n, = n — n, = n — n		
6	8 00	080	04	04.0	06.5	00.0	.	= n — n		
7	4 10*	100	10	10.0	00.0	00.0	.	= n — n, * n — n, = n — n, = n — n		
8	3 10	10=	10	10.0	00.0	01.2	01	= n — n, = n — n, = n — n		
9	6 10	10	10	10.0	00.0	.	01	= n — n, * n — n		
10	6 10	10*	10	10.0	00.0	00.0	01	= n — n, * n — n		
11	3 10*=	10=	10=	10.0	00.0	00.2	01	= n — n, * n — n, = n — n, = n — n		
12	5 08	09	100	09.0	00.7	00.0	01	= n — n, = n — n, = n — n		
13	4 10*	10	08=	09.3	00.0	00.6	.	= n — n, = n — n		
14	1 10=	10=	10=	10.0	00.0	01.7	.	= n — n, = n — n		
15	5 10	100	10*	10.0	00.0	00.2	.	= n — n, = n — n, = n — n, = n — n, = n — n		
16	4 10*=	10	10	10.0	00.0	17.9	13	* n — n, = n — n, = n — n, = n — n, = n — n		
17	4 10	10*	10*	10*	00.0	00.1	10	= n — n, = n — n, = n — n		
18	6 10	08	10	09.3	01.4	13.9	21	= n — n, = n — n		
19	6 10	10	10	10.0	00.0	00.1	16	* n — n, = n — n		
20	6 10*	10	10	10.0	00.0	00.0	15	= n — n, = n — n, = n — n, = n — n		
21	6 10*	10	10	10.0	00.0	01.3	17	= n — n, * n — n		
22	6 10	10	10	10.0	00.0	02.0	20	= n — n, * n — n		
23	6 10	10*	10	10.0	00.0	.	15	= n — n, * n — n		
24	6 10	10	10	10.0	00.1	00.0	14	= n — n		
25	5 10	09	10=	09.7	00.7	00.0	09	* n, = n — n, = n — n, = n — n		
MES. RED.		08.8	08.9	08.1	08.6	33.9	45.7			

1	6 09	000	00	03.0	07.3	.	.	= n — n, = n — n, = n — n		
2	4 10	10	10	10.0	00.0	.	.	= n — n, = n — n, = n — n		
3	3 10=	10=	10	10.0	00.0	00.3	.	= n — n, = n — n, = n — n, = n — n		
4	5 10	10	10	10.0	00.0	00.1	.	= n — n, = n — n, = n — n		
5	6 10	10	10	10.0	00.0	00.0	.	= n — n		
6	5 10*	10*	10*	10.0	00.0	00.0	.	= n — n, * n — n		
7	6 10	10	10*	10.0	00.0	00.4	.	= n — n, * n — n		
8	6 10*	10*	07	09.0	00.0	01.6	03	= n — n, * n — n, = n — n		
9	6 10	10	10	10.0	00.1	00.0	.	= n — n, * n — n		
10	6 10	10	10	10.0	00.2	00.0	.	= n — n, * n — n		
11	3 10	10*	10*	10.0	00.0	00.8	.	= n — n, = n — n, = n — n, = n — n, = n — n		
12	7 10	040	04	06.0	07.5	09.6	.	= n — n, = n — n, = n — n		
13	3 10=	10=	10	10.0	00.0	01.2	.	= n — n, = n — n		
14	5 10	070	08	08.3	02.9	.	.	= n — n		
15	5 06	010	00	02.3	05.8	.	.	= n — n		
16	5 07	10	10	09.0	03.5	.	.	* n, = n — n		
17	5 10	10	10	10.0	00.0	00.6	.	= n — n		
18	5 10*	040	04	06.0	06.4	05.0	06	= n — n, * n — n		
19	4 10	10*	10*	10.0	00.0	00.7	04	= n — n, * n — n		
20	5 10	10	00	06.7	00.0	10.4	15	= n — n, * n — n, = n — n		
21	3 20=	060	00	02.0	08.6	02.3	18	= n — n, = n — n		
22	4 08=	090	00	02.7	07.5	.	14	= n — n, = n — n		
23	7 07=	10	06	07.7	02.9	.	13	= n — n, = n — n, = n — n		
24	6 10	10	10	10.0	00.0	.	.	= n — n		
25	4 13=	10	10	10.0	00.4	.	.	= n — n, = n — n, = n — n		
26	6 09	10	10*	09.7	03.7	00.9	.	= n — n, * n — n		
27	3 100=	100=	03	07.0	00.0	08.0	.	* n — n, = n — n, = n — n, = n — n, = n — n		
28	5 08=	100	05	07.7	00.1	03.1	.	= n — n, = n — n, = n — n		
MES. RED.		09.1	08.3	07.0	08.1	53.4	45.0			

$\varphi = 45^{\circ}49' N \lambda = 15^{\circ}59' E$ Gr. $\Delta G = + 1 h 04 min.$

BR. ST. 56

D S	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodenе pare e mm			Relativna vlažnost U %				Pravac i jačina veta D, f (0-12)				
	7	14	21	7	14	21	Sred Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21			
1	743.1	743.7	745.0	08.8	10.1	09.8	09.6	11.1	08.1	-	08.1	08.1	08.2	95	88	90	91	E	1	W	1	-	0
2	745.1	743.9	744.5	07.5	15.9	10.5	11.1	15.9	07.4	-	06.9	06.9	06.8	88	51	71	70	W	1	WSW	4	W	2
3	744.6	743.3	743.0	08.0	16.8	14.1	13.3	17.5	07.7	-	06.2	06.3	06.5	77	44	54	58	W	2	SW	2	NE	2
4	742.7	741.5	742.4	07.0	16.8	12.8	12.4	16.9	06.3	-	06.1	07.8	08.1	82	55	73	70	NE	1	SE	2	NE	1
5	742.5	742.5	743.7	08.5	12.6	10.9	10.7	12.9	08.4	-	07.6	08.0	09.0	91	73	92	85	SSE	2	WNW	1	E	1
6	745.3	745.6	746.4	08.9	09.2	07.9	08.5	11.8	07.9	-	06.7	07.2	04.9	78	82	61	74	ENE	2	NNW	1	ENE	4
7	749.9	750.6	750.9	01.1	02.6	01.5	01.7	07.9	00.3	-	04.7	04.4	04.6	95	79	90	88	E	2	W	2	WNW	1
8	751.4	750.0	749.3	00.1	06.5	04.2	03.8	07.3	-00.3	-	04.3	04.1	04.5	93	56	73	74	E	1	SSW	2	NW	1
9	748.0	746.4	751.8	02.4	11.8	07.6	07.4	11.9	02.2	-	04.6	03.9	04.8	84	38	61	61	SW	1	SW	3	ENE	2
10	754.3	753.0	755.0	03.1	11.9	06.8	07.2	12.3	02.7	-	04.0	04.4	04.5	71	42	60	58	SSE	1	NNE	3	ESE	1
11	753.2	747.7	746.5	03.2	12.9	11.3	09.7	14.7	02.5	-	04.3	04.8	05.2	74	43	51	56	SW	2	WSW	3	NE	2
12	748.8	748.4	750.2	05.2	11.2	05.3	06.8	11.9	05.2	-	04.1	04.2	05.9	62	42	58	54	E	1	E	2	ENE	2
13	749.9	748.4	749.3	01.5	10.1	09.8	07.8	10.9	00.7	-	03.9	04.0	05.1	77	43	56	59	E	1	S	2	WNW	2
14	750.7	748.5	747.4	07.3	11.4	10.5	09.9	11.5	07.1	-	05.5	06.1	05.9	72	60	62	65	SW	2	WSW	3	SW	3
15	745.2	744.2	745.7	08.7	11.3	06.3	08.2	12.3	06.3	-	06.8	06.4	06.1	80	63	85	76	W	1	SSW	2	NW	1
16	745.2	743.0	739.6	05.1	13.8	11.4	10.4	14.4	04.7	-	05.5	06.3	05.4	84	53	53	63	NNW	2	WSW	4	SW	3
17	735.7	738.3	740.6	11.4	11.5	08.7	10.1	12.5	08.6	-	06.2	06.4	05.2	62	63	61	62	SW	4	ENE	2	W	2
18	743.3	746.0	749.7	05.3	04.2	03.0	03.9	09.1	03.0	-	05.6	05.6	05.0	84	89	89	87	ENE	2	ENE	2	NNW	1
19	751.2	750.1	750.8	03.0	06.4	01.6	03.2	07.2	01.6	-	05.1	04.1	04.4	90	57	65	77	E	1	S	2	NW	2
20	746.5	740.0	737.9	-00.1	08.4	06.3	09.8	-01.1	-	04.1	04.1	05.3	89	50	64	68	WNW	2	WSW	4	NNW	2	
21	731.4	734.1	738.5	06.7	10.7	07.5	08.1	12.8	06.7	-	06.6	05.8	05.0	89	60	64	71	W	1	NNE	2	ENE	2
22	742.5	746.4	749.9	05.0	05.3	04.7	04.9	09.1	04.7	-	04.1	05.2	04.0	62	77	62	67	NE	2	ENE	3	ENE	2
23	748.6	743.8	743.2	02.8	11.3	07.5	07.3	11.5	02.0	-	04.4	05.2	05.3	78	51	68	66	NW	1	WSW	4	E	1
24	739.9	739.8	742.5	01.8	05.7	04.4	04.1	07.5	01.2	-	04.9	05.4	05.2	93	78	83	85	ENE	2	NNE	2	E	1
25	747.3	748.7	750.0	04.3	09.5	07.0	07.0	10.7	03.8	-	05.3	04.5	04.1	85	50	55	63	SW	1	N	3	SSE	1
26	745.9	743.5	747.0	03.4	11.5	04.4	05.9	11.5	03.4	-	04.2	03.7	05.1	73	37	82	64	WSW	2	WSW	3	E	2
27	748.8	749.0	751.0	04.1	11.0	06.9	07.2	11.2	03.6	-	04.2	03.6	04.4	68	37	59	55	NNW	2	E	2	ESE	1
28	752.0	752.0	751.7	06.9	15.3	13.3	12.2	16.1	06.4	-	04.4	05.6	05.7	59	43	49	50	WSW	2	ESE	2	ESE	2
29	750.4	748.6	748.6	06.8	20.1	13.1	13.3	20.1	05.7	-	05.4	06.0	05.1	74	34	45	51	WNW	2	WSW	4	W	3
30	747.2	744.9	744.5	08.2	20.4	15.7	15.0	20.8	07.6	-	04.9	05.8	04.8	61	32	36	43	WNW	2	WSW	4	NW	3
31	744.3	742.9	743.2	08.0	19.4	15.6	14.7	19.8	07.8	-	05.3	05.4	05.6	66	32	42	47	E	1	SSE	2	SW	2
MES.	RED.	746.3	745.4	746.4	05.3	11.5	08.5	08.4	12.6	04.6	-	05.3	05.5	05.5	78	55	66	66	1.6	2.5	1.8		

1	743.0	740.4	738.9	10.6	18.4	14.4	14.5	18.8	09.8	-	05.8	05.6	05.7	61	35	46	47	WSW	2	SSE	2	NNE	2
2	737.1	736.7	737.9	09.4	17.0	12.4	12.8	18.1	09.1	-	06.0	05.2	06.6	68	36	61	55	NE	1	NW	1	WNW	2
3	739.8	739.0	739.2	09.8	16.6	13.8	13.5	16.9	07.8	-	07.1	07.5	06.6	79	53	56	63	ENE	1	ENE	3	NE	4
4	740.1	740.8	742.0	11.1	15.5	12.5	12.9	16.4	10.7	-	06.8	06.6	06.6	69	50	60	60	ENE	3	NE	3	ENE	2
5	743.1	743.1	744.8	09.7	14.0	10.6	11.2	14.1	09.4	-	05.9	06.4	06.2	65	53	65	61	NNW	1	S	2	E	2
6	748.8	749.3	750.9	06.2	10.1	06.7	07.4	10.6	05.7	-	04.4	03.7	03.0	61	40	41	47	ENE	2	E	3	ESE	3
7	750.9	746.8	743.7	02.3	10.2	08.4	07.3	10.5	02.3	-	02.7	04.1	02.4	50	44	29	41	E	3	ESE	3	ESE	3
8	741.9	742.0	742.1	03.1	06.9	05.8	05.4	08.4	02.3	-	04.8	04.2	05.4	84	56	78	73	ENE	3	ENE	2	WSW	2
9	743.3	743.6	744.0	06.1	12.2	09.5	09.3	13.1	03.2	-	04.0	05.3	04.9	57	50	55	54	ESE	2	SE	2	ENE	1
10	743.6	743.7	743.8	08.3	13.4	11.2	11.0	14.1	07.2	-	06.2	06.7	08.3	75	58	83	72	NNW	1	SSW	1	WSW	2
11	744.6	743.7	744.6	10.0	16.7	12.4	12.9	17.4	09.3	-	06.8	05.7	06.0	74	40	56	57	NNW	2	WSW	4	WNW	2
12	743.2	744.5	746.3	10.9	09.2	05.3	07.7	14.4	05.3	-	08.6	06.7	04.9	89	77	74	80	NW	2	E	2	W	1
13	741.4	737.2	734.8	04.9	05.7	05.0	05.2	06.8	04.0	-	04.9	05.4	06.1	76	78	94	83	W	1	ENE	2	ESE	1
14	734.9	735.5	736.0	03.1	08.8	07.3	06.6	13.5	02.9	-	05.3	07.5	06.7	92	88	88	89	E	2	WSW	1	ENE	2
15	736.1	737.1	739.7	07.3	04.9	04.7	05.4	07.3	04.0	-	05.8	05.2	04.6	75	80								

BR. ST. 56

 $H_s = 157 \text{ m } H_b = 162,5 \text{ m } h_t = 6,0 \text{ m } h_r = 2,0 \text{ m}$

Dan	Vrijeme u časovima	Oblačnost N (0-10)					Insekt broj št	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dnes				
1	4 10*	08	03	07.0	00.0	05.9	.	$\oplus n-730, 10^{15} H^{30}; \equiv n-10, =n-n$		
2	8 08	04○	00	04.0	09.2	00.3	.	$=n-11^o, \Delta n-dn$		
3	7 07○	03○	02	04.0	09.4	.	.	$\equiv n-10^{15}$		
4	6 01○	01○	04	02.0	08.8	.	.	$\equiv n-n$		
5	6 10*	10	100	10.0	00.9	01.8	.	$\equiv n-n, \oplus^{15} n-H^{30} i, 13^{15} n i$		
6	5 10*	10*	10*	10.0	00.0	05.8	.	$\equiv n-n, \oplus^{15} n-740, 11^{15} H^{30}, 13^{15} n; \boxed{n-n} 17-21 i$		
7	5 10*	10	07	09.0	03.6	06.8	02	$\times^o n-10^o, \equiv n-10^o =n-10^o, \boxed{n}$		
8	6 02*	07	00	03.0	05.5	03.2	.	$\sqcup^o n-730, \equiv n-10^{15} =n-10^{15} n$		
9	7 10	09	00	06.3	02.9	00.0	.	$\equiv n-12^{15}, 13^{15} n, \oplus^{15} n-6^{15}, 16^{15}$		
10	7 02○	08○	00	03.3	07.6	00.1	.	$\equiv n-10^o, 13^{15} n$		
11	6 04○	02○	02	02.7	08.0	.	.	$\equiv n-n$		
12	8 00○	01○	00	00.3	10.1	.	.	$\equiv n-8^{15}$		
13	8 10	10	100	10.0	04.0	.	.	$\equiv n-2^{15} i, 13^{15} n; \equiv 7^{15} \oplus^{15}, \oplus 10^{15} H^{30}, \oplus^{15} 13^{15} n$		
14	8 10	09	08	09.0	01.4	00.1	.	$\oplus n-n, 10^o$		
15	8 10*	10	02	07.3	00.4	00.0	.	$\equiv n-12^o, \oplus^{15} n-9^{15}, 14^{15}-10^{15} i$		
16	7 10	09	09	09.3	02.3	01.9	.	$\equiv n-12^{15}, \boxed{n-12^{15}, 16^{15} i}$		
17	8 10*	09	02	07.0	00.8	00.0	.	$\boxed{n-6-730, \oplus^{15} n-730 i, =748 i}$		
18	6 10*	10*	100	10.0	00.0	01.3	.	$\equiv n-n, \oplus^{15} n-i$		
19	5 10	10	04	08.0	00.2	12.2	.	$\equiv n-14^{15}, \oplus^{15} n-19^{15}$		
20	7 10*	100	100	10.0	00.4	00.7	.	$\equiv n-14^{15}, \boxed{n-12^{15}-16^{15}}, \oplus^{15} n-v$		
21	6 07○	10	10	09.0	02.5	00.7	.	$\equiv n-n, \oplus^{15} n, H^{15}, 16^{15} i, n$		
22	7 07○	10	00	05.7	06.5	00.5	.	$\equiv n-9^{15}, \oplus^{15} n-15^{15} i$		
23	8 00○	10	10	06.7	05.7	00.4	.	$\equiv n-9^{15}, \boxed{n-14-1730 i}, \oplus^{15} n$		
24	6 100*	10○	13○	10.0	00.0	23.4	01	$\equiv n-n, \times n-730, \oplus^{15} n i, \boxed{n}$		
25	6 08	08	00	05.3	07.0	03.0	.	$\equiv n-15^{15}$		
26	7 05	10	10	08.3	01.9	.	.	$\equiv n-11, 18-n; \oplus^{15} n-10^{15}$		
27	9 04○	05○	07	05.3	08.7	00.8	.	$\equiv n-8^{15}$		
28	7 08	07○	00	05.0	07.6	.	.	$\equiv n-8^{15}$		
29	9 01○	03○	00	01.3	11.1	.	.	$\equiv n-8^{15}$		
30	9 01○	06○	00	02.3	11.0	.	.	$\equiv n-8^{15}$		
31	8 01○	02○	07	03.3	10.9	.	.	$\equiv n-8^{15}$		
MES. RED.		06.6	07.5	04.7	06.3	145.4	68.9			

1	7 08	04○	07	36.3	08.2	.	.	$\equiv n-n, \oplus^{15} n$	*	
2	6 08	10	06	08.0	06.2	.	.	$\equiv n-n$		
3	6 04○	08	10	07.3	05.4	00.1	.	$\equiv n-n$		
4	5 09	09○	10	09.3	02.9	.	.	$\equiv n-n, \oplus^{15} n-16^{15}, 19^{15}-20^{15}$		
5	5 10	10	10	10.0	00.0	.	.	$\equiv n-n, \oplus^{15} n-16^{15}, 19^{15}-20^{15}$		
6	6 10	08	07	08.3	03.0	00.2	.	$\equiv n-n$		
7	6 09	09○	10	09.3	06.8	.	.	$\equiv n-13^{15}$		
8	5 10*	10	10	10.0	00.0	05.5	.	$\equiv n-n, \oplus^{15} n-10^{15} i$		
9	6 08○	02○	02	04.0	06.2	00.0	.	$\equiv n-n$		
10	6 10	10	100	10.0	00.3	.	.	$\equiv n-n, \oplus^{15} n i$		
11	6 03	08○	10	07.0	06.7	00.4	.	$\equiv n-n, \boxed{n-13^{15}, \oplus^{15} n-19^{15}, 21^{15} n}$		
12	6 10*	10	10	10.0	00.2	02.5	.	$\equiv n-n, \oplus^{15} n-10^{15} i$		
13	6 10	10	100	10.0	00.1	00.0	.	$\equiv n-n, \oplus^{15} n-10^{15} i, \boxed{n-17^{15}, 17^{15}, R^{15}, 17^{15}, 19^{15} i}$		
14	5 10	08	06	08.0	02.5	18.6	.	$\oplus^o n-6^{15}, 12^{15}, 13^{15}, 16^{15}, 15^{15}, 20^{15}, \equiv n-n$		
15	5 10	10	100	10.0	00.0	14.2	.	$\equiv n-17, \boxed{n-12^{15}, \oplus^{15} n i}$		
16	6 10*	10	04	08.0	00.8	08.6	.	$\equiv n-n, \oplus^{15} n-10^{15} i, 13^{15}-15^{15}$		
17	7 08○	08	08	08.0	05.5	00.0	.	$\equiv n-11^{15}$		
18	7 09	07○	00	05.3	05.9	.	.	$\equiv n-9^{15}, \oplus^{15} n-12^{15}, 17^{15} n i$		
19	6 01○	10	10	07.0	01.4	00.0	.	$\equiv n-n$		
20	6 10	08○	10	09.3	06.8	01.0	.	$\equiv n-n, \oplus^{15} n$		
21	6 09	08	100	09.0	02.0	00.3	.	$\equiv n-n, \oplus^{15} n-10^{15} n, \oplus^{15} n$		
22	6 03○	09	00	04.0	03.8	02.3	.	$\equiv n-n$		
23	6 01○	09	00	03.3	08.7	.	.	$\equiv n-n, \Delta n-dn, \oplus^{15} n-13^{15}, 13^{15}$		
24	6 10	10	06	08.7	07.8	00.0	.	$\equiv n-n, R^{15}, 14^{15}, 14^{15}, \oplus^{15} n-15^{15}, 15^{15}$		
25	8 00○	03○	00	01.0	11.9	00.0	.	$\equiv n-10^{15}$		
26	6 02○	08○	01	03.7	09.6	.	.	$\equiv n-n, \boxed{n-13^{15}, 15^{15}, \oplus^{15} n-16^{15}}$		
27	8 10○	03	04	07.3	03.8	02.4	.	$\equiv n-14^{15}, \oplus^{15} n-9^{15}, 10^{15}, 15^{15}, \oplus^{15} n-22, \boxed{n-14^{15}, \boxed{n-14^{15}}}$		
28	7 08	09○	04	07.0	03.5	07.1	.	$\oplus^{15} n-14^{15}, \oplus^{15} n-4-16^{15} i$		
29	6 10○	05○	10	05.0	10.4	00.5	.	$\equiv n-13^{15}, \Delta n-dn$		
30	8 10	09○	100	19.7	07.2	.	.	$\equiv n-9^{15}, \oplus^{15} n-10^{15} n$		
MES. RED.		07.3	08.2	06.9	17.5	137.6	53.7			

1978 MAJ

ZAGREB-GRIC

 $\varphi = 45^{\circ}49' N \lambda = 15^{\circ}59' E$ Gr. $\Delta G = +1h\ 04\ min.$

BR. ST. 56

D S	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodenih pore e mm			Relativna vlažnost U %			Pravac i jačina veta D, f (0-12)		
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21
1	737.9	734.6	735.3	13.2	19.9	12.3	14.4	20.0	11.3	-	08.9	08.7	10.1	78	50	94	74	ENE 1	NNW 2	NNW 1
2	732.8	734.6	738.1	10.9	11.6	11.7	11.5	14.2	10.0	-	08.9	09.4	08.4	91	92	81	88	WSW 1	NW 2	NNW 2
3	742.7	739.9	748.7	11.6	19.7	13.3	14.5	20.4	10.5	-	08.7	08.2	09.8	85	48	86	73	W 1	SW 3	ENE 1
4	750.1	749.4	750.3	12.5	20.4	14.8	15.6	20.5	10.3	-	08.3	08.2	07.8	76	45	62	61	- 0	SW 3	NNW 2
5	751.0	749.4	747.7	12.1	20.5	18.2	17.3	21.3	09.3	-	07.9	07.6	07.6	75	52	49	55	W 1	S 2	NE 2
6	747.1	745.4	742.9	13.6	14.3	14.4	14.2	18.2	13.0	-	10.0	09.6	10.1	85	78	82	82	W 1	SW 1	ENE 1
7	740.3	739.1	739.7	13.1	19.6	15.4	15.9	19.7	12.5	-	10.8	08.9	08.9	96	52	68	72	S 1	WSW 2	NNW 2
8	741.0	739.9	740.5	12.7	18.4	15.5	15.5	18.4	10.2	-	08.8	09.5	09.4	80	60	71	70	- 0	SSE 1	ENE 1
9	742.1	742.2	744.8	12.3	17.5	13.0	14.0	19.7	12.0	-	09.3	07.8	09.4	87	52	84	74	SSW 1	NNW 3	ENE 2
10	748.1	749.3	751.0	11.6	13.5	09.8	11.2	15.7	09.8	-	09.7	08.4	08.0	94	73	89	85	SSW 1	SSW 2	NE 1
11	751.7	753.2	753.5	05.3	04.6	04.2	04.6	09.8	03.3	-	05.4	05.5	05.2	80	86	83	83	E 3	ENE 2	NW 1
12	751.8	748.7	745.9	04.0	10.4	08.6	07.9	10.9	01.2	-	04.4	04.1	04.2	72	43	50	55	NNE 1	WSW 2	S 2
13	743.7	742.7	741.5	06.8	07.1	07.0	07.0	08.6	05.3	-	05.0	07.1	06.6	67	93	88	83	NE 1	ENE 2	NE 2
14	743.3	745.9	747.1	07.6	12.6	08.9	09.5	12.8	06.5	-	06.8	06.1	06.7	87	56	79	74	NE 1	ENE 2	NNW 2
15	747.0	745.3	745.5	07.1	16.6	10.6	11.2	16.9	05.0	-	06.4	06.8	08.2	84	48	85	72	E 1	S 2	NE 1
16	747.1	747.3	748.7	11.1	18.4	11.8	13.3	18.6	09.0	-	07.8	07.6	07.7	78	48	74	67	SE 1	SSE 2	NNE 2
17	749.7	748.2	749.0	10.2	19.8	13.0	14.0	19.9	08.1	-	07.7	08.3	08.5	82	48	76	69	NNW 1	S 2	NNW 1
18	749.4	748.9	748.3	12.5	19.5	17.4	16.7	19.7	10.7	-	09.2	09.7	10.7	85	57	72	71	S 1	SSW 2	NE 1
19	747.0	746.0	746.1	15.4	21.3	14.9	16.6	21.3	13.5	-	11.0	11.4	12.0	84	60	95	80	ENE 1	SW 1	SSE 1
20	746.5	746.7	747.8	14.0	19.2	16.4	16.5	20.7	11.9	-	11.2	11.4	10.0	94	68	71	78	E 1	ENE 3	NE 2
21	747.8	747.1	745.3	15.0	18.4	17.0	16.9	19.4	13.1	-	09.9	13.2	11.8	77	83	81	80	NNE 1	S 2	NE 2
22	740.7	737.5	737.3	16.9	16.6	13.4	15.1	17.8	13.4	-	13.2	12.9	10.5	91	91	93	92	NE 2	N 2	S 2
23	737.6	739.3	740.8	12.8	18.4	15.4	15.5	19.3	11.0	-	09.3	10.0	09.0	86	63	69	73	WSW 1	WSW 4	WSW 2
24	742.5	743.9	745.3	14.7	17.4	14.2	15.1	18.3	13.2	-	09.6	09.4	08.6	77	63	71	70	WNW 1	NW 2	WNW 2
25	746.8	747.0	748.0	14.1	19.7	14.4	15.7	20.5	12.4	-	09.3	09.2	10.6	78	53	86	72	NE 1	W 2	NNE 1
MES. RED.	745.9	745.6	746.1	12.2	17.0	13.4	14.0	18.2	10.2	-	08.7	09.0	08.8	81	62	76	73	1.2	2.2	1.6

1978 JUN

ZAGREB-GRIC

1	752.5	752.1	752.1	16.8	25.3	21.4	21.2	25.4	14.5	-	11.4	09.4	11.7	79	39	61	60	SSW 1	ENE 2	W 2
2	752.0	751.0	750.2	17.2	23.2	21.1	20.7	25.0	15.2	-	10.8	13.4	09.0	73	63	48	61	N 1	W 2	NNE 2
3	750.2	749.4	749.3	17.9	27.2	21.0	21.8	27.4	15.2	-	10.4	07.8	10.6	68	29	57	51	N 1	S 2	NE 1
4	750.1	749.6	750.1	16.0	27.2	23.0	22.3	28.0	14.5	-	11.5	09.8	10.5	84	36	50	57	ENE 1	SSW 1	NE 2
5	750.8	749.4	749.7	18.3	27.5	19.5	21.2	28.2	16.0	-	11.5	10.4	13.3	73	38	78	63	WSW 1	NNW 2	NNW 2
6	749.5	748.4	748.7	17.5	27.1	23.9	23.1	27.6	15.0	-	11.0	12.9	13.2	74	48	59	60	SW 1	NW 2	N 2
7	746.8	748.1	748.4	19.1	27.3	22.0	22.6	28.1	16.9	-	11.3	10.9	11.7	68	40	59	56	WSW 1	WSW 3	W 2
8	747.7	746.1	749.0	21.0	28.0	20.5	22.5	28.4	18.0	-	11.1	12.5	12.0	60	44	66	57	W 2	WNW 2	S 1
9	749.8	748.0	747.2	19.1	25.8	22.7	22.6	26.6	16.1	-	12.9	12.8	14.1	78	51	68	66	SE 1	S 2	ENE 1
10	746.6	745.5	746.4	19.0	27.3	22.9	23.0	27.4	17.3	-	13.1	12.6	10.4	80	46	50	59	WSW 1	SW 3	NNW 2
11	749.5	752.5	752.3	17.3	14.7	14.9	15.5	22.9	14.5	-	11.9	11.6	12.1	80	92	95	89	ENE 2	NE 2	NE 1
12	748.9	744.9	743.3	15.0	17.4	16.0	16.1	18.0	13.9	-	11.9	11.7	12.5	93	79	92	88	ENE 1	E 1	NNE 1
13	746.1	747.4	747.3	11.4	10.6	10.5	10.8	16.0	10.4	-	08.6	07.9	09.0	85	82	94	87	NE 2	E 1	W 2
14	745.8	746.0	745.6	11.1	14.4	12.5	12.6	15.8	10.5	-	08.8	09.4	09.2	88	77	85	83	NNE 1	S 2	SW 2
15	745.9	743.5	741.1	10.5	19.0	15.0	14.9	19.8	08.5	-	08.4	09.6	09.2	88	58	72	73	S 1	SE 2	NE 2
16	739.8	739.8	740.3	14.5	22.0	17.6	17.9	22.1	11.2	-	09.7	09.5	11.6	79	48	77	68	SSE 1	SE 2	ENE 2
17	741.0	740.3	740.7	15.5	21.4	17.6	18.0	22.2	14.5	-	12.1	13.0	11.8	92	68	78	79	SSW 1	SE 2	W 1
18	744.1	746.7	749.0	16.4	23.2	18.3	19.1	24.2	14.9	-	11.0	08.5	09.3	79	40	59	59	WNW 2	WNW 2	NE 3
19	750.6	749.5	748.6	16.2	21.0	17.7	18.2	22.4	13.6	-	09.0	10.4	10.1	65	56	66	62	SE 1	SE 2	NNE 2
20	749.4	747.7	746.0	17.3	24.1	19.8	20.3	24.7	13.4	-	10.8	09.5	09.6	73	42	55	57	- 0	SSE 2	NE 2
21	744.1	742.1	743.1	18.8	21.5	15.9	18.0	22.3	15.9	-	11.4	10.8	09.5	70	56	70	65	- 0	NE 2	NNW 2
22	744.5	743.5	742.5	16.0	23.3	19.8	19.7	24.9	13.3	-	11.1	10.3	11.6	82	48	67	66	ENE 1	W 2	WSW 1
23	742.5	741.0	740.5	16.4	25.7	19.8	20.4	25.9	14.1	-	10.5	10.8	10.7	75	43	62	60	W 1	SSW 3	WSW 2
24	740.2	739.8	741.1	19.7	23.0	14.4	17.9	25.7	14.4	-	10.6	11.6	10.8	61	55	88	68	SSE 2	W 3	NNW

BR. ST. 56

 $H_s = 157 \text{ m } H_b = 162,5 \text{ m } h_t = 6,0 \text{ m } h_r = 2,0 \text{ m}$

Dan	Vrijeme 0-10	Oblačnost N (0-10)					Intenzitet brzine vjetra km/h	Padavina R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dies				
1	7 09	10	04	07.7	01.2	00.1	.	= n-n, 0° 14° 17°		
2	5 08	10	04	07.3	00.2	08.0	.	= n-n, 0° 10° 17° i		
3	7 08	04	10	07.3	07.4	07.6	.	= n-8°, 0° 12° R ²⁰ , R ¹⁵ , 0° 15° 17°		
4	8 09	09	04	07.3	06.6	01.8	.	= n-9°		
5	8 08	10	10	09.3	03.4	.	.	= n-12°, 0° 12° n		
6	6 10	10	10	10.0	00.6	01.5	.	= n-17, 0° 17°, R ²⁰ , R ¹⁵ , R ¹⁰		
7	7 10	03	02	05.0	08.1	13.3	.	• n-6° = n-9°, R ²⁰ , R ¹⁵ , R ¹⁰		
8	7 08	07	04	06.3	05.3	00.2	.	= n-8°		
9	7 09	10	10	09.7	04.2	00.1	.	= n-10°, 0° 17°, R ²⁰ , R ¹⁵ , R ¹⁰		
10	6 10	10	10	10.0	03.7	06.4	.	= n-n, 0° 10°, R ²⁰ , R ¹⁵ , R ¹⁰		
11	5 10	10	10	10.0	01.4	04.6	.	= n-n, 0° 17°, R ²⁰		
12	7 01	07	10	36.0	09.5	01.9	.	= n-9°		
13	4 10	10	10	10.0	00.0	.	.	= n-n, 0° 17°, R ²⁰		
14	7 10	09	10	09.7	03.9	14.6	.	= n-10°, 0° 17°, R ²⁰ , R ¹⁵ , R ¹⁰		
15	7 07	08	10	08.3	08.8	00.0	.	= n-n, 0° 10°, R ²⁰		
16	7 08	03	09	06.7	07.2	00.9	.	= n-10°, R ²⁰ , R ¹⁵ , 0° 10°, R ¹⁰ , 0° 10°, R ¹⁰		
17	7 10	10	04	04.7	09.1	01.6	.	= n-n, 0° 14°, R ²⁰ , R ¹⁵		
18	7 04	10	02	05.3	05.7	00.6	.	= n-H°		
19	6 08	09	08	08.3	02.0	.	.	= n-n, 0° 17°, R ²⁰ , R ¹⁵ , R ¹⁰		
20	6 08	08	07	07.7	05.6	05.0	.	= n-H°		
21	5 08	10	10	09.3	02.1	.	.	= n-n, 0° 17°, R ²⁰		
22	6 10	10	05	08.3	00.0	01.5	.	= n-n, 0° 17°, R ²⁰		
23	8 08	07	10	08.3	06.8	23.3	.	= n-8°, 0° 17°, R ²⁰ , R ¹⁵ , R ¹⁰ , 0° 14°, R ¹⁰ , 0° 14°, R ¹⁰		
24	6 10	08	10	09.3	03.2	01.4	.	• n-7° = n-n, 0° 17°, R ²⁰ , R ¹⁵ , R ¹⁰		
25	6 10	10	07	09.0	02.7	00.0	.	= n-n, 0° 17°, R ²⁰		
26	6 09	10	05	08.0	00.4	01.4	.	= n-n, 0° 17°, R ²⁰ , R ¹⁵ , R ¹⁰ , R ¹⁰ , R ¹⁰		
27	6 06	06	04	05.3	08.8	00.4	.	= n-n		
28	6 09	08	04	07.0	02.4	00.5	.	= n-n, 0° 17°, R ²⁰ , R ¹⁵ , R ¹⁰ , R ¹⁰ , R ¹⁰		
29	7 06	10	10	08.7	08.1	06.0	.	= n-8°, 0° 17°, R ²⁰ , R ¹⁵ , R ¹⁰ , R ¹⁰		
30	7 04	09	10	07.7	06.3	03.0	.	= n-9°, R ²⁰ , R ¹⁵ , R ¹⁰ , R ¹⁰ , R ¹⁰		
31	6 09	10	07	08.7	06.3	08.7	.	= n-n, 0° 17°, R ²⁰ , R ¹⁵ , R ¹⁰		
MES.	RED.	07.9	08.5	07.4	07.9	138.0	114.4			

1	7 09	02	00	03.7	08.8	00.2	.	= n-9°		
2	8 02	07	00	03.0	09.8	.	.	= n-13°, 0° 10°, R ²⁰		
3	7 00	01	00	00.3	12.2	02.9	.	= n-H°		
4	7 00	02	29	03.7	13.0	.	.	= n-H°, 0° 10°, R ²⁰		
5	7 18	04	06	06.0	10.3	.	.	= n-n, 0° 17°, R ²⁰ , 0° 17°, R ²⁰		
6	6 01	06	10	05.7	12.7	03.2	.	= n-n		
7	7 09	08	05	07.3	09.6	.	.	= n-8°, 0° 17°, R ²⁰		
8	7 17	10	10	07.3	08.9	.	.	= n-17°, R ²⁰		
9	8 09	07	06	07.3	08.9	.	.	= n-9°, R ²⁰ , R ¹⁵		
10	6 23	10	10	17.7	05.2	.	.	= n-n, 0° 17°, R ²⁰		
11	6 100	100	100	10.0	00.0	00.3	.	= n-n, 0° 17°, R ²⁰		
12	6 100	10	10	10.0	00.0	16.6	.	= n-n, 0° 17°, R ²⁰ , R ¹⁵ , R ¹⁰		
13	5 100	100	100	10.0	00.0	09.7	.	= n-n, 0° 17°, R ²⁰		
14	6 100	09	05	08.0	12.6	09.9	.	= n-n, 0° 17°, R ²⁰		
15	6 04	09	04	05.7	08.9	03.0	.	= n-15°		
16	6 09	09	04	04.3	11.2	.	.	= n-16°		
17	6 09	10	10	09.7	03.2	01.5	.	= n-13°, 0° 17°		
18	9 00	05	01	02.0	11.7	02.0	.	• n-H°, n-H°		
19	8 02	07	01	03.3	09.1	.	.	= n-8°		
20	6 14	02	00	02.0	10.8	.	.	= n-13°		
21	7 28	10	00	06.0	02.8	.	.	= n-10°, 0° 17°, R ²⁰		
22	6 01	03	00	01.3	12.4	00.0	.	= n-13°		
23	6 10	09	10	06.7	12.0	.	.	= n-13°		
24	7 09	04	100	07.7	03.5	.	.	= n-9°, R ²⁰ , R ¹⁵ , R ¹⁰ , 0° 17°, 0° 17°, R ²⁰ , R ¹⁵ , R ¹⁰		
25	8 09	05	00	07.7	17.1	08.4	.	R n, 0° 17°, R ²⁰ , R ¹⁵ , R ¹⁰		
26	8 10	04	05	06.3	06.3	04.2	.	= n-10°, 0° 17°, R ²⁰		
27	7 10	10	06	08.7	00.1	01.0	.	= n-7°, 0° 16°, 0° 17°, 0° 17°		
28	8 18	09	04	07.0	07.1	00.0	.	= n-8°		
29	7 23	04	03	03.3	13.3	.	.	= n-10°, 16°-n		
30	8 11	02	07	03.3	12.3	.	.	= n-9°		
MES.	RED.	15.4	26.6	05.5	25.8	233.7	61.9			

1978 JULY

ZAGREB-GRIC

 $\varphi = 45^{\circ}49' N \lambda = 15^{\circ}59' E$ Gr. $\Delta G = + 1h 04 min.$

BR. ST. 56

D S	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodené pare e mm			Relativna vlažnost u %				Pravac i jačina veta D, f (0-12)			
	7	14	21	7	14	21	Sred Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dnes	7	14	21		
1	749.2	748.3	748.3	17.6	25.4	22.0	21.8	26.0	15.3	-	11.0	11.0	10.9	73	45	55	58	NE	1	SW	3	NNW 2
2	748.5	749.5	749.4	17.9	17.5	16.2	17.0	22.0	16.2	-	12.5	12.9	11.8	82	86	85	84	SE	1	NW	1	W 2
3	748.0	746.4	745.0	14.4	25.2	21.5	20.7	26.3	13.3	-	10.9	10.6	11.2	89	44	58	64	WSW	1	SW	2	SSE 1
4	744.7	743.7	743.4	18.4	25.2	22.1	22.0	26.8	15.6	-	11.4	11.8	09.8	72	49	55	59	W	1	WSW	4	WSW 3
5	742.0	741.0	745.1	19.2	18.4	13.4	16.1	23.5	13.2	-	11.5	14.2	10.4	69	89	90	83	W	1	WSW	2	SE 2
6	747.8	745.7	745.5	14.6	22.6	16.2	17.4	23.7	11.6	-	11.1	10.5	11.6	89	51	84	75	N	1	SE	2	SE 1
7	745.5	746.6	747.5	14.9	17.9	16.3	16.4	20.1	14.2	-	10.9	10.6	10.4	86	69	75	77	NE	1	NW	2	NW 1
8	750.1	749.1	749.9	15.2	20.5	14.2	16.0	21.5	14.0	-	10.4	09.8	09.6	80	54	79	71	WSW	1	SSW	2	SSE 1
9	748.1	744.3	743.4	12.1	22.2	19.0	18.1	23.0	10.5	-	09.4	09.2	09.8	88	46	59	64	WSW	1	SSW	2	W 2
10	744.9	745.3	746.7	14.1	16.6	16.5	15.9	19.9	13.5	-	11.4	11.3	12.4	95	80	88	88	SSE	1	ENE	1	ENE 2
11	747.8	747.5	747.0	14.4	21.0	19.8	18.8	22.2	14.2	-	10.9	13.6	14.4	89	73	83	82	ENE	2	SW	1	NE 2
12	747.9	747.6	747.8	17.9	27.8	23.5	23.2	28.7	16.4	-	13.8	14.0	14.6	90	50	67	69	W	1	SSW	2	NE 1
13	751.1	750.4	751.3	19.8	27.4	23.2	23.4	28.1	18.3	-	13.1	12.0	13.8	76	44	65	62	SW	1	SSE	2	ENE 2
14	751.7	750.5	749.1	19.5	26.1	22.7	22.8	26.9	18.6	-	14.0	12.2	13.2	82	48	64	65	NE	1	S	2	NNE 2
15	747.4	747.4	748.9	19.9	23.9	17.3	19.6	24.6	15.4	-	15.0	14.9	13.2	86	67	89	81	NE	1	SE	2	NNW 1
16	750.4	748.7	748.5	16.3	21.8	19.0	19.0	22.8	15.1	-	09.3	12.5	12.4	67	64	75	69	NE	2	SE	2	NNE 2
17	750.4	749.6	748.8	19.0	25.0	21.4	21.7	25.2	18.1	-	11.1	13.3	14.3	67	56	75	66	E	1	S	2	NE 2
18	746.9	743.6	743.1	19.3	26.8	24.1	23.6	28.0	17.7	-	14.5	14.8	12.6	87	56	56	66	SSE	1	SW	3	NW 2
19	741.3	742.7	745.1	17.3	17.4	17.1	17.2	24.1	14.0	-	12.2	10.8	11.1	82	73	76	77	S	1	NNW	3	NNW 1
20	747.2	745.5	744.2	15.4	24.9	20.2	20.2	25.0	13.4	-	10.8	10.4	10.2	82	44	57	61	W	1	SSW	2	NE 2
21	745.0	745.0	748.5	17.6	17.1	12.3	14.8	20.2	12.3	-	11.5	10.8	09.8	76	74	92	81	NNE	1	ENE	3	SE 2
22	750.5	751.5	752.4	12.3	17.3	14.9	14.9	19.9	10.1	-	13.0	09.3	08.4	93	63	66	74	NW	1	SSE	2	NNE 2
23	752.6	751.7	751.3	13.0	20.9	16.1	16.7	21.1	11.3	-	08.5	08.6	09.4	73	46	68	62	E	1	ESE	2	NE 2
24	751.0	750.3	750.3	14.1	21.8	17.6	17.8	22.7	12.4	-	09.6	10.4	10.0	79	53	66	66	NNE	1	ENE	2	NNE 2
25	750.5	749.7	749.9	15.7	23.5	19.2	19.4	24.7	13.3	-	10.2	09.6	11.2	77	44	67	63	NE	1	SSE	2	NNW 1
26	750.0	749.1	749.2	16.6	25.0	20.8	20.8	25.7	15.0	-	11.2	11.4	11.1	79	48	60	62	-	0	SSE	2	NE 2
27	750.2	750.7	751.4	17.4	26.1	22.1	21.9	26.5	15.8	-	11.5	10.2	10.0	77	40	50	56	NE	1	ENE	2	NNE 2
28	752.5	752.4	752.8	19.2	27.6	23.6	23.5	27.8	16.5	-	12.3	09.7	11.4	74	35	52	54	-	0	E	2	NNE 2
29	753.2	751.7	750.9	19.6	27.2	23.6	23.5	27.8	17.1	-	13.1	12.5	12.7	77	46	58	60	NE	1	SSE	2	NNE 2
30	750.0	749.4	748.9	19.6	20.3	19.7	19.8	25.0	18.0	-	13.9	15.4	13.0	82	87	75	81	NE	1	NNE	1	NE 1
31	748.3	747.8	748.2	18.0	26.8	22.3	22.4	27.0	16.3	-	12.9	13.5	12.9	83	51	64	66	-	0	SSE	2	NE 2
MES. RED.	748.5	747.8	748.1	16.8	22.8	19.3	19.6	24.4	14.7	-	11.6	11.7	11.5	81	57	69	69	1.0	2.1	1.7		

1978 AVGUST

ZAGREB-GRIC

1	749.1	748.7	748.6	19.0	27.9	24.1	23.8	28.0	17.4	-	13.0	13.8	11.2	79	49	50	59	ENE	1	SE	2	NE 2
2	748.9	748.2	748.2	20.8	28.9	25.0	24.9	29.8	20.1	-	11.9	15.2	15.2	65	51	64	60	E	1	SE	2	NNE 2
3	748.5	746.8	747.8	20.3	29.1	22.6	23.7	30.0	19.1	-	14.8	16.0	18.0	83	53	69	68	ENE	1	WSW	2	E 2
4	748.0	747.9	747.9	21.2	20.0	19.1	19.9	22.6	18.0	-	14.9	16.5	15.8	78	94	95	89	ENE	1	S	1	W 1
5	749.1	748.5	748.1	19.7	26.0	22.2	22.5	26.8	17.3	-	14.2	11.8	14.3	83	47	71	67	W	2	SSW	2	NE 2
6	748.3	747.0	745.6	18.7	26.6	24.0	23.3	27.2	17.2	-	14.4	15.2	15.0	89	58	67	71	ENE	1	S	2	NNE 2
7	743.4	741.0	737.4	19.7	29.8	25.2	25.0	30.0	18.1	-	14.9	16.7	14.0	87	53	58	66	ENE	1	SW	2	E 1
8	735.0	738.3	742.4	24.5	23.9	17.0	20.6	26.4	17.0	-	12.7	09.2	11.0	55	41	76	57	SW	3	WSW	4	SSW 2
9	745.8	745.2	746.1	15.3	25.0	19.9	20.0	25.2	13.7	-	10.2	08.8	09.2	78	37	53	56	SW	2	SSW	2	NNW 2
10	748.7	748.6	748.7	14.3	15.3	15.5	15.2	19.9	14.0	-	11.3	11.1	09.8	93	85	74	84	ENE	1	NW	1	NNW 2
11	749.8	749.0	749.3	14.1	21.8	15.4	16.7	21.9	12.5	-	09.8	10.0	11.0	81	51	84	72	ENE	1	WWW	1	N 1
12	751.1	750.8	751.1	13.9	21.5	15.1	16.4	21.9	12.9	-	09.7	10.1	10.7	81	52	83	72	NW	1	S	2	NNE 2
13	751.1	750.1	748.6	13.9	16.4	15.7	15.4	18.3	12.6	-	10.5	11.5	10.8	88	42	81	84	WWN	1	WWN	2	NE 1
14	749.6	750.4	750.8	14.7	18.9	17.4	17.1	19.3	14.3	-	11.6	12.3	12.1	93	75	81	83	NE	1	SSW	1	SE 1
15	751.1	749.9	749.7	14.0	22.2	18.5	18.3	23.3	12.8	-	10.9	12.4	13.1	91	62	82	78	NE	1	SSW	2	ENE 1
16	750.2	749.7	749.3	15.4	25.7	20.3	20.4	26.0	14.5	-	11.8	12.2	12.8	90	49	72</td						

BR. ST. 56

 $H_s = 157 \text{ m } H_b = 162,5 \text{ m } h_t = 6,0 \text{ m } h_r = 2,0 \text{ m}$

Dan	Vrijeme 0-9	Oblačnost N (0-10)					Insektocija broj sani	Padavine R mm	Snežni pokrijev h cm		Razvoj vremena w
		14	7	14	21	Sred Dnes					
1	7	03	07	06	05.3	08.2	.	.	.	==n-12,16-n, 8°10°	
2	6	10	10	06	08.7	00.0	00.0	.	.	==n-n, 8°7°, 0°9°, 8°5°	
3	8	00	08	09	02.7	13.7	01.8	.	.	==n-8°	
4	7	00	08	00	02.7	11.9	.	.	.	==n-8°	
5	6	08	10	100	09.3	02.8	.	.	.	==n-14°, R 0°, 8°10°, 8°2°, R 8°10°, 10°21°, R 10°10°, 8°10°, 10°, 10°, n	
6	8	09	05	09	07.7	10.6	22.1	.	.	● 17°17°, 17°17°, R 17°17°	
7	6	10	10	09	09.7	02.0	00.6	.	.	==n-7°, 0°10°, 0°10°, 10°10°	
8	8	07	08	06	07.0	05.5	00.0	.	.	==n-8°, 8°9°, 8°10°, 10°10°, R 10°10°, 0°10°, 10°	
9	7	08	03	07	06.0	09.0	01.6	.	.	==n-dr	
10	6	13	08	10	09.3	02.6	05.4	.	.	==n-n, 8°10°, 8°10°, 13°13°, 20°20°	
11	5	10	06	03	06.3	06.0	11.0	.	.	==n-n, 8°10°	
12	8	00	03	00	01.0	12.9	00.0	.	.	==n-4°	
13	8	00	01	100	03.7	12.0	.	.	.	==n-10°, R 10°, R 8°, 10°10°	
14	6	07	05	10	07.3	09.6	00.2	.	.	==n-n, 8°10°	
15	6	10	10	10	10.0	00.6	00.0	.	.	==n-n, 8°10°, 8°10°, 8°10°, R 8°10°, 8°10°, 8°10°	
16	6	10	09	04	07.7	05.4	48.8	.	.	==n-n	
17	5	06	09	06	07.0	07.5	.	.	.	==n-n	
18	5	00	08	03	03.7	07.3	.	.	.	==n-n, 8°10°, 10°10°	
19	9	10	08	00	06.0	04.9	00.0	.	.	● 8°10°, 10°10°, 10°10°, 10°10°, R 10°10°	
20	8	00	03	08	03.7	12.0	08.8	.	.	==n-H	
21	5	07	09	10	08.7	02.2	.	.	.	==n-n, 8°10°, R 8°10°	
22	7	00	09	04	04.3	08.0	10.4	.	.	==n-9°	
23	6	00	07	00	02.3	12.3	.	.	.	==n-10°	
24	5	00	05	00	01.7	10.8	.	.	.	==n-n, 8°10°-dr	
25	5	08	06	02	05.3	11.6	.	.	.	==n-n, 8°10°-10	
26	5	00	03	09	01.0	11.5	.	.	.	==n-n, 8°10°-dr	
27	6	00	02	00	00.7	11.3	.	.	.	==n-n, 8°10°	
28	6	06	06	00	04.0	11.4	.	.	.	==n-n	
29	6	07	10	05	07.3	10.2	.	.	.	==n-n	
30	5	10	08	04	07.3	06.3	.	.	.	==n-n, R 10°, 10°, R 10°, R 10°, R 10°	
31	6	00	03	03	02.0	11.0	04.6	.	.	==n-n	
MES. RED.		05.0	06.7	04.7	05.5	251.1	115.3				

1	6	00	00	04	01.3	11.6	.	.	.	==n-n	
2	6	00	01	03	01.3	12.0	.	.	.	==n-n	
3	6	08	03	02	04.3	11.5	.	.	.	==n-n	
4	5	10	10	10	10.0	20.1	.	.	.	==n-n, 8°10°	
5	7	03	02	10	05.0	09.6	11.3	.	.	==n-10°, n	
6	7	00	01	03	01.3	11.1	04.6	.	.	==n-10°, n	
7	6	09	06	05	06.7	08.9	00.0	.	.	==n-n, 8°10°	
8	9	04	05	10	06.3	09.1	.	.	.	● 17°17°, 8°8°, 8°8°, 10°10°, 10°10°	
9	9	00	03	04	02.3	11.4	00.3	.	.	● 17°17°, 8°8°, 10°10°, 10°10°	
10	6	10	08	05	07.7	02.0	01.8	.	.	==n-n, 8°10°, 8°10°, 8°10°	
11	6	01	05	03	03.0	18.6	00.9	.	.	==n-n, 8°10°-dr, 8°10°, 10°10°, R 10°, 10°, 10°, 10°	
12	6	02	08	10	06.7	08.0	02.2	.	.	==n-n, 8°10°, 8°10°, 8°10°, 8°10°, 8°10°, 8°10°, 8°10°	
13	4	06	10	10	08.7	03.3	04.4	.	.	● 10°10°, 10°10°, 10°10°, 10°10°, 10°10°, 10°10°	
14	6	10	10	04	08.0	00.1	04.0	.	.	==n-n, 8°10°, 8°10°, 8°10°	
15	6	00	03	00	01.0	11.7	00.0	.	.	==n-n, 8°10°	
16	6	00	02	05	02.3	12.1	.	.	.	==n-10°, 8°10°	
17	8	10	09	08	05.7	09.6	.	.	.	==n-10°, 8°10°	
18	8	10	09	05	08.0	04.8	.	.	.	● 10°10°	
19	7	00	00	00	01.7	12.0	.	.	.	==n-12°	
20	7	00	06	00	02.0	11.0	.	.	.	==n-9°	
21	7	11	06	02	02.7	10.9	.	.	.	==n-12°	
22	6	00	06	06	04.0	11.3	.	.	.	==n-n	
23	6	00	00	02	00.7	11.5	.	.	.	==n-n	
24	6	10	07	01	02.7	09.9	.	.	.	==n-n	
25	6	06	03	00	03.0	09.9	.	.	.	==n-n	
26	4	10	09	10	09.7	00.3	.	.	.	==n-n, 8°10°, 8°10°, 8°10°	
27	6	13	06	02	03.7	29.9	79.6	.	.	==n-n	
28	7	13	11	10	10.0	00.0	.	.	.	==n-10°, 8°10°	
29	7	14	02	00	04.0	25.6	.	.	.	==n-10°	
30	6	08	09	100	09.0	01.3	00.0	.	.	==n-n, R 10°, 10°, 10°, 10°	
31	6	10	10	05	08.3	00.0	31.2	.	.	● 10°10°, ==n-7°	
MES. RED.		04.2	05.6	04.8	14.9	299.1	71.3				

$\varphi = 45^{\circ}49' N \lambda = 15^{\circ}59' E$ Gr. $\Delta G = + 1h 04 min.$

BR. ST. 56

d	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodenog pare e mm			Relativna vlažnost U %				Pravac i jačina veta D, f (0-12)				
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21			
1	743.4	742.6	743.0	08.1	18.3	12.5	12.9	19.3	07.1	-	07.0	06.6	09.2	86	42	85	71	W	1	SW	2	W	1
2	744.7	744.1	744.7	10.0	19.0	15.3	14.9	19.6	09.2	-	08.8	08.4	08.8	95	51	68	71	E	1	SSE	2	NNE	2
3	747.0	745.7	745.7	12.0	20.6	16.0	16.2	21.3	10.7	-	09.1	09.5	10.5	87	52	77	72	NNW	1	S	2	N	1
4	745.9	744.4	743.9	12.6	22.2	18.4	17.9	22.9	11.6	-	09.3	10.4	10.8	85	52	68	68	-	0	SSW	2	W	2
5	742.7	742.0	741.9	14.7	23.5	18.8	19.0	23.5	13.8	-	10.6	11.5	13.0	85	53	80	73	W	1	SSE	2	ENE	1
6	741.1	740.7	741.3	16.3	22.2	17.2	18.2	22.3	14.9	-	12.4	12.6	13.0	89	63	88	80	-	0	ENE	1	ENE	1
7	740.6	741.1	743.2	15.3	17.4	15.3	15.8	20.9	14.9	-	11.8	14.3	14.2	91	96	94	94	NE	1	NNE	1	W	2
8	744.9	745.5	747.9	14.4	20.4	14.6	16.0	20.6	13.9	-	10.9	10.6	10.7	89	59	86	78	W	1	NNW	2	SW	2
9	750.1	749.4	749.8	13.8	20.6	17.0	17.1	21.7	13.6	-	10.8	11.1	11.0	92	61	76	76	SE	1	SW	2	NW	1
10	750.1	749.4	748.0	15.9	20.5	19.0	18.6	21.1	15.2	-	12.1	13.0	13.0	89	72	79	80	ENE	1	SW	1	NW	2
11	747.1	745.7	743.0	16.3	26.7	20.5	21.0	27.2	15.4	-	11.9	13.2	13.0	86	50	72	69	E	1	SW	2	W	3
12	744.4	746.8	748.7	14.8	13.2	12.2	13.1	20.5	11.2	-	11.1	10.4	08.7	88	91	82	87	NE	3	SW	2	NNW	2
13	752.3	752.6	754.8	13.8	17.8	13.4	14.6	18.1	10.6	-	07.8	06.4	06.9	66	42	60	56	SE	1	ENE	2	NE	2
14	754.1	751.5	750.4	10.8	17.6	13.9	14.1	17.9	10.0	-	07.2	07.2	08.0	74	48	67	63	E	1	SE	2	NNE	2
15	750.4	750.3	750.2	10.9	20.1	15.8	15.7	20.2	10.1	-	08.3	10.5	10.4	85	57	77	73	-	0	SSE	2	NNW	1
16	752.3	752.5	753.2	12.3	20.4	17.2	16.8	20.6	11.5	-	09.3	10.3	11.4	87	57	77	74	E	1	S	2	NNE	1
17	754.6	752.4	751.3	13.1	19.9	18.2	17.9	22.1	12.5	-	09.3	10.4	12.2	82	53	78	71	NE	1	SSW	2	NW	2
18	750.5	750.2	750.4	12.7	22.4	18.8	18.2	23.0	11.4	-	10.2	12.8	10.1	92	63	62	72	ENE	1	ENE	2	NE	3
19	749.8	748.8	747.6	16.1	19.8	13.2	14.6	19.0	13.2	-	07.8	08.8	09.8	56	65	86	69	NE	2	E	2	NNE	1
20	751.5	752.6	755.4	10.9	15.7	09.7	11.5	15.8	09.7	-	08.3	06.9	06.1	85	37	67	63	NE	3	ENE	3	NE	2
21	755.9	755.5	755.0	07.5	14.5	12.0	11.5	14.6	06.7	-	06.1	05.7	06.9	78	46	66	63	NNE	1	SW	2	NNW	1
22	754.2	752.2	750.9	08.8	18.4	15.4	14.5	19.2	07.8	-	07.2	08.8	09.2	85	55	70	70	W	1	SW	2	ENE	1
23	747.2	747.5	749.8	12.6	17.8	16.2	15.7	18.7	12.1	-	09.7	10.7	11.0	89	70	80	80	WNW	2	WSW	2	WSW	1
24	751.9	751.6	751.8	14.6	21.6	17.2	17.7	22.2	14.0	-	11.1	12.6	11.8	89	65	80	78	E	1	S	2	-	0
25	752.6	752.2	752.0	15.2	23.7	20.6	20.0	24.4	15.2	-	11.0	13.2	12.0	85	60	66	70	SW	1	SW	2	NW	3
26	752.3	750.6	748.9	15.8	24.0	18.3	19.1	24.1	15.5	-	11.5	07.2	13.3	85	53	84	74	NE	1	NE	2	SW	1
27	747.9	748.6	746.9	14.9	14.4	12.0	13.3	18.3	11.7	-	11.4	08.8	09.0	90	71	86	82	E	1	ENE	3	NNW	1
28	744.5	746.7	746.1	09.5	12.9	10.8	11.0	13.1	09.4	-	08.2	09.7	08.2	93	87	84	88	NW	1	NW	1	NNW	2
29	746.4	744.4	745.4	08.1	16.4	12.5	12.4	16.8	06.3	-	07.0	08.4	07.8	86	60	71	72	W	1	WSW	3	NNW	2
30	745.2	743.3	742.1	12.5	17.3	14.9	14.9	17.4	11.4	-	08.3	10.2	09.7	76	69	76	74	NNW	1	NNW	1	NE	1
MES.	MRED.			748.5	748.0	748.1	12.8	19.2	15.6	15.8	20.2	11.7	-	09.5	09.9	10.2	85	60	76	74	1.1	1.9	1.6

1	744.0	743.4	745.5	08.4	10.7	10.3	09.9	15.5	08.3	-	07.8	08.2	08.8	95	85	93	91	W	1	NE	1	S	1
2	747.5	749.1	749.2	09.9	11.1	11.3	10.9	11.7	09.4	-	08.6	09.2	09.5	94	92	94	93	SE	1	SW	1	SE	1
3	747.5	746.5	746.1	12.5	14.5	13.8	13.7	14.9	11.3	-	10.3	11.7	11.5	94	94	97	95	E	1	SW	1	ENE	2
4	743.5	744.4	745.5	12.2	13.6	13.0	13.0	16.4	12.0	-	09.9	10.5	10.2	93	90	91	91	W	1	SE	2	NNW	1
5	750.9	752.7	754.4	10.2	12.0	08.5	09.8	13.0	08.5	-	08.2	08.1	07.3	88	77	87	84	E	2	SSW	2	N	1
6	754.4	754.0	754.6	05.1	15.5	12.5	11.4	15.6	05.0	-	06.2	06.8	07.5	94	51	69	71	WSW	1	SW	2	NW	1
7	755.4	754.9	755.3	11.7	16.4	13.9	14.5	18.9	10.7	-	09.0	09.8	10.1	88	62	85	78	SSW	1	NNW	1	NE	1
8	755.4	755.1	755.1	10.9	18.2	14.6	14.5	18.7	10.7	-	09.2	09.7	10.0	94	62	81	79	ENE	1	ENE	2	NNE	2
9	754.8	754.4	754.6	11.6	15.0	15.4	15.4	19.1	11.5	-	09.4	10.6	10.8	92	64	75	77	NNE	1	ENE	2	NE	2
10	754.7	754.6	755.6	10.3	18.6	14.1	14.3	18.7	10.2	-	08.7	10.3	09.3	93	64	77	78	N	1	SSE	2	NNE	2
11	757.2	757.5	757.9	09.7	16.5	12.4	12.8	16.6	08.5	-	07.9	10.5	09.7	88	74	90	84	NNE	1	S	1	-	0
12	758.4	758.2	757.8	07.8	16.7	12.3	12.3	16.7	07.5	-	07.6	10.3	09.8	96	72	91	86	-	0	SSE	1	-	0
13	757.9	756.8	756.1	10.3	16.6	10.6	12.0	16.7	10.3	-	08.6	10.7	09.1	92	75	95	87	ENE	1	ESE	2	S	1
14	755.1	754.4	754.5	09.9	13.8	11.5	11.5	16.1	08.9	-	08.4	09.5	09.4	98	80	92	90	S	1	S	2	E	1

BR. ST. 56

 $H_s = 157 \text{ m } H_b = 162,5 \text{ m } h_t = 6,0 \text{ m } h_r = 2,0 \text{ m}$

Dan	Vrijeme 0-9 0	Oblačnost N (0-10)					Intenzitet broj sunca	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dnes				
1	7	000	10	09	06.3	06.6	00.9	.	$\Delta^2 n - dn, F_{\text{sun}} 4-15^{\circ}, \theta^{12} H^{30}, B^{30},$	
2	7	10≡	01○	08	06.3	09.2	00.1	.	$\Delta^2 n - 10, \equiv \gamma - 7^{\circ}, \equiv 7^{\circ} B^{30}, \theta^{12} H^{30},$	
3	8	02○	01○	00	01.0	10.7	00.4	.	$= n - 10$	
4	7	08○	03○	05	05.3	09.4	.	.	$= n - 10^2, 17 - n, \Delta^2 n - dn$	
5	6	06○	06○	06	06.0	08.0	.	.	$= n - n, \theta^{12} H^{30}, B^{30}$	
6	6	08○	10	10	09.3	00.6	.	.	$= n - n, \theta^{12} H^{30}, \theta^{12} H^{30}, B^{30}, R^{30}, B^{30}$	
7	4	09○	10○	10○	09.7	00.6	00.0	.	$= n - n, \theta^{12} H^{30}, B^{30}, R^{30}, K^{30}$	
8	8	06○	07○	10	07.7	05.3	17.0	.	$= n - n, \theta^{12} H^{30}, B^{30}, R^{30}, 17^{\circ}, 17^{\circ}, \theta^{12} H^{30}, \gamma - 17^{\circ}, 17^{\circ}$	
9	6	01○	01○	04	02.0	10.0	02.1	.	$\Delta^2 n - \gamma - n$	
10	6	10	10	10	10.0	00.0	.	.	$= n - n, \theta^{12} H^{30}, B^{30}$	
11	7	00○	00○	00	00.0	11.3	00.0	.	$= n - g^{30}$	
12	7	100%	10	01	07.0	01.9	00.5	.	$= \gamma - 12^{\circ}, \theta^{12} H^{30}, \theta^{12} H^{30}, \gamma - 7^{\circ}, B^{30}$	
13	7	09	03○	00	04.0	09.8	21.5	.	$= n - n$	
14	7	02○	01○	00	01.0	10.1	.	.	$= \gamma - 12^{\circ}$	
15	6	00○	02○	00	00.7	09.7	.	.	$= \gamma - n$	
16	6	09	06○	08	07.7	06.2	.	.	$= \gamma - n, \Delta^2 n - dn$	
17	6	06○	00○	01	02.3	10.6	.	.	$= n - n$	
18	6	10≡	03○	09	07.3	07.5	.	.	$= n - \delta^{30}, \equiv \theta^{12} H^{30}, B^{30}$	
19	6	10○	10	10○	10.0	00.0	00.0	.	$= n - n, \theta^{12} H^{30}, B^{30}, B^{30}, n$	
20	9	07○	02○	00	03.0	09.7	08.4	.	$\bullet n - \gamma, \theta^{12} H^{30}, n$	
21	8	00○	08○	08	05.3	08.2	.	.	$= \gamma - g^{30}$	
22	7	01○	09○	09	06.3	07.6	.	.	$= n - n$	
23	5	10○	10	10	10.0	01.1	00.0	.	$= n - n, \theta^{12} H^{30}, B^{30}$	
24	6	10	03○	09	04.3	07.3	01.3	.	$= \gamma - n$	
25	6	04○	02○	02	02.7	09.6	.	.	$= n - n$	
26	5	00○	01○	01	00.7	08.9	.	.	$= n - n$	
27	6	10	10○	10○	10.0	00.0	.	.	$= n - n, \theta^{12} H^{30}, B^{30}, R^{30}, n$	
28	6	10○	10	04	08.0	00.6	19.5	.	$= n - n, \theta^{12} H^{30}, \gamma - 6^{\circ}, B^{30}, R^{30}$	
29	6	10	04	01	05.0	06.2	03.6	.	$\Delta^2 \gamma - \delta, = \gamma - n, \theta^{12} H^{30}$	
30	6	08	08○	08	08.0	02.2	.	.	$\Delta^2 \gamma - \delta, = \gamma - n, \theta^{12} H^{30}$	
MES. VRED.					06.2	05.4	05.1	05.6	188.9	75.3

ZAGREB-GRČ

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1	8	10	10○	10	10.0	00.0	11.6	.	$= n - 8, \theta^{12} H^{30}, H^{30}, H^{30}, B^{30}, R^{30}, K^{30}$	
2	4	10○	10	13	10.0	00.0	22.5	.	$\bullet n - H^{30}, \equiv H^{30}, = n - n$	
3	5	10≡	10	10	10.0	00.0	07.4	.	$= n - \gamma - H^{30}, = H^{30}, n, \theta^{12} H^{30}, n$	
4	5	09	10	10	09.7	01.2	00.7	.	$= n - n, \theta^{12} H^{30}, B^{30}, B^{30}, R^{30}, H^{30}, H^{30}, R^{30}, R^{30}, H^{30}, B^{30}$	
5	6	10○	09	00	06.3	00.7	05.4	.	$= n - n, \theta^{12} H^{30}, \gamma - g^{30},$	
6	7	01○	01○	10	04.0	08.5	00.2	.	$= n - 10^{\circ}$	
7	6	01○	04○	05	03.3	08.2	.	.	$= n - n$	
8	6	00○	07○	09	05.3	06.0	.	.	$= n - n, \theta^{12} H^{30}, B^{30}$	
9	5	00○	01○	00	00.3	08.7	.	.	$= n - n, \Delta^2 \gamma - dn, \equiv 7^{\circ}, B^{30}$	
10	6	00○	00○	00	00.0	09.0	.	.	$= n - n, \Delta^2 \gamma - dn$	
11	5	00○	00○	00	00.0	08.0	.	.	$= n - n, \Delta^2 \gamma - dn$	
12	5	10≡	00○	00	03.3	05.8	.	.	$= \gamma - g^{30}, \equiv \theta^{12} H^{30}, = 9^{\circ}, n$	
13	5	04	01○	03	01.7	08.3	.	.	$= n - n$	
14	3	10≡	10≡	10≡	10.0	00.2	.	.	$\Delta^2 n - dn, \equiv n - 10^{\circ}, \equiv n - 10^{\circ}, n$	
15	4	10≡	06○	01	05.7	01.8	.	.	$\Delta^2 n - dn, \equiv n - 7^{\circ}, \equiv 7^{\circ}, n$	
16	5	10	06	03	06.3	03.6	.	.	$= n - n$	
17	4	08	06○	03	05.7	01.7	.	.	$= n - n, \Delta^2 \gamma - g^{30}$	
18	5	07≡	06○	07	06.7	03.8	.	.	$\Delta^2 n - g^{30}, \equiv n - 7^{\circ}, \equiv 7^{\circ}, n$	
19	4	10	10	10	10.0	00.0	.	.	$= n - n, g^{30}, g^{30}$	
20	5	10○	10	10	10.0	00.0	00.0	.	$= n - n, \theta^{12} H^{30}$	
21	6	06	05○	06	05.7	05.9	00.0	.	$= n - 10^{\circ}$	
22	8	11○	12○	18	03.7	27.9	.	.	$\Delta^2 n - 10^{\circ}, \equiv 10^{\circ}, = 10^{\circ}, n$	
23	7	10	03○	08	07.0	04.9	.	.	$= 10^{\circ}, n$	
24	7	09	02○	00	03.7	07.3	.	.	$= n - n$	
25	7	01	08○	10	06.3	07.6	.	.	$= n - 12^{\circ}, K^{30}, n$	
26	6	10○	10○	10○	10.0	00.0	00.0	.	$\bullet n - 14^{\circ}, 20^{\circ}, n, \equiv 7^{\circ}, n$	
27	9	22	13○	13	05.0	07.1	06.5	.	$\text{F} \equiv 8^{\circ}, K^{30}, \Delta^2 n - 10^{\circ}, K^{30}$	
28	7	10○	07○	10	03.3	08.6	.	.	$= n - H^{30}, K^{30}, n$	
29	5	12	05○	10	05.7	02.3	00.2	.	$\bullet n - n = n - n$	
30	6	08	03○	10	07.0	06.9	.	.	$= n - n$	
31	6	11	09	05	08.0	01.3	.	.	$= n - n$	
MES. VRED.					16.1	15.4	16.3	15.9	134.8	52.5

VIDLJIVOST OSMAIRANA U 13 ČASOVA

$\varphi = 45^{\circ}49' N \lambda = 15^{\circ}59' E$ Gr. $\Delta G = + 1h 04 min.$

BR. ST. 56

D	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodene pare e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0-12)			
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21	
1	759.4	759.9	761.2	05.0	12.6	09.0	08.9	12.7	04.9	-	05.7	06.6	06.4	87	60	74	74	-	0	SSE 2	NNE 2
2	761.2	759.9	759.8	05.3	11.2	06.7	07.5	11.2	05.1	-	06.0	07.3	07.1	90	73	96	86	NNE 1	SSE 2	E 1	
3	758.6	758.8	759.3	06.0	07.2	07.0	06.8	07.3	04.9	-	06.5	06.7	06.8	93	88	90	90	ENE 1	NE 1	E 1	
4	759.3	759.1	759.3	07.1	08.6	07.6	07.7	09.2	07.0	-	06.5	06.3	06.6	85	74	84	81	E 1	E 2	ENE 1	
5	759.6	760.7	761.2	05.7	07.9	05.5	06.2	08.3	05.2	-	05.8	05.2	05.0	85	66	73	75	E 2	ESE 2	E 2	
6	761.7	761.5	761.9	04.5	05.9	05.2	05.2	06.0	04.4	-	05.4	05.1	05.2	85	74	79	79	E 1	E 1	ENE 1	
7	761.5	761.5	762.6	05.4	06.0	05.3	05.5	06.1	05.2	-	04.7	04.5	04.5	69	64	67	67	SW 1	SSE 2	N 1	
8	762.1	761.7	761.9	04.2	04.9	04.1	04.3	05.3	04.1	-	04.5	04.8	05.0	74	74	80	76	NE 1	E 1	ENE 1	
9	761.4	760.9	761.2	03.6	03.7	03.3	03.5	04.1	03.3	-	04.9	04.9	04.9	83	83	84	83	S 1	SSW 2	S 2	
10	760.8	759.0	759.6	02.4	02.5	02.4	02.4	03.3	02.1	-	04.5	04.5	04.4	82	82	81	82	S 2	SSE 2	SSW 1	
11	759.4	758.9	759.5	01.6	01.8	01.4	01.6	02.4	01.4	-	04.2	04.3	04.2	82	83	83	83	SSE 1	SW 1	SW 1	
12	759.0	758.6	758.6	01.1	00.7	00.4	00.7	01.4	00.2	-	04.3	04.2	03.8	86	87	81	85	S 2	S 1	S 1	
13	759.4	759.8	761.4	00.1	00.5	00.4	00.4	00.9	-00.4	-	04.0	03.8	03.8	86	81	80	82	N 1	SSW 1	WNW 1	
14	763.5	764.2	765.1	-00.4	01.0	-00.3	00.0	01.2	-00.4	-	03.7	03.8	03.8	84	77	83	81	W 1	SW 2	NN 1	
15	763.7	762.8	761.5	00.4	01.5	-00.7	00.1	01.5	-00.7	-	04.1	04.4	03.9	86	86	90	87	SW 1	S 1	SW 1	
16	758.8	757.3	758.0	-01.9	-00.2	-01.4	-01.2	00.3	-01.9	-	03.8	04.2	04.0	96	92	97	95	S 1	SSE 1	E 1	
17	761.8	762.0	762.6	-00.1	03.0	01.7	01.6	03.0	-01.5	-	04.3	04.8	04.8	95	85	92	91	SW 1	WNW 1	SW 1	
18	761.8	760.9	761.4	-00.6	01.4	00.9	00.7	01.7	-00.9	-	04.3	04.6	04.4	98	91	93	93	WNW 1	SSW 1	WSW 1	
19	760.3	758.7	757.3	00.3	01.9	00.1	00.6	02.1	00.1	-	04.0	04.1	04.1	86	79	89	85	S 1	S 2	SSE 2	
20	755.5	755.5	757.4	-01.2	01.1	00.2	00.1	01.3	-01.7	-	03.9	04.2	04.3	92	85	92	90	WSW 1	SE 1	SW 1	
21	758.8	759.5	761.9	-01.2	00.7	-00.3	-00.3	00.7	-01.2	-	04.0	04.3	04.3	96	90	96	94	SSW 1	SSE 1	SSW 1	
22	764.0	764.7	765.3	-00.9	00.9	-00.5	-00.5	00.3	-01.0	-	04.2	04.3	04.2	98	94	96	96	SW 1	WSW 1	SSW 1	
23	763.7	763.5	763.5	-01.8	00.3	-00.8	-00.8	00.5	-02.0	-	03.9	04.6	04.1	96	97	96	96	W 2	S 1	SW 1	
24	761.7	758.6	757.4	-01.7	-00.5	-00.5	-00.8	-00.2	-02.2	-	04.0	04.2	04.2	98	97	97	97	W 1	WSW 1	SSW 1	
25	753.8	750.6	749.7	-02.6	00.0	-00.6	-01.0	00.1	-02.6	-	03.6	04.3	04.2	96	94	96	95	W 1	SSW 1	ENE 1	
26	747.8	745.5	744.8	-01.0	01.1	01.6	00.8	01.6	-02.0	-	04.1	04.6	05.0	96	96	95	96	ENE 1	E 2	E 1	
27	741.4	739.9	738.0	01.4	01.1	00.5	00.9	01.6	00.5	-	04.4	04.8	04.5	87	88	96	90	NE 3	ENE 2	SSW 1	
28	737.2	736.2	737.1	-00.4	01.5	01.5	01.0	01.8	-00.4	-	04.3	04.5	03.2	96	87	63	82	SSW 1	SSW 1	N 4	
29	738.6	738.6	739.8	01.4	02.4	01.7	01.8	02.7	00.5	-	03.6	03.8	03.8	70	70	74	71	N 3	ENE 2	W 1	
30	739.8	741.2	744.1	01.5	05.6	00.3	01.9	05.8	-00.4	-	03.3	03.5	04.0	64	51	85	67	NW 3	W 2	E 1	
MES.	RED. 757.2 756.7 757.1 01.4 03.2 02.0 02.2 03.5 01.0 - 04.5 04.7 04.6 87 82 86 85 1.3 1.4 1.2																				

1978 DECEMBER

ZAGREB-GRIC

1	746.7	747.6	749.1	-04.4	00.2	-02.0	-02.1	00.2	-04.4	-	03.0	04.0	03.6	92	85	91	89	S 1	SE 1	S 1	
2	750.1	751.3	752.5	-00.2	02.3	00.7	00.9	02.6	-02.0	-	04.0	03.6	03.9	89	68	82	80	-	0	E 1	SE 1
3	751.3	749.0	747.6	00.4	01.4	-01.0	-00.1	01.9	-01.0	-	04.1	04.1	03.8	88	81	89	86	WNW 1	SSW 1	ENE 1	
4	747.1	747.0	748.2	-02.3	-00.8	-01.0	-01.3	-00.7	-04.3	-	03.6	03.5	03.6	92	81	85	86	WNW 1	SSW 1	W 1	
5	751.2	754.3	757.0	-00.6	-01.1	-03.4	-02.1	00.6	-03.4	-	03.7	02.5	02.6	85	59	71	72	E 2	NE 3	ENE 2	
6	757.7	757.1	757.1	-06.6	-03.7	-05.5	-05.3	-03.4	-06.8	-	02.4	02.3	02.1	84	65	70	73	ENE 1	SE 2	NE 2	
7	755.7	753.4	753.7	-05.4	-04.7	-05.1	-05.1	-04.7	-06.0	-	02.2	02.0	02.0	71	62	63	65	ENE 1	E 1	NE 1	
8	753.3	752.2	750.1	-05.8	-04.5	-05.2	-05.2	-04.5	-06.4	-	02.0	02.0	02.5	66	63	80	70	W 2	SW 2	W 1	
9	746.8	747.6	750.8	-04.4	00.0	-00.5	-01.4	00.0	-05.2	-	02.9	04.5	04.3	87	98	98	94	SSW 1	-	0	
10	751.0	750.6	750.5	-01.4	00.0	00.1	-00.3	00.7	-01.4	-	04.1	04.4	04.6	99	95	97	97	-	0	ENE 1	WSW 1
11	749.3	747.1	745.8	-00.3	01.7	01.8	01.3	02.0	-00.3	-	04.5	05.0	05.2	100	96	99	98	SE 1	ENE 1	N 1	
12	740.5	739.4	737.5	07.2	09.9	09.6	09.1	10.0	01.7	-	07.1	07.6	07.8	93	84	87	88	W 3	W 2	W 2	
13	735.6	736.5	734.0	09.3	10.5	07.8	08.9	10.8	07.8	-	08.1	08.0	07.3	93	84	92	90	W 2	WSW 2	W 2	
14	728.7	731.9	732.5	07.3	06.6	05.3	06.1	09.5	05.1	-	07.2	06.0	05.8	93	81	87	87	ENE 1	N 1	W 1	
15	735.1	737.3	739.1	00.6	04.6	02.6	02.6	05.3	00.3	-	04.6	05.8	05.2	96	90	94	93	WNW 1	SE 1	SSE 1	
16	738.7	736.9	733.5	05.6	10.3	08.3	08.1	10.5	00.6	-	05.5	06.2	07.2	80	66	89	78	SE 1	W 2	S 2	
17	738.8	742.9	745.6	05.8	07.3	07.0	06.8	08.3	05.8	-	06.1	06.9	06.6	89	91	88	89	NW 2	E 1	NE 2	
18	749.9	753.5	756.0	00.9	-01.4	-02.6	-01.4	07.0	-02.6	-	04.6	02.9	02.3	93	70	69	74	E 2	ENE 2	NE 3	
19	754.0	750.4	746.8	-03.7	-04.1	-03.4	-03.7	-02.6	-												

BR. ST. 56

 $H_s = 157 \text{ m } H_b = 162,5 \text{ m } h_t = 6,0 \text{ m } h_r = 2,0 \text{ m}$

Dan	Vrijeme G. G.	Oblačnost N (0-10)					Intenzitet snežnog snijega mm	Padavina R mm	Snežni pokrivač h cm	Razvoj vremene w
		14	7	14	21	Sred Dnes				
1	6 00	04○	01	01.7	06.5	
2	4 00	04○	10	04.7	01.0	
3	3 10	10	10	10.0	00.0	
4	3 10	10	10	10.0	00.0	00.5	.	.	.	
5	5 10	10	10	10.0	00.0	00.0	.	.	.	
6	6 10	10	10	10.0	00.0	00.0	.	.	= n-n	
7	6 10	10	10	10.0	00.0	.	.	.	= n-n	
8	6 10	10	10	10.0	00.0	.	.	.	= n-n	
9	5 10*	10	10	10.0	00.0	00.0	.	.	= n-n, g-rj-g	
10	6 10	10	10	10.0	00.0	00.0	.	.	= n-n	
11	6 10	10	10	10.0	00.0	.	.	.	= n-n	
12	5 10	10	10	10.0	00.0	.	.	.	= n-n	
13	5 10	10	10	10.0	00.0	.	.	.	= n-n	
14	5 10	10	10	10.0	00.0	.	.	.	= n-n	
15	4 10	10	10	10.0	00.0	.	.	.	= n-n	
16	3 10	10	10	10.0	00.0	.	.	.	= n-10 ³⁰ , Δ 7 ³⁰ g ¹⁵ , = 10 ³⁰ n	
17	5 10	10	10	10.0	00.0	00.0	.	.	= n-H ³⁰ 80 ³⁰ n, = H ³⁰ 10 ³⁰	
18	3 10	10	10	10.0	00.0	.	.	.	= n-H ³⁰ , = H ³⁰ n	
19	4 10	10	10	10.0	00.0	.	.	.	= rj-n	
20	2 10	10	10	10.0	00.0	.	.	.	= n-n	
21	2 10	10	10	10.0	00.0	.	.	.	= 14-11 ³⁰ , 16 ³⁰ n, = 11 ³⁰ 16 ³⁰	
22	2 10	10	10	10.0	00.0	.	.	.	= 14-9 ³⁰ , 16 ³⁰ n, = 19 ³⁰ 16 ³⁰ , g ¹⁵ 8 ³⁰ 0 ³⁰	
23	2 10	10	10	10.0	00.0	00.0	.	.	= 14-10 ³⁰ , 13 ³⁰ n, = 10 ³⁰ 13 ³⁰	
24	2 10	10	10	10.0	00.0	.	.	.	= 14-n, = 11 ³⁰ 13 ³⁰ , g ¹⁵ 14 ³⁰ 16 ³⁰	
25	3 10	10	10	10.0	00.0	00.0	.	.	= n-n, V ¹⁵ n, H ³⁰	
26	4 10	10	10	10.0	00.0	00.0	.	.	= rj-10, g-rj, 0 ³⁰ 10 ³⁰ , 19 ³⁰	
27	4 10*	10*	10*	10*	00.0	04.6	01	.	* n-0, = n-n, * 8 n, = 8 ³⁰ 10 ³⁰	
28	4 10	10	10	10.0	00.0	11.3	05	.	= rj-8, 12 ³⁰ n; = 8 ³⁰ 12 ³⁰ , n, 17 ³⁰	
29	6 10*	10	10	10.0	00.0	10.6	07	.	= n-n, * n-13 ³⁰ , []	
30	6 01	05○	00	02.0	06.8	00.0	04	.	= n-n, []	
MES. RED.	09.0	09.4	09.4	09.3	14.3	17.0				

1	4 00	08	00	02.7	00.5	.	03	= n-10 ³⁰ , = 10 ³⁰ n, []
2	3 10	00○	00	03.3	04.2	.	02	= n-H ³⁰ 15 ³⁰ n, = H ³⁰ 15 ³⁰ , []
3	4 10	08	00	06.0	03.5	.	02	= n-n, []
4	6 10	10	10	10.0	00.0	.	02	= n-8 ³⁰ , H ³⁰ n, = 8 ³⁰ 14 ³⁰ , []
5	6 06	01○	00	02.3	03.9	.	01	= n-n, * 9 ³⁰ 10 ³⁰ , []
6	4 00	00○	10	03.3	04.0	00.0	01	= n-9 ³⁰ , = 9 ³⁰ n, []
7	5 10*	10*	10	10.0	00.0	00.0	01	= n-n, X ¹⁵ n, rj-14 ³⁰ , []
8	6 10*	10	10*	10.0	00.0	00.0	01	= n-n, X ¹⁵ n, rj-14 ³⁰ , B ¹⁵ n, []
9	3 10	10	10	10.0	00.0	04.9	04	= n-4 ³⁰ , B ¹⁵ n, B ¹⁵ 10 ³⁰ , B ¹⁵ 13 ³⁰ , = 11 ³⁰ 17 ³⁰ , = 17 ³⁰ n, []
10	2 10	10	10	10.0	00.0	75.2	03	= rj-n, []
11	1 10	04	10	08.0	00.8	.	02	= 12 rj-14 ³⁰ , 16 ³⁰ n, = 14 ³⁰ 16 ³⁰
12	7 08	09○	09	08.7	01.8	.	01	= n-9 ³⁰ , 16 ³⁰ n, = 16 ³⁰ 17 ³⁰ , []
13	6 10	02○	07	06.3	04.5	01.9	.	= n-n, 15 ³⁰ n, g ¹⁵ n, g ¹⁵ 9 ³⁰
14	7 10	09○	01	06.7	03.7	04.3	.	= n-rj, 15 ³⁰ n, = n-7 ³⁰ , 16 ³⁰ n, = 7 ³⁰ 9 ³⁰
15	3 00	05	00	01.7	03.4	00.0	.	= 12 rj-15 ³⁰ , 15 ³⁰ n, = 12 7 ³⁰ g ¹⁵ , 15 ³⁰ 13 ³⁰
16	3 06	10*	10*	08.7	01.2	.	.	= n-13 ³⁰ , 0 ³⁰ 13 ³⁰ n, = 13 ³⁰
17	5 10	10*	10	10.0	00.0	26.5	.	= n-n, 10 ³⁰ n, []
18	5 10	10	10*	10.0	00.0	01.9	.	= n-n, 0 ³⁰ 10 ³⁰ , 10 ³⁰ 14 ³⁰ , X ¹⁵ 14 ³⁰ , X ¹⁵ 13 ³⁰ , 10 ³⁰ n
19	6 10*	10	10*	10.0	00.0	26.6	09	= n-n, X ¹⁵ n, 12 ³⁰ , 13 ³⁰ n, = 8 ³⁰ 9 ³⁰ , 0 ³⁰ 13 ³⁰ , []
20	6 10	03○	00	04.3	04.1	19.0	23	= n-n, []
21	3 10	06	10	08.7	00.0	.	19	= n-7 ³⁰ , = 7 ³⁰ 16 ³⁰ , = 16 ³⁰ n, []
22	4 10	10	10	10.0	00.0	.	16	= n-n, g ¹⁵ 17 ³⁰ n, 0 ³⁰ n, []
23	4 10	10	10	10.0	00.0	00.7	13	= n-n, 10 ³⁰ n, n, d ¹⁵ n, n, d ¹⁵ n, []
24	4 10	10	10	10.0	00.0	02.3	12	= n-n, 10 ³⁰ n, d ¹⁵ n, []
25	4 10	10	10	10.0	00.0	00.0	07	= rj-6 ³⁰ , 0 ³⁰ 10 ³⁰ , = 15 ³⁰ n, []
26	4 10	10	10	10.0	00.8	11.7	04	= rj-10 ³⁰ , 15 ³⁰ n, g ¹⁵ n, = 10 ³⁰ 10 ³⁰ , = 14 ³⁰ 15 ³⁰ , 18 ³⁰ n, []
27	5 10	19	05	08.0	11.7	11.2	02	= rj-n, []
28	5 08	10*	03	07.0	11.0	.	.	= 10 ³⁰ n, 0 ³⁰ 14 ³⁰ , 15 ³⁰ n, 0 ³⁰ 14 ³⁰
29	7 05	10	00	05.0	07.0	01.0	.	= 10 ³⁰ n, 13 ³⁰ , 14 ³⁰ , 0 ³⁰ 14 ³⁰
30	8 11	11○	00	03.7	04.2	14.4	.	= 12 rj-12 ³⁰ , 13 ³⁰ , 0 ³⁰
31	9 07	09	09	08.3	10.2	.	.	
MES. RED.	08.4	07.5	06.6	07.5	34.8	60.6		

$\varphi = 43^{\circ}31' N \lambda = 16^{\circ}26' E$ Gr. $\Delta G = + 1h 06 min.$

BR. ST. 87

d	Vazdušni pritisak P mm			Temperatura vazduha T °C								Napon vodene pare e mm			Relativna vlažnost u %				Pravac i jačina veta D, f (0-12)				
				7	14	21	Sred Dnes	Max	Min	Min 5 cm	7	14	21	Sred Dnes	7	14	21	Sred Dnes	7	14	21		
		7	14	21	7	14	21	Sred Dnes	Max	Min	Min 5 cm	7	14	21	Sred Dnes	7	14	21	Sred Dnes	7	14	21	
1	750.3	753.8	758.2	04.3	07.2	06.3	06.0	07.5	03.3	-	03.1	02.3	02.7	50	31	38	40	NNW	3	NNE	3	NE	4
2	760.2	759.7	759.4	03.8	09.4	07.0	06.8	09.7	03.5	-	03.0	04.7	05.6	50	53	75	59	NE	3	SSW	2	ESE	1
3	757.3	755.5	752.9	05.9	07.3	07.9	07.3	09.7	05.2	-	04.2	05.3	05.7	61	69	71	67	ENE	3	ENE	2	ESE	2
4	749.4	748.5	749.6	09.2	03.7	05.6	06.0	09.7	03.0	-	07.0	05.3	03.5	81	89	51	74	SE	4	ENE	5	NE	4
5	759.6	752.3	755.7	04.2	04.4	-00.2	02.1	06.0	-00.4	-	02.3	02.2	01.7	37	35	37	36	NE	7	NE	8	NE	8
6	760.8	760.3	759.8	-00.4	03.6	02.7	02.2	04.0	-01.5	-	01.6	01.3	01.5	36	22	28	29	ENE	3	NE	3	NNW	3
7	758.0	758.1	759.2	03.3	08.1	04.4	05.6	08.6	02.1	-	03.3	03.1	02.8	49	39	45	44	NNW	3	NNE	2	NE	4
8	758.2	758.1	758.5	03.2	07.8	04.4	05.0	08.0	02.5	-	01.7	01.5	01.6	29	19	26	25	NE	6	E	2	NE	2
9	757.7	757.3	757.6	02.5	07.4	05.2	05.1	07.8	02.1	-	01.5	02.5	02.5	27	32	38	32	ENE	2	SSW	1	NE	2
10	756.7	755.7	755.3	04.2	08.0	06.6	06.4	08.2	03.4	-	02.7	04.2	03.9	44	52	53	50	ENE	2	SE	1	ENE	2
11	753.1	749.7	746.8	05.4	08.0	09.4	08.1	09.7	04.7	-	04.0	06.4	06.9	60	80	78	73	ENE	3	ESE	4	SSE	7
12	743.9	744.1	747.3	11.8	12.6	10.8	11.5	13.0	08.9	-	07.6	08.9	09.0	74	82	93	83	SSE	6	SSE	5	SE	7
13	750.2	753.4	754.6	10.8	12.2	11.5	11.5	12.6	10.1	-	09.0	08.3	08.0	93	78	79	83	SSE	7	SE	6	ESE	4
14	754.0	753.3	753.3	11.8	13.8	13.5	13.2	14.1	10.6	-	08.1	06.9	06.1	78	58	53	63	SSE	4	SE	5	SE	4
15	751.9	750.4	749.0	12.3	11.0	11.6	11.6	12.1	09.8	-	06.6	08.0	09.1	62	82	89	78	E	3	NE	3	SE	4
16	749.0	749.0	749.1	10.7	12.9	10.9	11.4	13.3	09.8	-	08.2	09.4	08.5	85	84	87	85	NNW	1	WSW	1	ENE	2
17	743.9	738.8	740.0	10.0	10.6	08.9	09.6	11.5	08.6	-	08.1	08.0	08.1	88	84	95	89	ESE	4	ESE	5	WSW	4
18	745.4	745.8	746.0	07.8	10.9	09.8	09.6	11.0	07.3	-	06.2	06.1	06.5	78	62	72	71	E	2	SE	3	E	2
19	744.3	743.4	742.4	09.4	10.4	09.5	09.7	11.1	07.6	-	06.9	06.8	06.2	78	72	69	73	SSE	5	ESE	4	NE	3
20	741.7	741.8	741.7	08.2	09.8	09.2	09.1	10.2	07.6	-	06.5	06.9	06.9	80	76	79	78	ENE	2	ESE	5	ESE	5
21	740.3	739.8	741.2	08.2	08.3	07.8	08.0	10.0	07.2	-	06.7	06.6	04.2	82	80	53	72	NE	5	E	4	NNE	4
22	743.1	744.8	746.0	06.6	07.2	07.6	07.3	08.6	05.1	-	05.2	06.3	05.9	71	83	76	77	NNE	2	NNE	2	NE	2
23	746.7	748.0	748.7	07.1	10.1	08.7	08.7	11.2	06.9	-	05.5	06.2	06.5	73	67	77	72	NNE	2	ESE	2	NE	1
24	749.0	747.6	744.6	06.3	07.7	09.3	08.2	11.2	05.4	-	04.8	07.2	07.3	67	91	83	80	NE	2	ENE	1	ESE	4
25	739.4	740.9	746.1	09.9	08.4	08.2	08.7	10.2	07.5	-	08.8	07.3	04.4	96	89	54	80	SSE	5	W	3	N	3
MES.																							
VRED.	749.1	748.7	749.4	07.0	08.8	07.7	07.8	10.0	05.5	-	05.3	05.8	05.4	66	66	66	66	3.5	3.5	3.5	3.5		

1978 FEBRUAR

SPLIT-MARJAN

1	747.1	746.5	747.1	04.7	09.1	06.1	06.5	09.5	04.0	-	03.0	03.8	03.1	47	44	43	45	NE	4	SSW	2	NNW	1
2	743.3	739.3	741.2	03.5	07.7	06.7	06.2	07.8	02.6	-	03.3	04.3	03.4	57	55	46	53	E	3	ESE	4	NE	4
3	741.8	743.3	746.7	05.3	10.0	06.5	07.1	10.3	05.0	-	02.3	03.0	03.2	34	33	44	37	NE	5	SE	3	NE	4
4	748.3	748.8	750.1	06.7	09.0	06.3	07.1	09.4	06.0	-	03.0	03.1	03.2	41	36	45	41	NE	4	ESE	4	NE	5
5	750.4	748.6	747.6	05.2	09.6	05.7	06.3	09.7	04.7	-	03.2	03.3	03.1	48	37	47	44	ENE	4	NNE	3	NE	5
6	744.3	742.3	742.3	03.6	09.5	05.4	06.0	09.7	03.4	-	03.0	04.2	03.2	50	47	48	48	NE	3	SW	2	NE	4
7	741.7	741.5	741.4	05.4	07.6	04.6	05.6	09.9	04.5	-	03.1	03.2	02.8	46	41	44	44	NE	3	NE	3	NE	5
8	746.4	740.5	741.5	02.5	06.1	03.6	04.0	06.2	02.0	-	02.4	02.6	02.4	43	36	40	40	NE	5	NE	4	NE	3
9	743.2	744.9	747.4	03.1	05.5	03.9	04.1	06.3	02.4	-	04.5	06.8	07.4	73	77	75	75	ESE	2	SSE	6	SSE	7
10	747.4	744.2	741.0	02.6	08.4	10.9	08.2	11.1	01.8	-	03.8	06.0	06.4	69	73	65	69	E	3	SE	7	SE	4
11	736.1	737.0	738.6	12.4	12.3	11.9	12.1	14.0	09.0	-	09.4	09.2	07.5	87	86	72	82	SSE	6	S	5	S	4
12	740.3	740.0	741.7	10.1	09.8	08.8	09.4	12.3	07.4	-	07.8	06.9	07.4	85	76	88	83	SSW	5	WSW	2	NE	2
13	740.3	740.3	739.2	08.6	11.0	09.7	09.5	11.4	07.8	-	07.7	08.9	05.0	92	82	58	77	ENE	2	W	1	NE	1
14	735.1	737.7	739.5	08.9	08.5	06.6	07.7	09.6	06.5	-	04.3	03.7	03.9	50	44	53	49	NE	5	NE	5	E	2
15	741.0	743.3	746.5	02.3	04.5	02.0	02.7	07.7	00.4	-	02.8	02.2	02.0	51	34	37	41	NE	5	NE	6	NE	4
16	746.8	745.5	743.4	00.6	05.6	06.9	05.0	07.0	00.2	-	02.0	03.2	05.1	42	47	69	53	ENE	2	SE	3	SE	5
17	741.8	742.5	742.9	05.7	10.4	09.4	08.7	10.7	05.3	-	06.2	07.3	07.5	90	77	84	84	ESE	3	ESE	3	ESE	2
18	742.0	744.8	748.7	10.4	09.8	06.9	08.5	11.0	06.6	-	08.8	03.8	02.8	93	41	37	57	ESE	2	NE	6	NE	4
19	749.2	746.4	743.7	06.4	09.9	11.4	09.8	11.7															

SPLIT-MARJAN

1978 JANUAR

BR. ST. 87

$$H_s = 122 \text{ m } H_b = 128.0 \text{ m } h_t = 6.5 \text{ m } h_r = 1.0 \text{ m}$$

SPLIT-MAR 1981

1972 FEBRUAR

1	8	01	000	00	00.3	09.1
2	8	08	10	01	06.3	00.0	.	.	$\oplus^{+1} 15^{\circ}-16^{\circ}$.
3	8	10	090	00	06.3	08.0	00.7	.	.	.
4	8	09	060	07	07.3	05.6	.	.	$\boxplus_{\text{mag}} 9-14.6$.
5	8	00	010	00	00.3	08.9
6	8	00	030	01	01.3	08.4
7	8	10	09	09	09.3	01.4
8	8	04	10	03	05.7	01.3
9	7	10	09	03	07.3	09.9	.	.	$\oplus^{+1} 15^{\circ}-16^{\circ}$.
10	7	06	10	10	08.7	03.3	00.0	.	$\boxplus_{\text{mag}} 12-24.6$.
11	7	10	10	10	10.0	00.4	03.8	.	$\oplus^{+1} 0-4^{\circ} 6, 12^{\circ}-17^{\circ} 6; \boxplus_{\text{mag}} 0-24.6$.
12	8	100	100	100	10.0	03.5	01.1	.	$\oplus^{+1} 14^{\circ}-16^{\circ}, 12^{\circ}-14^{\circ}; \boxplus_{\text{mag}} 7^{\circ}-9$.
13	7	10	10	10	10.0	00.0	14.4	.	$\oplus^{+1} 0-8^{\circ} 6$.
14	8	10	090	08	09.0	04.2	00.2	.	$\boxplus_{\text{mag}} 0-10^{\circ} 6, 12^{\circ}-24.6; \boxplus_{\text{mag}} 23^{\circ}-24.6$.
15	7	10	01	00	03.7	05.3	04.1	.	$\oplus^{+1} 0-3^{\circ}, \boxplus_{\text{mag}} 0-10^{\circ} 6, \boxplus_{\text{mag}} 0-10^{\circ} 6$.
16	8	07	10	10	09.0	00.0	.	.	$\oplus^{+1} 12^{\circ}-24$.
17	8	100	09	10	09.7	00.1	01.8	.	$\oplus^{+1} 0-7^{\circ} 6, 14^{\circ}-14^{\circ}$.
18	8	100	020	00	04.0	03.7	02.8	.	$\oplus^{+1} 12^{\circ}-8^{\circ} 6 = 6^{\circ}-8^{\circ} = 8^{\circ}-9^{\circ}, \boxplus_{\text{mag}} 11^{\circ}-15^{\circ}$.
19	8	10	10	100	10.0	00.0	00.2	.	$\oplus^{+1} 0-10^{\circ} 6, 15^{\circ}-23^{\circ} 6; \boxplus_{\text{mag}} 13^{\circ}-23^{\circ} 6$.
20	8	10	09	02	07.0	00.2	11.7	.	$\oplus^{+1} 0-11^{\circ} 6, \boxplus_{\text{mag}} 10-24$.
21	8	00	030	08	03.7	10.1	01.3	.	$\boxplus_{\text{mag}} 0-7.6$.
22	8	04	010	00	01.7	18.0
23	8	08	05	06	06.3	05.3
24	7	29	10	09	00.3	19.1	.	.	$\boxplus_{\text{mag}} 10^{\circ}-24.6$.
25	7	10	10	100	10.0	00.0	.	.	$\boxplus_{\text{mag}} 0-24, 0^{\circ}-15^{\circ}-17^{\circ} 6, 20^{\circ}-24.6$.
26	6	09	10	08	09.0	00.0	00.7	.	$\oplus^{+1} 0-0^{\circ} 6, 12^{\circ}-16^{\circ} 6, 22^{\circ}-34, \boxplus_{\text{mag}} 0-1, 9^{\circ}-16^{\circ}, 23-24$.
27	8	100	070	03	16.7	11.3	38.5	.	$\oplus^{+1} 0-8^{\circ} 6, 11^{\circ}-16^{\circ}, \boxplus_{\text{mag}} 0-0^{\circ} 6, \boxplus_{\text{mag}} 9^{\circ}-10^{\circ} 6$.
28	7	100	090	09	09.3	21.3	01.6	.	$\oplus^{+1} 6^{\circ}-10^{\circ}, 13^{\circ}-14^{\circ}, \boxplus_{\text{mag}} 7-16$.

$\varphi = 43^{\circ}31' N$ $\lambda = 16^{\circ}26' E$ Gr. $\Delta G = + 1h 06 min.$

BR. ST. 87

d	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodené pare e mm			Relativna vlažnost U %				Pravac i jačina veta D, f (0-12)				
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21			
1	746.8	748.2	749.9	11.0	14.4	11.4	12.1	14.9	10.3	-	08.9	09.3	08.3	91	76	82	83	NNW	1	SW	1	SE	1
2	749.8	749.3	748.7	09.3	15.6	11.9	12.2	16.0	08.7	-	07.0	08.2	08.3	79	62	79	73	NE	3	SW	2	NNE	1
3	747.8	746.1	745.5	09.8	16.0	12.2	12.6	16.4	09.0	-	06.3	08.4	09.4	70	62	88	73	NE	3	SW	2	E	1
4	745.7	746.5	746.5	09.2	13.6	12.1	11.8	15.4	08.7	-	08.2	08.5	08.7	94	73	82	83	NE	1	NNE	1	NNE	1
5	745.6	745.8	745.2	13.5	13.6	14.0	13.8	15.6	10.6	-	07.7	08.5	07.5	66	73	63	67	SSE	5	ESE	3	SSE	6
6	745.3	744.6	744.8	10.2	11.6	10.9	10.9	14.4	09.1	-	08.3	09.4	08.9	89	92	91	91	ESE	2	ESE	3	ENE	3
7	747.6	748.8	749.5	10.6	14.3	10.8	11.6	14.7	09.1	-	08.5	08.1	08.0	88	66	83	79	NNE	1	S	2	ENE	2
8	749.8	750.0	750.0	08.0	13.5	10.3	10.5	14.9	07.6	-	04.6	04.2	04.3	57	36	46	46	ENE	3	SW	1	NNE	1
9	750.1	749.6	750.6	06.8	12.4	12.1	10.9	15.0	06.4	-	03.7	05.1	04.1	50	47	38	45	ENE	2	SW	1	NNE	4
10	754.1	754.5	754.2	08.6	11.1	08.8	09.3	12.2	07.6	-	03.2	03.4	03.7	39	34	44	39	NE	5	NE	4	NNE	6
11	755.0	753.4	749.0	07.8	14.0	10.9	10.9	14.4	07.3	-	03.1	05.5	05.0	39	46	51	45	NE	1	NW	2	NW	2
12	748.2	748.7	751.5	09.8	12.0	07.8	09.4	12.2	07.8	-	03.7	02.6	02.8	40	24	36	33	NE	2	N	5	NE	2
13	752.3	753.7	754.5	05.8	12.2	08.4	08.7	12.5	04.8	-	01.9	04.7	04.3	27	44	52	41	NE	2	SW	1	ESE	1
14	755.1	754.4	753.6	08.5	10.5	09.4	09.5	11.1	07.2	-	04.8	06.8	08.8	58	71	100	76	ESE	2	SE	5	SE	5
15	751.1	749.5	750.3	10.4	12.1	08.7	10.0	13.0	07.8	-	08.6	09.4	06.7	91	89	79	86	SE	5	NNW	1	SSW	1
16	751.8	750.6	748.1	07.0	13.9	11.6	11.0	15.0	06.7	-	06.5	07.4	08.2	87	62	80	76	NE	1	SE	3	SSE	6
17	745.1	744.6	745.7	12.0	07.0	08.4	09.0	12.5	06.5	-	06.7	06.4	06.2	64	85	75	75	SSE	6	NNE	2	ESE	1
18	746.4	748.3	750.8	08.8	10.5	08.4	09.0	11.2	07.7	-	05.9	06.4	06.1	70	67	74	70	N	3	SE	1	E	1
19	751.5	749.9	750.2	07.2	11.4	07.9	08.6	13.1	06.5	-	06.0	06.8	04.2	79	67	52	66	WSW	2	NNW	2	NNE	2
20	751.6	749.5	746.2	05.0	09.2	09.1	08.1	10.6	04.0	-	03.6	03.6	04.5	55	41	52	49	E	1	SW	2	ESE	4
21	737.7	736.1	735.3	09.6	14.4	10.3	11.2	14.5	08.2	-	08.5	09.7	04.2	95	79	44	73	ESE	2	SSE	1	NE	6
22	738.6	745.1	750.3	07.9	10.1	08.2	08.6	10.6	07.0	-	03.1	03.1	02.7	39	33	33	35	NNE	6	NNE	5	N	4
23	752.3	750.9	748.3	05.3	11.8	09.4	09.0	12.5	04.4	-	02.7	04.2	03.8	40	41	43	41	E	1	SW	3	SE	4
24	741.7	741.3	742.2	07.4	09.7	07.6	08.1	11.0	05.5	-	07.0	06.1	04.5	91	67	57	72	WNW	1	W	3	NE	2
25	745.1	748.7	751.7	07.4	09.8	08.4	08.5	10.5	05.0	-	03.0	03.2	04.1	39	35	49	41	NNE	2	NNW	3	SSW	3
26	751.4	749.4	746.7	06.9	13.2	10.4	10.2	13.6	06.3	-	03.6	05.1	04.3	48	45	46	46	ENE	2	W	3	ESE	3
27	746.8	749.3	753.0	07.7	11.4	09.3	09.4	11.8	06.8	-	03.9	03.3	03.0	49	33	34	39	NE	5	NE	5	NE	3
28	755.1	755.6	755.6	10.0	14.4	12.0	12.1	15.4	08.0	-	02.6	07.0	05.3	29	57	51	46	ESE	2	WSW	3	SSE	2
29	755.5	754.8	753.8	09.8	17.2	12.4	13.0	17.2	09.0	-	05.3	06.7	08.0	58	46	74	59	NNE	1	SSW	1	NNW	1
30	752.0	750.7	749.2	11.1	16.9	12.9	13.5	17.1	09.2	-	05.8	07.7	05.3	58	53	47	53	ENE	2	SSE	3	ESE	4
31	747.9	747.7	747.9	11.8	14.5	12.0	12.6	15.2	10.5	-	06.5	07.5	07.7	62	61	73	65	ESE	4	SE	5	SE	4
MES.	748.9			08.8	12.6	10.2	10.5	13.7	07.5	-	05.4	06.3	05.8	63	57	61	60	2.9	2.6	2.8			
REFD.	748.9																						

1978 APRIL

SPLIT-MARJAN

1	746.1	744.4	742.9	11.8	14.3	11.6	12.3	15.2	10.6	-	06.3	08.3	07.1	60	68	69	66	ESE	3	SW	2	NNW	2
2	742.0	741.8	742.8	10.2	15.1	11.4	12.0	16.4	09.7	-	08.0	07.5	08.3	86	58	82	75	SE	2	SW	1	NNW	1
3	741.7	740.2	738.6	11.2	15.2	12.5	12.9	15.8	09.7	-	06.7	07.7	07.7	67	60	71	66	ENE	2	SSE	2	WSW	1
4	738.7	739.8	742.7	12.3	16.3	14.2	14.3	16.5	10.4	-	08.0	06.2	05.8	74	44	48	55	NNW	1	NE	3	NE	3
5	744.0	745.0	746.4	13.0	16.5	12.3	13.5	16.6	10.6	-	06.6	09.0	09.3	59	64	87	70	ENE	1	SSW	2	SE	1
6	747.4	747.5	747.9	11.0	15.4	12.0	12.6	17.4	10.1	-	06.7	06.7	04.7	68	51	45	55	ENE	1	NNE	1	ENE	3
7	745.5	742.2	737.2	11.6	12.7	12.5	12.3	13.5	10.8	-	04.7	05.4	08.9	46	49	82	59	ESE	4	E	5	S	5
8	739.2	739.1	740.9	11.7	10.4	10.8	10.9	12.9	10.1	-	08.5	07.6	07.9	82	80	82	81	ESE	3	ENF	3	NNW	1
9	742.5	744.1	745.9	10.2	11.2	10.6	10.7	12.3	09.6	-	08.2	09.3	08.9	88	93	93	91	ESE	1	E	1	SSE	1
10	746.5	748.4	749.2	10.6	12.5	11.4	11.5	12.8	09.4	-	09.0	09.4	08.7	94	87	86	89	SE	2	SW	2	ESE	2
11	749.7	750.2	750.2	12.3	14.3	13.1	13.2	15.4	11.0	-	08.7	07.5	09.3	81	61	82	75	SSE	4	SE	5	SE	6
12	749.3	748.1	745.9	13.5	16.2	15.9	15.4	16.6	12.6	-	08.1	07.0	06.3	70	51	46	56	SSE	7	SE	6	SE	6
13	741.3	737.9	736.9	15.5	15.7	14.7	15.2	17.5	14.6	-	08.8	09.5	10.6	66	71	85	74	SE	1	SE	5	SE	5
14	739.8	739.9																					

BR. ST. 87

 $H_s = 122 \text{ m } H_b = 128.0 \text{ m } h_t = 6.5 \text{ m } h_r = 1.0 \text{ m}$

Dan	Vrijeme	Oblačnost N (0-10)					Intenzitet sunca	Padavina R mm	Snežni pokrivač h cm	Razvoj vremena W
		14	7	14	21	Sred Dnes				
1	8 10	09	00	06.3	01.9	02.8	.	= 6 ²⁰ -7 ²⁰		
2	8 020	06	00	02.7	09.2	.	.	Δ ¹ 0 ² -1 ⁰ , 80 ²⁰ -84 ²⁰ = 123 ²⁰ -84 ²⁰		
3	8 040	010	00	01.7	09.6	.	.	Δ ¹ 0 ² -9 ²⁰ , 80 ²⁰ -84 ²⁰ = 9-9 ²⁰ 0 ² -83 ²⁰ -24 ²⁰		
4	6 10	070	00	05.7	05.2	.	.	8 ²⁰ -0-1 ²⁰ , 40 ²⁰ -23 ²⁰ ; F _{NE} 2 ²⁰ -H ²⁰ , F _{SE} 23 ²⁰ -24 ²⁰ , F _{SW} 23 ²⁰ -24 ²⁰		
5	7 10	100	100	10.0	00.0	00.5	.			
6	7 100	100	100	10.0	00.0	27.4	.	8 ²⁰ -0-23 ²⁰ , F _{SE} 0-0 ²⁰ , F _{SE} 0-1 ²⁰		
7	8 09	080	01	06.0	00.9	18.5	.	8 ²⁰ -0-5 ²⁰		
8	8 030	08	00	03.7	06.5	00.2	.			
9	7 050	10	09	08.0	01.0	.	.			
10	8 010	020	00	01.0	10.5	.	.	F _{NE} 6 ²⁰ -10 ²⁰		
11	8 010	010	08	03.3	08.4	.	.	F _{NE} 0-4 ²⁰		
12	8 010	030	00	01.3	10.3	.	.	F _{NE} 5 ²⁰ -10 ²⁰		
13	8 000	09	00	03.0	08.9	.	.	8 ²⁰ -3 ²⁰ -13 ²⁰ , 10 ²⁰ -24 ²⁰		
14	7 100	10	100	10.0	00.0	.	.	8 ²⁰ -7 ²⁰ , 12 ²⁰ -0 ²⁰		
15	7 10	090	01	06.7	01.9	11.2	.	8 ²⁰ -1-5 ²⁰ , 10 ²⁰ -14 ²⁰ , 17-10 ²⁰		
16	8 07	080	01	05.3	06.9	01.3	.	F _{NE} 10 ²⁰ -14 ²⁰		
17	6 10	100	09	09.7	00.0	.	.	8 ²⁰ -1-10 ²⁰ , 8 ²⁰ -15 ²⁰		
18	8 05	06	06	05.7	04.5	05.9	.	8 ²⁰ -6 ²⁰ -13 ²⁰		
19	9 080	070	04	06.3	08.0	02.6	.	8 ²⁰ -7 ²⁰ , 12 ²⁰ -0 ²⁰		
20	8 000	10	10	06.7	13.2	00.3	.	8 ²⁰ -22-24 ²⁰ , 8 ²⁰ -12 ²⁰ -24 ²⁰		
21	8 100	09	10 ^R	09.7	03.6	08.7	.	8 ²⁰ -1-27 ²⁰ , 6 ²⁰ -5 ²⁰ , 15 ²⁰ -10 ²⁰ , F _{SE} 9 ²⁰ -12 ²⁰ , F _{SE} 19 ²⁰ -24 ²⁰		
22	8 09	050	00	04.7	05.9	00.8	.	F _{NE} 0-0-15 ²⁰		
23	8 020	050	10	05.7	08.9	.	.	8 ²⁰ -5 ²⁰ -24 ²⁰		
24	8 090	10	10	09.7	03.9	18.5	.	8 ²⁰ -1-12 ²⁰ , 19 ²⁰ -19 ²⁰ , F _{SE} 8 ²⁰ -0 ²⁰		
25	8 05	09	01	05.0	05.3	05.0	.	F _{NE} 6 ²⁰ -14 ²⁰		
26	8 010	070	10	06.0	07.1	.	.	8 ²⁰ -19 ²⁰ , F _{NE} -10 ²⁰ -17 ²⁰		
27	9 09	06	00	05.0	07.1	00.0	.	8 ²⁰ -19 ²⁰ , F _{NE} -10 ²⁰ -17 ²⁰		
28	9 010	010	00	00.7	11.3	.	.			
29	8 010	040	01	02.0	10.4	.	.	Δ ¹ 17-9		
30	8 010	010	00	00.7	11.0	.	.	Δ ¹ 17-9		
31	7 030	060	05	04.7	09.9	.	.	F _{NE} 10 ²⁰ -16 ²⁰		
MES. RED.		05.4	06.7	04.1	05.4	181.3	103.7			

1	7 10	10	10	10.0	00.8	.	.			
2	8 10	050	03	06.0	06.3	00.0	.	8 ²⁰ -6 ²⁰ -8 ²⁰		
3	8 060	09	10	08.3	03.4	00.1	.	Δ ¹ 10-9, 8 ²⁰ -12 ²⁰ -24 ²⁰		
4	8 19	09	09	09.0	00.1	00.7	.	8 ²⁰ -0-2 ²⁰ , 5 ²⁰ -6 ²⁰		
5	8 10	080	00	06.0	04.3	.	.	8 ²⁰ -7 ²⁰ , 0 ²⁰ -4 ²⁰ , = 19 ²⁰ -24, Δ ¹ 19 ²⁰ -24 ²⁰		
6	8 19	09	10	09.3	03.2	01.2	.	Δ ¹ 0-3 ²⁰ = 0-1 ²⁰ , 8 ²⁰ -16 ²⁰ -19 ²⁰		
7	7 10	100	100 ^R	10.0	00.0	00.0	.	8 ²⁰ -4 ²⁰ -16 ²⁰ , T ¹ 19 ²⁰ -24 ²⁰ , F _{NE} -10 ²⁰ -17 ²⁰		
8	7 100	100	100	10.0	00.0	19.4	.	8 ²⁰ -0-2 ²⁰ , 6 ²⁰ -22 ²⁰ , T ¹ 0-2 ²⁰ , F _{SE} 0-1		
9	6 100	100	100	10.0	00.0	13.4	.	8 ²⁰ -10 ²⁰ -24 ²⁰ , = 19 ²⁰ -24 ²⁰		
10	8 10	10	10	10.0	00.0	04.1	.	= 0-3 ²⁰ , 8 ²⁰ -14 ²⁰		
11	6 09	08	10	09.0	04.8	00.5	.	= 17 ²⁰ -16 ²⁰ , 8 ²⁰ -16 ²⁰ -22 ²⁰ , F _{SE} 13-24		
12	7 09	07	06	07.3	08.5	00.3	.	F _{NE} -10-16, 8 ²⁰		
13	7 10	10	10	10.0	01.2	.	.	8 ²⁰ -0-20 ²⁰ , 0-20 ²⁰ = 23-23 ²⁰		
14	8 100	09	04	07.7	03.1	03.6	.	8 ²⁰ -2-9 ²⁰ , 8 ²⁰ -9 ²⁰ -9 ²⁰ , F _{SE} 10-15		
15	8 100 ^R	080 ^R	10	09.3	02.4	05.0	.	8 ²⁰ -1-30 ²⁰ , 24 ²⁰ -24 ²⁰ , F _{SE} 3 ²⁰ -17 ²⁰ , T ¹ 6 ²⁰ -7 ²⁰ , 13 ²⁰ -14 ²⁰		
16	8 09	10	09	09.3	01.5	12.3	.	8 ²⁰ -0-4 ²⁰ , 10 ²⁰ -H ²⁰ , T ¹ 0-2 ²⁰		
17	8 10	07	08	05.0	12.3	00.?	.	F _{NE} 10 ²⁰ -11 ²⁰		
18	8 07	03	01	03.7	11.8	.	.	F _{NE} 5-13 ²⁰		
19	8 01	08	09	06.0	08.2	.	.			
20	8 09	08	03	06.7	01.9	.	.			
21	7 060	09	09	18.0	19.8	.	.	Δ ¹ 17-9		
22	8 15	070	01	24.3	28.6	.	.			
23	8 010	050	03	23.0	11.0	.	.			
24	7 040	080	10	27.3	29.6	.	.	8 ²⁰ -13 ²⁰ -24 ²⁰ , F _{SE} 20 ²⁰ -23 ²⁰		
25	6 10	100	100	10.0	10.0	02.4	.	8 ²⁰ -0-5 ²⁰ , 8 ²⁰ -23 ²⁰ , T ¹ 22 ²⁰ -23 ²⁰		
26	7 09	070	00	25.3	05.7	07.1	.	8 ²⁰ -0-1 ²⁰ , 10 ²⁰ -H ²⁰		
27	8 07	040	03	24.7	19.0	22.4	.	F _{NE} 0-2 ²⁰ , 8 ²⁰ -10 ²⁰		
28	9 050	040	00	23.1	10.2	00.?	.	8 ²⁰ -1-7 ²⁰		
29	8 040	090	00	24.3	29.1	01.?	.	= 17-6 ²⁰ , Δ ¹ 17-9 ²⁰		
30	8 140	09	01	24.2	12.0	.	.	8 ²⁰ -10 ²⁰ , F _{SE} H-24 ²⁰		
MES. RED.		17.4	28.0	06.3	17.2	151.5	74.1			

$\varphi = 43^{\circ}31' N \lambda = 16^{\circ}26' E$ Gr. $\Delta G = + 1h 06 min.$

BR. ST. 87

d	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodené pare e mm			Relativna vlažnost u %				Pravac i jačina veta D, f (0-12)				
	7	14	21	7	14	21	Sred Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dnes	7	14	21			
1	742.1	739.3	740.3	18.1	18.9	16.5	17.5	19.0	16.5	-	07.1	08.8	11.1	46	54	79	60	ESE	6	SE	8	SE	5
2	736.0	739.1	744.0	12.2	14.0	12.6	12.9	17.0	11.3	-	09.9	10.4	09.9	85	86	90	87	NW	2	W	3	SSW	2
3	748.4	751.0	752.8	13.4	19.0	14.9	15.6	19.3	11.4	-	29.7	09.9	09.9	84	60	78	74	SE	1	SSW	1	NNW	2
4	753.7	754.7	754.4	14.0	18.7	15.9	16.1	19.8	12.1	-	07.8	10.4	08.2	65	64	61	63	NE	3	SSW	3	NNW	1
5	754.7	753.1	751.3	15.4	21.1	17.4	17.8	22.5	12.5	-	08.6	09.0	08.1	65	48	54	56	ENE	1	SW	2	SSE	1
6	749.4	749.4	747.7	18.8	13.8	13.2	14.8	19.5	12.2	-	07.2	09.6	10.4	44	81	91	72	SE	6	ESE	5	ESE	5
7	744.2	744.0	744.0	13.4	16.3	14.3	14.6	17.1	12.4	-	10.9	10.7	10.3	95	77	85	86	SE	5	ESE	3	SSE	1
8	743.3	743.7	744.7	12.0	16.7	13.3	13.8	16.9	10.9	-	09.3	10.3	10.1	89	72	88	83	NE	2	SW	2	S	3
9	745.6	746.6	748.3	13.0	18.9	14.7	15.3	19.3	11.0	-	09.3	09.8	10.8	83	60	86	76	ESE	2	SW	1	SW	2
10	750.0	751.0	751.8	13.5	17.0	13.0	14.1	18.0	12.4	-	09.9	10.5	09.9	85	72	88	82	E	2	S	2	ESE	2
11	750.2	749.5	749.7	12.2	18.0	10.7	12.9	18.3	09.7	-	07.6	10.1	04.5	71	65	46	61	W	2	SW	3	NE	5
12	750.0	750.0	749.4	08.1	13.7	10.4	10.7	14.2	06.3	-	02.2	03.3	04.2	28	28	45	34	NE	6	WSW	1	NNE	2
13	747.8	745.7	742.5	10.3	10.5	13.2	11.8	13.5	07.9	-	04.5	08.5	10.6	48	89	94	77	ESE	4	SE	6	SSE	5
14	745.3	748.1	749.3	11.8	14.9	11.8	12.6	16.2	10.1	-	09.6	09.0	08.3	92	70	80	81	NE	1	SW	3	WSW	1
15	749.2	748.7	749.0	11.6	17.7	13.4	14.0	18.1	09.5	-	06.9	09.3	08.4	67	61	73	67	ENE	1	WSW	2	NNE	1
16	750.0	750.5	752.1	13.3	17.6	15.3	15.4	18.6	11.3	-	08.6	10.1	08.5	75	67	65	69	WWN	1	SW	4	NNE	1
17	753.2	753.4	752.7	15.0	17.6	15.6	16.0	19.5	12.1	-	08.5	08.8	09.4	67	58	71	65	SSE	1	SW	2	ESE	1
18	752.5	752.2	751.8	15.5	22.4	18.1	18.5	22.7	14.5	-	09.3	10.2	07.8	70	50	50	57	NE	2	SW	2	WSW	1
19	751.0	750.0	748.9	17.2	20.1	18.3	18.5	20.9	13.7	-	10.4	11.0	11.4	71	63	72	69	ESE	2	ESE	4	ESE	4
20	749.1	749.9	750.0	18.8	22.5	17.9	19.3	23.5	17.9	-	10.4	12.9	12.1	64	63	79	69	ESE	4	SW	3	ESE	1
21	751.2	749.3	747.8	17.8	20.1	20.7	19.8	21.0	15.8	-	12.2	11.6	08.6	86	66	47	66	N	1	ESE	5	ESE	5
22	743.2	742.1	741.9	18.8	15.5	16.0	16.6	21.5	15.3	-	09.5	12.5	12.6	58	95	92	82	ESE	7	ESE	7	ESE	3
23	744.0	745.5	746.6	16.1	18.9	17.2	17.4	23.4	13.3	-	11.6	11.1	10.9	84	68	74	75	E	2	SSW	5	SE	3
24	747.5	748.6	749.1	16.0	21.0	16.8	17.7	21.2	15.2	-	11.2	10.5	10.1	82	56	70	69	SE	4	SSE	3	ESE	4
25	748.6	749.8	751.0	13.6	18.2	16.1	16.0	19.2	13.1	-	10.7	10.9	11.1	91	70	81	81	ENE	4	SSE	2	NW	2
26	750.7	750.9	750.8	16.0	21.4	17.9	18.3	22.4	14.0	-	11.0	12.6	08.9	81	66	58	68	NE	1	WSW	2	ENE	2
27	750.0	749.7	749.4	14.8	16.8	16.7	16.3	18.5	13.6	-	08.2	08.5	06.9	65	59	48	57	NE	4	NNE	5	NE	4
28	749.2	749.8	749.9	16.8	20.1	16.8	17.6	21.2	14.6	-	07.2	07.0	06.9	50	39	48	46	NE	3	NE	3	NE	4
29	749.3	748.2	748.2	16.3	19.9	17.6	17.9	21.5	15.1	-	07.2	07.5	06.5	52	43	43	46	NE	4	NE	5	NNE	3
30	747.8	748.4	750.1	17.0	21.8	18.8	19.1	22.5	15.9	-	07.1	07.2	07.8	49	37	48	45	NE	3	NE	4	NE	2
31	751.4	752.3	753.4	17.6	23.7	19.5	20.1	24.2	16.4	-	07.2	09.8	09.2	48	45	54	49	NE	1	SW	3	WNW	2
MES.	RED.	748.3	748.5	748.8	14.8	18.3	15.6	16.1	19.6	12.8	-	08.7	09.7	09.1	69	62	69	67	2.8	3.4	2.6		

1978 JUN

SPLIT-MARJAN

1	754.7	754.4	754.4	19.0	23.8	19.6	20.5	24.7	16.1	-	10.5	11.1	09.8	64	50	57	57	NNE	1	WSW	2	ENE	2
2	754.1	753.1	752.0	19.8	24.6	22.3	22.3	25.6	17.9	-	10.3	11.7	09.9	59	51	49	53	ENE	1	SW	2	NE	3
3	752.0	751.2	752.0	20.5	27.5	21.8	22.9	28.0	18.9	-	10.7	11.8	10.7	59	53	52	51	SW	2	ESE	3		
4	753.2	753.7	753.9	21.0	25.8	21.2	22.3	26.9	19.7	-	09.8	12.5	09.4	52	50	50	51	NE	1	SW	2	NE	2
5	754.9	754.7	754.1	19.8	25.8	21.6	22.2	26.2	18.1	-	10.9	13.7	13.5	63	55	70	63	ENE	2	SW	2	NNE	1
6	754.0	753.0	752.9	21.0	26.5	22.0	22.9	27.1	18.3	-	13.5	13.5	12.3	73	52	62	62	ENE	1	SW	2	ENE	1
7	753.4	754.1	753.6	21.2	26.2	23.2	23.5	27.5	18.7	-	12.6	10.1	09.6	67	39	45	50	ESE	1	SW	3	NW	1
8	753.1	752.8	752.5	21.6	26.7	22.4	23.3	27.6	20.2	-	12.2	13.4	12.7	63	51	62	59	ESE	1	SSW	2	WNW	1
9	752.3	751.5	750.9	22.1	28.0	23.8	24.4	28.2	20.6	-	15.6	12.6	11.0	78	44	50	57	SSE	1	SSW	2	SW	1
10	751.3	751.2	751.3	22.6	27.9	23.9	24.6	28.8	20.1	-	11.9	12.5	13.6	58	44	61	54	SE	1	SSW	1	WNW	1
11	751.6	751.7	751.0	23.4	26.4	25.4	25.7	29.6	22.5	-	11.3	12.9	10.1	52	44	41	46	E	2	ESE	2	ESE	4
12	747.8	746.7	745.8	25.8	26.1	24.0	25.0	27.9	24.0	-	10.7	13.1	12.8	63	52	57	51	ESE	5	SE	6	SW	1
13	745.7	746.0	746.1	20.0	22.4	21.1	21.2	28.7	19.5	-	16.0	12.6	14.4	91	62	77	77	WSW	1	NNE	2	ESE	3
14	746.3	747.3	748.2	20.7	25.0	18.7	20.8	26.7	18.0	-	12.4	10.8	13.7	68	46	85	66	NNE	1	WNW	2	WNW</td	

BR. ST. 87

 $H_s = 122 \text{ m } H_b = 128.0 \text{ m } h_t = 6.5 \text{ m } h_r = 1.0 \text{ m}$

Dan	Vrh O. v. o.	Oblačnost N (0-10)					Intenzitet sunca Broj	Padavina R mm	Snežni pokrival h cm	Razvoj vremene w
		14	7	14	21	Sred Dnes				
1	8 09	10	07	08.7	02.1	00.0	.	0-100-0-20, 0-10-24	.	.
2	8 10	09	09	09.3	00.2	14.0	.	0-10-0-20-24	.	.
3	8 00	02	00	00.7	12.8	11.7	.	0-0-0-0	.	.
4	8 08	05	00	04.3	06.1	.	.	0-14-12-24	.	.
5	9 08	08	08	08.0	08.6	.	.	0-14-12-24	.	.
6	7 24	10	10	08.0	01.9	00.0	.	0-14-4-8-6-8-10-13-24	.	.
7	8 10	09	09	06.3	05.0	54-5	.	0-10-2-24-24-0-6-T22-24	.	.
8	8 10	09	08	09.0	02.3	11.1	.	0-10-4-23-23-0-6-T0-5-24	.	.
9	8 10	08	08	08.7	06.6	00.7	.	0-10-5-23-23-0-6-14-6-12-23-24	.	.
10	7 10	09	10	09.7	00.0	03.1	.	0-0-0-6-14-6-14-16-16-17-24	.	.
11	8 06	04	00	03.3	08.0	15.9	.	0-10-0-20-17-24, T'4-15-24, F10-10-24	.	.
12	8 01	04	00	01.7	13.0	01.9	.	F10-0-6-24	.	.
13	6 12	10	10	10.0	00.0	.	.	0-10-4-14-14-12-19	.	.
14	8 09	08	08	05.7	06.7	23.1	.	0-10-0-7-14	.	.
15	8 06	02	00	02.7	11.8	00.0	.	0-10-0-6-14-6-14-16-17-24	.	.
16	8 08	03	00	03.7	11.6	.	.	0-10-10-24	.	.
17	8 09	10	03	07.3	05.3	.	.	0-10-0-6-24	.	.
18	8 09	01	05	05.9	09.9	00.2	.	0-10-0-20-23-23-13-23-24	.	.
19	8 23	07	09	06.3	08.8	03.9	.	0-10-0-20-23-23-13-23-24	.	.
20	8 06	01	06	04.3	09.4	00.0	.	0-10-0-6-14-6-14-16-17-24	.	.
21	7 28	10	10	09.3	01.9	.	.	0-10-0-6-14-6-14-22-24	.	.
22	6 10	10	10	10.0	00.0	00.4	.	0-10-0-6-24-24	.	.
23	8 04	09	01	04.7	09.4	16.3	.	0-10-0-20-24-24-0-0-0	.	.
24	8 09	04	09	07.3	10.1	.	.	0-10-10-10-16-16-16-16-24	.	.
25	6 10	07	08	08.3	03.3	19.2	.	0-10-10-10-16-16-16-16-24	.	.
26	7 01	09	09	06.3	07.6	03.0	.	0-10-0-20-23-23-13-15-15-16-24	.	.
27	8 10	09	10	09.7	02.2	01.2	.	0-10-0-20-23-23-13-15-15-16-24	.	.
28	8 09	08	04	07.0	03.2	02.2	.	0-10-12-16	.	.
29	8 08	08	10	08.7	04.2	.	.	0-10-10-16-16-17-24	.	.
30	8 08	05	09	07.3	08.7	00.0	.	0-10-10-16-16-17-24	.	.
31	8 09	04	09	07.3	08.8	00.0	.	R-6-16-16-17-22-24	.	.
MES. VRED.		07.5	06.8	05.9	06.7	189.5	182.4			

SPLIT-MARJAN

1978 JUN

1	8 00	06	00	02.0	08.7	00.8	.	0-10-3	.	.
2	8 01	05	00	02.0	12.8
3	8 00	03	03	02.0	12.4
4	8 00	03	00	01.0	09.1
5	8 04	05	00	03.0	12.1
6	7 00	04	00	01.3	12.1	.	.	==12-11	.	.
7	8 02	09	00	03.7	09.3	.	.	==3-6-10, 0-10-14-25	.	.
8	8 24	09	09	07.3	07.6	00.0
9	7 06	01	00	02.3	11.1	.	.	==16-11	.	.
10	7 00	09	08	05.7	07.4
11	8 10	08	09	09.0	05.2
12	8 06	07	09	07.3	04.4	.	.	0-10-7-17-24	.	.
13	7 10	07	10	10	03.9	04.0	.	0-10-23-30-6-9-17-24; ==9-13-20, T13-15-15-20-21-20	.	.
14	7 04	03	10	05.7	10.3	02.6	.	0-10-10-10	.	.
15	8 10	10	10	10.0	09.7	01.7	.	0-23-30-7-8-8-16-16-17-17-24	.	.
16	8 04	07	08	06.3	10.2	79-2	.	0-10-10	.	.
17	8 09	04	09	07.3	08.0	00.0	.	0-10-6-6-6	.	.
18	8 04	03	07	04.7	12.2
19	7 08	09	05	07.3	03.5	.	.	0-10-8-8	.	.
20	8 30	04	01	01.3	12.5	00.1
21	8 10	10	03	07.7	02.6	.	.	0-10-10-15-24	.	.
22	7 00	01	00	00.3	12.1	03.4
23	7 01	00	00	01.0	13.4	.	.	0-10-6-24	.	.
24	8 04	02	00	02.0	10.0
25	7 01	04	01	02.0	12.3
26	8 04	02	00	02.0	12.5	00.3	.	0-10-20-5-5-0	.	.
27	7 10	10	10	10.0	00.0	01.4	.	0-10-10-0-0	.	.
28	8 13	07	04	04.7	11.1	12.2
29	8 11	05	05	01.7	13.7
30	8 00	01	05	02.0	12.2
MES. VRED.		07.8	05.3	04..	14.4	273.3	115.7			

1978 JUL'

SPLIT-MARJAN

 $\varphi = 43^{\circ}31' N$ $\lambda = 16^{\circ}26' E$ Gr. $\Delta G = + 1h 06 min.$

BR. ST. 87

d	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodené pory e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0-12)				
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21	
1	753.3	753.2	751.6	20.9	26.5	21.5	22.6	26.6	18.4	-	12.3	11.2	12.6	66	43	65	58	E	1	SSE 1	NNE 3
2	751.3	751.7	752.1	22.6	26.3	22.0	23.2	26.4	20.4	-	10.3	14.2	15.1	50	55	76	60	SE	5	SSW 4	SW 1
3	750.6	750.6	749.9	21.6	25.1	21.5	22.4	25.9	19.4	-	15.5	14.2	12.4	80	59	65	68	WSW	1	SW 3	SSW 1
4	749.9	749.0	748.4	21.0	25.4	23.1	23.2	25.9	18.5	-	12.7	13.7	12.2	68	56	58	61	ENE	1	SE 4	ESE 3
5	747.0	746.3	748.1	22.4	22.9	21.6	22.1	24.8	21.6	-	15.9	15.3	16.1	78	73	83	78	SE	6	SE 6	WNW 2
6	748.9	749.1	748.4	21.0	23.1	22.8	22.4	27.0	18.1	-	11.0	15.5	09.8	59	73	47	60	NNE	1	SE 5	WNW 1
7	747.4	748.2	748.8	21.0	24.8	19.3	21.1	26.0	19.2	-	11.4	11.5	11.3	61	49	67	59	ENE	1	SW 4	NNW 4
8	749.9	750.3	750.0	19.4	25.1	21.8	22.0	25.3	17.1	-	07.9	08.5	07.8	47	36	40	41	NE	4	SW 2	NE 2
9	750.5	749.4	748.4	18.4	24.0	20.4	20.8	24.3	16.7	-	07.9	10.2	11.6	50	46	64	53	NE	2	SW 3	SSW 1
10	748.1	748.7	749.4	20.3	26.8	21.5	22.6	27.0	18.0	-	08.4	10.8	15.4	46	41	80	56	ENE	2	SSE 3	WNW 1
11	750.1	750.7	750.6	22.0	28.6	24.4	24.9	28.9	18.2	-	14.8	13.4	12.6	75	46	55	59	ESE	1	SW 2	NW 1
12	751.4	751.1	751.5	24.0	31.6	26.4	27.1	31.7	21.0	-	11.9	12.7	13.2	53	36	51	47	E	1	SSW 2	WNW 1
13	752.4	752.1	751.7	25.6	31.2	28.2	28.3	32.4	24.0	-	11.4	14.4	11.7	46	42	41	43	NNE	1	WSW 3	NW 2
14	751.8	751.4	750.1	26.4	31.3	25.5	27.2	31.7	24.5	-	13.1	14.8	16.4	51	43	67	54	NE	2	WSW 3	SSE 1
15	749.7	748.2	748.8	22.0	28.8	24.2	24.8	29.1	21.6	-	16.7	18.0	09.7	84	61	43	63	NW	3	NNW 2	ESE 5
16	750.4	750.0	750.0	23.4	28.9	24.4	25.3	29.6	21.8	-	10.2	11.8	14.2	47	40	62	50	NE	3	SW 3	NNW 2
17	751.6	752.0	752.0	23.7	29.8	25.0	25.9	30.4	21.0	-	11.6	13.0	14.7	53	41	62	52	ENE	1	SSW 2	SW 1
18	751.4	750.5	747.5	24.7	31.9	26.6	27.5	32.2	22.0	-	11.5	11.6	12.5	49	33	48	43	ESE	2	SSE 4	SE 5
19	743.2	743.6	744.9	25.3	30.0	23.1	25.4	30.1	23.0	-	12.4	14.5	10.4	51	45	49	48	SE	6	SSE 2	NW 2
20	748.0	747.8	746.8	22.5	28.4	24.0	24.7	28.8	20.9	-	08.4	10.1	09.0	41	35	40	39	ENE	3	WSW 3	S 2
21	746.7	746.2	745.9	22.0	29.6	24.4	25.1	29.8	21.5	-	07.5	11.6	10.1	38	37	44	40	ENE	2	SW 2	NNW 2
22	749.3	751.2	752.6	19.4	23.8	19.5	20.6	24.6	17.3	-	07.1	07.0	06.3	42	31	37	37	ENE	5	NNE 5	NE 4
23	753.2	752.4	751.4	19.4	25.0	20.6	21.4	25.6	17.0	-	05.6	08.3	06.9	33	35	38	35	NE	4	SW 3	NE 5
24	751.5	751.1	750.9	19.6	26.2	22.0	22.5	26.7	17.3	-	06.8	06.7	07.5	40	26	38	35	NE	4	SW 3	NE 5
25	752.0	751.0	751.3	20.7	27.8	21.3	22.8	27.8	18.8	-	07.9	09.1	13.1	43	33	69	48	NE	2	WSW 2	ESE 1
26	751.4	751.3	751.6	22.1	28.2	23.6	24.4	28.6	20.5	-	08.8	09.5	10.3	44	33	47	41	ENE	2	SW 3	NNE 1
27	751.6	751.7	752.0	22.2	29.7	25.8	25.9	30.0	20.3	-	10.5	10.4	10.1	52	33	41	42	ESE	1	WSW 2	ENE 2
28	752.7	752.7	752.8	25.2	31.4	27.0	27.7	31.9	23.5	-	10.4	11.2	11.7	43	32	44	40	NE	2	WSW 3	NE 5
29	754.3	752.8	752.5	25.2	31.8	26.3	27.4	32.1	23.9	-	09.0	08.9	09.6	38	25	37	33	ESE	2	WSW 3	ENE 2
30	751.6	750.4	750.6	24.9	29.3	23.8	25.5	31.1	23.5	-	10.9	09.5	09.9	46	31	45	41	ENE	1	WSW 3	ENE 2
31	750.0	750.2	750.7	23.0	29.3	23.9	25.0	30.4	21.5	-	10.1	12.7	14.5	48	42	65	52	ENE	2	SW 2	SSW 1
MES.	750.4	750.2	750.0	22.3	27.8	23.4	24.2	28.5	20.3	-	10.6	11.8	11.6	52	42	54	50	2.4	3.0	2.3	
RED.																					

SPLIT-MARJAN																				
1	751.6	751.6	751.0	22.6	30.8	26.6	26.7	30.8	21.1	-	11.3	10.6	11.2	55	32	43	43	NNE 2	SW 2	N 1
2	751.6	751.4	750.9	24.7	31.4	26.9	27.5	32.1	22.1	-	11.1	12.5	12.8	48	36	48	54	ESE 3	WSW 3	SE 1
3	751.5	751.1	751.0	24.4	31.2	25.3	26.6	31.3	23.2	-	12.6	13.6	15.9	55	40	66	54	SE 1	SW 2	ESE 1
4	751.5	751.4	750.6	24.6	26.7	24.1	24.9	27.3	23.6	-	13.7	13.7	14.1	59	52	63	58	NE 1	NW 2	WNW 1
5	750.7	750.1	749.5	23.8	30.6	26.1	26.7	31.2	21.5	-	12.9	13.5	15.3	58	41	60	53	NNE 1	WSW 3	ENE 1
6	750.2	749.7	748.9	25.0	30.6	25.3	26.6	31.4	23.1	-	11.1	14.7	15.7	47	45	65	52	ENE 1	WSW 3	ESE 2
7	748.4	747.5	744.7	24.4	32.4	27.7	28.1	32.8	22.4	-	14.4	13.5	10.8	63	37	39	46	ESE 2	S 3	ESE 6
8	741.9	743.1	746.7	24.8	29.2	21.8	24.4	30.0	21.2	-	15.1	13.1	10.7	64	43	55	54	SE 6	SW 2	NNW 4
9	749.0	749.3	749.1	21.2	26.3	22.3	23.0	27.8	19.7	-	10.9	13.9	11.9	58	54	59	57	NNE 2	SW 4	ENE 1
10	748.8	748.9	749.1	20.6	27.1	21.8	22.8	28.1	19.8	-	08.4	10.6	11.3	46	40	58	48	NE 4	SW 3	WSW 2
11	750.0	749.8	749.9	20.1	23.2	21.6	21.6	26.8	18.4	-	08.3	09.2	08.1	47	43	42	44	NE 4	NNW 3	NE 4
12	751.5	752.3	752.0	20.3	27.2	22.1	22.9	27.7	19.0	-	07.3	07.5	08.6	41	28	43	37	NE 4	SW 3	NNM 3
13	753.1	752.6	751.2	20.2	26.4	22.0	22.7	27.6	18.8	-	07.1	09.8	09.7	40	38	49	42	ESE 1	SSW 2	SSE 1
14	750.2	751.5	752.1	18.4	21.1	20.2	20.0	23.4	15.2	-	09.5	12.6	10.5	60	67	59	62	ENE 3	SE 2	WNW 3
15	753.1	752.6	752.9	19.8	26.7	22.2	22.7	27.1	17.8	-	09.9	11.0	11.4	57	42	57	52	ENE 2	SW 2	NNW 1
16	753.5	753.6</td																		

BR. ST. 87

 $H_s = 122 \text{ m } H_b = 128.0 \text{ m } h_t = 6.5 \text{ m } h_r = 1.0 \text{ m}$

Dan	M es.	Oblačnost N (0-10)					Leskobran broj	Padavina R mm	Snežni pokrivač h cm	Rezanj vremena w
		14	7	14	21	Sred Dnes				
1	8	000	050	10	05.0	09.8
2	7	040	010	09	04.7	11.0	.	.	.	$\oplus 12^{\circ} 23^{\circ}$
3	7	08	010	00	03.0	10.8	00.2	.	.	$= 1^{\circ} 5^{\circ} 8^{\circ}$
4	8	000	050	00	01.7	13.4	.	.	.	$= 1^{\circ} 5^{\circ} 8^{\circ} \Delta 1^{\circ} 7^{\circ} 9^{\circ}$
5	7	030	09	00	04.0	08.1	.	.	.	$= 1^{\circ} 11^{\circ} 10^{\circ} n, T^{\circ} R^{\circ} \text{ne-ns} 4-17, \oplus 12^{\circ} 42^{\circ}$
6	7	010	10	05	05.3	10.9	00.2	.	.	.
7	8	030	03	10	05.3	11.1
8	8	010	030	00	01.3	11.7
9	8	070	050	01	04.3	12.7
10	8	000	010	07	02.7	12.2
11	8	000	010	00	00.3	12.9	.	.	.	$= 1^{\circ} 7^{\circ} 9^{\circ}$
12	8	000	000	00	00.0	13.6	.	.	.	$= 1^{\circ} 7^{\circ} 9^{\circ}$
13	8	000	010	01	00.7	12.3	.	.	.	$= 1^{\circ} 7^{\circ} 9^{\circ}$
14	7	020	020	00	01.3	13.3	.	.	.	$\oplus 1^{\circ} 6^{\circ} g, R^{\circ} 6^{\circ} 7^{\circ}, T^{\circ} 7^{\circ} 7^{\circ}$
15	7	100R	06	02	06.0	07.8	01.6	.	.	$\oplus 1^{\circ} 6^{\circ} g, R^{\circ} 6^{\circ} 7^{\circ}, T^{\circ} 7^{\circ} 7^{\circ}$
16	7	000	010	00	00.3	12.9	01.1	.	.	$= 1^{\circ} 7^{\circ} 11^{\circ}$
17	7	000	010	00	00.3	11.9	.	.	.	$= 1^{\circ} 7^{\circ} 11^{\circ}$
18	8	000	010	04	01.7	12.2
19	7	09	030	00	04.0	09.9	.	.	.	$R^{\circ} 0-11^{\circ}$
20	8	000	010	01	00.7	13.4
21	8	10	040	04	06.0	09.7	.	.	.	$\oplus 1^{\circ} 7^{\circ} n$
22	8	000	010	00	00.3	13.6	.	.	.	$R^{\circ} 0-ns 0-10^{\circ} i$
23	8	010	000	00	00.3	13.2
24	8	000	000	03	00.0	13.3
25	8	000	010	00	00.3	12.7
26	8	000	010	00	00.3	12.5
27	7	000	010	02	01.0	12.2
28	7	010	020	00	01.0	11.5	.	.	.	$= 1^{\circ} 7^{\circ} 9^{\circ}$
29	8	000	070	00	02.3	09.3
30	8	000	040	01	01.7	10.4	.	.	.	$= 1^{\circ} 7^{\circ} 9^{\circ}$
31	8	000	030	00	01.0	08.3
MES. VRED.		01.9	02.7	01.8	02.2	358.6	03.1			

SPLIT-MARJAN

1978 AVGUST

1	7	000	010	00	00.3	12.8	.	.	.	$= 1^{\circ} 7^{\circ} 8^{\circ}$
2	8	000	000	00	00.0	12.9	.	.	.	$= 1^{\circ} 7^{\circ} 9^{\circ}$
3	7	000	030	00	01.0	12.3	.	.	.	$= 1^{\circ} 7^{\circ} 8^{\circ}$
4	7	09	10	00	06.3	00.0	.	.	.	$= 1^{\circ} 7^{\circ} 13^{\circ}, \oplus 1^{\circ} 12^{\circ} 4^{\circ}, 15^{\circ} 16^{\circ} i$
5	8	000	080	00	02.7	12.9	00.2	.	.	.
6	8	000	010	00	00.3	12.9
7	8	010	000	10	03.7	10.2
8	8	04	020	04	03.3	09.0	.	.	.	$R^{\circ} 0-9^{\circ}, \oplus 1^{\circ} 9^{\circ} 9^{\circ}, 13^{\circ} 20^{\circ} i$
9	8	100	040	02	02.0	13.2	00.0	.	.	.
10	8	120	030	01	02.0	11.4
11	8	010	10	01	04.0	07.2	.	.	.	$T^{\circ} 0^{\circ} 13^{\circ}$
12	7	000	020	01	01.9	12.7	.	.	.	$= 1^{\circ} 7^{\circ} 12^{\circ}$
13	8	010	09	01	03.7	13.8
14	8	100	080	00	06.0	05.6	00.6	.	.	$\oplus 1^{\circ} 12^{\circ} 4^{\circ}, T^{\circ} 7^{\circ} 7^{\circ}, R^{\circ} 7^{\circ} 9^{\circ} 9^{\circ}$
15	7	000	010	00	00.3	12.7	19.9	.	.	$= 1^{\circ} 7^{\circ} 12^{\circ}$
16	8	000	010	00	00.3	12.7	.	.	.	$= 1^{\circ} 7^{\circ} 9^{\circ}, \Delta 1^{\circ} 7^{\circ} 8^{\circ}$
17	8	010	020	04	02.3	11.9	.	.	.	$= 1^{\circ} 7^{\circ} 10^{\circ} b$
18	7	000	010	03	00.3	12.0	.	.	.	$= 1^{\circ} 7^{\circ} 13^{\circ}$
19	8	000	010	00	00.3	12.7
20	8	000	040	01	01.7	12.6
21	8	000	000	00	00.0	12.6
22	8	000	000	00	00.0	12.1
23	8	000	000	00	00.0	12.2
24	7	000	020	03	01.7	11.3	.	.	.	$= 1^{\circ} 7^{\circ} 9^{\circ}$
25	7	000	010	00	00.3	11.5	.	.	.	$= 1^{\circ} 7^{\circ} 13^{\circ}, R^{\circ} 8^{\circ} R$
26	6	010	010	04	02.0	11.7	.	.	.	$= 1^{\circ} n-n$
27	8	030	09	10	07.3	03.8
28	6	10	07	06	07.7	02.7	00.0	.	.	$\oplus 1^{\circ} 12^{\circ} 4^{\circ}$
29	7	000	010	00	00.3	11.5	11.2	.	.	$= 1^{\circ} 10^{\circ} n$
30	6	09	09	100R	09.3	15.7	.	.	.	$\oplus 1^{\circ} 14^{\circ} 4^{\circ}, \oplus 2^{\circ} 7^{\circ} 11^{\circ}, 20^{\circ} 21^{\circ}, T^{\circ} 20^{\circ} n$
31	7	10	10	01	07.0	10.6	19.0	.	.	$\oplus 1^{\circ} 15^{\circ} 4^{\circ}, R^{\circ} 9^{\circ} 12^{\circ} 4^{\circ}, R^{\circ} 11^{\circ} 12^{\circ} 4^{\circ}$
MES. VRED.		12.1	23.6	01.9	02.5	313.2	26.9			

$\varphi = 43^{\circ}31' N$ $\lambda = 16^{\circ}26' E$ Gr. $\Delta G = + 1h 06 min.$

BR. ST. 87

d	Vazdušni pritisak P mm			Temperatura vazduha T °C								Napon vodenih parova e mm			Relativna vlažnost U %			Pravac i jačina veta D, f (0-12)			
				7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	7	14	21	7	14	21	Sred. Dnes	7	14	21
		7	14	21	7	14	21														
1	746.8	747.0	746.9	14.1	21.0	17.8	17.7	21.6	13.2	-	07.2	08.2	07.1	59	44	47	50	NNW 1	SW 3	ENE 1	
2	746.4	747.2	748.0	12.7	21.7	17.9	17.6	21.8	11.1	-	09.2	11.3	12.7	84	58	82	75	NE 3	SSW 2	NW 1	
3	749.0	749.7	749.6	17.0	24.0	19.2	19.9	24.0	15.9	-	10.5	13.2	11.1	72	59	66	66	NE 2	SSW 2	NNE 1	
4	749.2	749.2	748.5	17.6	24.5	20.2	20.6	24.7	16.1	-	09.2	11.6	12.9	61	50	73	61	ENE 2	SSW 2	SE 2	
5	746.1	745.9	745.6	20.0	19.2	20.0	19.8	21.0	17.6	-	13.8	13.6	14.3	78	81	82	80	SE 2	ENE 3	ESE 4	
6	742.5	742.0	743.2	17.8	18.8	18.9	18.6	20.2	16.8	-	14.4	14.8	13.3	94	91	81	89	ESE 4	ESE 4	WNW 2	
7	742.6	742.9	743.5	17.4	23.4	20.1	20.3	23.6	17.0	-	13.1	13.7	12.4	88	63	70	74	ENE 2	SSW 1	NNE 2	
8	745.7	747.4	748.4	19.7	24.7	21.8	22.0	25.0	19.1	-	09.5	08.3	08.1	55	36	41	44	NE 2	WSW 3	NNE 3	
9	759.8	751.1	752.7	18.6	24.2	20.1	20.8	25.0	18.1	-	07.7	09.8	07.3	48	43	41	44	N 3	SSW 2	ENE 1	
10	753.1	752.2	752.0	20.0	24.3	21.6	21.9	24.8	18.4	-	07.9	12.2	13.5	45	53	70	56	NNE 1	SW 2	E 1	
11	751.5	751.1	749.7	19.4	25.0	21.0	21.6	25.2	18.7	-	12.5	13.2	13.8	74	55	74	68	E 1	SW 2	E 1	
12	746.1	744.8	747.5	20.9	11.2	16.7	16.4	23.6	10.7	-	12.2	09.5	05.9	66	95	41	67	ESE 5	N 6	NNE 4	
13	750.7	752.3	753.3	17.1	18.8	17.3	17.6	19.4	15.6	-	05.2	05.9	05.0	36	37	34	36	NNE 3	WNW 2	NNE 1	
14	751.3	751.0	751.1	17.1	24.8	19.7	20.1	23.8	16.0	-	05.1	08.1	09.7	35	37	56	43	NE 5	SW 1	SSW 2	
15	750.0	749.9	750.3	17.4	24.1	22.4	21.6	25.2	15.8	-	08.8	13.2	08.4	59	58	42	53	NNE 1	SW 2	NE 4	
16	752.6	753.5	755.0	20.6	25.5	21.4	22.2	26.1	18.6	-	07.3	09.2	07.7	40	37	40	39	NE 2	WSW 2	NNE 2	
17	756.5	755.1	755.0	19.2	23.9	20.4	21.0	24.2	18.4	-	08.4	10.9	11.7	50	49	65	55	ENE 2	WSW 2	WSW 2	
18	753.6	753.1	752.6	18.3	24.3	19.8	20.6	24.4	17.0	-	09.8	12.5	13.0	62	55	75	64	ENE 1	SSW 2	W 1	
19	751.3	750.1	749.5	18.6	24.4	21.0	21.3	24.5	17.5	-	10.5	11.1	09.9	65	48	53	55	ENE 2	SSW 2	ESE 1	
20	748.9	750.6	753.4	12.5	17.1	13.9	14.4	21.5	12.5	-	09.1	06.6	04.7	84	45	39	56	NNE 6	NNE 5	NE 7	
21	755.4	754.8	755.9	12.4	17.1	13.8	14.3	17.4	11.5	-	03.6	04.2	04.4	34	29	37	33	NE 6	NNE 5	NE 4	
22	755.9	755.1	754.1	14.2	20.9	17.9	17.7	21.1	12.0	-	06.1	07.8	07.7	50	42	50	47	ENE 2	SW 2	NNE 2	
23	752.8	752.0	752.7	16.0	20.2	16.8	17.5	20.2	15.4	-	07.6	10.7	12.0	56	60	84	67	NNE 1	SSW 1	W 1	
24	754.7	755.2	756.1	17.2	23.1	19.1	19.6	23.2	15.9	-	08.2	09.5	12.1	55	45	73	58	NE 2	WSW 1	ESE 1	
25	756.9	756.9	756.9	17.8	23.3	18.9	19.7	23.7	16.5	-	10.2	12.8	12.3	67	60	75	67	ENE 1	SSW 1	SSW 1	
26	755.4	754.3	753.2	18.2	23.8	19.2	20.1	24.1	17.5	-	11.5	13.2	13.6	73	60	81	71	NE 1	SSW 2	SW 1	
27	751.0	749.5	746.8	16.9	20.9	19.0	19.0	21.4	16.4	-	12.8	13.2	11.7	88	71	71	77	-	SSW 2	ESE 4	
28	743.2	743.5	749.8	17.8	13.8	13.0	14.4	19.2	10.4	-	13.6	09.6	05.5	89	81	49	73	SSW 1	NE 3	NNW 3	
29	749.5	750.1	751.2	12.4	18.4	14.1	14.8	18.7	11.5	-	04.8	07.6	07.5	45	48	62	52	NNE 3	SSW 2	FNE 2	
30	751.5	750.0	747.4	16.4	19.2	18.5	18.2	19.2	14.1	-	10.5	11.5	12.5	75	69	78	74	SE 6	SE 6	SE 6	
MES.																					
RED.	750.4	750.2	750.5	17.2	21.5	18.7	19.0	22.6	15.5	-	09.3	10.6	10.1	63	55	61	60	2.4	2.5	2.5	

1978 OKTOBAR

SPLIT-MARJAN

1	745.3	744.8	746.3	18.3	20.1	18.7	19.0	20.8	17.9	-	12.4	12.3	13.7	78	70	85	78	SSE 4	ESE 5	SE 4
2	746.6	747.5	749.0	18.4	19.8	20.4	19.8	20.5	18.0	-	13.3	12.0	11.7	84	69	65	73	SE 6	ESE 6	ESE 5
3	747.0	747.1	748.3	21.5	24.0	16.7	19.7	24.4	16.3	-	08.8	08.7	12.2	46	39	86	57	SE 5	ESE 6	ESE 4
4	748.1	749.0	750.0	17.7	19.6	17.8	18.2	20.4	16.6	-	11.8	10.9	12.2	78	64	80	74	SE 5	SSW 5	SSE 4
5	749.4	751.0	752.7	16.2	14.0	14.9	15.0	18.0	11.7	-	11.7	06.5	04.9	84	55	39	59	ESE 3	NE 6	NE 5
6	754.3	754.2	755.2	13.6	19.0	15.9	16.1	19.2	12.4	-	04.3	05.2	06.2	37	31	45	38	NNE 5	SW 2	NNE 3
7	754.9	755.1	755.0	16.7	20.6	18.7	18.7	22.4	15.9	-	07.2	09.2	07.8	51	51	48	50	NE 2	SSW 2	NE 3
8	755.8	755.4	755.1	15.7	21.6	18.1	18.4	21.8	15.1	-	07.5	09.0	10.2	56	46	65	56	NE 2	SSW 2	SSE 1
9	755.3	755.0	755.5	16.9	22.6	18.0	18.9	22.6	16.5	-	08.3	09.3	09.4	58	45	60	54	NE 3	SSW 2	NE 1
10	755.6	755.9	756.4	15.7	21.8	17.8	18.3	21.8	15.6	-	08.9	10.7	10.9	67	55	71	64	NE 2	SSW 1	SE 2
11	757.0	757.1	757.5	16.1	21.8	18.7	18.8	22.1	15.6	-	09.4	11.7	10.9	69	60	68	66	NE 2	SSE 1	SSE 1
12	757.5	756.9	756.7	17.3	23.6	21.0	20.7	23.6	16.6	-	08.0	08.9	07.1	54	41	38	44	NE 3	SSW 2	NE 1
13	757.0	756.7	756.4	18.6	23.6	19.3	20.2	23.6	18.5	-	06.2	08.0	07.5	38	36	44	39	NE 1	WSW 2	WNW 1
14	755.8	754.7	754.3	15.6	21.4	17.2	17.9	21.6	15.6	-	07.5	09.1	12.6	57	47	86	63	NE 2	WSW 1	SSE 1
15	753.6	752.7	752.4	14.6	19.7	16.3	16.7	20.4	13.2	-	07.7	11.0	10.7	62	64	77	68	NE 3	WSW 2	SW 1
16	751.3	750.2	749.9	13.1	18.8	15.1	15.5	19.3	12.6	-</										

BR. ST. 87

$$H_s = 122 \text{ m } H_b = 128.0 \text{ m } h_t = 6.5 \text{ m } h_r = 1.0 \text{ m}$$

Dan	Vlajková čísla O-F	Oblačnosť N (0-10)					Inšedencia bez súčtu v hodinách	Padavina R mm	Snežný pokrývavý h cm	Razový výkon W
		14	7	14	21	Sred Dies				
1	8	010	020	10	04.3	11.3	06.8	.	$\oplus \Delta^2 H^{10}$	
2	8	090	010	00	03.3	08.6	11.9	.	$\oplus^2 3^2 7^2 i$	
3	8	210	010	00	00.7	12.1	00.0	.		
4	8	010	020	00	01.0	10.7	.	.	$\Delta^1 H^9 9^2$	
5	8	100	10	03	07.7	01.7	00.3	.	$\oplus^2 6^2 13^2 i, R^2 8-13^2$	
6	6	100	10	07	09.0	00.0	19.3	.	$\square^2 5^2 7^2 i, \oplus^2 5^2 10^2 i, \cap 17^2 6^2 i$	
7	7	10	09	10	09.7	02.6	22.6	.	$\oplus^2 13^2 13^2$	
8	8	040	020	08	04.7	09.5	00.0	.		
9	8	010	040	00	01.7	11.2	.	.		
10	7	08	070	01	05.3	06.3	.	.		
11	8	000	010	00	00.3	11.4	.	.	$= H^9 9^2, \Delta^1 H^7-10^2$	
12	2	020	100	03	05.0	05.0	.	.	$\oplus^2 10^2 10^2 i, 13^2 15^2 i, \square^2 13^2 10^2 i, R^2 13^2 14^2 i, \Delta^2 H^4-14^2$	
13	8	050	050	03	04.3	10.5	13.2	.	$\square^2 13^2 14^2 i$	
14	8	000	010	00	00.3	11.4	.	.	$H^2 H^2 0-5^2 i$	
15	8	010	000	04	01.7	11.2	.	.		
16	8	020	08	02	04.0	09.1	.	.		
17	8	090	030	01	04.3	10.3	.	.		
18	8	090	000	00	00.0	10.9	.	.		
19	8	000	010	00	00.3	10.5	.	.	$\Delta^1 H^9 9^2$	
20	9	100	09	00	06.3	01.9	02.1	.	$\square^2 13^2 24^2 i, \oplus^2 5^2 5^2 i$	
21	8	050	000	00	01.7	10.6	01.0	.	$\square^2 H^2 H^2 0-9^2 i$	
22	8	020	020	00	01.3	10.3	.	.	$\Delta^2 H^2 3$	
23	8	08	09	10	09.0	02.6	.	.	$\oplus^2 H^2 5^2$	
24	8	09	040	00	04.3	07.5	00.0	.	$= H^2 H^2$	
25	6	040	010	00	01.7	10.0	.	.	$= H^2 - n$	
26	6	010	000	00	00.3	09.8	.	.	$\Delta^1 H^9 9^2, = H^2 - n$	
27	6	07	08	08	07.7	01.3	.	.	$\oplus^2 H^2 - H, = H^2 4^2, \square^2 H^2 H^2 0-8^2 i, \square^2 H^2 H^2 0-10^2$	
28	6	10	100	00	06.7	00.5	05.2	.	$\oplus^2 H^2 7^2 17^2, = H^2 7^2, \square^2 H^2 0^2$	
29	9	010	010	00	30.7	10.4	05.6	.		
30	7	09	090	08	08.7	07.4	.	.	$\square^2 4^2 21^2 i$	

SPLIT-MAR 1AN

1830 OCTOBER

1	8	98	040	10	07.3	75.6	.	
2	8	99	100	10	09.7	90.0	90.2	.
3	8	09	09	100R	09.3	01.7	90.0	.
4	7	04	04	05	04.3	05.3	15.2	.
5	8	09	100	10	09.7	90.0	90.3	.
6	8	090	000	00	00.0	10.3	01.7	.
7	9	96	03	00	03.0	98.6	.	.
8	8	300	000	00	00.0	10.3	.	.
9	8	000	010	00	00.3	99.9	.	.
10	7	000	000	00	00.0	99.6	.	.
11	7	000	030	00	00.3	99.7	.	.
12	8	230	010	00	01.3	99.7	.	.
13	8	200	000	00	00.0	19.5	.	.
14	6	000	000	00	00.0	99.5	.	.
15	6	310	000	00	00.0	99.5	.	.
16	6	000	010	00	00.3	99.2	.	.
17	6	06	10	00	18.3	92.7	.	.
18	7	220	08	06	05.3	04.1	.	.
19	8	09	09	10	09.3	11.9	11.1	.
20	7	09	100	100	09.7	99.1	.	.
21	8	19	09	01	06.3	00.1	03.8	.
22	9	020	010	01	01.3	19.4	00.2	.
23	7	140	030	00	02.3	17.7	.	.
24	9	000	050	00	01.7	99.8	.	.
25	8	170	140	00	13.7	19.5	.	.
26	7	18	09	00	15.7	72.6	.	.
27	8	26	030	00	03.0	17.3	42.0	.
28	9	210	010	00	00.7	19.6	.	.
29	9	020	010	00	01.0	99.6	.	.
30	9	010	010	00	00.7	99.5	.	.
31	8	000	000	00	00.3	19.1	.	.

$\varphi = 43^{\circ}31' N$ $\lambda = 16^{\circ}26' E$ Gr. $\Delta G = + 1h 06 min.$

BR. ST. 87

d	Vzdušní průtok P mm			Temperatura vzduchu T C°								Napětí vodného paru e mm			Relativní vlhkost u %			Pravac i. jačina větra D, f (0-12)					
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21			
1	760.3	760.7	761.3	10.3	16.4	13.2	13.3	16.8	10.1	-	06.6	08.4	09.0	70	60	79	70	NE	2	SSW	2	NE	1
2	761.3	760.0	759.9	10.9	16.8	12.8	13.3	17.0	10.2	-	05.2	05.5	05.4	53	38	49	47	NE	3	SSW	2	NE	3
3	758.8	758.4	758.7	11.1	16.2	13.2	13.4	16.6	10.7	-	05.3	06.7	06.1	53	48	53	51	NE	2	SSW	1	ENE	2
4	758.5	758.6	758.9	12.4	16.4	12.1	13.3	16.8	12.1	-	05.4	05.7	05.4	50	41	51	47	NE	3	SSE	1	NE	4
5	758.9	759.3	760.0	09.2	14.4	11.8	11.8	14.6	08.8	-	04.6	05.6	05.3	53	45	51	50	NE	4	SSW	1	NE	3
6	761.1	761.0	761.2	08.4	14.0	11.2	11.2	14.4	08.2	-	04.7	05.9	06.0	56	49	60	55	NE	3	SW	2	NNE	1
7	760.4	759.1	759.6	08.0	14.8	12.2	11.8	14.8	07.4	-	04.4	07.4	05.3	54	58	50	54	NE	3	SW	2	S	1
8	760.3	759.8	760.1	09.6	15.1	11.8	12.1	15.2	09.2	-	02.8	06.4	05.2	32	50	50	44	NE	2	SSW	1	NE	2
9	759.8	759.7	760.1	09.2	15.0	11.3	11.7	15.4	08.6	-	04.1	06.6	07.0	47	52	70	56	NE	2	SSW	1	NNE	1
10	759.9	758.7	758.5	08.7	14.7	11.7	11.7	15.0	08.3	-	05.2	07.1	07.2	61	56	69	62	NNE	3	SW	1	SE	1
11	758.4	757.7	758.0	08.9	14.4	11.2	11.4	14.5	08.6	-	05.5	05.8	06.4	64	47	65	59	ENE	1	SSW	1	NNE	2
12	757.7	757.7	758.0	08.9	14.4	11.2	11.4	14.6	08.3	-	04.3	07.8	08.5	50	63	85	66	NE	3	SW	1	ESE	1
13	759.1	759.2	759.6	09.0	14.2	11.2	11.4	14.4	08.1	-	05.5	07.8	07.4	64	64	74	67	NE	2	SSW	2	ENE	1
14	760.1	760.0	761.4	08.2	15.0	15.6	13.6	15.6	08.0	-	04.2	06.5	02.7	51	51	21	41	NE	2	SSW	2	NNE	2
15	761.8	762.1	762.3	12.4	16.2	12.6	13.3	16.4	12.0	-	02.3	04.8	04.9	21	35	45	34	NE	2	SSW	1	N	1
16	761.6	760.5	760.0	08.6	14.6	11.1	11.4	14.6	08.2	-	03.2	06.6	08.0	39	53	81	58	NNE	2	SSW	1	N	1
17	758.3	758.2	759.3	09.4	16.7	11.1	12.1	16.8	08.6	-	05.3	04.3	03.5	60	30	35	42	ESE	2	NNE	3	NNE	5
18	758.9	759.0	759.6	11.0	15.8	11.8	12.6	16.1	10.6	-	02.2	03.3	04.9	23	25	47	32	NE	4	SSW	2	ENE	2
19	760.2	759.5	759.0	08.7	13.8	11.2	11.2	14.1	08.2	-	03.0	04.5	04.2	36	38	42	39	NE	2	SSW	1	ENE	2
20	758.5	758.2	758.9	08.1	13.6	10.2	10.5	13.8	08.0	-	03.3	06.7	06.5	41	58	70	56	NE	3	SSW	1	NME	2
21	759.5	759.7	760.9	07.4	12.7	10.2	10.1	13.0	07.0	-	05.3	07.0	06.5	69	63	70	67	NNE	2	SSW	2	SW	1
22	762.3	762.8	764.0	09.9	15.5	13.2	13.0	15.6	09.0	-	04.5	06.9	05.3	49	52	47	49	NNE	2	SSW	1	NNE	2
23	763.2	762.5	762.5	10.0	15.5	12.8	12.8	15.6	10.0	-	03.7	06.0	04.5	40	46	41	42	NE	3	SSW	2	S	2
24	761.7	760.6	759.9	10.3	15.4	11.6	12.2	15.6	10.0	-	03.9	05.8	05.8	41	45	57	48	NE	3	SW	2	SW	1
25	757.6	755.3	754.3	09.0	13.1	11.7	11.4	14.4	08.6	-	05.3	08.3	08.2	62	74	80	72	ESE	2	SE	3	SSE	3
26	750.7	748.0	746.1	10.4	13.3	12.8	12.3	14.0	09.3	-	06.6	08.1	10.1	70	71	91	77	E	3	SE	5	SE	6
27	740.7	737.9	736.9	13.2	11.0	08.5	10.3	13.6	08.5	-	09.1	08.7	06.9	80	88	82	83	SSP	5	SE	4	NW	3
28	734.9	733.1	732.4	06.1	06.7	05.8	06.1	09.3	04.6	-	05.1	06.2	05.0	72	84	73	76	NE	4	ESE	4	NE	5
29	733.6	732.3	736.6	04.6	06.8	05.7	05.7	08.0	03.3	-	04.7	03.5	03.1	75	47	45	56	NE	6	NE	6	NE	5
30	739.4	742.7	746.0	06.0	09.7	06.1	07.0	10.0	05.4	-	03.4	03.7	03.2	48	41	45	45	NE	5	NE	4	NNE	2
MES.	PRED.			756.6	756.1	756.4	09.2	14.1	11.2	11.4	14.6	08.6	-	04.6	06.2	05.9	53	52	59	55	2.8	2.1	2.3

1	749.1	749.9	750.8	04.0	09.6	06.1	06.5	09.7	03.6	-	02.8	03.3	03.7	46	37	52	45	NE	3	ENE	1	NE	2
2	750.9	751.5	752.0	05.6	09.5	06.6	07.1	09.6	05.1	-	02.9	04.4	03.9	42	49	53	48	NE	1	WNW	1	NE	4
3	752.3	750.9	750.7	04.4	08.9	06.3	06.5	09.4	04.2	-	03.2	03.9	03.5	51	46	49	49	NE	2	ESE	1	NE	3
4	747.8	746.4	746.6	05.3	07.7	08.0	07.3	08.4	04.3	-	03.6	05.3	05.9	55	67	74	65	NE	3	ENE	2	NE	3
5	744.3	746.0	748.8	06.6	07.6	04.9	06.0	09.3	04.3	-	03.3	02.8	01.6	46	35	24	35	NE	6	NE	6	NE	5
6	750.6	750.3	751.7	04.2	07.0	03.4	04.5	07.3	03.4	-	01.5	01.8	01.8	24	25	31	27	NE	5	NE	5	NNE	3
7	751.7	751.7	753.3	00.0	05.8	04.0	03.5	06.2	-00.3	-	01.6	02.0	02.4	34	29	40	34	NE	3	SSW	1	WNW	1
8	753.9	753.9	754.2	03.6	06.4	04.0	04.5	06.8	01.7	-	03.0	03.6	05.1	51	50	84	62	NNE	1	ENE	1	ENE	2
9	750.2	749.6	751.1	07.0	07.0	08.2	07.6	08.3	03.3	-	07.1	07.0	06.9	95	93	85	91	E	4	NE	3	NNE	3
10	754.4	754.6	754.3	07.6	10.9	08.4	08.8	11.2	05.3	-	06.3	07.1	07.6	81	73	92	82	WSW	1	SE	1	SW	1
11	753.8	752.4	751.3	07.9	10.8	10.3	09.8	11.3	07.0	-	05.1	07.2	06.9	64	74	73	70	NNE	1	NNW	1	NNE	2
12	747.6	745.0	743.5	12.3	13.6	12.8	12.9	14.0	09.6	-	07.6	09.1	10.4	71	78	93	81	ESE	5	ESE	5	SSE	3
13	740.8	741.4	740.5	12.3	13.7	12.5	12.8	14.1	12.0	-	09.7	10.3	09.6	90	87	88	88	SSF	2	SE	1	ESE	5
14	734.8	736.5	736.6	12.7	14.2	11.4	12.4	15.4	11.3	-	10.5	05.7	05.8	96	47	58	67	WSW	2	W	3	NNE	1
15	738.9	742.7	745.6	09.2	11.9	10.7	10.6	12.2	08.2	-	07.4	08.0	07.5	85									

BR. ST. 87

 $H_s = 122 \text{ m } H_b = 128.0 \text{ m } h_t = 6.5 \text{ m } h_r = 1.0 \text{ m}$

D	T	Oblačnost N (0-10)					P	Podzemna voda h mm	Snožni pokrivač h cm	Razvoj vremene w	
		14	7	14	21	Sred Dnes					
1	7	010	050	02	32.7	09.6	
2	7	040	020	00	02.0	07.1	
3	7	08	040	02	04.7	04.9	
4	7	08	050	04	05.7	01.8	
5	7	05	050	00	03.3	07.2	
6	6	01	000	00	00.3	07.1	.	.	=0% n	.	
7	6	000	000	00	00.0	08.7	.	.	=n-14%	.	
8	7	000	000	00	00.0	08.4	
9	7	000	000	00	00.0	08.3	
10	5	000	000	00	00.0	08.3	.	.	=7% H%	.	
11	6	000	000	00	00.0	07.9	.	.	=7% n	.	
12	5	000	000	00	00.0	07.7	.	.	=7% n	.	
13	6	01	070	03	03.7	06.8	.	.	=7% n	.	
14	7	01	030	03	02.3	07.3	.	.	=7% g% =7% H%	.	
15	8	01	000	00	00.3	09.0	.	.	=0% n	.	
16	7	00	000	01	00.3	08.1	
17	8	05	030	00	02.7	08.1	
18	8	00	010	00	00.3	08.6	
19	7	08	040	00	04.0	07.4	
20	6	01	010	00	00.7	07.5	.	.	=0% n	.	
21	6	00	000	00	00.0	07.1	.	.	=n-n	.	
22	8	00	000	00	00.0	07.5	.	.	=n-g%	.	
23	8	00	000	00	00.0	08.4	
24	8	01	010	00	00.7	08.4	
25	6	01	09	07	05.7	03.6	.	.	=0% g%	.	
26	7	03	080	100	07.0	03.9	03.0	.	P=H=23, G=15-24%, R=13% n i	.	
27	6	09	10	100	09.7	00.0	13.9	.	G=15-22%, R=9%, P=9%, X=9%, Y=9%, Z=10%	.	
28	7	05	10	100	08.3	00.7	17.7	.	R=7%, G=7%, H=7%, P=7%, X=7%, Y=7%, Z=10%	.	
29	7	10	10	09	09.7	00.1	12.3	.	O=0-14%, Y=8%, P=6-8%, R=6-8%	.	
30	8	04	030	00	02.3	07.3	03.1	.	.	.	
MES.	RED.	02.6	03.0	02.0	02.5	196.8	47.0				

SPLIT-MARJAN

1978 DECEMBAR

1	8	01	050	00	02.0	06.2	
2	7	09	09	00	06.0	09.4	
3	8	01	010	00	00.7	08.3	
4	7	06	100	100	08.7	00.0	.	.	=0% g%	.	
5	8	05	020	00	02.3	06.1	01.8	.	=5% g%	.	
6	8	01	000	00	00.3	08.4	.	.	P=0-12%	.	
7	7	01	010	09	03.7	08.1	
8	7	08	10	100	09.3	00.0	.	.	=0% n	.	
9	6	100	100	02	07.3	00.0	13.5	.	=0% g%	.	
10	8	00	010	01	00.7	08.3	16.9	.	=1% g%	.	
11	7	04	09	03	05.3	03.7	.	.	=7% n	.	
12	7	08	10	09	09.0	00.4	.	.	P=14-15%, G=17-19%	.	
13	7	09	05	100	08.0	03.5	00.9	.	G=15-22%, R=22%	.	
14	8	09	08	100	09.0	04.6	13.1	.	O=0-0%, G=2-4%, R=10%	.	
15	8	100	010	09	06.7	05.6	04.9	.	O=0-7%, G=7%, R=7%, T=7%	.	
16	7	05	10	10	08.3	02.6	01.6	.	P=16%, R=16%	.	
17	8	04	050	00	03.0	06.1	00.6	.	P=0-0%, G=2-4%, R=4-6%, X=8%	.	
18	8	10	09	08	09.0	00.9	03.6	.	O=5-5%, R=5-5%, G=5-5%, P=5-5%, R=5-5%, X=5-5%	.	
19	7	090	09	100	09.3	00.0	01.6	.	O=5-5%, R=5-5%, G=5-5%, P=5-5%, R=5-5%, X=5-5%	.	
20	7	10	020	00	04.0	07.9	22.0	.	P=22%, G=22%	.	
21	8	03	09	01	04.3	03.5	.	.	P=22%, G=22%, R=17-19%	.	
22	8	06	09	100	08.3	00.7	.	.	O=14-15%, G=15-17%, R=6-8%	.	
23	7	100	03	03	07.7	00.0	07.2	.	O=3-7%	.	
24	7	090	09	10	09.3	03.6	05.1	.	O=3-7%	.	
25	7	10	100	100	10.0	00.0	00.0	.	O=7-9%	.	
26	8	100	09	01	06.3	12.3	12.0	.	O=1-2%	.	
27	7	08	10	02	06.7	00.0	10.4	.	O=7-9%	.	
28	6	09	100	01	09.7	00.0	.	.	P=5-5%, R=5-5%, G=5-5%	.	
29	8	09	080	10	09.0	04.0	03.6	.	P=5-5%, R=5-5%, G=5-5%	.	
30	8	08	09	01	05.7	15.1	01.6	.	O=2-2%	.	
31	6	18	100	02	16.7	00.0	.	.	P=5-5%, R=5-5%, G=5-5%	.	
MES.	RED.	06.8	17.1	05.2	06.3	177.3	107.4				

$\varphi = 43^{\circ}43' N$ $\lambda = 18^{\circ}16' E$ Gr. $\Delta G = + 1h\ 13\ min.$

BR. ST. 137

	Vazdušni pritisak P mm			Temperatura vazduha T °C								Napon vodenе pare e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0-12)					
	7	14	21	7	14	21	Sred Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dies	7	14	21			
1	582.0	587.8	590.0	-13.0	-12.8	-13.2	-13.1	-10.7	-13.4	-	01.5	01.5	01.5	88	88	88	88	N	13	N	13	N	13
2	594.0	596.3	596.0	-11.2	-08.0	-06.8	-08.2	-06.8	-13.2	-	01.8	02.3	02.6	90	92	94	92	N	9	N	5	NNW	6
3	599.4	593.4	591.0	-05.4	-03.4	-04.4	-04.4	-03.4	-06.8	-	02.9	03.5	03.2	95	97	96	96	NW	5	N	6	SW	7
4	587.6	587.3	588.2	-04.6	-09.4	-08.2	-07.6	-04.4	-10.3	-	03.1	02.1	02.3	96	91	92	93	SW	8	N	8	ENE	6
5	587.5	587.9	588.0	-12.9	-13.2	-16.4	-14.7	-08.2	-16.4	-	01.5	01.5	01.1	88	88	85	87	N	10	N	10	N	11
6	591.2	592.8	593.3	-19.3	-18.4	-16.6	-17.7	-16.4	-19.4	-	00.8	00.9	01.1	83	80	85	83	N	12	N	10	NNE	9
7	590.0	591.9	593.2	-13.4	-13.4	-14.6	-14.0	-13.0	-16.6	-	01.4	01.4	01.3	88	88	87	88	N	12	N	12	N	12
8	593.4	594.6	595.5	-15.4	-13.9	-11.6	-13.1	-11.6	-15.4	-	01.2	01.3	01.0	86	81	53	73	N	9	N	7	NE	6
9	595.2	595.3	595.2	-08.6	-04.2	-04.4	-05.4	-04.0	-11.6	-	00.8	01.0	01.4	32	29	41	34	NE	6	NNE	2	W	2
10	594.1	593.3	593.3	-05.4	-04.8	-05.9	-05.5	-03.8	-06.1	-	01.4	02.4	00.9	45	73	31	50	NW	2	-	0	-	0
11	590.9	587.9	585.3	-07.4	-06.4	-05.6	-06.3	-05.6	-07.4	-	02.0	02.7	02.9	74	94	95	88	S	6	SSW	8	SSW	12
12	584.8	584.7	587.9	-04.1	-02.6	-03.1	-03.2	-02.4	-05.6	-	03.3	03.7	03.5	96	97	97	97	SW	12	SSW	13	SW	14
13	590.9	593.5	595.6	-02.7	-01.8	-02.1	-02.2	-01.3	-03.4	-	03.7	03.9	03.8	97	98	98	98	SW	13	SW	12	SSW	7
14	594.8	595.4	595.2	-03.1	-03.1	-02.8	-03.0	-02.1	-03.1	-	03.5	03.5	03.6	97	97	96	97	SSW	8	SW	4	SSW	5
15	594.6	593.1	591.4	-02.4	-01.4	-01.7	-01.3	-02.8	-	03.6	04.0	04.0	94	97	97	96	SSW	5	S	7	SSW	7	
16	590.0	589.5	589.5	-02.6	-02.0	-02.4	-02.4	-01.4	-02.6	-	03.7	03.9	03.8	97	98	98	98	SSW	9	SSW	9	S	9
17	587.8	583.6	580.0	-01.0	-00.7	-01.2	-01.0	-00.7	-02.4	-	04.2	04.3	04.2	99	99	99	99	SE	6	S	7	S	13
18	585.2	586.8	587.2	-03.1	-02.9	-02.7	-02.9	-01.2	-03.7	-	03.5	03.6	03.7	97	97	97	97	SSW	7	SSW	4	SSW	4
19	586.4	585.6	584.8	-02.8	-01.5	-02.1	-02.1	-01.4	-02.8	-	03.6	04.0	03.8	97	99	98	98	SSW	4	S	4	-	0
20	583.9	584.1	583.9	-02.7	-02.2	-02.8	-02.6	-02.1	-02.9	-	03.7	03.8	03.6	97	98	97	97	-	0	SSW	5	SSW	8
21	583.7	582.9	583.9	-03.0	-02.6	-06.4	-04.6	-01.9	-06.6	-	03.6	03.7	02.6	97	97	90	95	E	7	ENE	6	E	4
22	584.2	585.0	586.3	-03.1	-02.7	-03.1	-03.0	-02.6	-07.0	-	03.5	03.7	03.5	97	97	97	97	SSW	7	SSW	7	SSW	6
23	587.4	588.8	589.2	-03.6	-03.8	-02.9	-03.3	-02.7	-04.8	-	03.4	03.3	03.6	97	96	97	97	-	0	NE	2	S	3
24	588.4	584.4	583.0	-02.4	-02.4	-04.0	-03.2	-02.2	-04.0	-	03.8	03.8	03.3	98	98	96	97	SW	5	SW	12	SW	11
25	580.5	582.1	584.8	-04.3	-03.8	-09.0	-06.5	-03.0	-09.0	-	03.2	03.3	02.1	96	96	92	95	SW	13	NW	5	N	8
MES. VRFD.	588.0	588.1	588.3	-06.2	-05.6	-06.1	-06.0	-04.4	-08.0	-	02.7	02.9	02.7	89	91	89	90	7.3	7.4	7.4	7.3		

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1	585.6	585.0	585.0	-10.6	-05.7	-04.1	-06.1	-04.1	-10.9	-	01.8	02.8	03.3	90	95	96	94	-	0	SW	6	SW	6
2	583.0	581.1	581.6	-04.7	-04.4	-08.6	-06.6	-04.0	-08.6	-	03.1	03.2	02.2	95	96	92	94	SW	5	SW	6	N	5
3	582.0	583.6	585.8	-10.8	-09.3	-10.0	-10.0	-08.6	-10.8	-	01.8	02.1	01.9	90	91	91	91	N	7	N	7	N	6
4	586.8	588.0	589.4	-10.4	-09.2	-10.4	-10.1	-09.1	-10.4	-	01.9	02.1	01.9	90	91	90	90	N	8	N	7	N	7
5	589.0	588.0	587.3	-10.8	-09.6	-10.1	-10.2	-04.4	-10.8	-	01.8	02.0	01.9	90	91	91	91	N	6	E	5	N	5
6	584.0	583.5	583.0	-09.3	-06.7	-10.3	-09.2	-06.6	-10.3	-	02.1	02.6	01.9	91	94	90	92	N	6	NE	5	NNE	4
7	581.5	581.3	581.2	-11.8	-10.1	-11.9	-11.4	-10.0	-11.9	-	01.7	01.9	01.6	89	91	89	90	N	7	N	6	N	5
8	580.0	580.2	580.5	-13.9	-11.6	-12.2	-12.5	-10.3	-14.1	-	01.4	01.7	01.6	87	89	89	88	N	3	N	2	E	2
9	581.3	582.6	584.3	-08.4	-04.8	-06.0	-06.3	-04.6	-12.2	-	02.2	03.1	02.8	92	95	94	94	S	5	SW	6	SW	7
10	585.3	584.0	582.8	-05.0	-04.1	-04.9	-04.7	-03.7	-06.8	-	03.0	03.3	03.0	95	96	95	95	SW	8	SW	12	SSW	13
11	579.1	579.8	578.9	-03.2	-01.1	-02.1	-02.1	-01.0	-04.9	-	03.5	04.2	03.8	97	99	98	98	SSW	13	SSW	13	SSW	13
12	579.4	581.9	583.3	-04.6	-04.0	-02.8	-03.6	-02.1	-04.6	-	03.1	03.3	03.6	96	96	97	96	SSW	12	SSW	10	SSW	11
13	582.0	582.5	582.5	-03.0	-02.0	-02.3	-02.4	-01.8	-03.0	-	03.6	03.9	03.8	97	98	98	98	SSW	8	SSW	7	-	0
14	576.8	578.3	580.4	-07.7	-09.0	-08.3	-08.3	-02.3	-09.0	-	02.4	02.1	02.3	93	92	92	92	N	8	N	6	SW	2
15	580.3	581.3	583.2	-11.6	-13.7	-15.8	-14.2	-07.7	-15.8	-	01.7	01.4	01.1	89	85	82	85	NW	6	NNW	7	NNW	7
16	583.5	582.1	579.5	-15.6	-06.8	-06.8	-09.0	-06.4	-15.9	-	01.1	02.6	02.6	83	94	94	90	NNW	2	SW	9	SSW	11
17	582.3	584.4	583.6	-06.9	-05.5	-04.2	-05.2	-04.2	-07.0	-	02.6	02.9	03.2	93	95	96	95	SSW	10	SSW	4	SW	7
18	583.7	586.1	588.0	-02.3	-08.9	-12.0	-08.8	-02.3	-12.0	-	03.8	02.1	01.6	98	92	89	93	SSW	8	NNW	7	N	4
19	587.4	586.7	584.7	-05.2	-04.2	-01.9	-03.3	-01.9	-12.0	-	03.0	03.2	03.9	95	96	98	96	SW	9	SSW	10	SSW	12
20	585.2	586.7	588.5	-01.5	-01.8	-13.4	-07.5	-00.7	-13.4	-	04.0	03.9	01.4	99	98	88	95	NW	5	N	1</		

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BR. ST. 137

$$H_s = 2067 \text{ m } H_b = 2070,4 \text{ m } h_t = 3,0 \text{ m } h_r = 1,5 \text{ m}$$

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1	8	10≡	00○	00≡	03.3	07.0	05.8	171	*0-4≡, V0-24, =0-8≡, 15≡, 24, P0-24, f ² , 17≡, 24, □
2	7	01	09	10≡	06.7	03.0	.	164	V0-24, =0-25, 9≡, 15≡, 15≡, 24, 20≡, 24, P0-24, f ² , 0-3≡, 14≡, 20, P0-24, f ² , 15≡, 20, □
3	0	10≡	10≡*	10≡*	10.0	00.0	.	155	V0-24, =0-24, P0-24, f ² , 0-24, *8≡, 24, □
4	0	10≡*	10≡*	10≡*	10.0	00.0	09.1	164	V0-24, =0-24, *0-23, P0-24, □
5	1	10≡	10≡	10≡	10.0	03.8	06.4	172	V0-24, =0-24, P0-24, □
6	0	10≡	10≡	10≡	10.0	00.0	.	170	V0-24, =0-24, P0-1020, □
7	0	10≡*	10≡*	10≡*	10.0	00.0	01.3	165	V0-24, =0-24, P0-24, f ² , 15≡, 24, f ² , 15≡, 24, □
8	0	10≡	10≡	10≡	10.0	00.0	09.9	179	V0-24, =0-24, *0-3≡, 8≡, 10≡, 14≡, 15≡, 20, □
9	0	10≡*	10≡*	10≡*	10.0	00.0	04.0	185	V0-24, =0-24, *0-24, P0-24, f ² , 13≡, 24, □
10	0	02	10≡	10≡	07.3	01.4	02.8	184	V0-24, =0-5≡, 10≡, 24, *0-1≡, P0-24, f ² , 0-24, *5≡, 10≡, □
11	1	10≡*	10≡	10≡	10.0	00.0	06.0	187	V0-24, =0-24, P0-24, f ² , 0-24, *4≡, 7≡, 24, □
12	0	10≡	10≡*	10≡*	10.0	00.0	02.0	186	V0-24, P0-24, =0-24, f ² , 0-24, *14-24, □
13	0	10≡*	10≡*	10≡*	10.0	00.0	34.0	210	V0-24, =0-24, P0-24, f ² , 0-17, 23≡, 24, *0-24, f ² , 0-17, □
14	1	10≡*	10≡*	10≡*	10.0	00.0	22.0	225	V0-24, =0-16≡, 16≡, 24, *0-4≡, P0-24, f ² , 0-4≡, P0-24, f ² , 0-4≡, □
15	0	10≡*	10≡*	10≡	10.0	00.0	09.0	232	V0-24, =0-24, *0-14≡, P0-24, f ² , 6≡, 24, f ² , 9-24
16	8	00○	09	10≡	06.3	02.3	01.6	233	V0-24, =0-2, 15≡, 24, f ² , 0-10, P0-24, f ² , 0-8, 9-24
17	0	10≡	10≡	10≡	10.0	00.0	.	231	V0-24, =0-24, P0-24, f ² , 0-10, *14-13, □
18	8	10≡	10	00	06.7	01.4	00.7	228	V0-24, =0-13, P0-24, f ² , 0-10, *14-5, 10≡, 12, f ² , 0-15, 14≡, 15, P0-24, f ² , 0-13-14, □
19	0	09	10≡	10≡*	09.7	00.0	00.4	226	V0-24, P0-24, f ² , 0-14, f ² , 0-8, 5≡, 24, *5≡, 24, *14-24, □
20	1	10≡	10≡	10≡	10.0	00.0	09.9	220	V0-24, =0-22, P0-22, f ² , 0-5, 6≡, 24, f ² , 0-4≡, P0-24, f ² , 0-4≡, *14-24, *0-14≡, 14≡, 20, 24, 23≡, 24, □
21	9	00○	00○	01	00.3	10.9	07.3	223	V0-24, P0-24, 0-5≡, 14≡, 6≡, f ² , 0-23, P0-24, 0-9≡, 13≡, 24, □
22	9	08	00○	00	02.7	10.4	.	213	V0-5≡, P0-24, f ² , 0-10, P0-24, f ² , 14≡, 24, □
23	8	04○	06	02	04.0	07.4	.	200	P0-24, 24, □
24	8	08	09	10	09.0	30.9	.	190	P0-24, □
25	8	10	08	10≡	09.3	01.6	.	170	P0-24, =18≡, 24, □, 19≡, 24, f ² , 19≡, 22≡, □
26	0	10≡	10≡*	10≡	10.0	00.0	02.3	159	P0-24, f ² , 0-24, =0-24, V0-10≡, 23≡, 24, P0-24, f ² , 17≡, 19≡, □
27	0	10≡	10≡	10≡	10.0	00.0	09.7	150	P0-24, =0-24, V0-9≡, *25≡, 5≡, 10≡, f ² , 25≡, 10≡, V0-24, P0-11≡, 13≡, □
28	0	10≡	10≡*	10≡*	10.0	00.0	02.6	152	P0-24, =0-24, V0-24, f ² , 10≡, 20≡, 23≡, f ² , 13≡, 24, □

$\varphi = 43^{\circ}43' N$ $\lambda = 18^{\circ}16' E$ Gr. $\Delta G = + 1h\ 13\ min.$

BR. ST. 137

d	Vazdušni pritisak P mm			Temperatura vazduha T °C								Napon vodenih parova e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0-12)					
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21			
												7	14	21	7	14	21						
1	588.6	589.4	590.8	-00.8	-00.4	-01.0	-00.8	-00.3	-01.6	-	04.3	04.4	04.2	99	100	99	99	SSW	7	SW	5	SW	5
2	590.9	591.7	592.0	-02.4	-00.5	00.3	-00.6	00.3	-02.6	-	03.8	04.2	04.5	98	95	95	96	SW	5	SW	2	SW	2
3	591.4	591.0	591.0	-01.6	01.4	01.1	00.5	01.4	-01.6	-	03.9	04.3	04.7	95	84	94	91	-	0	S	2	S	4
4	590.2	590.3	590.7	01.4	02.6	01.4	01.7	02.6	01.0	-	04.8	04.8	04.5	94	86	88	89	SSW	6	SSW	6	SSW	7
5	589.4	588.9	589.6	01.0	02.4	01.3	01.5	02.7	00.6	-	04.5	04.7	04.8	91	86	96	91	SW	9	S	10	S	10
6	589.8	589.3	588.3	01.3	01.4	00.4	00.9	01.6	00.4	-	05.0	05.0	04.7	100	99	100	100	S	8	E	4	E	5
7	589.3	590.5	591.0	-01.7	00.8	-03.2	-01.8	00.9	-03.2	-	04.0	04.9	03.5	98	100	97	98	S	6	SW	3	W	2
8	590.0	590.2	590.5	-09.8	-03.2	-03.9	-05.2	-02.7	-09.8	-	02.0	03.5	03.3	91	97	96	95	NNW	4	SW	2	WSW	4
9	590.0	590.0	589.2	-05.0	-24.2	-06.8	-05.7	-03.9	-06.8	-	02.4	02.4	02.6	75	71	94	80	N	2	N	3	N	9
10	589.4	589.3	589.5	-08.7	-08.0	-09.0	-08.7	-06.8	-09.3	-	02.2	02.3	02.1	92	92	92	92	N	12	N	11	N	12
11	591.1	590.3	589.2	-09.3	-05.1	-04.0	-05.6	-04.0	-09.4	-	02.1	03.0	03.3	91	95	96	94	N	9	N	10	N	10
12	583.5	587.5	588.0	-09.4	-10.4	-11.0	-10.5	-04.0	-11.0	-	02.1	01.9	01.8	91	90	90	90	N	13	N	11	N	10
13	590.6	592.4	593.5	-11.6	-06.8	-04.0	-06.6	-04.0	-11.8	-	01.7	02.4	02.4	89	87	71	82	N	3	W	2	NW	5
14	594.2	592.6	592.4	-04.0	-02.2	-02.8	-03.0	-01.8	-04.3	-	02.9	03.0	03.0	85	78	80	81	SW	3	SW	8	SSW	11
15	590.6	589.0	588.8	-02.8	-01.4	-03.8	-03.0	-01.2	-03.8	-	03.6	04.1	03.3	97	99	96	97	SSW	8	SSW	8	SW	7
16	590.3	590.0	588.0	-06.6	-01.2	-02.2	-03.1	-01.0	-06.6	-	02.6	04.0	03.8	94	96	98	96	N	7	SW	10	SW	9
17	582.2	583.1	585.0	-03.4	-02.6	-01.8	-02.4	-01.8	-04.0	-	03.5	03.7	03.9	97	97	98	97	SW	13	SW	15	SW	11
18	586.3	587.0	590.0	-02.8	-02.8	-04.6	-03.7	-01.6	-04.6	-	03.6	03.6	03.1	97	97	96	97	SW	8	SW	10	SW	7
19	590.4	589.2	588.6	-06.2	-04.4	-08.0	-06.7	-04.2	-08.0	-	02.7	03.2	02.3	94	96	92	94	SW	4	SW	3	N	4
20	588.0	585.5	585.0	-11.2	-03.6	-04.2	-05.8	-03.2	-11.4	-	01.8	03.4	03.2	90	97	96	94	N	8	SW	11	SSW	11
21	578.3	580.5	578.6	-04.0	-01.6	-07.5	-05.2	-01.0	-07.5	-	03.3	04.0	02.4	96	98	93	96	SW	13	W	4	N	11
22	576.8	579.8	584.0	-09.0	-10.0	-09.9	-09.7	-07.5	-10.0	-	02.1	01.9	02.0	92	91	91	91	N	13	N	11	N	14
23	588.3	588.8	587.4	-12.7	-09.9	-05.0	-08.2	-04.8	-12.7	-	01.5	02.6	03.0	88	91	95	91	N	7	SW	4	SSW	9
24	578.8	581.4	582.3	-05.2	-04.5	-05.9	-05.4	-03.9	-05.9	-	03.0	03.1	02.8	95	96	94	95	SSW	13	SW	7	N	2
25	582.5	584.1	587.2	-09.8	-08.8	-07.6	-08.5	-05.9	-09.8	-	02.0	02.2	02.4	91	92	93	92	N	10	N	11	N	11
26	588.7	589.1	588.6	-09.4	-08.1	-07.0	-07.9	-06.8	-09.4	-	02.1	02.3	02.5	91	92	93	92	N	8	NW	1	-	0
27	586.0	587.9	590.6	-08.0	-07.9	-08.2	-08.1	-06.7	-08.4	-	02.3	02.3	02.3	92	93	92	92	N	8	N	9	N	7
28	592.0	594.4	595.7	-09.0	-05.2	-04.0	-05.6	-04.0	-09.4	-	02.1	03.0	03.3	92	95	96	94	N	9	N	7	N	5
29	595.9	596.1	596.0	-04.0	-01.6	-01.2	-02.0	-01.2	-04.3	-	03.3	03.9	04.1	96	97	97	97	N	5	N	2	SE	1
30	594.1	593.7	592.5	-02.1	-01.0	-00.5	-01.0	-00.4	-02.1	-	03.8	04.2	04.4	96	97	98	97	SSW	3	SSW	3	SSW	3
31	590.6	589.9	589.8	-00.7	00.2	-00.3	-00.3	00.3	-01.1	-	04.2	04.5	04.5	97	97	100	98	SSE	5	SSW	8	SSW	8
MES.				588.3	588.8	589.2	-05.4	-03.4	-04.0	-04.2	-02.4	-06.1	-	03.0	03.4	03.3	93	93	94	93	7.2	6.5	7.0

1978 APRIL

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1	588.4	587.0	585.5	-01.2	-00.9	-01.2	-01.1	00.4	-01.2	-	03.9	04.2	04.2	94	97	100	97	SSW	7	NE	2	N	4
2	583.8	584.2	585.0	-02.6	00.7	00.3	-00.3	00.9	-02.6	-	03.8	04.8	04.7	100	100	100	100	N	2	-	0	S	4
3	585.3	585.0	583.2	00.1	01.6	-00.7	00.1	02.7	-00.7	-	04.5	04.5	04.4	97	88	100	95	-	0	E	2	NNE	8
4	582.6	583.6	586.0	-01.6	-01.4	-02.3	-01.9	-00.7	-02.3	-	04.1	04.1	03.8	100	100	98	99	N	7	N	7	N	7
5	587.0	587.3	588.0	-01.9	00.4	00.1	-00.3	00.8	-02.4	-	03.9	04.7	04.6	98	100	100	99	E	3	S	4	SW	6
6	589.0	590.4	590.2	-03.0	-02.0	-04.2	-03.4	00.1	-04.2	-	03.6	03.9	03.2	97	98	96	97	NW	5	N	3	N	7
7	589.0	587.3	584.4	-07.2	-06.2	-01.6	-04.2	-01.6	-07.4	-	02.5	02.7	04.0	93	94	98	95	NE	7	E	6	S	8
8	583.0	583.9	584.8	-01.6	00.4	00.1	-00.3	00.6	-01.7	-	04.0	04.7	04.6	98	100	100	99	S	7	S	6	S	5
9	585.8	587.3	588.2	00.0	03.4	01.6	01.7	03.4	00.0	-	04.6	05.8	05.1	100	100	100	100	E	3	SE	3	S	3
10	588.3	589.4	589.5	-00.3	02.4	-01.1	00.0	02.6	-01.1	-	04.5	05.4	04.2	100	100	99	100	S	6	SSW	7	SSW	8
11	589.7	590.5	591.2	-02.4	-01.0	-01.4	-01.6	-00.8	-02.4	-	03.8	04.8	04.1	98	100	99	99	SW	8	SW	11	SSW	9
12	588.3	590.6	588.8	-01.1	01.8	01.0	00.7																

BR. ST. 137

$$H_s = 2067 \text{ m } H_b = 2070,4 \text{ m } h_t = 3,0 \text{ m } h_x = 1,5 \text{ m}$$

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1978 APRIL

$\varphi = 43^{\circ}43' N$ $\lambda = 18^{\circ}16' E$ Gr. $\Delta G = + 1h 13 min.$

BR. ST. 137

d	Vazdušni pritisak P mm			Temperatura vazduha T °C°								Napon vodenе pare • mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0-12)			
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21	
1	588.3	586.7	586.3	02.3	05.2	03.2	03.5	05.2	01.6	-	03.0	03.4	05.8	56	51	100	69	SSW 11	SSW 11	SSW 8	
2	580.7	580.3	585.0	03.0	00.1	-01.2	00.2	03.4	-01.2	-	05.7	04.6	04.2	130	100	99	100	SSW 7	WSW 7	SW 9	
3	589.8	592.5	594.3	-00.3	01.1	00.1	00.3	01.4	-01.2	-	04.5	05.0	04.3	100	100	94	98	SW 7	SW 7	SW 6	
4	595.8	596.9	597.5	01.4	03.1	02.6	02.4	03.5	-00.4	-	02.2	04.1	04.0	44	71	72	62	WSW 5	SW 5	N 3	
5	597.6	598.0	597.0	03.6	07.4	05.4	05.5	07.4	02.3	-	04.0	03.7	04.3	68	48	64	60	SW 4	S 4	S 6	
6	594.4	593.7	590.8	04.2	04.1	02.2	03.2	05.4	02.0	-	02.7	03.1	05.4	44	51	100	65	SSW 9	SSW 10	S 10	
7	586.3	587.6	587.9	01.2	01.7	01.1	01.3	02.4	01.1	-	05.0	05.2	05.0	100	100	100	100	S 11	S 7	SW 5	
8	587.0	587.0	587.3	00.8	02.9	00.3	01.1	03.9	00.2	-	04.9	05.6	04.7	130	100	100	100	S 3	S 4	SW 2	
9	588.1	589.3	591.0	00.0	02.4	00.2	00.7	02.8	00.0	-	04.6	05.1	04.7	100	94	100	98	NW 3	SW 6	SW 6	
10	591.7	593.1	593.8	00.6	01.2	-00.2	00.4	02.1	-00.3	-	04.8	05.0	04.5	100	100	100	100	SW 5	SW 5	N 3	
11	592.4	591.8	591.1	-04.0	-03.4	-06.4	-05.1	-00.2	-06.4	-	03.3	03.5	02.7	96	97	94	96	N 5	N 5	N 6	
12	588.5	588.3	588.6	-11.0	-08.6	-06.0	-07.9	-06.0	-11.0	-	01.8	02.2	02.8	90	92	94	92	N 5	N 6	SW 3	
13	588.4	586.5	584.3	-02.4	-01.6	-00.4	-01.2	-00.4	-08.2	-	03.6	03.9	04.5	94	95	100	96	SW 6	SSW 9	SSW 11	
14	586.6	589.4	590.7	-01.8	-00.2	-01.2	-01.1	00.6	-01.8	-	03.9	04.5	04.2	98	100	99	99	WSW 5	SW 4	SW 3	
15	590.8	590.7	591.0	-01.4	00.8	-00.2	-00.3	01.8	-02.2	-	04.1	03.7	04.4	99	76	98	91	-	0	SW 8	SW 3
16	591.7	592.9	594.8	-01.8	03.0	01.0	00.8	03.0	-01.8	-	03.4	04.3	04.9	85	76	100	87	WSW 3	SW 4	- 0	
17	595.0	596.0	595.2	02.4	04.4	03.8	03.6	04.4	00.3	-	04.4	04.5	06.0	80	72	100	84	SW 2	SW 4	SW 7	
18	595.5	595.8	596.2	02.8	05.4	05.0	04.6	05.6	02.2	-	05.1	06.2	05.7	92	92	87	90	SW 6	SW 6	SW 6	
19	594.4	594.9	594.4	03.4	07.0	35.0	05.1	07.6	03.0	-	05.2	06.5	05.9	89	86	90	88	SSW 3	SW 6		
20	593.7	594.5	595.4	04.8	07.8	06.8	06.6	08.0	04.6	-	06.3	06.8	05.7	97	86	77	87	SW 5	SW 5	SW 3	
21	595.3	596.1	595.8	07.4	08.2	06.6	07.2	08.6	04.8	-	04.6	06.9	06.3	60	84	86	77	SW 3	SSW 3	S 8	
22	590.7	590.8	586.9	06.0	04.8	03.8	04.6	06.8	03.8	-	05.8	06.1	05.7	83	95	95	91	S 8	S 11	S 8	
23	586.4	588.1	589.3	02.8	02.6	02.4	02.6	03.9	02.2	-	05.3	05.2	05.3	94	94	97	95	SSW 9	SSW 9	SSW 8	
24	590.7	591.5	593.0	01.8	04.0	03.6	03.3	04.8	01.8	-	05.1	05.8	05.5	97	95	92	95	SW 6	SSW 8	SW 5	
25	592.5	593.2	593.8	01.0	04.4	03.0	02.9	05.5	00.8	-	04.8	05.6	05.5	97	90	97	95	-	0	WSW 2	N 5
26	593.3	595.0	595.0	02.0	02.8	01.2	01.8	03.5	00.8	-	05.3	05.4	05.0	100	97	100	99	NNW 6	N 2	N 4	
27	594.8	593.9	593.2	00.6	-00.2	-00.8	-00.3	01.4	-00.8	-	04.8	04.5	04.3	100	100	99	100	N 3	NE 1	NE 5	
28	592.1	593.1	593.0	00.0	00.0	-00.1	-00.1	00.5	-01.0	-	04.6	04.6	04.5	100	100	100	100	NNE 5	NNW 7	NNW 7	
29	591.8	590.8	591.0	-00.2	-00.2	00.2	00.0	01.5	-00.6	-	04.5	04.5	04.7	100	100	100	100	N 6	NNE 11	N 7	
30	591.0	593.3	594.9	00.0	01.0	01.8	01.2	01.8	-00.6	-	04.6	04.9	05.2	130	100	100	100	NNE 5	NNE 3	E 4	
31	596.6	597.0	597.7	01.2	04.2	03.8	03.3	05.0	00.9	-	05.0	06.0	05.9	100	97	97	98	NE 4	ENE 2	E 3	
MES.	VRED.	591.4	591.9	592.1	01.0	02.4	01.5	01.6	03.4	-00.2	-	04.4	04.8	04.9	89	88	94	91	5.2	5.8	5.5

1	598.5	599.0	599.2	04.0	04.6	04.8	04.6	06.1	03.3	-	05.8	05.9	06.3	95	92	97	95	ENE 2	N 4	N 4	
2	598.4	598.4	597.5	04.6	06.6	04.6	05.1	07.2	04.2	-	05.7	05.3	05.8	90	73	91	85	NNE 6	N 4	N 6	
3	596.3	597.2	597.8	04.0	07.4	05.4	05.6	07.5	03.7	-	06.1	05.3	06.1	100	69	91	87	N 8	N 6	N 6	
4	598.4	599.4	599.7	07.8	10.0	07.9	08.4	10.1	05.0	-	06.2	06.2	05.5	78	68	68	71	-	0	N 2	
5	599.7	599.9	600.0	07.9	10.3	09.2	09.2	11.1	06.8	-	05.6	05.4	05.9	70	57	68	65	-	0	NNW 4	
6	599.5	599.0	599.0	10.2	11.6	09.0	10.0	12.4	08.0	-	07.0	06.4	06.4	75	63	75	71	-	0	N 2	SW 3
7	599.0	599.7	599.5	10.3	13.0	10.8	11.2	13.4	07.7	-	05.7	06.2	07.0	60	56	72	63	-	0	SW 5	SW 4
8	598.0	598.3	598.0	09.4	11.3	09.0	09.7	11.9	08.6	-	06.0	07.3	06.9	68	73	80	74	W 5	W 6	W 6	
9	597.4	598.2	598.0	05.3	09.6	09.8	08.6	10.8	05.3	-	06.5	06.7	07.1	97	74	79	83	N 6	N 3	SW 3	
10	597.8	598.1	597.9	11.3	15.4	10.2	11.8	15.4	08.8	-	06.9	08.1	07.4	69	62	79	70	SW 3	SW 2	SSW 8	
11	598.3	599.5	599.5	09.6	14.0	11.4	14.2	09.0	-	07.6	09.5	07.8	85	79	79	81	SW 7	SW 6	SW 6		
12	597.1	594.7	593.0	11.4	13.0	08.8	10.5	14.8	08.8	-	05.9	06.7	07.7	59	59	91	70	S 7	SSW 9	SSW 7	
13	591.5	592.2	592.8	08.8	08.0	07.0	07.7	09.0	06.3	-	08.3	08.0	07.5	98	100	100	99	SSW 8	SSW 4	SW 5	
14	591.7	592.8	592.6	07.0	08.6	05.6	06.7	09.0	05.6	-	07.5	06.9	06.1	100	82	90	91	SW 4	SW 6	SW 6	
15	592.3	591.8	590.0	05.0	07.6	04.6	05.5	07.7	04.6	-	06.4	07.5	06.4	97	95	100	97	SSW 7	WSW 4	- 0	
16	586.4	589.5	590.0	05.4	06.6	06.0	06.0	07.2	02.2	-	06.2	07.0	06.8	92	95	98	95	-	0	- 0	SW 7
17	501.1	592.3	592.5	06.4	06.6	06.0	06.3	07.4	05.2	-	07.3	07.1	06.8	98	98	98	98	SSW 7	SSW 6	SSW 7	
18	592.9	596.5	597.5	06.2	08.2	06.3	06.8	08.3	06.0	-	06.9	07.4	06.0	9							

BR. ST. 137

$$H_s = 2067 \text{ m } H_b = 2070,4 \text{ m } h_t = 3,0 \text{ m } h_r = 1,5 \text{ m}$$

Den	Výška 0-9	Obločnost N (0-10)					R mm	Podzemní R mm	Snožní pokrývka h cm	Rozvoj vremena w
		14	7	14	21	Sred Dies				
1	8	06○	05○	10=*	07.0	07.5	00.6	110	■■ 0-24, = 50° 9, ≡ 17° 24, ○ 10° 24, □	
2	1	10=*	10=*	10=*	10.0	00.0	47.4	94	≡ 0-24, ■ 0-24, ○ 0-10°, □ 7-3, ♀ 5-6*, ♀ 8-9*, * 12-19°, □	
3	0	10=	10=	00	06.7	00.0	14.7	92	≡ 0-20°, ■ 0-22°, □	
4	9	04○	09	00	04.3	06.5	.	88	□	
5	8	02○	06○	04	04.0	09.3	.	82	■■ 20° 24, □	
6	8	05	10	10=*	08.3	00.9	.	73	■ 0-24, ○ 14° 24, ≡ 15-24, □	
7	0	10=*	10=*	10=*	10.0	00.0	11.3	64	≡ 0-23, ■ 0-12, ○ 0-16°, □	
8	0	10=	10=*	10=*	10.0	00.0	01.9	59	■ 0-8°, ≡ 3-24, ♀ 8-9*, * 10-24, □	
9	7	10=	09*	10=	09.7	01.4	10.7	62	≡ 0-23, ○ 2-10°, □ 20, 23-24; ■ 0-26, 12-24, ♀ 4-15, ○ 15-16°, □	
10	0	10=	10=*	10=*	10.0	00.0	00.9	59	≡ 0-24, □ 0-25, * 10-24, ○ 15-16°, □	
11	0	10=*	10=*	10=*	10.0	00.0	13.3	74	≡ 0-24, ○ 10°, 19° 21°, ■ 3-5, H 24, V 10° 24, □ H-13°, ○ 10° 11°, □ 10°, □	
12	0	10=*	10=	00	06.7	02.1	04.4	74	≡ 0-19°, ■ 0-16°, V 0-24, □ 20° 40°, □ 6° 13°, □	
13	0	00○	10=*	10=*	06.7	00.0	00.6	70	▽ 0.9°, ■ 0-24, ≡ H 20, 20° 24, □ 12-24, □ 12-24, □ 12-24, □ 12-24, □	
14	3	10=*	09*	10=	09.7	04.2	38.2	89	≡ 0-24, □ 0-25, 0-26, 0-27, 0-28, 0-29, 0-30, 0-31, 0-32, 0-33, 0-34, 0-35, 0-36, 0-37, 0-38, 0-39, 0-40, V 10-24, □	
15	8	06○	06○	01	04.3	08.9	00.6	79	≡ 0-6°, V 0-8°, 0-10°, 0-12°, □ 12-19°, □	
16	8	05○	06○	10	07.0	08.8	.	67	* 10° 12°, ≡ 21° 22°, □	
17	8	01○	09○	10	06.7	10.0	00.3	59	■ 0-4-9°, ■ 10° 24, ≡ 21° 23°, □	
18	8	09	10	06	08.3	02.2	00.0	53	■ 0-24, ○ 3-7, 7-24, ≡ 9° 13°, □	
19	8	10	08○	04	07.3	08.1	00.0	50	■ 0-6, 10-24, ≡ 11-22, □	
20	8	10=	06○	05	07.0	05.6	01.0	49	■ 0-23, ○ 0-24, 0-25, ≡ 3-13°, □ 9-24 H, □ 10°-10°, □ 17-22, □ 20°, □	
21	8	05○	09	08	07.3	04.7	05.2	43	■ 0-24, 9-11, 20° 24, ♀ 27-32, □	
22	0	10	10=*	10=*	10.0	00.0	.	35	■ 0-24, ○ 9-10°, ≡ 9-24, □	
23	0	10=*	10=	10=	10.0	00.0	21.5	33	○ 0-12°, 17-24, ≡ 0-24, * 13-35, ■ 3-24, # 11°, □	
24	1	10=	10=	04	08.0	01.0	03.8	30	≡ 0-24, ■ 0-24, ○ 0-12°, □	
25	3	10=*	10=	10=	10.0	00.0	12.4	27	○ 3-6°, 14-22, ♀ 6-7, ♀ 7-10°, ≡ 9-24, □ 7-11, ♀ 7-11°, □	
26	0	10=	10=	10=	10.0	01.5	01.6	26	≡ 0-24, □ 0-12, ○ 5-16°, □	
27	0	10=	10=*	10=	10.0	00.0	01.3	26	≡ 0-24, ○ 10-14°, ≡ 10-15°, □	
28	0	10=	10=	10=	10.0	00.0	02.3	27	≡ 0-24, ■ 0-24, * 12-24, □ 12-24, □	
29	0	10=	10=	10=	10.0	00.0	14.7	28	≡ 0-24, ■ 0-24, □ 0-16°, □ 18-21, ♀ 21-24, * 22-23°, □	
30	0	10=	10=*	12=	10.0	00.0	01.3	28	≡ 0-24, ■ 0-9, ♀ 13-14°, □	
31	8	10=	09○	06	08.3	03.2	00.0	28	≡ 0-24, □ 10-13°, ○ 13-14°, □	

BJELAŠNICA

1978 JUN

1	7	10≡	05	10≡	08.3	06.3	00.0	22	≡≡ 6 ¹⁵ 10.17 ²⁰ 24, # ¹⁴ 10.17 ²⁰ T 16.17 ²⁰ , △ 16 ²⁰ 17 ²⁰ , ▲ 16 ²⁰ 18 ²⁰ , □ 17 ²⁰ 18 ²⁰ , ▨
2	8	08	04○	10	07.3	09.7	02.1	19	≡ 0.40 21 ²⁰ 24, □ 0.24 # ^{0.04} 14 ²⁰ 12, △ 19 ²⁰ 19 ²⁰ , ▲ 23 24, ▨
3	8	10≡	08○	00≡	06.0	06.7	00.1	18	≡≡ 0.8-20 23, □ 0.24 # ^{0.04} 18 20, △ 8-12, 17 ²⁰ 20, T 18 ²⁰ 18, ▨ 15 ²⁰ 16 ²⁰
4	8	00○	08○	00	02.7	09.9	00.0	17	# ^{0.04} 2.9, = 5.9, T 12 ²⁰ 14 ²⁰ , ▨
5	8	08○	06○	00	04.7	11.2	.	13	# ^{0.04} 5.8-20 T 14 ²⁰ 14 ²⁰ , ▨
6	8	04○	08	02	04.7	07.2	.	10	# ¹⁴ 5.9 15 17, = 5.9, ▨
7	8	02○	04○	01	02.3	13.2	.	08	# ^{0.04} 9.12 13 ²⁰ , ▨
8	8	09	08	09	08.7	02.9	.	06	□ 2-24, ▲ 20-22, ▨
9	8	10≡	06○	02	06.0	05.3	01.6	14	# ¹⁴ 3-12, □ 3.9 # ^{3.56} 530 ≡ 6-9 ¹⁰ , ▨
10	8	00○	06	05	03.7	10.3	.	12	# ¹⁴ 5.8 ²⁰ □ 14 ²⁰ 24, ▨
11	1	05○	10≡	04	06.3	05.9	.	01	□ 0-24, □ 13 ²⁰ 14 ²⁰ T 13 ²⁰ 14, ≡ 13 ²⁰ 14 15, # ¹⁴ 16 17, 21 ²⁰ 24, ▨
12	8	06○	09	10	08.3	04.4	00.0	.	# ¹⁴ 0.8 ²⁰ □ 24, □ 18 ²⁰ 19 ²⁰ , 22 ²⁰ 23
13	0	10≡	10≡	10≡	10.0	00.0	00.1	.	≡ 0.24 □ 0.24 □ 0.9 19, ▲ 16 ²⁰ 18 ²⁰
14	8	19≡	08○	05	07.7	03.3	26.1	.	≡ 0-13 ²⁰ 23 ²⁰ 24, □ 2-24
15	0	10≡	10≡	10≡	10.0	00.0	00.1	.	≡ 0.24 □ 0.24 □ 0.15
16	8	10≡	10≡	10≡	10.0	00.4	49.6	.	≡ 0.24 □ 0.14-15 T 20.49 # ¹⁴ 16 14, ≡ 15 24
17	0	10≡	10≡	10≡	10.0	01.2	00.8	.	≡ 0.24, □ 0.24 □ 0.5 ²⁰ 12
18	8	10≡	10≡	10≡	10.0	00.8	01.4	.	≡ 0.13 ²⁰ ≡ 0.24
19	0	10≡	10≡	10≡	02	07.3	00.1	.	≡ 0.18 # ^{0.20} □ 0.9 15 ²⁰ # ¹⁴ 18 27
20	8	02○	04○	02	02.7	13.3	05.8	.	≡ 0.04 14 0.2 13 ²⁰ # ¹⁴ 18 10-15, □ 12 ²⁰ 14 24, ▨ 13 ²⁰ 24
21	0	10≡	10≡	10≡	10.0	02.6	.	.	△ 0.20 □ 0.24 # ^{0.28} 13 ²⁰ 14 30 ≡ 14 0.25 14 20 24, □ 12 ²⁰ 14 ²⁰ ▲ 14 15 17 ²⁰ □ 14 15 17 ²⁰ 24, ▨ 16 ²⁰ 16 ²⁰
22	8	10≡	05○	02	05.7	06.1	23.3	.	≡ 0.4 0.9 14 20, □ 13 ²⁰ ▲ 0.25 17 17
23	8	11○	06○	03	02.3	13.6	01.1	.	# ¹⁴ 0.12 0.20 ≡ 14 0.20
24	8	10≡	09	10	06.3	05.2	.	.	□ 0.24 ≡ 0.15 20 □ 0.15 12
25	8	10≡	06○	01	05.7	05.2	10.6	.	□ 0.24 ≡ 0.15 20
26	3	28○	10≡	10≡	09.3	02.5	.	.	≡ 0.24 # ^{0.28} 10.100 12-15 ≡ 14 16 17, □ 12 ²⁰ 14 20, ▨ 14 16 17, ▨
27	1	10≡	10≡	10≡	10.0	00.1	00.5	.	≡ 0.24 # ^{0.28} 10.100 12-15 ≡ 14 16 17, □ 12 ²⁰ 14 20, ▨ 14 16 17, ▨
28	0	10≡	10≡	10≡	10.0	00.0	33.9	18	≡ 0.24 ≡ 0.28 10.100 12-15 ≡ 14 16 17, □ 12 ²⁰ 14 20, ▨ 14 16 17, ▨
29	8	10≡	05○	00	05.0	05.2	12.1	08	≡ 0.24 21 ²⁰ ≡ 0.28 10.100 12-15 ≡ 14 16 17, □ 12 ²⁰ 14 20, ▨ 14 16 17, ▨
30	8	34≡	02○	32	02.7	13.6	.	.	≡ 0.24 0.9 ≡ 0.28 10.100 12-15 ≡ 14 16 17, □ 12 ²⁰ 14 20, ▨ 14 16 17, ▨

$\varphi = 43^{\circ}43' N$ $\lambda = 18^{\circ}16' E$ Gr. $\Delta G = + 1h 13 min.$

BR. ST. 137

D S	Vazdušni pritisak P mm			Temperatura vazduha T °C							Napon vodenog pare • mm			Relativna vlažnost U %			Pravac i jačina veta D, f (0-12)				
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21	
1	598.1	599.5	599.1	08.8	14.1	10.5	11.0	14.3	05.8	-	04.3	08.0	07.1	50	66	75	64	NNW 4	SSW 2	SW 5	
2	597.5	597.7	596.8	09.9	10.8	07.2	08.8	11.7	07.2	-	06.4	07.4	06.1	69	76	80	75	SSW 7	SW 7	SW 7	
3	595.8	596.4	596.1	07.5	10.8	08.3	08.7	11.6	05.7	-	07.6	08.2	07.8	98	84	95	92	SW 4	WSW 4	WSW 3	
4	595.7	595.9	593.8	10.1	11.3	07.9	09.3	11.8	06.0	-	06.5	07.4	07.6	70	74	95	80	W 3	SSW 7	SSW 8	
5	593.1	592.0	593.1	07.4	11.5	08.5	09.0	11.9	07.1	-	07.4	07.2	08.3	95	70	100	88	SSW 9	SSW 10	SSW 8	
6	595.5	595.5	595.1	08.1	11.0	08.9	09.2	11.8	06.6	-	06.5	07.2	06.3	81	73	74	76	SSW 6	SSW 7	SSW 7	
7	592.6	593.9	593.7	05.7	10.0	04.4	06.1	10.6	04.4	-	06.9	07.1	06.2	100	77	99	92	SSW 7	SSW 7	W 2	
8	594.2	595.1	595.5	02.2	02.9	02.3	02.4	04.4	01.6	-	05.4	05.6	05.4	100	100	100	100	N 5	N 3	- 0	
9	594.4	594.2	593.7	04.1	08.9	05.7	06.1	09.0	01.9	-	06.1	06.3	06.1	100	74	89	88	SE 3	WSW 3	SW 5	
10	593.3	593.6	595.4	06.7	09.5	07.4	07.8	09.8	04.6	-	06.1	06.8	06.6	83	76	86	82	WSW 6	SW 6	SW 6	
11	596.2	597.7	598.0	09.0	13.6	10.4	10.9	13.6	07.0	-	06.9	09.7	08.6	80	83	91	85	- 0	WNW 2	SSW 3	
12	599.0	600.1	600.2	12.6	17.8	12.6	13.9	18.0	10.0	-	05.6	10.2	07.8	52	67	71	63	S 3	SSW 4	SSW 4	
13	600.4	600.8	601.3	12.6	14.6	11.4	12.5	14.9	11.4	-	07.1	07.5	10.1	65	63	100	76	NW 1	N 4	N 4	
14	600.0	600.3	599.1	11.8	12.8	11.2	11.8	13.7	08.1	-	07.1	08.8	09.0	68	79	91	79	E 3	E 2	N 2	
15	596.8	595.8	595.9	11.7	10.2	06.7	08.8	12.6	06.6	-	08.2	09.3	07.4	80	100	100	93	S 2	S 6	N 6	
16	596.6	597.4	597.6	05.6	08.4	08.3	07.7	09.2	05.5	-	06.8	07.9	06.2	100	95	75	90	N 6	E 2	N 4	
17	598.5	599.5	599.8	08.7	14.6	11.0	11.3	14.8	07.4	-	06.0	09.0	07.8	71	73	79	74	N 3	SW 4	SW 4	
18	599.0	598.7	595.9	13.7	15.3	12.4	13.5	15.7	10.0	-	06.6	07.2	07.4	56	55	68	60	WSW 3	SW 7	SW 10	
19	593.0	591.1	593.0	13.8	13.9	06.2	10.0	15.1	06.2	-	06.7	07.7	07.1	57	65	100	74	SW 11	SW 10	N 4	
20	594.2	594.8	594.3	02.8	07.8	06.8	06.1	08.0	02.2	-	05.6	06.3	05.3	100	80	72	84	N 6	NNE 3	N 1	
21	593.8	593.7	593.3	08.4	12.4	08.0	09.2	12.5	06.2	-	04.9	07.1	08.0	59	66	100	75	N 3	S 2	N 5	
22	593.2	595.2	595.6	00.6	02.0	00.8	01.1	08.0	00.6	-	04.8	05.3	04.9	100	100	100	100	N 8	N 9	N 8	
23	594.7	596.9	596.3	-00.4	03.2	01.8	01.6	03.6	-00.6	-	04.5	05.4	05.2	100	94	100	98	N 13	NNE 6	N 6	
24	595.6	596.6	596.5	01.2	06.0	03.8	03.7	06.2	00.2	-	05.0	05.6	06.0	100	80	100	93	NNE 5	NE 5	N 6	
25	596.0	597.2	597.6	03.4	06.6	05.2	05.1	07.2	02.0	-	05.8	05.9	06.3	100	81	95	92	N 6	N 5	N 3	
26	597.1	598.1	598.2	05.4	10.2	08.0	07.9	10.3	03.6	-	05.9	07.0	06.8	87	75	84	82	E 5	- 0	NE 3	
27	597.9	599.2	599.7	10.0	11.6	08.4	09.6	12.0	06.8	-	06.9	07.6	07.9	75	74	95	81	- 0	NNE 4	N 3	
28	599.8	600.7	601.2	09.6	11.4	08.8	09.7	12.0	07.0	-	07.6	07.8	06.4	85	78	76	80	E 3	ENE 5	NE 6	
29	600.2	600.0	599.7	07.4	10.6	07.8	08.4	11.2	06.2	-	06.6	07.2	07.9	86	75	100	87	NE 6	N 6	N 6	
30	598.5	598.2	598.8	07.8	10.6	08.0	08.6	11.0	06.6	-	07.2	06.8	06.3	91	71	78	80	- 0	NE 2	NE 3	
31	597.2	597.8	598.2	08.4	11.0	09.8	09.8	11.8	06.8	-	06.1	07.2	07.5	73	73	83	76	SE 2	- 0	- 0	
MES.	WRED.	596.4	596.9	596.8	07.6	10.5	07.7	08.4	11.2	05.5	-	06.3	07.4	07.0	82	77	89	82	4.6	4.6	4.6

1	598.5	599.8	599.9	09.8	13.0	11.9	11.7	13.0	07.8	-	07.6	08.2	07.8	84	73	75	77	- 0	N 3	- 0
2	599.9	600.4	600.1	13.4	16.5	13.4	14.2	17.4	11.9	-	07.0	08.2	08.4	61	58	73	64	SW 2	NE 2	NNW 2
3	599.0	599.9	599.7	12.3	18.0	13.7	14.4	18.1	10.1	-	06.3	08.6	07.1	59	55	61	58	SW 2	W 2	NNW 5
4	599.5	599.4	598.2	12.9	13.6	11.2	12.2	14.2	11.2	-	07.7	09.2	07.9	69	79	79	76	W 3	SSW 4	SW 5
5	597.3	598.0	598.3	09.0	10.1	09.6	09.6	12.1	09.0	-	08.6	09.3	09.0	100	100	100	100	WNW 2	N 7	N 6
6	598.0	598.4	598.0	10.2	13.2	12.4	12.1	15.3	07.6	-	05.9	08.5	07.4	63	75	69	69	N 3	NE 2	- 0
7	597.3	597.2	594.1	12.4	19.0	13.8	14.8	19.0	09.8	-	06.5	07.7	06.2	60	47	52	53	SW 3	S 8	S 8
8	590.9	591.0	590.9	-	11.0	07.5	-	13.8	07.5	-	-	09.2	06.7	-	94	86	-	S 9	SSW 8	S 8
9	594.1	595.7	595.6	06.7	12.2	08.0	08.7	12.9	06.5	-	06.3	09.4	07.5	86	88	93	89	SSW 2	SW 3	S 4
10	595.0	595.3	595.3	06.7	08.4	04.2	05.9	08.6	04.2	-	06.7	08.3	06.2	90	100	100	97	N 1	- 0	N 2
11	595.3	595.5	595.1	03.6	05.0	04.0	04.2	05.1	03.6	-	05.9	06.5	06.1	100	100	100	100	N 3	N 3	N 6
12	595.4	597.1	597.1	03.2	04.8	03.2	03.6	05.6	03.0	-	05.8	06.5	05.8	100	100	100	100	N 6	N 4	N 4
13	597.3	597.7	597.2	04.4	08.2	06.7	06.5	08.4	02.1	-	05.9	05.9	04.9	93	72	66	77	N 4	N 1	SW 3
14	596.0	597.5	597.8	06.2	08.2	05.6	06.4	10.0	05.6	-	04.4	06.3	06.8	62	77	100	80	SW 2	NNE 2	N 3
15	598.3	599.3	599.3	07.2	11.6	09.8	09.6	12.6	05.3	-	05.7	07.6	07.2	74	74	80	76	SW 3	- 0	- 0
16	599.4	600.3	600.6	09.0	15.0	11.2	11.6	15.3	08.7	-	05.8	05.2	06.2	68	40	62	57	SSW 6	S 2	SW 4
17	599.5	599.7	599.8	11.0	15.0	11.0	12.0	16.3	09.4	-	04.9	07.0	07.8	50	55	79	61	S 3	SE 3	- 0
18	598.7	599.7	599.8	10.0	13.8	07.3	09.6	15.4	07.3	-	06.0	09.8	07.7	66	83	100	83	S 4	S 2	N 4
19	599.4	599.3	598.6	03.0	08.1	05.6	05.6	08.5	03.0</td											

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1978 JUN

BR. ST. 137

$$H_s = 2067 \text{ m } H_b = 2070,4 \text{ m } h_t = 3,0 \text{ m } h_r = 1,5 \text{ m}$$

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1978 AUGUST

MES. 03.7 06.9 03.1 04.6 217.4 105.0
YRFD.

$\varphi = 43^{\circ}43' N$ $\lambda = 18^{\circ}16' E$ Gr. $\Delta G = + 1h 13 min.$

BR. ST. 137

D	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodenе pare • mm			Relativna vlažnost u%			Pravac i jačina veta D, f (0-12)						
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21			
1	586.6	590.4	590.7	-02.4	00.0	00.6	-00.3	00.9	-03.7	-	03.8	04.6	04.6	98	100	95	98	N	12	WSW 4	SSW 6		
2	591.1	591.8	592.6	-00.7	03.2	03.0	02.1	04.9	-00.7	-	04.4	05.8	05.1	100	100	89	96	-	0	SSW 3	SSW 2		
3	593.2	594.5	594.7	03.1	08.8	05.0	05.5	09.0	02.4	-	05.5	04.8	06.4	96	57	97	83	NW	2	SW 3	W 2		
4	594.0	594.8	594.3	04.6	09.8	06.1	06.7	10.4	03.9	-	03.8	01.9	06.3	59	21	89	56	WSW 4	S 4	WSW 6			
5	592.6	592.7	592.5	06.6	06.8	07.2	07.0	08.4	05.3	-	07.3	07.4	07.6	100	100	100	100	S	10	SSW 5	S 7		
6	590.8	589.9	589.7	07.2	07.0	07.3	07.2	07.4	05.9	-	07.6	07.5	07.7	100	100	100	100	SSW 7	SSW 5	S 2			
7	589.1	589.7	590.0	06.2	08.1	06.1	06.6	08.2	05.7	-	07.1	08.1	07.1	100	100	100	100	NW	3	N 2	N 7		
8	590.1	592.7	593.0	03.3	04.0	03.4	03.5	06.1	02.9	-	05.8	06.1	05.8	100	100	100	100	NNW	9	N 8	N 8		
9	591.7	593.6	595.3	00.6	01.8	02.8	02.0	03.4	00.6	-	04.8	05.2	05.6	100	100	100	100	N	12	N 10	N 8		
10	595.9	596.8	596.7	03.8	05.2	07.0	05.8	07.0	02.4	-	06.0	06.6	06.5	100	100	87	96	N	8	N 8	N 8		
11	596.5	598.4	597.0	09.1	14.2	11.8	11.7	15.8	07.0	-	06.1	06.2	06.9	71	51	67	63	N	7	NNW 4	SW 6		
12	592.5	591.0	588.0	09.0	00.6	-02.6	01.1	11.8	-02.8	-	08.2	04.8	03.7	96	100	97	98	SW	9	N 7	N 12		
13	588.0	589.0	593.0	-02.8	-00.8	-00.1	-01.0	00.0	-03.2	-	03.6	04.3	04.6	97	99	100	99	N	14	N 13	N 12		
14	596.3	597.0	596.5	-01.0	02.8	07.8	04.4	07.8	-01.0	-	04.2	05.6	06.5	95	100	82	94	N	4	SW 3			
15	595.3	596.1	596.3	07.5	04.5	03.5	04.8	08.2	03.1	-	06.1	06.3	03.7	78	100	62	80	NW	4	N 5	NE 5		
16	596.6	598.5	598.3	03.8	06.2	04.4	04.7	06.2	03.5	-	04.8	06.2	06.3	80	88	100	89	N	9	N 5	N 7		
17	597.7	599.7	600.1	02.4	06.9	09.4	07.0	09.4	02.4	-	05.4	05.8	02.3	100	78	26	68	NNE	8	N 6	N 5		
18	599.3	599.2	598.5	10.6	14.8	07.9	10.3	14.8	07.9	-	04.2	05.0	07.6	44	40	95	60	NNE	4	SW 3	- 0		
19	597.0	595.4	594.9	08.8	10.4	07.4	04.9	12.1	07.3	-	06.3	08.3	07.0	74	87	91	84	-	0	WSW 2	SW 5		
20	593.1	593.5	594.0	-00.4	-02.0	-03.8	-02.5	07.4	-03.8	-	04.4	03.9	03.3	100	98	96	98	N	5	N 7	N 6		
21	593.8	595.5	595.6	-05.5	-02.9	-14.2	-04.2	-02.9	-05.5	-	02.9	03.6	03.2	95	97	96	96	N	6	N 6	N 6		
22	595.7	596.5	595.7	-02.2	-00.1	00.0	-00.6	00.0	-05.3	-	03.8	04.5	04.6	98	100	100	99	N	6	N 6	N 6		
23	595.1	595.5	596.6	04.6	05.1	03.2	04.0	05.2	00.3	-	05.2	05.6	05.8	82	85	100	89	N	5	NNW 6	NNW 5		
24	596.2	598.4	599.6	03.0	04.6	06.0	04.9	06.0	03.0	-	05.7	05.9	05.8	100	92	83	92	NNW	6	N 6	N 6		
25	600.6	602.5	602.6	08.0	12.0	10.2	10.1	12.2	05.9	-	06.2	05.3	05.2	77	51	56	61	NNW	6	N 3	N 2		
26	601.5	601.0	600.0	11.0	13.4	10.7	11.5	15.8	10.0	-	05.0	05.9	07.0	51	51	72	58	N	3	N 2	SW 2		
27	597.0	595.3	592.8	09.4	08.4	05.8	07.4	10.9	05.8	-	04.6	08.3	06.9	52	100	100	84	W	2	SW 6	SSW 7		
28	589.3	587.6	586.8	05.6	-00.4	-03.0	-00.2	05.8	-03.0	-	06.8	04.5	03.6	100	100	97	99	SSW	8	N 6	N 9		
29	589.0	592.1	593.3	-04.0	00.3	01.0	-00.4	02.2	-04.0	-	03.3	04.0	03.9	96	86	79	87	N	10	SW 5	SW 8		
30	593.0	592.8	591.3	01.3	03.4	04.1	03.2	04.1	00.2	-	05.0	05.8	06.1	100	100	100	100	SSW11	SSW 9	SSW 9	SSW 9		
MES.	594.0			594.7	594.7	03.7	05.2	04.3	04.4	07.3	01.7	-	05.3	05.6	05.6	88	86	88	88	6.6	5.4	5.9	
VRD.																							

1	589.6	592.3	591.8	04.4	05.5	04.9	04.9	05.5	04.1	-	06.3	06.8	06.5	100	100	100	100	SSW 9	SSW 7	SW 6	
2	592.7	596.5	595.8	05.3	06.9	06.6	06.4	07.1	04.9	-	06.7	07.5	07.3	100	100	100	100	SSW 8	S 8	S 6	
3	595.5	596.0	592.0	06.4	12.6	04.2	06.9	12.8	04.2	-	05.3	05.3	06.2	74	49	103	74	SSW 7	SSW 9	SSW13	
4	592.0	592.2	593.5	04.6	03.6	03.0	03.6	05.6	02.6	-	06.4	05.9	05.7	100	100	100	100	SSW 8	SSW 1	SSW 8	
5	593.2	594.0	595.0	02.5	-02.0	-03.0	-01.4	03.2	-03.0	-	05.5	03.9	03.6	100	98	97	98	SSW 6	N 5	N 5	
6	596.0	597.0	598.0	-04.6	-00.4	-02.0	-02.3	-00.1	-04.8	-	00.3	04.4	03.9	10	100	98	69	N	5	N 3	N 5
7	598.0	598.8	599.1	00.8	02.6	01.4	01.6	02.7	-02.0	-	04.9	05.5	05.1	100	100	100	100	N	5	N 4	E 6
8	599.2	599.9	599.7	05.2	06.6	04.0	05.0	08.7	00.7	-	03.9	05.6	06.1	58	77	100	78	S	3	N 6	E 5
9	599.1	599.4	599.8	02.2	09.5	04.1	05.0	09.7	01.7	-	05.4	03.6	06.1	100	40	100	80	NE	5	SSE 4	E 2
10	599.8	600.6	601.6	06.7	11.2	06.2	07.6	11.3	04.0	-	04.0	04.8	06.1	55	48	85	63	E	4	SE 3	N 2
11	601.5	602.4	602.9	06.9	08.8	07.0	07.4	10.0	05.5	-	04.0	06.4	02.5	54	76	33	54	N	3	N 3	NE 3
12	602.0	602.3	602.2	06.6	06.2	05.0	05.7	07.4	03.4	-	01.2	03.2	02.6	17	45	39	34	NE	3	NNE 4	N 5
13	601.5	601.4	600.9	03.3	07.2	03.7	04.5	07.8	03.2	-	02.8	04.7	05.9	47	61	99	69	NE	5	SE 4	E 3
14	599.5	599.0	598.8	06.0	08.1	06.9	07.0	08.4	03.5	-	02.4	04.5	03.0	34	55	41	43	ESE 2	N 2	- 0	0
15	597.3	596.8	596.3	06.1	10.0	06.3	07.2	10.6	05.9	-	02.8	03.4	02.9	40	37	41	39	-	0	- 0	S 2
16	594.7	594.1	593.5	04.2	06.8	03.1	04.3	09.4	03.0	-	03.9	05.4	05.7	63	73	100	79	-	0	SSW 2	SSW 5
17	591.0	590.2	590.1	00.4	02.4	01.0	01.2	03.1	-00.2	-	04.7	05.1	04.9	100	94	100	98	SSW 8	SSW 9	SSW 8	
18	590.9	593.3	595.0	00.8	02.8	02.3</															

BR. ST. 137

$$H_s = 2067 \text{ m } H_b = 2070,4 \text{ m } h_t = 3,0 \text{ m } h_r = 1,5 \text{ m}$$

Dan	Vlajkovost 0-9	Oblačnosť N (0-10)					Inštalácia v m -100 -200 -300	Podzemie R mm	Snežný pokrývav. h cm	Razovia vremena w
		14	7	14	21	Sred Dies				
1	8	10≡	06○	92	06.0	35.3	43.0	17	≡ 0-4*, □ 0-12, ↓=0-8, □	
2	1	10≡*	10≡	01	07.0	01.1	04.0	07	≡ 0-2, * 0-8, ≡ 0-2, 10*, □	
3	8	06○	02○	00	02.7	09.4	09.0	01	* 10-2, H, △ 10-2, 24, □	
4	8	02○	06○	00	02.7	10.2	*		△ 0-6, * 10-6, □ 10-24	
5	5	10	10	00	06.7	00.7	00.6	*	□ 2-14, 0-12, 13*, 0-12	
6	0	10≡*	10≡*	10≡*	10.0	00.0	02.2	*	≡ 0-24, □ 0-16, 0-5*, 23*, 0-12, 13*	
7	3	10≡*	10≡	10≡*	10.0	00.0	35.2	*	≡ 0-24, 0-5*, 0-16, 0-12, 0-14, □ 10-24	
8	0	10≡*	10≡	10≡*	10.0	00.0	18.7	*	≡ 0-24, □ 0-14, 0-10, 10-23	
9	0	10≡	10≡	10≡	10.0	00.0	01.9	*	≡ 0-24, □ 0-14, 0-13, 13-15	
10	3	10≡	10≡	06	08.7	00.0	00.4	*	≡ 0-4*, □ 0-24	
11	8	01○	02○	00	01.0	10.8	*	*	□ 0-24, 0-8, 24, * 10-5, 9	
12	0	08	10≡	10≡*	09.3	00.2	*	*	□ 0-24, ≡ 0-24, ≡ 13-20, R, 14*, 18, * 10-24, ↑= 17-24, □	
13	0	10≡*	10≡	10≡	10.0	00.0	09.7	15	≡ 0-24, * 0-13, 0-24, ↑= 0-24, □ 0-10, 0-8, V 0-24, □	
14	0	10≡	10≡	00	06.7	03.6	02.0	20	≡ 0-13, 0-5, V 0-10, * 13-10, 0-5-10, 10-24, □	
15	0	04○	10≡	02	05.3	05.8	*	10	* 10-24, ≡ 0-24, ≡ 10-12, 13-15	
16	7	02○	10≡	10≡	07.3	02.5	*	06	□ 0-24, ≡ 0-3, 13-24, * 10-4, 1-24, □	
17	8	10≡	04○	01	05.0	08.1	*	05	≡ 0-7, □ 0-24, * 10-10, 7-24, 12, 13-24, □	
18	9	00○	00○	00	00.0	12.0	*	02	* 10-4, 0-15, □	
19	8	02○	06	06	04.7	06.8	*	02	* 10-5, 9-9, ≡ 10-13*	
20	0	10≡	10≡	10≡	10.0	00.0	10.5	*	≡ 0-24, □ 6-7*, □ 6-24, * 7-13, V 13-24, ↓= 13-17*	
21	0	10≡	00≡	10≡	06.7	00.0	04.0	05	≡ 0-24, V 0-24, □ 0-24, □	
22	0	10≡	10≡	10≡	10.0	00.0	*	05	≡ 0-24, V 0-24, □ 0-24, □	
23	8	10	08	10≡	09.3	02.0	*	02	≡ 0-4*, 0-10, 0-24, □ 0-24, V 0-3, * 10-4, 10-20*	
24	8	10≡	05○	10	08.3	02.3	*	00	≡ 0-13, □ 0-24, □	
25	9	04○	02○	00	02.0	10.9	*	*	≡ 0-12, * 10-5, 5-11	
26	9	01○	02○	00	01.0	11.6	*	*	* 10-5, 9	
27	1	06○	10≡*	10≡	08.7	01.8	*	*	* 10-5, 13, 0-12, 17, 23-24, ≡ 13-24, □ 10-24	
28	0	10≡	10≡*	10≡*	10.0	00.0	07.9	*	≡ 0-14, □ 0-24, 0-14, * 14-24, ↑= 13-24, □	
29	8	10≡	01○	00	03.7	07.5	10.9	12	≡ 0-9, □ 0-24, * 0-3, ↑= 0-5, V 3-14, * 10-15, □	
30	0	10≡	10≡	10≡	10.0	00.0	*	03	□ 0-24, ≡ 5-24, □	

BIELENHAGEN

1978 OKTOBAR

1	1	10≡●	10≡●	10≡	10.0	00.0	04.2	.	≡ 0-24, F 0-24, F 2-14 ¹⁵ , 0-15, 14, 23-24
2	0	10≡●	10≡●	10≡	10.0	00.0	08.1	.	≡ 0-24, F 0-24, 0-17 ¹⁵
3	8	08	04	09	07.0	-	10.3	.	≡ 0-24, ≡ 0 ¹⁵ 2, # 14 ¹⁵ 10 ¹⁵ , 0-15, 10 ¹⁵
4	0	10≡●	10≡	10≡	10.0	00.0	03.4	.	≡ 0-24, ≡ 0 ¹⁵ 24, 0-15, 5 ¹⁵ 22 ¹⁵ 24, # 15 ¹⁵ 8 ¹⁵
5	0	10≡	10≡*	10≡*	10.0	00.0	04.2	.	≡ 0-24, ≡ 0-24, 0-15, 8 ¹⁵ 14, *
6	8	00○	00○	00	20.0	10.5	04.6	02	≡ 0-6 ¹⁵ 23 ¹⁵ 24, F 0-9 ¹⁵ V 0-14 ¹⁵ # 15 ¹⁵ 13 ¹⁵ □
7	0	10≡	10≡●	10≡●	10.0	00.0	.	.	≡ 0-24, F 2-24, 13 ¹⁵ , 20 ¹⁵ 24, # 8 ¹⁵ 12 ¹⁵ , 10-23 ¹⁵
8	8	00○○	01○	10≡	03.7	10.8	00.9	.	≡ 0-7 ¹⁵ 10 ¹⁵ 24, F 0-5 ¹⁵ 14 ¹⁵ 24, # 15 ¹⁵ 8 ¹⁵ , H-15 ¹⁵
9	7	00≡○	02○	00≡	00.7	10.6	.	.	≡ 0-10 ¹⁵ 17-21 ¹⁵ , F 0-8.3, # 15 ¹⁵ 7 ¹⁵ 24
10	8	00○	00○	00	00.0	10.6	.	.	# 15 ¹⁵ 5 ¹⁵ 24, □ 10-24
11	8	00○	01○	00	00.3	10.6	.	.	□ 0-1, 10 ¹⁵ 20, # 15 ¹⁵ 0-24
12	9	02○	01○	00	01.0	10.3	.	.	# 10-14 0-14, F 0-24, □ 0-10
13	9	01○	01○	00	00.7	10.6	.	.	# 14-16 0-24, F 0-11, □ 10-24
14	9	01○	00○	00	00.3	10.6	.	.	# 15-18 0-24, □ 0-3, 18-20 ¹⁵
15	9	00○	00○	00	00.0	10.6	.	.	# 15-17 0-24, □ 17 ¹⁵ 20
16	8	00○	02○	00	00.7	10.6	.	.	# 15-17 0-24, □ 17 ¹⁵ 21 ¹⁵ , F 0-24, = 19-21 ¹⁵ , ≡ 21 ¹⁵ 24
17	7	00≡○	08	10≡	06.0	02.0	.	.	≡ 0-9 ¹⁵ 15 ¹⁵ 24, F 0-24
18	0	10≡	10≡	10≡	10.0	00.0	03.5	.	≡ 0-24, F 0-24, 0-10 ¹⁵ 24
19	8	08	09	10≡●	29.0	02.5	.	.	≡ 0-24, 17 ¹⁵ 24, # 15 ¹⁵ 5 ¹⁵ H ¹⁵ , 0-15 ¹⁵ 24
20	0	10≡●	10≡	10≡●	10.0	00.0	03.0	.	≡ 0-24, 9-10 ¹⁵ 17 ¹⁵ 20 ¹⁵ , 0-24, F 0-24
21	0	10≡●	10≡*	10≡*	10.0	00.0	14.8	.	≡ 0-24, 0-24, 3 ¹⁵ 24, H ¹⁵ , # 8 ¹⁵ 24, V 10 ¹⁵ 24, * 10-22 ¹⁵
22	8	10≡	01○	02	04.3	19.1	25.1	.	≡ 0-24, F 0-24, 0-24, 22 ¹⁵ , 22 ¹⁵ 24
23	8	26○	06	10≡	07.3	04.6	.	.	V 0-24, 13 ¹⁵ 24, F 0-24, 10-24, # 10 ¹⁵ 24
24	8	05○	01○	00	02.0	07.1	.	.	≡ 0-10 ¹⁵ 12 ¹⁵ , 0-24, 0-15 ¹⁵ 17 ¹⁵ 24
25	9	02○	01○	00	01.0	29.7	.	.	# 10-24, # 15-24, 17 ¹⁵ 22 ¹⁵ , F 0-24
26	0	09	10≡	10≡	05.7	00.0	.	.	# 15-17 15 ¹⁵ 24, # 15-15 24, # 20-15 24, # 19-24, 24 ¹⁵ , * 14-20, 16 ¹⁵ , / 14 ¹⁵ 24
27	9	10≡*	10≡*	10≡*	10.0	00.0	03.2	02	≡ 0-24, 11-24, F 0-24, 12 ¹⁵ 24, # 15-15 24, F 0-24, 24, # 15-15 24
28	0	10≡	10	10○	10.0	00.0	13.8	05	≡ 0-24, 0-15 ¹⁵ , 0-24, F 0-24, 10-24, # 10-24
29	0	02	10	10○	07.3	16.2	.	04	≡ 0-24, 12 ¹⁵ , F 0-24, 0-24, 10-24, # 10-24, 11 ¹⁵
30	0	10≡	10○	10○	10.0	00.0	.	04	≡ 0-24, 0-24, F 0-24, 10-24, # 10-24, 11 ¹⁵
31	8	10≡	00○	00	03.3	06.5	.	13	≡ 0-24, 0-24, F 0-24, 10-24, 24, # 15-15 24

$\varphi = 43^{\circ}43' N \lambda = 18^{\circ}16' E$ Gr. $\Delta G = + 1h\ 13\ min.$

BR. ST. 137

d	Vazdušni pritisk P mm			Temperatura vazduha T C°							Napon vodenе pare • mm			Relativna vlažnost u%			Pravac i jačina veta D, f (0-12)							
	7	14	21	7	14	21	Sred. Dnes	Max	Min	MM 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21				
1	600.4	601.2	601.5	04.0	04.8	01.8	03.1	04.9	01.8	-	02.0	02.2	01.8	32	33	34	33	N	4	N	3	N	3	
2	600.3	600.0	599.6	-04.0	-03.0	-02.8	-03.2	02.0	-04.0	-	03.3	03.6	03.6	96	97	97	97	N	5	N	3	N	2	
3	598.5	599.0	599.0	-02.0	-00.8	-02.8	-02.1	04.4	-02.8	-	03.9	04.3	03.6	98	100	97	98	SSE	3	-	0	N	1	
4	598.3	598.5	598.6	-05.1	-02.9	-03.2	-03.6	-02.8	-05.1	-	03.0	03.6	03.4	95	97	93	95	N	1	N	2	NE	2	
5	598.8	599.5	599.1	-01.6	-01.3	-01.0	-01.2	-01.0	-05.7	-	02.7	03.4	01.7	65	81	40	62	E	5	N	4	E	4	
6	599.8	600.3	600.9	-00.6	01.3	00.1	00.2	01.3	-01.0	-	03.2	03.7	02.7	73	74	59	69	SE	3	E	2	E	3	
7	600.3	600.8	600.8	-00.3	00.1	-00.4	-00.3	00.5	-00.6	-	01.4	02.0	01.6	30	44	37	37	N	3	N	6	N	5	
8	600.8	601.1	601.1	02.1	03.4	02.4	02.6	03.7	-00.4	-	01.8	03.1	03.9	33	53	72	53	E	3	NE	2	N	4	
9	601.0	601.5	601.7	02.1	04.2	03.3	03.2	05.3	01.9	-	02.8	03.1	03.1	52	49	54	52	E	3	E	4	S	5	
10	601.5	601.1	600.8	04.0	<u>05.3</u>	04.6	04.6	<u>05.4</u>	03.2	-	02.8	04.0	02.5	45	59	39	48	SSW	4	SE	2	-	0	
11	599.7	599.1	599.8	03.6	03.8	02.7	03.2	04.8	02.7	-	02.1	02.1	01.9	35	34	35	35	N	2	N	4	N	2	
12	599.1	599.2	599.3	03.0	04.3	02.2	02.9	05.2	02.2	-	02.8	02.4	02.9	49	38	54	47	-	0	E	3	E	2	
13	599.7	599.8	600.7	00.8	03.0	02.0	02.0	03.4	00.6	-	02.5	02.2	01.9	51	39	35	42	-	0	N	2	N	2	
14	600.5	602.8	603.0	-00.8	00.0	-00.8	-00.6	02.0	-00.8	-	02.7	01.8	02.0	62	40	46	49	N	5	N	6	N	7	
15	602.8	603.3	603.4	00.8	02.8	02.6	02.2	03.0	-00.8	-	01.6	02.0	02.2	32	36	40	36	N	4	S	2	SW	3	
16	601.6	601.1	600.4	01.2	04.2	04.8	03.8	04.8	01.0	-	02.0	02.1	02.0	40	34	31	35	SW	2	-	0	-	0	
17	598.9	599.0	599.2	-03.8	-03.4	-08.2	-05.9	04.8	-08.2	-	03.5	03.5	02.3	100	97	92	96	N	9	N	9	N	8	
18	599.0	599.5	600.7	-07.4	-02.6	-02.3	-03.7	-02.0	-08.2	-	02.4	02.4	02.6	90	68	71	74	N	6	E	5	E	3	
19	600.1	599.8	599.3	-00.6	02.4	01.0	01.0	02.6	-02.3	-	01.3	01.8	01.6	29	33	33	32	ENE	3	S	3	-	0	
20	598.0	597.9	598.3	00.0	03.2	00.0	00.8	03.7	00.0	-	01.6	03.5	02.1	34	61	45	47	W	2	-	0	W	2	
21	598.3	599.3	600.4	-01.6	00.1	-02.4	-01.6	00.1	-02.8	-	01.9	02.3	03.8	47	50	100	66	NNW	2	N	5	N	5	
22	601.5	602.5	603.5	-02.4	-02.6	-01.4	-02.0	-01.4	-03.4	-	03.8	03.7	03.3	100	97	79	92	N	6	N	6	N	5	
23	602.5	602.2	602.3	-01.7	-01.7	-00.8	-01.3	-00.8	-03.8	-	03.5	02.7	03.8	87	68	87	81	N	5	N	7	N	6	
24	601.7	601.1	600.2	-00.4	03.4	02.0	01.8	03.4	-02.4	-	03.9	03.7	03.2	87	63	61	70	N	6	S	3	-	0	
25	597.6	595.0	593.0	01.0	02.4	00.0	00.9	02.7	00.0	-	04.0	<u>05.0</u>	04.6	82	92	100	91	SW	2	S	6	SSW	6	
26	591.2	588.6	587.9	-03.6	-02.6	-02.6	-02.9	00.6	-03.6	-	03.4	03.7	03.7	97	97	97	97	SSW	6	SSW	7	SSW	7	
27	584.5	581.2	580.0	-03.4	-01.6	-03.8	-03.2	-01.4	-03.8	-	03.5	04.0	03.3	97	98	96	97	SSW	7	SSW	8	SSW	7	
28	578.6	577.0	577.3	-04.2	-00.4	00.9	-00.7	01.0	-04.2	-	03.2	04.4	04.9	96	100	100	99	SSW	3	SSW	4	SSE	5	
29	578.0	577.3	577.0	-05.2	-11.0	-12.0	-10.1	01.0	-12.0	-	03.0	01.8	01.6	95	90	89	91	N	3	N	6	N	7	
30	577.6	579.7	583.0	-10.8	-09.8	-10.8	-10.6	-09.7	-12.0	-	01.8	02.0	01.8	90	91	90	90	N	8	N	0	N	9	
MES.	597.0			596.9	597.0	-01.2	00.2	-00.8	-00.7	01.7	-02.5	-	02.7	03.0	02.8	67	67	67	67	3.8	3.8	3.8	3.8	
RFD.	587.4			587.8	587.9	-03.7	-03.1	-03.7	-03.6	-01.6	-05.5	-	03.5	03.5	03.4	95	91	93	93	7.5	7.5	6.8	6.8	

1978 DECEMBAR

BJELAŠNICA

1	587.2	588.4	589.3	-10.0	-09.2	-09.0	-09.3	-09.0	-10.9	-	01.9	01.2	01.3	91	53	56	67	N	7	NW	5	N	6
2	589.0	590.1	590.9	-08.2	-07.0	-10.0	-08.8	-06.3	-10.0	-	02.3	02.5	01.8	92	93	86	90	N	7	N	5	NW	3
3	590.3	589.9	589.4	-08.7	-04.0	-05.1	-05.7	-04.0	-10.3	-	02.1	02.3	02.2	90	68	71	76	NW	3	S	2	SW	3
4	586.3	586.9	586.9	-04.2	-04.2	-04.0	-04.1	-00.2	-05.2	-	03.2	03.2	03.3	96	96	96	96	SW	6	SW	3	-	0
5	585.7	586.7	588.2	-11.4	-13.8	<u>-16.4</u>	-14.5	-02.2	-16.4	-	01.7	01.4	01.1	89	87	85	87	N	7	N	8	N	8
6	588.9	589.3	589.4	-16.1	-15.2	-14.7	-15.2	-14.7	-16.8	-	01.1	01.2	00.9	82	83	59	75	N	9	N	7	E	7
7	588.8	588.0	588.8	-09.5	-08.2	-10.0	-09.4	-07.8	-14.7	-	01.5	02.3	01.9	68	92	91	84	-	0	SSW	6	SW	4
8	589.0	590.2	591.0	-10.5	-06.4	-05.0	-06.7	-04.8	-10.5	-	01.9	00.5	02.7	90	18	84	64	SW	7	NNW	5	W	4
9	588.7	589.2	591.0	-05.0	-02.6	-04.2	-04.0	-01.6	-05.8	-	03.0	03.7	03.2	95	97	96	96	W	8	SW	10	N	9
10	592.6	593.9	594.0	-04.2	-03.2	-03.0	-03.4	-03.0	-04.9	-	03.2	03.5	03.4	96	97	94	96	N	12	NW	7	NW	7
11	594.0	593.3	592.0	-02.6	01.0	-01.6	-01.2	01.4	-03.0	-	02.8	03.7	04.0	74	75	98	82	NW	3	W	4	SW	6
12	588.4	586.7	584.0	-01.0	-00.4	00.3	-00.2	00.3	-01.6	-	04.2	04.4	04.7	99	100	100	100	SW	11	SW	10	SW	12
13	582.4	583.8	582.5	00.0	-00.4	-01.3	-00.8	00.4	-01.4	-	04.6	04.4	04.1	130	100	99	100	SW	10	SW	10	SW	9
14	578.9	577.8	579.3	-00.4	-02.0	-03.5	-02.4	-00.3	-03.5	-	04.4	03.9	03.4	100	98	97	98	SW	7	SW	12	SW	7
15	581.2	583.8	585.2	-03.0	-02.0	-04.4	-03.5	-01.6	-04.4	-	03.6	03.9	03.2	97	98</td								

BR. ST. 137.

 $H_s = 2067 \text{ m } H_b = 2070,4 \text{ m } h_t = 3.0 \text{ m } h_r = 1.5 \text{ m}$

Dan	Vremensko	Oblačnost N (0-10)					Precip. mm	Padavina R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dnes				
1	8	010	040	00	01.7	09.4	.	.	0-14-10-23-24, ≡ 23-24	
2	0	10≡	10≡*	10≡	10.0	00.0	.	.	≡ 0-24, V 5-24, 6-17, * 12-17	
3	0	10≡	10≡	02	07.3	00.0	00.0	.	≡ 0-18, 23-24, V 0-11, ≡ 10-23-24	
4	1	02≡	10≡	05	05.7	04.8	.	.	≡ 0-14, V 4-24, ≡ 12-24, H-24, ≡ 23-24	
5	8	01	07	00	02.7	07.9	.	.	≡ 0-17, ≡ 0-24, ≡ 10-24, ≡ 10-18-24	
6	9	000	010	00	00.3	09.6	.	.	0-17-24 0-24	
7	9	000	000	00	00.0	09.7	.	.	0-18-24, ≡ 9-23	
8	9	000	000	00	00.0	09.7	.	.	0-14-24	
9	9	000	000	00	00.0	09.7	.	.	0-18-24	
10	9	000	000	00	00.0	09.7	.	.	0-11-24	
11	9	000	000	00	00.0	09.7	.	.	0-17-24 0-24	
12	9	000	000	00	00.0	09.6	.	.	0-14-24	
13	9	000	040	03	02.3	09.3	.	.	0-11-24	
14	9	010	040	01	02.0	09.5	.	.	0-14-24, ≡ 10-24	
15	9	000	000	01	00.3	09.5	.	.	0-17-24, ≡ 0-24	
16	9	000	040	08	04.0	09.4	.	.	0-18-24 0-24	
17	8	10≡	080	00	06.0	02.7	.	.	0-24, 0-18, ≡ 10-24, ≡ 6-24, ≡ 6-24, ≡ 6-24, ≡ 6-24, ≡ 15-24, V 16-24	
18	9	010	000	01	00.7	09.4	.	.	V 0-14, ≡ 10-24, ≡ 0-24, ≡ 0-5-24, ≡ 0-5-24, ≡ 0-15-24	
19	9	040	070	00	03.7	09.2	.	.	0-17-24 0-24	
20	9	000	000	00	00.0	09.3	.	.	0-17-24, ≡ 0-24	
21	9	00	000	00≡	00.0	09.2	.	.	0-17-24 0-20, ≡ 0-24, ≡ 0-24, ≡ 0-24	
22	0	10≡	00≡	00	03.3	00.0	.	.	≡ 0-18, ≡ 0-24, ≡ 0-24, ≡ 19-24	
23	9	00	000	00	00.0	08.6	.	.	0-14-24, ≡ 0-24	
24	9	00	010	00	00.3	09.0	.	.	0-18-24, ≡ 0-24	
25	9	00	010	10≡	03.7	08.2	.	.	0-18-24, ≡ 0-24, ≡ 0-24	
26	0	07≡	10≡	10≡	09.0	00.0	.	.	0-24, ≡ 0-24, V V 3-24, ≡ 10-24, ≡ 10-24	
27	0	10≡*	10≡*	10≡*	10.0	00.0	04.0	05	0-24, V 0-24, ≡ 0-24, ≡ 3-24, ≡ 8-24, ≡ 10-24, ≡ 10-24	
28	0	10≡*	10≡*	10≡*	10.0	00.0	09.0	30	0-24, V 0-24, ≡ 0-24, ≡ 0-24, ≡ 0-24, ≡ 0-24, ≡ 0-24, ≡ 0-24, ≡ 0-24	
29	0	10≡*	10≡*	10≡*	10.0	00.0	10.2	50	0-24, V 0-24, ≡ 0-24, ≡ 0-24, ≡ 0-24, ≡ 0-24, ≡ 0-24, ≡ 0-24, ≡ 0-24	
30	0	10≡	10≡	10≡	10.0	00.0	05.1	64	0-23, V 0-24, ≡ 0-24, ≡ 0-24, ≡ 0-24, ≡ 0-24, ≡ 0-24, ≡ 0-24, ≡ 0-24	
MES.	VRED.	03.2	04.0	03.0	03.4	193.1	29.3			

BJELAŠNICA

1978 DECEMBER

1	8	00	020	00	00.7	09.0	00.0	64	0-24, ≡ 0-24, ≡ 0-3, ≡ 10-23-24, ≡ 0-24, ≡ 23-24, ≡ 24
2	1	10≡	10≡	00	06.7	02.7	.	63	0-24, ≡ 0-16-24, ≡ 0-17, 23-24, ≡ 24
3	8	00	000	00	00.0	08.9	.	60	0-24, ≡ 0-5, ≡ 10-24, ≡ 10-24
4	0	10≡	10≡*	10≡	10.0	00.2	.	55	0-24, ≡ 0-5, ≡ 2-12, ≡ 5-24, ≡ 9-24, ≡ 10-24
5	0	10≡	10≡	00	06.7	00.0	03.2	59	≡ 0-16, ≡ 0-24, ≡ 5-24, ≡ 0-24, ≡ 10-24
6	9	01	010	00	00.7	08.3	.	59	0-16-24, ≡ 0-24, ≡ 0-24, ≡ 10-24, ≡ 10-24
7	3	00	10≡	10≡	06.7	04.6	.	56	0-24, ≡ 0-16-24, ≡ 0-5-24, ≡ 10-24
8	9	00≡	040	10	04.7	07.5	.	52	0-24, ≡ 0-7, ≡ 2-24, ≡ 2-24, ≡ 10-24, ≡ 10-24
9	0	10≡	10≡*	10≡*	10.0	00.0	02.2	52	0-24, ≡ 0-24, ≡ 0-30, ≡ 0-30, ≡ 0-24, ≡ 0-24, ≡ 0-24
10	9	05	06	09	06.7	07.7	12.8	63	0-17, ≡ 0-24, ≡ 0-24, ≡ 0-24, ≡ 0-24, ≡ 0-24, ≡ 0-24
11	9	04	06	05	05.0	06.7	.	60	0-10-24, ≡ 0-10-24, ≡ 0-24, ≡ 0-24, ≡ 0-24
12	0	06	10≡	10≡	08.7	00.0	.	50	0-10-24, ≡ 0-24, ≡ 10-24, ≡ 10-24, ≡ 10-24, ≡ 10-24
13	0	10≡	10≡*	10≡	10.0	00.0	13.2	44	0-24, ≡ 0-24, ≡ 0-60, ≡ 0-24, ≡ 10-24, ≡ 10-24, ≡ 10-24
14	2	10≡*	08≡	10≡	09.3	00.0	11.6	54	0-14, ≡ 0-24, ≡ 2-24, ≡ 2-24, ≡ 10-24, ≡ 10-24
15	9	10	040	10≡	08.0	04.7	02.7	56	0-24, ≡ 0-5, ≡ 10-24, ≡ 0-10-24, ≡ 0-10-24, ≡ 0-10-24
16	0	10≡*	10≡	10≡	10.0	00.0	03.2	57	0-24, V 0-24, ≡ 0-24, ≡ 10-24, ≡ 10-24, ≡ 10-24, ≡ 10-24
17	8	10≡	040	08	07.3	05.5	17.0	57	0-8, ≡ 10-20, ≡ 0-60, ≡ 0-24, ≡ 0-24, ≡ 0-24
18	1	10≡*	10≡*	10≡*	10.0	00.0	00.8	57	0-10-24, ≡ 0-10-24, ≡ 0-24, ≡ 0-24, ≡ 0-24, ≡ 0-24
19	1	06	10≡	10≡*	08.7	00.8	12.8	74	0-40, ≡ 10-24, ≡ 1-24, ≡ 1-24, ≡ 1-24, ≡ 1-24, ≡ 1-24
20	8	10≡	040	00	04.7	02.2	08.9	80	* 0-2, ≡ 0-24, ≡ 0-13, ≡ 0-13, ≡ 0-13, ≡ 0-13, ≡ 0-13, ≡ 0-13
21	1	10≡	10≡	10≡	10.0	01.8	.	79	0-24, ≡ 0-24, ≡ 0-24, ≡ 0-24, ≡ 0-24, ≡ 0-24, ≡ 0-24, ≡ 0-24
22	0	10≡	10≡	10≡*	10.0	02.7	.	78	0-24, ≡ 0-24, ≡ 0-14, ≡ 24, ≡ 10-24, ≡ 10-24, ≡ 10-24
23	8	10≡*	040	00	04.7	00.8	03.1	79	0-13, ≡ 0-24, ≡ 0-14, ≡ 0-14, ≡ 0-14, ≡ 0-14, ≡ 0-14
24	8	01	010	10≡	04.0	07.4	00.3	77	0-24, ≡ 0-24, ≡ 0-24, ≡ 0-24, ≡ 0-24, ≡ 0-24, ≡ 0-24
25	1	10≡	10≡*	10≡*	10.0	00.2	00.2	77	0-24, ≡ 0-24, ≡ 0-24, ≡ 0-24, ≡ 0-24, ≡ 0-24, ≡ 0-24
26	1	10≡*	10≡	00	06.7	00.0	05.8	81	0-20, V 0-24, ≡ 0-10-24, ≡ 0-20, ≡ 0-24, ≡ 0-24
27	8	04	08	10≡	07.3	04.0	01.2	83	0-24, ≡ 0-20-24, ≡ 5-24, ≡ 9-24, ≡ 24, ≡ 20-24, ≡ 24
28	0	10≡	10≡	10≡	10.0	00.0	.	81	0-24, V 0-24, ≡ 0-24, ≡ 0-24, ≡ 0-24, ≡ 0-24
29	0	10≡	10≡	10≡	10.0	01.0	.	93	0-24, V 0-24, ≡ 0-24, ≡ 0-24, ≡ 0-24, ≡ 0-24
30	7	08	09	00≡	05.7	01.0	.	74	0-24, V 0-24, ≡ 0-24, ≡ 0-24, ≡ 0-24, ≡ 0-24
31	0	10≡	10≡	10≡	10.0	00.1	.	79	0-22, V 0-24, ≡ 0-24, ≡ 0-24, ≡ 0-24, ≡ 0-24
MES.	FEĐ.	17.3	17.5	16.8	17.2	83.5	99..		

1978 JANUAR

SARAJEVO

 $\varphi = 43^{\circ}52' N \lambda = 18^{\circ}26' E$ Gr. $\Delta G = + 1h\ 14\ min.$

BR. ST. 139

D d	Vazdušni pritisak P mm			Temperatura vazduha T C°							Napon vodenе pore • mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0—12)							
	7	14	21	7	14	21	Sred. Diēs	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Diēs	7	14	21				
1	704.0	708.2	713.5	-02.7	-01.6	-03.4	-02.8	01.3	-03.5	-02.3	03.5	03.9	03.3	94	95	93	94	W	2	W	2	-	0	
2	715.0	713.7	712.5	-07.2	03.3	-02.2	-02.1	04.0	-07.4	-09.2	02.4	03.1	03.0	88	54	76	73	SW	2	ESE	1	ESE	4	
3	710.7	709.7	706.9	-02.8	01.6	00.8	00.1	02.0	-04.7	-06.3	03.1	03.7	04.2	82	71	87	80	ESE	2	-	0	ESE	2	
4	709.8	705.9	705.9	01.6	00.6	-01.4	-00.2	02.6	-01.5	-01.5	04.4	04.6	03.8	86	97	91	91	-	0	-	0	-	0	
5	708.7	709.8	713.5	-03.6	-01.0	-05.0	-03.7	00.8	-05.0	-07.4	03.3	02.9	02.9	93	68	91	84	-	0	NNW	2	S	2	
6	717.2	716.6	715.9	-08.5	-01.6	-10.6	-07.8	-01.5	-10.6	-10.7	02.0	02.1	01.6	85	51	79	72	ENE	2	E	3	ESE	2	
7	714.4	715.0	716.5	-07.8	-04.6	-03.7	-05.0	-03.6	-10.9	-12.0	02.1	02.6	02.7	83	81	79	81	-	0	-	0	E	2	
8	716.2	715.5	715.8	-06.3	-00.4	-09.1	-06.2	-00.4	-09.1	-07.8	01.9	02.5	01.8	68	56	79	68	NE	2	SSE	1	E	3	
9	714.7	713.1	712.6	-13.2	-04.0	-08.4	-08.5	-03.2	-13.7	-14.9	01.4	02.2	02.0	81	65	82	76	ESE	2	SE	1	-	0	
10	711.8	709.9	711.2	-12.0	-02.1	-04.6	-05.8	-00.8	-12.4	-13.3	01.6	02.3	02.6	89	59	79	76	ESE	1	-	0	-	0	
11	708.9	705.4	703.2	-09.4	-01.9	03.8	-00.9	04.0	-09.6	-11.2	01.9	02.9	03.9	86	71	66	74	-	0	-	0	-	0	
12	701.5	701.8	705.2	05.9	08.6	06.8	07.0	09.3	03.2	01.5	04.3	05.1	05.1	61	61	68	63	ESE	2	-	0	ESE	1	
13	708.3	709.4	711.6	05.7	11.0	05.0	06.7	11.3	05.0	03.1	05.1	05.6	04.9	75	57	75	69	ESE	2	-	0	ESE	2	
14	710.7	710.6	710.4	02.0	09.0	03.6	04.8	10.5	01.8	00.2	04.5	05.4	04.7	84	59	79	74	E	4	-	0	E	3	
15	709.6	708.6	707.9	00.6	03.3	01.5	01.7	03.7	00.4	-01.1	04.5	05.2	04.9	93	89	97	93	-	0	-	0	-	0	
16	706.2	705.3	706.2	00.2	02.2	01.4	01.3	03.0	00.2	-00.4	04.6	05.2	04.9	98	97	97	97	-	0	W	2	W	2	
17	702.4	697.9	696.4	00.9	03.6	04.0	03.1	04.8	00.9	00.6	04.8	05.6	04.7	98	94	77	90	-	0	E	4	E	6	
18	700.5	701.4	702.4	03.4	10.4	02.0	04.5	11.0	02.0	00.7	05.0	04.1	04.1	85	43	78	69	W	2	W	2	ESE	3	
19	701.6	699.6	699.3	00.0	07.9	01.2	02.6	09.1	-00.1	-01.9	04.3	04.3	04.0	93	54	81	76	ESE	2	SSW	2	ESE	3	
20	699.2	698.9	700.1	-01.3	03.0	00.6	00.7	03.2	-01.8	-03.0	03.7	04.2	04.3	89	73	90	84	ESE	3	ESE	5	NW	2	
21	698.9	698.3	701.3	-00.1	01.0	-02.8	-01.2	03.4	-02.8	-01.0	04.3	04.6	03.5	95	93	94	94	W	1	NW	2	NW	2	
22	701.8	700.9	702.9	-03.6	-00.8	-01.4	-01.8	-00.6	-04.0	-03.6	03.4	03.6	03.6	97	82	88	89	NW	1	NW	1	NW	1	
23	703.7	704.4	706.2	-02.4	01.6	-00.4	-00.4	01.8	-02.4	-04.0	03.6	04.0	03.8	94	78	86	86	MNW	1	NNW	1	NW	1	
24	704.8	702.1	698.8	-00.6	08.4	06.4	05.2	08.4	-00.6	-03.6	04.1	04.4	04.5	93	54	62	70	-	0	NW	2	SW	4	
25	695.9	697.0	701.9	07.0	03.6	01.4	03.4	08.0	01.3	34.8	04.7	05.4	04.9	63	91	97	84	S	5	W	2	E	1	
26	704.5	702.8	704.3	-03.3	04.7	01.4	01.1	05.2	-03.6	-04.2	03.3	03.9	04.2	93	60	84	79	E	2	E	1	SE	1	
27	706.2	707.4	709.4	-03.4	-01.2	-01.8	-02.1	01.6	-03.5	-33.9	03.0	03.9	03.9	85	92	96	91	ESE	3	NW	1	ENE	1	
28	709.1	705.8	702.6	-05.4	06.0	06.5	03.4	06.5	-05.6	-36.0	02.8	02.6	04.4	91	37	60	63	ESE	4	S	6	S	4	
29	694.5	691.9	691.5	09.8	08.4	05.2	07.2	12.0	05.0	06.0	04.6	05.9	06.1	51	71	92	71	S	5	S	4	SE	4	
30	691.8	691.9	694.6	02.6	03.8	00.6	01.9	06.0	00.5	02.5	05.2	05.1	04.3	94	86	90	90	SW	1	SW	2	SE	2	
31	697.6	699.9	702.4	00.4	01.1	00.1	00.4	01.2	-00.4	J1.1	04.6	04.5	04.1	97	90	88	92	NW	1	W	3	W	1	
MES.	VRED.	705.6	705.1	705.9	-01.7	02.7	-00.1	00.2	04.0	-03.0	-03.5	03.6	04.0	03.9	86	72	83	80	1.7	1.6	1.6	1.9		

1978 FEBRUAR

SARAJEVO

1	703.5	702.1	702.0	-02.2	02.2	-01.2	-00.6	03.2	-02.2	-01.7	03.5	03.6	03.5	89	67	84	80	ESE	1	ESE	2	SE	2
2	699.4	696.1	698.4	-05.3	02.2	-02.4	-02.0	02.6	-05.3	-05.2	02.7	03.9	03.5	87	72	90	83	ESE	4	E	3	ESE	1
3	699.9	731.2	703.7	-03.3	-00.2	00.4	-00.6	00.8	-04.0	-04.0	03.4	03.9	03.9	93	86	83	87	ESE	1	NW	1	-	0
4	705.4	706.5	708.0	-01.0	00.4	-00.2	-00.3	00.6	-01.0	00.0	04.1	04.4	03.8	96	93	83	91	W	1	WNW	1	ENE	2
5	707.5	706.3	705.1	-01.2	00.8	-00.6	-00.4	01.6	-01.3	-00.8	03.9	03.9	03.5	92	80	79	84	WNW	1	NW	1	ESE	2
6	701.6	700.5	700.7	-01.6	-00.2	-01.2	-01.1	-00.1	-01.6	-00.4	03.4	03.4	03.9	84	76	93	84	WNW	1	WNW	1	W	1
7	699.6	698.9	698.5	-03.0	-01.0	-02.6	-02.3	-00.6	-03.0	-01.5	03.6	03.6	03.6	97	83	94	91	WNW	1	WNW	1	W	2
8	698.3	697.8	698.7	-04.6	-01.8	-03.0	-03.1	-01.5	-04.6	-03.8	03.1	03.1	02.7	96	77	73	82	NW	1	W	2	ESE	3
9	699.6	699.9	702.1	-04.4	-00.2	-02.6	-02.5	-00.2	-04.4	-03.6	03.0	03.3	03.6	92	73	94	86	SSW	1	SW	1	NW	2
10	703.3	700.5	699.4	-06.4	05.2	04.0	01.7	07.4	-06.5	-06.5	02.6	04.2	04.4	92	63	72	76	E	3	SE	2	SE	2
11	694.4	694.0	694.5	05.4	13.1	39.0	09.1	14.2	03.8	33.4	06.4	06.1	05.4	95	54	63	71	N	3	S	4	SE	3
12	696.3	698.1	698.0	08.4	07.7	34.8	06.4	10.4	04.8	07.0	04.3	05.9	06.0	51	74	93	73	S	4	W	2	-	0
13	696.6	696.5	696.3	03.0	04.4	02.4	03.1	05.0	02.4	04.4	05.5	05.9	05.1	97	94	96	95	NW	2	WNW	1	WNW	1
14	692.7	693.8	697.3	00.2	00.0	-J1.0	-00.5	02.5	-01.2	-J2.0	04.5	04.4	04.0	97	97	93	96	SW	1	WNW	2	W</td	

SARAJEVO

1978 JANUAR

BR. ST. 139

$$H_s = 630 \text{ m } H_b = 637.0 \text{ m } h_f = 2.0 \text{ m } h_r = 1.0 \text{ m}$$

SARAJEVO

1978 FEBRUAR

1	6	10	09	00	06.3	01.0	03.7	02	=0-4, * 2 ^o -6 ^o , □ 9-24, □
2	7	01	10	00	03.7	03.5	.	.	□ 9-10 ^o -24
3	4	10	10*	10*	10.0	00.0	.	.	□ 0-6 ^o , =0-24, △ 9 ^o -13 ^o , * 13 ^o -24
4	6	10*	10*	10*	10.0	00.0	02.1	02	* 0-24, =0-24, □
5	6	10*	10	10	10.0	00.0	00.9	00	* 0-7 ^o , =0-24, □
6	6	10	10	10*	10.0	00.0	00.0	.	=0-24, * 13 ^o -24
7	5	10*	10*	10*	10.0	00.0	03.5	03	* 0-24, =0-24, □
8	6	10*	10*	10*	10.0	00.0	07.9	09	* 0-6 ^o , =0-24, □
9	6	10	10*	10*	10.0	00.0	00.5	08	* 0 ^o -6 ^o , □ 23 ^o -5 ^o -24, □
10	7	06	08	06	06.7	02.8	00.7	08	=0-14, □ 0 ^o -10 ^o , □
11	7	100	060	05	07.0	04.0	06.0	.	□ 3 ^o -1-2 ^o , 14 ^o -4 ^o -8 ^o -11, 13 ^o -14 ^o , 17 ^o -22 ^o , 04 ^o -10 ^o , 13 ^o -17 ^o , □
12	7	09	100	100	09.7	01.1	00.5	.	□ 3 ^o -12 ^o , 05 ^o -24
13	5	10	100	100	10.0	00.0	19.2	.	04 ^o -13 ^o -14 ^o , □ 3 ^o -6 ^o , =6 ^o -24, * 13 ^o -21 ^o , * 12 ^o -24, □
14	3	10*	10*	10*	10.0	00.0	30.4	15	* 0-24, =0-14, □
15	4	10*	10*	10*	10.0	00.0	15.4	23	* 0-12 ^o , =0-24, □
16	5	01	10	09	06.7	02.6	00.8	22	=0-19, □ 22 ^o -23 ^o , □
17	6	10*	09	02	07.0	31.5	00.2	15	* 5-7 ^o , =6 ^o -20, □ 7 ^o -11 ^o , □
18	6	05	10	10	08.3	00.2	00.2	10	=3-15 ^o -4, 21 ^o -24, * 0 ^o -13, □
19	6	06	10	10	08.7	00.3	04.0	10	* 0-6 ^o , * 10 ^o -14 ^o , □ 6 ^o -10 ^o , □
20	5	10*	10*	09	09.7	00.0	14.2	08	● 24 ^o , =2 ^o -22, □ 3 ^o , * 9 ^o -15 ^o , □
21	7	00	00	00	30.0	09.5	07.5	13	□
22	5	06	00	00	02.0	07.4	.	11	= 5-24, □
23	8	03	04	00	02.3	07.2	.	07	□
24	6	09	08	10	09.0	02.8	.	04	= 9-17, □
25	8	10	09	09	09.3	31.5	.	.	□ 18 ^o -19 ^o , 02 ^o -22 ^o
26	7	09	10	09	09.3	00.0	00.2	.	09 ^o -16 ^o
27	7	08	10	04	07.3	00.0	00.2	.	00 ^o -10 ^o
28	8	08	100	090	09.0	00.6	.	.	□ 5 ^o , 04 ^o -24 ^o

1978 MART

SARAJEVO

 $\varphi = 43^{\circ}52' N$ $\lambda = 18^{\circ}26' E$ Gr. $\Delta G = + 1h\ 14\ min.$

BR. ST. 139

Dan	Vazdušni pritisk P mm			Temperatura vazduha T C°								Napon vodenе pare e mm			Relativna vlažnost u %				Pravac i jačina veta D, f (0—12)			
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21		
1	702.5	702.6	704.9	05.8	14.6	09.1	09.7	15.4	05.5	37.0	06.4	07.0	05.8	92	57	67	72	E	2	S	4	WNW 2
2	705.6	703.8	704.8	02.4	15.2	07.6	08.2	16.4	02.3	03.0	04.8	05.5	05.7	88	42	73	68	ESE	3	WSW	2	ESE 3
3	704.7	702.3	702.4	02.0	17.8	08.8	09.4	18.4	01.8	32.6	04.8	05.7	04.6	90	37	54	60	ESE	4	WSW	1	ESE 3
4	702.5	701.0	703.2	02.6	21.1	10.8	11.3	21.2	02.4	33.1	04.7	06.3	06.1	85	34	63	61	SE	2	W	3	E 1
5	702.8	702.5	703.6	08.4	18.0	13.8	13.5	18.8	06.9	06.6	05.2	05.7	05.7	63	37	48	49	SE	1	S	6	S 1
6	702.7	700.8	701.6	09.8	13.6	09.0	10.4	14.4	08.8	09.5	06.6	07.1	08.0	73	61	93	76	SSE	1	-	0	- 0
7	704.1	703.3	707.2	05.6	04.1	02.8	03.8	09.0	02.8	37.0	06.4	05.0	04.6	94	81	82	86	NW	1	WSW	1	NW 1
8	707.8	706.6	707.1	01.0	05.6	01.2	02.3	06.3	01.0	33.5	03.6	03.4	04.7	74	49	93	72	-	0	-	0	ESE 2
9	706.8	705.3	708.1	-02.8	09.0	03.6	03.4	09.8	-03.2	-01.0	03.2	03.8	04.9	86	44	82	71	ESE	2	WNW	2	- 0
10	710.3	709.2	710.6	01.5	03.8	01.0	01.8	04.4	00.5	34.2	04.5	05.1	04.6	89	85	93	89	W	1	SE	2	- 0
11	710.7	707.9	704.9	00.2	05.8	03.6	03.3	05.9	00.2	02.5	04.5	04.2	04.9	97	61	82	80	NNW	2	N	1	ESE 2
12	704.7	705.5	708.0	02.2	02.3	01.2	01.7	03.7	01.0	04.1	03.2	03.2	03.2	60	59	65	61	N	2	S	4	- 0
13	708.7	707.4	708.4	-02.9	10.8	05.0	04.5	12.0	-03.6	-01.0	02.6	02.9	03.5	71	30	53	51	ESE	4	WNW	2	- 0
14	709.7	708.5	708.5	01.6	10.4	08.0	07.0	10.6	00.0	01.5	03.4	03.3	03.9	67	35	48	50	ESE	3	NW	2	S 5
15	706.7	704.0	704.5	07.4	11.0	06.2	07.7	12.4	06.0	07.8	06.0	05.9	05.6	77	60	79	72	N	1	S	4	- 0
16	706.2	704.5	704.1	01.6	13.9	09.4	08.8	14.2	01.4	03.0	04.8	03.5	04.3	94	29	49	57	ESE	1	W	5	S 3
17	699.1	699.4	701.6	09.3	09.8	03.9	06.7	10.8	03.9	10.2	04.2	06.0	05.9	48	66	97	70	S	3	S	3	- 0
18	702.0	703.5	706.2	01.6	02.2	01.8	01.9	04.0	01.5	04.0	05.0	05.2	04.9	97	97	94	96	-	0	-	0	E 1
19	707.4	705.5	706.7	01.8	07.3	-00.4	02.1	07.6	-00.4	02.6	04.9	04.7	04.3	94	62	96	84	E	2	ENE	1	W 2
20	706.2	702.3	700.5	-02.2	05.6	05.6	03.7	07.5	-02.4	-00.4	03.7	03.6	03.4	94	53	50	66	ENE	2	W	2	WNW 2
21	692.8	692.2	696.2	08.0	13.8	00.8	05.9	14.1	00.8	06.5	05.5	06.6	04.7	69	56	97	74	S	3	ENE	4	E 1
22	696.6	700.7	706.4	00.2	01.2	00.4	00.6	03.5	00.2	00.5	04.6	04.7	04.4	98	93	93	95	NW	2	N	3	- 0
23	707.8	704.8	703.1	-04.8	08.6	06.0	04.0	09.5	-05.2	-02.2	02.8	02.5	01.9	87	30	27	48	ESE	3	S	2	S 5
24	696.5	695.3	698.4	-04.4	08.4	01.6	04.0	09.5	01.5	05.9	04.2	04.4	05.1	67	54	98	73	S	3	WNW	2	WSM 2
25	701.5	704.4	707.0	00.4	02.2	01.2	01.3	03.0	00.4	01.0	04.6	05.0	04.8	97	94	97	96	WNW	2	W	2	- 0
26	706.5	703.2	703.7	-01.0	11.6	06.6	06.0	12.4	-01.4	01.4	04.0	02.9	04.9	93	28	67	63	ESE	1	SSW	2	WSM 3
27	704.5	706.5	708.9	01.0	02.4	01.2	01.5	06.6	01.0	01.5	04.8	05.1	04.7	97	94	93	95	-	0	MSW	2	- 0
28	711.6	711.0	711.9	-01.4	10.3	05.0	04.7	11.6	-02.5	-03.5	03.7	04.0	04.4	89	42	67	66	-	0	MSW	2	ESE 3
29	710.9	709.2	708.5	01.6	18.4	08.8	09.4	18.6	00.8	-00.5	04.4	04.2	05.2	86	26	62	58	ESP	3	MSW	2	ESE 4
30	708.0	705.2	704.8	04.2	19.0	10.6	11.1	19.7	03.2	02.0	04.6	04.5	04.9	74	28	51	51	ESE	3	SW	3	ESE 2
31	703.9	702.1	703.5	04.6	18.2	10.8	11.1	18.4	03.4	02.5	05.5	05.0	05.1	86	32	53	57	ESE	3	MSW	3	SE 3
MES.	VRED.	704.9	704.0	705.1	02.4	10.2	05.3	05.8	11.3	01.2	03.1	04.6	04.7	04.8	83	53	73	70	1.9	2.3	1.6	

1978 APRIL

SARAJEVO

1	702.8	699.1	698.2	04.4	16.0	11.0	10.6	16.0	03.5	02.5	04.7	04.9	06.1	75	36	62	58	E	3	S	2	E 2
2	697.4	696.6	698.2	04.2	10.4	06.4	06.9	14.3	04.0	02.5	05.9	06.0	05.8	96	63	81	80	ESE	1	ESE	5	ESE 1
3	698.9	696.8	695.7	04.1	15.6	12.0	10.9	15.9	02.8	02.0	05.1	05.0	05.2	83	37	50	57	ESE	3	SE	4	E 3
4	696.1	697.7	700.0	08.6	09.6	07.4	08.3	12.0	07.4	07.5	06.8	06.3	06.8	81	70	87	79	-	0	E	3	- 0
5	700.6	700.9	702.3	07.0	08.9	07.2	07.6	09.7	06.6	06.5	06.9	07.8	07.1	92	92	94	93	ENE	1	-	0	WNW 1
6	704.3	705.4	707.1	06.1	07.2	05.0	05.8	07.3	05.0	05.4	06.5	05.7	04.9	92	75	75	81	-	0	E	2	E 3
7	706.2	702.6	699.8	02.8	07.0	03.4	04.2	07.3	02.8	02.3	03.9	04.2	05.0	70	55	85	70	ESE	4	SE	3	ESE 3
8	697.9	698.5	699.4	02.9	04.2	03.2	04.4	01.4	01.2	05.1	06.0	05.4	97	97	94	96	-	0	NW	1	WNW 1	
9	700.5	701.4	702.4	03.0	07.2	06.8	06.0	08.0	01.4	03.0	05.5	06.3	06.6	97	82	90	90	-	0	WSW	1	- 0
10	702.6	703.3	704.3	05.5	14.4	09.6	09.8	15.0	05.0	04.0	06.5	06.1	05.7	96	49	64	70	-	0	SW	2	S 2
11	705.2	705.7	706.9	10.0	13.8	10.6	11.3	14.3	08.5	J7.5	04.9	05.3	J5.4	54	45	57	52	S	5	W	3	W 1
12	706.1	704.5	703.5	12.4	20.4	14.6	15.5	21.1	08.8	J8.0	05.0	05.2	03.6	46	29	28	34	S	6	S	3	W 3
13	699.2	695.8	694.1	15.6	18.0	14.4	15.6	18.0	10.4	10.3	05.4	07.3	07.2	40	47	58	48	E	2	S	6	S 3
14	695.1	695.1	696.2	11.1	13.4	07.2	09.7	14.4	07.2	J9.0	05.8	04.0	04.6	59	35	61	52	S	3	S	6	ENE 2
15	694.5	694.8	696.5	06.6	J9.4	J5.0	06.5	10.3	04.9	04.5	05.5	05.8	05.6	76	66	86	76	ESE	5	S	2	E 1
16	697.2	699.8	702.4	03.8	35.0	03.2	03.8	05.0	03.1	01.7												

BR. ST. 139

 $H_s = 630 \text{ m } H_b = 637.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$

Dan	Vrij.	Oblačnost N (0-10)					Inodrž. broj	Padavina R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dnes				
1	7 09	090	00	06.0	04.0	03.0	.	0-6°, □ 22-24		
2	8 01	080	01	03.3	08.8	.	.	□ 0-9		
3	6 000	010	00	00.3	09.8	.	.	= 70°, 10°		
4	8 000	010	01	00.7	08.4	.	.	□ 0-9		
5	8 08	090	08	08.3	04.8	.	.	□ 140°, 120°, 22°, 23°		
6	7 10	09	09	09.3	00.2	00.0	.	0-6°, 10°, 10°		
7	6 10*	10	10	10.0	00.0	06.5	.	0-0°, = 0-16, 9, 11°-17		
8	7 09	09	00	06.0	02.3	00.6	.	0-0°, □ 13-14		
9	6 07	09	10*	08.7	03.5	.	.	□ 0-1, □ 1-7°, = 6°, 19°, 0-13-14		
10	7 10*	09*	09	09.3	01.3	00.9	.	0-3°, * 3°, 0-10°, 13°, 11°; = 11°, 13°, 0-13°		
11	6 08	10	08	08.7	00.9	04.8	.	* 0-4°, = 0-19°, 0-22°, 13°		
12	7 08	080	08	08.0	02.4	00.3	.	□ 50°, 60°, * 7-15		
13	8 000	030	00	01.0	08.9	00.1	.	□ 0-8		
14	7 09	09	09	09.0	00.6	.	.	□ 0-9		
15	7 09*	10*	08	19.0	03.0	00.0	.	0-5°, 10°		
16	8 010	020	09	04.0	08.8	04.8	.	□ 5°, 13°		
17	8 10	10*	10*	10.0	01.2	.	.	□ 0-0°, 10°, 0-13-14, = 12-14		
18	6 10*	10*	09	09.7	00.0	30°	.	0-5°, 10°, = 0-15°, 13°, 6, * 6-9°, 13°-14°		
19	6 09	09	10*	09.3	01.6	18.4	.	= 0-4°, 0-16-17, 2-17-19°, * 17-24, 13°		
20	8 000	10	09	06.3	33.1	06.5	08	* 0-2°, = 0-16, □ 13°, 12°, 13°, 0-23°, 24°, 13°		
21	8 10*	090	10*	09.7	32.1	00.4	.	0-12°, 15°, 19°, □ 14°, 0-16°, 17°, 18°, 19°, 20°, 21°, □ 15°, = 13-14, * 19°-21°		
22	7 10*	10*	09	09.7	30.7	17.7	02	= 0-12°, 13°, 14°, * 1-15°, 13°		
23	8 000	060	09	05.0	10.5	03.8	.	□ 0-1°, 0-6°, 10°		
24	8 10*	09	10*	09.7	04.0	00.0	.	□ 0-1°, 0-6°, 10°, 11°, * 10-20°, = 0-10°		
25	6 10*	10*	10	09	06.3	00.0	01.3	= 0-24, 0-16, 13°, 12°, 13°, 0-23°, 24°		
26	8 01	010	10*	04.0	08.7	01.6	.	= 0-30°, 20°, 24°, □ 3-8, 0-10°, 24		
27	6 10*	10*	00	06.7	20.0	04.0	.	= 0-15°, 0-3°, 14°, 17°, * 20°, 21°, 22°, 23°		
28	8 09	070	00	05.3	08.7	01.0	.	□ 0-8		
29	8 000	000	00	00.0	10.9	.	.	□ 0-4°, 22-24, □ 4-6°		
30	8 000	080	00	02.7	11.0	.	.	□ 0-9		
31	8 000	040	05	03.0	10.3	.	.	□ 0-9		
MES.	VRED.	06.1	07.4	06.2	06.5	140.5	106.3			

1	7 08	090	09	08.7	04.8	.	.	△ 0-10, 0-12°, 13°		
2	7 03	10	00	04.3	03.3	00.7	.	0-5°, 5°, □ 0-2-24		
3	8 000	09	10	06.3	05.5	00.0	.	△ 0-3, □ 16°, 17, 0-21-24		
4	7 10*	10	10*	10.0	00.0	01.0	.	0-5°, 15°, 14°		
5	6 10*	10*	10*	10.0	00.0	00.4	.	0-1, 6°, 23°, = 0-24		
6	6 10*	10	10	10.0	00.0	07.1	.	= 0-16, 0-3°, 0-10, 21°, 24		
7	8 09	090	10	09.3	09.0	02.1	.	0-4°, 12°, 17°, 21°, 24, □ 5-9°		
8	6 10*	10*	10*	10.0	00.0	05.2	.	□ 2°, 24°, = 3-24		
9	6 10*	10	10*	10.0	00.0	04.3	.	0-6°, 10°, 22°, = 0-24, 9, 20, 21		
10	7 08	09	09	08.7	01.7	00.3	.	= 0-1, □ 0-8, 0-12, 0-22		
11	8 09	09	09	09.0	04.3	00.0	.	△ 0-8, □ 7-15, 17-18		
12	8 030	050	00	02.7	09.9	.	.	□ 15°, 16°, 17°, 18°, 19°, 20°, 21°, 22°, 23°		
13	8 08	09	09	08.7	31.6	.	.	□ 3°, 19°, 21°, 0-4-9, 12, 13, 14, 15, 16, 17		
14	8 070	050	08	06.7	11.1	04.1	.	0-5, 22°, 24°, □ 3-8, 10°, 11°		
15	7 10*	08	05	07.7	01.2	01.5	.	0-10°, 0-12, 13, 14, 15, 16, 17, 18, 19, 20, 21, 22, 23, □ 6-10°, 9-11°, 12-13°, □ 24-25°, 26-27°, 28-29°, 2-10°, 11-12°, 13-14°, 15-16°, 17-18°, 19-20°, 21-22°, 23-24°, 25-26°, 27-28°, 29-30°, 31-32°, 33-34°, 35-36°, 37-38°, 39-40°, 41-42°, 43-44°, 45-46°, 47-48°, 49-50°, 51-52°, 53-54°, 55-56°, 57-58°, 59-60°, 61-62°, 63-64°, 65-66°, 67-68°, 69-70°, 71-72°, 73-74°, 75-76°, 77-78°, 79-80°, 81-82°, 83-84°, 85-86°, 87-88°, 89-90°, 91-92°, 93-94°, 95-96°, 97-98°, 99-100°, 101-102°, 103-104°, 105-106°, 107-108°, 109-110°, 111-112°, 113-114°, 115-116°, 117-118°, 119-120°, 121-122°, 123-124°, 125-126°, 127-128°, 129-130°, 131-132°, 133-134°, 135-136°, 137-138°, 139-140°, 141-142°, 143-144°, 145-146°, 147-148°, 149-150°, 151-152°, 153-154°, 155-156°, 157-158°, 159-160°, 161-162°, 163-164°, 165-166°, 167-168°, 169-170°, 171-172°, 173-174°, 175-176°, 177-178°, 179-180°, 181-182°, 183-184°, 185-186°, 187-188°, 189-190°, 191-192°, 193-194°, 195-196°, 197-198°, 199-200°, 201-202°, 203-204°, 205-206°, 207-208°, 209-210°, 211-212°, 213-214°, 215-216°, 217-218°, 219-220°, 221-222°, 223-224°, 225-226°, 227-228°, 229-221°, 223-224°, 225-226°, 227-228°, 229-230°, 231-232°, 233-234°, 235-236°, 237-238°, 239-231°, 233-234°, 235-236°, 237-238°, 239-240°, 241-242°, 243-244°, 245-246°, 247-248°, 249-241°, 243-244°, 245-246°, 247-248°, 249-250°, 251-252°, 253-254°, 255-256°, 257-258°, 259-251°, 253-254°, 255-256°, 257-258°, 259-260°, 261-262°, 263-264°, 265-266°, 267-268°, 269-261°, 263-264°, 265-266°, 267-268°, 269-270°, 271-272°, 273-274°, 275-276°, 277-278°, 279-271°, 273-274°, 275-276°, 277-278°, 279-280°, 281-282°, 283-284°, 285-286°, 287-288°, 289-281°, 283-284°, 285-286°, 287-288°, 289-290°, 291-292°, 293-294°, 295-296°, 297-298°, 299-291°, 293-294°, 295-296°, 297-298°, 299-300°, 301-302°, 303-304°, 305-306°, 307-308°, 309-301°, 303-304°, 305-306°, 307-308°, 309-310°, 311-312°, 313-314°, 315-316°, 317-318°, 319-311°, 313-314°, 315-316°, 317-318°, 319-320°, 321-322°, 323-324°, 325-326°, 327-328°, 329-321°, 323-324°, 325-326°, 327-328°, 329-330°, 331-332°, 333-334°, 335-336°, 337-338°, 339-331°, 333-334°, 335-336°, 337-338°, 339-340°, 341-342°, 343-344°, 345-346°, 347-348°, 349-341°, 343-344°, 345-346°, 347-348°, 349-350°, 351-352°, 353-354°, 355-356°, 357-358°, 359-351°, 353-354°, 355-356°, 357-358°, 359-360°, 361-362°, 363-364°, 365-366°, 367-368°, 369-361°, 363-364°, 365-366°, 367-368°, 369-370°, 371-372°, 373-374°, 375-376°, 377-378°, 379-371°, 373-374°, 375-376°, 377-378°, 379-380°, 381-382°, 383-384°, 385-386°, 387-388°, 389-381°, 383-384°, 385-386°, 387-388°, 389-390°, 391-392°, 393-394°, 395-396°, 397-398°, 399-391°, 393-394°, 395-396°, 397-398°, 399-400°, 401-402°, 403-404°, 405-406°, 407-408°, 409-401°, 393-394°, 395-396°, 397-398°, 399-400°, 401-402°, 403-404°, 405-406°, 407-408°, 409-410°, 411-412°, 413-414°, 415-416°, 417-418°, 419-411°, 413-414°, 415-416°, 417-418°, 419-420°, 421-422°, 423-424°, 425-426°, 427-428°, 429-421°, 423-424°, 425-426°, 427-428°, 429-430°, 431-432°, 433-434°, 435-436°, 437-438°, 439-431°, 433-434°, 435-436°, 437-438°, 439-440°, 441-442°, 443-444°, 445-446°, 447-448°, 449-441°, 433-434°, 435-436°, 437-438°, 439-440°, 441-442°, 443-444°, 445-446°, 447-448°, 449-450°, 451-452°, 453-454°, 455-456°, 457-458°, 459-451°, 453-454°, 455-456°, 457-458°, 459-460°, 461-462°, 463-464°, 465-466°, 467-468°, 469-461°, 453-454°, 455-456°, 457-458°, 459-460°, 461-462°, 463-464°, 465-466°, 467-468°, 469-470°, 471-472°, 473-474°, 475-476°, 477-478°, 479-471°, 473-474°, 475-476°, 477-478°, 479-480°, 481-482°, 483-484°, 485-486°, 487-488°, 489-481°, 473-474°, 475-476°, 477-478°, 479-480°, 481-482°, 483-484°, 485-486°, 487-488°, 489-490°, 491-492°, 493-494°, 495-496°, 497-498°, 499-491°, 493-494°, 495-496°, 497-498°, 499-500°, 501-502°, 503-504°, 505-506°, 507-508°, 509-501°, 493-494°, 495-496°, 497-498°, 499-500°, 501-502°, 503-504°, 505-506°, 507-508°, 509-510°, 511-512°, 513-514°, 515-516°, 517-518°, 519-511°, 513-514°, 515-516°, 517-518°, 519-520°, 521-522°, 523-524°, 525-526°, 527-528°, 529-521°, 513-514°, 515-516°, 517-518°, 519-520°, 521-522°, 523-524°, 525-526°, 527-528°, 529-530°, 531-532°, 533-534°, 535-536°, 537-538°, 539-531°, 533-534°, 535-536°, 537-538°, 539-540°, 541-542°, 543-544°, 545-546°, 547-548°, 549-541°, 533-534°, 535-536°, 537-538°, 539-540°, 541-542°, 543-544°, 545-546°, 547-548°, 549-550°, 551-552°, 553-554°, 555		

$\varphi = 43^{\circ}52' N \lambda = 18^{\circ}26' E$ Gr. $\Delta G = +1h\ 14\ min.$

BR. ST. 139

d	Vazdušni pritisak P mm			Temperatura vazduha T °C								Napon vodenе pare ø mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0-12)					
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21			
1	700.0	696.0	697.0	15.5	24.8	16.8	18.5	25.0	12.6	09.5	05.1	06.5	07.6	39	28	53	40	SW	2	S	4	SE 2	
2	691.8	694.1	699.3	11.8	07.8	08.0	08.9	16.8	07.8	11.2	09.9	07.3	07.8	96	92	98	95	NW	1	W	5	NNW 1	
3	703.3	705.0	708.1	09.2	17.9	12.2	12.9	18.2	07.3	07.8	08.3	06.4	04.9	95	41	46	61	-	0	W	4	S 1	
4	710.1	709.5	710.2	07.4	18.6	11.6	12.3	19.0	05.0	03.7	05.6	05.2	06.8	73	32	66	57	E	1	WSW	2	ESE 2	
5	711.1	708.7	708.0	08.8	23.4	16.2	16.2	24.0	06.2	04.9	06.4	06.3	06.3	75	29	46	50	ESE	1	W	1	ESE 1	
6	706.7	706.1	704.3	14.0	20.2	12.0	14.6	23.0	12.0	11.6	06.7	05.0	08.7	56	28	83	56	E	2	WSW	2	ESE 1	
7	700.8	700.3	700.0	13.2	13.6	11.0	12.2	16.5	10.5	05.0	07.1	08.7	08.1	62	74	82	73	S	3	-	0	ENE 1	
8	699.6	698.6	700.2	07.6	15.0	09.8	10.6	15.3	05.6	04.6	07.2	06.9	07.7	92	54	85	77	E	3	SSW	1	-	0
9	701.0	701.0	704.2	09.8	16.6	10.9	12.1	17.4	08.7	09.9	08.5	07.9	08.9	93	56	91	80	-	0	W	2	-	0
10	705.5	707.4	709.1	09.6	10.0	08.0	08.9	15.0	07.7	07.5	08.1	08.9	07.8	91	96	97	95	-	0	SW	2	-	0
11	708.1	707.3	709.1	05.0	07.0	04.2	05.1	08.2	04.2	05.0	06.2	06.0	04.6	94	80	74	83	ESE	3	ENE	3	SSE 1	
12	707.4	706.2	705.3	01.0	05.4	01.2	02.2	06.4	00.5	01.3	03.8	03.2	03.5	77	47	71	65	W	2	MNW	1	-	0
13	703.3	702.4	699.7	02.4	09.8	09.2	07.7	10.6	-00.9	-01.5	03.9	06.0	07.5	72	66	86	75	E	1	ESE	2	ESE 2	
14	701.1	703.1	705.4	04.0	12.8	08.0	08.2	13.8	04.0	05.0	05.9	07.6	07.6	97	68	95	87	E	4	W	2	WSW 2	
15	705.9	703.5	704.5	06.4	15.8	11.0	11.1	16.6	06.2	06.4	06.6	06.7	06.7	92	50	68	70	-	0	MNW	2	-	0
16	705.8	706.1	708.0	05.6	15.3	10.6	10.5	17.5	04.2	03.4	06.4	05.8	08.0	93	44	83	73	ESE	1	W	2	ENE 2	
17	709.0	707.9	708.3	07.8	19.8	13.8	13.8	20.4	05.6	04.8	06.8	05.5	07.6	86	32	65	61	ESE	3	NW	2	-	0
18	708.9	708.3	708.4	11.4	19.0	12.4	13.8	19.5	10.2	10.0	08.6	08.4	09.4	85	51	87	74	-	0	W	2	E	1
19	707.5	705.0	706.0	11.2	23.2	14.4	15.8	23.5	10.0	09.3	08.6	07.9	09.6	87	37	78	67	-	0	W	1	ENE 1	
20	705.9	705.5	707.4	11.8	21.7	13.4	15.1	22.8	11.2	10.5	10.2	10.8	10.8	98	56	94	83	E	2	NW	2	ENE 2	
21	707.4	706.4	706.3	12.6	20.6	16.0	16.3	21.0	10.2	09.0	09.7	10.7	09.6	88	59	70	72	E	1	ESE	2	E 3	
22	702.5	700.3	698.4	16.8	18.8	15.2	16.5	20.0	14.0	14.0	08.5	08.8	08.1	59	54	63	59	E	2	S	4	SSW 2	
23	699.7	701.6	702.8	12.0	17.8	13.2	14.1	18.0	09.7	09.8	08.7	07.9	07.3	83	51	64	66	W	1	S	4	NW 2	
24	703.7	704.1	705.3	12.8	18.4	14.1	14.9	19.6	09.2	08.0	07.9	07.5	07.8	71	47	65	61	W	1	W	3	-	0
25	705.7	705.4	707.2	10.6	17.2	12.2	13.1	17.4	08.3	07.7	07.5	08.3	10.2	79	56	96	77	-	0	W	2	-	0
26	708.0	706.4	708.8	11.2	16.2	11.6	12.7	18.1	11.0	10.5	09.4	08.7	09.8	94	63	96	84	-	0	SE	4	-	0
27	707.9	708.1	708.0	10.2	09.6	08.4	09.2	11.8	08.4	10.4	08.9	08.1	08.1	95	91	98	95	-	0	MNW	1	-	0
28	707.3	707.6	707.9	08.4	11.9	09.2	09.7	13.5	07.2	08.5	08.1	09.1	08.3	98	87	95	93	-	0	WSW	2	-	0
29	706.5	705.7	705.5	08.9	12.4	10.2	10.4	15.0	08.6	09.0	08.2	09.2	08.7	96	85	93	91	-	0	W	1	-	0
30	705.7	706.6	708.1	09.6	12.6	10.6	10.9	13.5	08.5	09.0	08.3	09.5	09.1	93	87	95	92	-	0	W	1	-	0
31	710.0	708.8	710.7	10.0	21.8	14.4	15.2	22.0	07.9	07.5	08.4	07.8	08.2	91	40	67	66	-	0	E	3	ESE 2	
MES.	VRED.	705.1	704.6	705.5	09.6	16.0	11.3	12.0	17.4	07.8	07.7	07.5	07.5	07.9	84	57	79	73	1.1	2.2	0.9		

1	712.1	711.2	711.8	10.4	21.0	13.2	14.5	21.6	08.2	07.3	08.2	08.3	09.3	86	45	81	71	-	0	ESE	1	ESE 1	
2	711.9	709.8	710.0	11.2	22.4	14.6	15.7	23.5	08.5	07.6	08.5	06.6	09.2	86	32	74	64	-	0	NE	2	ESE 2	
3	710.0	708.3	710.0	12.0	24.2	13.8	16.0	24.8	08.9	08.3	08.8	05.7	09.2	84	25	78	62	-	0	NE	3	E 2	
4	711.0	710.3	710.8	11.6	21.4	14.4	15.5	24.8	09.0	08.4	08.9	08.3	09.6	87	43	78	69	-	0	NE	3	-	0
5	711.6	710.1	710.7	12.0	25.4	16.6	17.7	25.6	09.3	08.5	08.1	09.2	08.6	77	38	61	59	E	1	W	2	ESE 2	
6	710.6	709.0	709.9	13.8	22.0	16.4	17.2	27.0	10.2	09.5	09.1	08.2	09.4	77	41	67	62	ESE	1	W	2	ESE 2	
7	710.4	709.4	709.2	14.3	27.4	20.0	20.4	27.4	11.8	11.0	09.3	08.0	10.4	76	29	60	55	ESE	1	W	2	-	0
8	709.2	708.1	708.1	16.0	26.4	20.2	20.7	26.4	13.4	12.5	10.6	10.7	09.7	77	41	55	58	ESE	2	W	3	-	0
9	709.6	708.2	707.9	17.4	24.8	18.6	19.9	26.0	16.4	18.0	10.6	10.9	10.1	71	46	63	60	W	2	W	2	ESE 2	
10	708.1	706.9	707.9	16.3	28.4	22.8	22.6	28.5	13.8	12.0	10.2	10.3	09.9	73	36	48	52	E	1	NW	2	NW 1	
11	709.0	709.1	710.7	18.4	24.2	17.0	19.2	27.6	16.8	15.6	11.7	10.9	13.2	74	48	91	71	-	0	NW	3	ESE 2	
12	707.5	704.2	702.8	18.0	27.8	21.6	22.3	31.4	14.1	14.6	12.4	08.1	08.9	80	29	46	52	E	3	S	4	W 3	
13	702.2	703.9	704.9	16.6	13.4	12.0	13.5	21.6	09.8	13.9	11.8	10.8	09.8	83	94	93	90	-	0	SW	1	NW 2	
14	704.0	702.9	703.4	10.8	22.4	16.6	16.6	22.7	10.5	10.6	09.4	11.3	08.8	97	56	62	72	SE	2	MNW	3	-	0
15	704.2	702.8	701.4	13.0	18.0	13.2	14.4	18.8	12.2	10.8	12.0	10.9	09.9										

BR. ST. 139

 $H_s = 630 \text{ m } H_b = 637.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$

Dan	Vreme god. v. y.	Oblačnost N (0-10)					Intenzitet suncobijanja broj	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dnes				
1	8 08	040	08	06.7	09.7	00.0	.			
2	7 100	100	100	10.0	00.2	26.0	.			
3	8 09	050	00	04.7	10.7	30.0	.			
4	8 040	10	00	04.7	06.5	.	.			
5	8 010	040	08	04.3	10.3	.	.			
6	8 09	10	100	09.7	01.8	00.0	.			
7	8 09	100	03	07.3	J1.0	04.4	.			
8	8 06	09	100	08.3	02.6	00.6	.			
9	8 09	09	09	09.0	03.4	01.1	.			
10	7 09	100	100	09.7	00.5	00.7	.			
11	7 100	10	100	10.0	00.0	19.6	.			
12	7 10*	08	00	06.0	02.2	00.5	.			
13	7 10	090	100	09.7	00.0	00.0	.			
14	8 080	09	090	08.7	04.1	38.8	.			
15	7 10	08	04	07.3	06.4	01.1	.			
16	7 050	070	090	07.0	10.0	.	.			
17	8 040	08	070	06.3	08.2	01.3	.			
18	7 100	09	00	06.3	01.5	00.4	.			
19	8 08	090	00	05.7	07.8	00.4	.			
20	7 09	020	09%	06.7	05.8	02.4	.			
21	8 070	10	10	09.0	04.8	06.1	.			
22	8 10	09	09	09.3	00.3	.	.			
23	8 06	08	04	06.0	09.6	15.5	.			
24	8 06	080	G3	05.7	08.2	00.3	.			
25	8 090	08	100	09.0	01.5	00.0	.			
26	7 100	100	100	10.0	01.3	01.9	.			
27	6 100	100	10	10.0	00.0	15.3	.			
28	6 100	100	10	10.0	00.1	07.5	.			
29	7 100	10	080	09.3	00.9	20.9	.			
30	6 10	100	10	10.0	00.2	03.9	.			
31	8 09	080	06	07.7	08.5	04.6	.			
MES. VRED.		08.2	08.4	07.0	07.9	127.8	203.3			

SARAJEVO

1978 JUN

1	8 040	03	08	05.0	08.1	.	.			
2	8 030	06	03	04.0	10.4	00.2	.			
3	8 020	03	04	03.0	10.4	00.0	.			
4	8 000	090%	00	03.0	09.2	01.0	.			
5	7 060	070	00	04.3	12.0	00.0	.			
6	8 010	090%	01	03.7	09.7	.	.			
7	8 020	020	00	01.3	12.8	00.2	.			
8	8 08	040	10	07.3	06.0	.	.			
9	8 10	030	04	05.7	10.1	.	.			
10	8 000	080	08	05.3	09.5	.	.			
11	8 10	090	05	08.0	03.1	.	.			
12	8 08	080	08	08.0	09.3	06.4	.			
13	7 090	100	100	09.7	00.1	00.0	.			
14	8 100	050	01	05.3	08.6	29.8	.			
15	7 100	10	100	10.0	00.0	03.4	.			
16	7 10	09	01	06.7	00.8	47.1	.			
17	8 09	080	08	08.3	06.1	00.1	.			
18	8 050	040	04	04.3	10.2	.	.			
19	8 090	100	10	09.7	00.7	00.2	.			
20	7 080	010	04	04.3	11.7	01.2	.			
21	7 09	10	100	09.7	03.7	.	.			
22	8 09	08	00	05.7	19.4	13.4	.			
23	7 01	050	00	02.0	13.6	.	.			
24	8 01	080	00	13.0	10.4	.	.			
25	8 01	060	00	02.3	17.5	.	.			
26	7 09	100	06	18.3	01.4	.	.			
27	6 10	100	100	19.0	03.0	03.8	.			
28	6 100	100	10	19.0	01.5	00.3	.			
29	8 10	08	01	16.0	16.7	12.4	.			
30	7 01	030	00	01.0	01.0	0.1	.			
MES. VRED.		06.2	06.9	04.5	15.8	217.1	143.5			

1978 JUL

SARAJEVO

 $\varphi = 43^{\circ}52' N$ $\lambda = 18^{\circ}26' E$ Gr. $\Delta G = + 1h 14 min.$

BR. ST. 139

D	Vazdušni pritisk P mm			Temperatura vazduha T C°								Napon vodené pory e mm			Relativna vlažnosť u %			Pravac i jačina veta D, f (0-12)			
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21	
1	710.1	709.1	709.6	11.4	26.4	18.2	18.6	26.8	08.7	36.8	08.6	06.0	10.8	85	23	69	59	ENF	1	WSW	1
2	708.3	707.6	708.2	17.7	26.0	19.0	20.4	26.2	13.0	12.3	10.1	07.9	08.8	67	31	53	50	E	1	S	3
3	707.4	706.3	706.3	15.6	23.8	18.4	19.1	24.3	14.6	14.4	12.8	10.9	12.0	96	49	75	73	-	0	-	0
4	706.6	705.4	705.5	15.0	26.0	20.2	20.4	26.4	12.8	11.0	10.5	09.2	09.3	82	36	53	57	ESE	1	W	2
5	704.7	703.4	705.0	19.6	26.2	15.8	19.4	26.6	15.3	13.6	10.2	09.1	12.5	60	36	93	63	S	1	S	4
6	707.0	705.7	705.8	12.8	25.2	17.8	18.4	25.5	11.6	11.0	10.7	10.1	08.5	97	42	56	65	S	1	W	2
7	704.0	705.1	706.2	17.2	18.4	13.4	15.6	21.4	13.2	14.5	09.7	09.6	10.1	66	60	88	71	WNW	3	S	1
8	707.8	709.0	709.0	11.2	13.2	11.6	11.9	14.4	10.4	10.4	09.2	08.7	08.7	92	76	85	84	-	0	-	0
9	707.7	705.0	704.8	11.1	22.2	17.5	17.1	22.4	09.6	08.8	08.3	07.6	07.8	83	38	52	58	-	0	WSW	2
10	704.8	704.5	705.9	12.2	23.4	19.2	18.5	24.4	09.6	09.0	08.6	08.8	09.5	81	41	57	60	SE	1	W	4
11	707.2	707.1	707.5	15.0	26.8	19.6	20.3	27.0	12.5	11.5	09.6	10.3	12.5	75	39	73	62	ESE	1	WSW	2
12	709.1	708.2	708.8	15.6	30.0	21.4	22.1	30.5	13.4	11.6	12.1	10.6	11.6	91	33	61	62	ESE	1	WNW	2
13	710.8	710.0	710.9	16.8	28.5	21.0	21.9	28.6	13.8	13.0	10.4	12.0	13.5	73	41	72	62	-	0	WSW	3
14	710.8	709.3	709.6	16.2	28.4	20.2	21.3	28.4	15.0	13.6	12.1	12.1	12.2	88	42	69	66	-	0	ENE	3
15	708.0	707.0	708.3	16.7	16.6	15.6	16.1	23.6	14.9	13.2	12.9	13.6	12.8	91	96	96	94	-	0	NE	2
16	709.1	707.8	708.4	14.6	23.2	16.3	17.6	23.7	14.0	14.2	10.5	08.0	10.5	84	38	76	66	ESE	2	NE	2
17	709.8	708.9	709.5	14.0	26.6	20.8	20.6	26.7	11.3	10.8	09.9	11.4	14.2	83	44	77	68	ESE	2	W	1
18	709.0	706.3	705.0	15.4	29.4	23.8	23.1	29.5	14.2	13.3	12.1	11.0	08.7	92	36	39	56	-	0	W	4
19	701.8	700.2	704.2	24.0	27.4	16.0	20.9	28.2	15.9	20.0	08.7	08.1	11.2	39	30	82	50	WSW	3	S	3
20	706.5	705.3	705.2	13.0	23.0	15.8	16.9	24.0	11.3	10.6	09.4	08.3	09.0	83	39	67	63	-	0	SW	1
21	705.1	703.0	704.3	12.2	24.4	17.6	18.0	25.2	09.8	09.0	08.5	07.1	10.2	80	31	67	59	-	0	-	0
22	708.4	709.5	710.6	10.2	16.2	11.6	12.4	18.0	10.0	10.5	09.1	07.4	06.8	98	54	66	73	-	0	ENE	2
23	711.2	710.3	710.2	08.4	18.0	12.0	12.6	19.0	06.4	05.2	07.5	06.9	07.4	90	45	70	68	ESE	2	W	2
24	710.3	708.7	709.3	08.2	20.8	13.9	14.2	20.9	05.9	05.3	07.0	08.1	08.5	85	44	71	67	-	0	W	2
25	710.3	708.3	709.2	09.4	22.6	17.0	16.5	22.6	07.3	06.5	07.4	07.9	08.5	84	39	59	61	-	0	ESE	2
26	709.8	708.1	708.8	10.6	24.8	17.0	17.4	24.8	09.5	09.5	08.6	09.0	10.1	90	38	69	66	-	0	ESE	2
27	709.7	708.9	710.3	12.4	25.8	18.4	18.8	26.2	11.0	09.6	09.2	11.8	10.9	85	47	69	67	-	0	W	2
28	711.4	710.9	712.2	13.6	27.8	19.0	19.9	27.8	11.5	10.6	09.5	08.1	08.2	82	29	50	54	ESE	1	SE	3
29	712.9	710.7	710.9	13.0	24.8	17.8	18.4	25.3	11.0	09.8	09.1	09.5	10.6	81	40	69	63	ESE	1	E	2
30	710.3	708.1	708.8	13.0	21.6	16.0	16.7	23.5	11.5	10.4	10.1	10.7	11.3	89	55	83	76	ESE	1	WNW	2
31	708.7	707.5	708.4	12.0	26.7	17.4	18.4	26.8	10.2	09.0	10.1	06.3	10.1	96	24	68	63	SW	1	W	2
MES.	VRED.	708.3	707.3	708.0	13.8	24.0	17.4	18.2	24.8	11.6	11.0	09.8	09.2	10.2	83	42	69	65	0.8	2.0	1.3

1978 AVGUST

SARAJEVO

1	709.8	708.7	709.5	13.6	27.0	19.0	19.7	27.7	11.3	10.6	09.5	09.0	10.9	82	34	66	61	SE	1	WNW	2	ESE	2	
2	710.0	708.5	708.7	15.8	30.6	22.3	22.8	31.0	13.4	12.1	10.6	10.4	13.0	79	32	64	58	ESE	1	NW	1	ESE	1	
3	709.9	707.7	708.6	16.2	29.8	21.6	22.3	30.0	15.0	13.7	12.7	12.0	12.9	92	38	67	66	ESE	2	WSW	2	-	0	
4	709.0	708.4	707.1	17.2	24.6	20.4	20.7	25.4	15.5	14.0	12.5	13.0	14.1	85	56	78	73	ESE	3	-	0	-	0	
5	707.9	708.5	708.5	18.2	25.2	17.6	19.7	25.6	16.9	16.8	13.4	12.1	11.8	86	50	78	71	-	0	NW	2	ESE	2	
6	708.8	707.1	707.0	14.4	28.5	20.2	20.8	28.8	12.6	11.5	10.8	08.6	10.6	88	29	60	59	ESE	1	SW	1	ESE	2	
7	706.6	704.0	703.3	15.6	31.4	24.2	23.9	31.9	13.9	12.4	10.4	11.3	07.2	78	33	32	48	-	0	WSW	2	ENE	2	
8	699.1	699.5	702.3	25.4	27.7	21.0	23.8	28.0	13.5	19.0	09.6	10.7	07.6	39	39	40	39	S	6	S	5	S	3	
9	706.0	705.8	705.9	14.8	24.6	17.6	18.7	25.2	13.6	11.6	09.2	07.8	08.4	73	33	55	54	-	0	N	2	E	1	
10	707.0	706.7	708.0	12.0	20.6	13.2	14.8	20.6	10.5	08.2	10.4	11.1	78	57	98	78	-	0	SSW	1	-	0	-	0
11	708.6	707.4	708.3	11.6	16.4	14.8	14.6	19.3	10.6	10.5	09.9	12.1	08.6	97	87	68	84	-	0	E	2	NNE	1	
12	709.7	709.4	710.1	11.2	18.2	12.2	13.5	19.5	09.7	09.3	09.5	08.8	08.6	96	56	81	78	-	0	W	2	E	2	
13	711.1	709.0	708.2	08.2	22.2	15.3	15.3	22.6	06.7	06.1	07.2	06.4	08.1	88	32	62	61	ESE	1	SW	2	ESE	2	
14	708.2	707.8	709.6	11.6	21.2	14.8	15.6	24.4	10.8	10.0	08.2	09.6	11.4	80	51	90	74	-	0	ENE	2	E	3	
15	710.9	708.8	709.7	11.0	26.2	16.8	17.7	26.2	10.0	09.0	09.5	08.8	10.2	97	35	71	68	E	1	NNW	2	E	2	
16	710.9	709.3	709.6	12.8	28.6	18.2	19.5	29.0	11.0	10.0	08.8	08.3	09.3	79	28	59	55	-	0	W	1</td			

SARAJEVO

1978 JUL

BR. ST. 139

$$H_s = 630 \text{ m } H_b = 637.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$$

SARAJEVO

1970 AUGUST

1	7	000	010	00	00.3	12.5	.	.	Δ 0-0,20-24
2	8	000	010	00	00.3	12.5	.	.	Δ 0-0,21-24
3	8	000	040	00	01.3	12.4	.	.	Δ 0-0
4	8	000	10	07	05.7	03.4	.	.	Δ 0-0,01 ² 12 ²⁰ ,13 ²⁰ 12 ²⁰
5	7	09	060	00	05.0	06.4	70.8	.	00 ² 4,9 ² 10 ²⁰ ; Δ 20-24
6	8	000	030	00	01.0	12.4	00.0	.	Δ 0-0
7	8	350	010	01	02.3	12.6	.	.	Δ 0-0,15 ² 5 ²⁰
8	8	030	040	01	02.7	11.9	.	.	Δ 0-0,17 ²⁰
9	8	050	030	01	03.0	12.1	.	.	Δ 3-0,20-24
10	7	310	07	06	04.7	14.3	.	.	Δ 0-0,010 ² 10 ²⁰ ,17 ²⁰ 20 ²⁰ ; R 44 ² -R ² ,17 ²⁰ -20 ²⁰ = 10-20 ²⁰
11	7	10	100	13	10.0	17.9	09.4	.	0 13 ² 44 ²⁰
12	7	37	09	00	05.3	06.4	03.0	.	Δ 0-0
13	8	000	060	04	03.3	11.7	.	.	Δ 0-0,20 ²⁰ 24
14	7	39	09	09	09.0	05.2	.	.	Δ 0-0,013 ² 15 ²⁰ ,20-20 ²⁰ ; R 15 ² -15 ²⁰
15	8	390	050	00	01.7	12.5	00.3	.	Δ 2-0
16	8	000	010	00	00.3	12.6	.	.	Δ 40-0
17	8	000	050	07	04.0	10.9	.	.	Δ 0-0,22-24
18	7	300	040	10	04.7	08.3	.	.	Δ 0-0,005 ² 10 ²⁰
19	8	08	050	04	05.7	19.3	01.8	.	Δ 0-0,010 ² 10 ²⁰
20	8	010	050	03	03.0	11.1	.	.	Δ 20-20 ²⁰ ,21-24
21	7	05	06	00	03.7	18.9	.	.	Δ 0-0,22-24
22	8	110	030	00	01.3	19.8	.	.	Δ 0-0,20 ²⁰ ,20 ²⁰ 24
23	8	340	030	00	02.3	14.2	.	.	Δ 0-0,=5 ²⁰ 9 ²⁰
24	7	090	07	34	06.7	36.4	.	.	Δ 0-0
25	7	000	040	00	01.3	13.9	.	.	Δ 2-20
26	7	000	040	100	14.7	17.2	.	.	Δ 10-0 ²⁰ ,=5 ²⁰ 9 ²⁰ ,R 5 ²⁰ 17,0 10 ²⁰ 15 ²⁰
27	7	10	07	13	19.1	14.6	74.2	.	Δ 22-24
28	6	10	100	130	10.3	11.1	11.4	.	Δ 0-20 ²⁰ ,02 ²⁰ -5,10 ² 14 ²⁰ ,17 ²⁰ 17 ²⁰ ; = 40-24,9 20 ²⁰ -24
29	6	11	09	09	19.3	11.6	06.0	.	90-60 ²⁰ =0-15
30	7	01	13	05	25.3	17.9	.	.	Δ 0-0,=9 10 ²⁰ 0 10 ²⁰ 13,4 20 ²⁰ 24
31	6	100	100*	100*	16.0	11.1	13.3	.	Δ 0-0, R 0 15,10 ² 14 ²⁰ ,0 0 17 ²⁰ ,9 20 ²⁰ -24; = 6-24, & 17 ²⁰ 20 ²⁰

1978 SEPTEMBAR

SARAJEVO

 $\varphi = 43^{\circ}52' N \lambda = 18^{\circ}26' E$ Gr. $\Delta G = + 1h 14m$

BR. ST. 139

d	Vazdušni pritisak P mm			Temperatura vazduha T °C								Napon vodenе pare e mm			Relativna vlažnost U %			Pravac i jačina veta D, f (0—12)					
	7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21			
1	703.4	703.3	703.6	06.0	16.0	09.4	10.2	17.4	01.2	06.4	06.8	06.4	36.6	97	47	74	73	-	0	W	1	-	0
2	705.4	704.3	704.8	08.2	16.7	11.4	11.9	17.7	08.0	06.4	07.8	08.3	08.6	95	58	85	79	-	0	SW	1	ESE	2
3	706.3	705.8	706.1	07.4	21.0	12.6	13.4	21.5	06.3	05.5	07.1	07.2	08.6	92	39	79	70	-	0	NNW	1	SE	1
4	706.1	705.1	705.3	09.2	24.0	15.3	16.0	24.1	07.4	06.5	07.5	08.0	09.7	86	36	74	65	-	0	W	2	-	0
5	703.9	702.9	702.8	12.4	18.0	16.4	15.8	20.0	11.0	09.8	09.0	12.2	11.1	83	79	79	80	ESE	2	-	0	ESE	1
6	701.4	700.5	700.0	13.8	16.6	14.8	15.0	17.6	12.8	10.3	10.6	12.6	12.1	90	89	96	92	E	3	ENE	1	-	0
7	700.0	699.3	701.2	14.2	20.6	14.9	16.2	20.6	13.6	12.9	11.7	11.0	12.0	96	60	94	83	-	0	NNW	1	-	0
8	703.8	703.2	706.6	12.0	17.0	13.0	13.8	19.0	11.5	09.0	10.1	09.8	09.0	96	68	80	81	WSW	1	NNW	2	-	0
9	708.2	708.0	709.3	10.6	16.8	13.0	13.4	17.5	10.5	09.6	09.1	07.8	08.9	95	54	79	76	-	0	W	2	-	0
10	710.6	709.5	709.3	09.6	17.8	14.6	14.2	18.1	08.6	07.4	08.5	10.0	10.5	95	65	84	81	-	0	W	1	-	0
11	708.7	707.3	705.8	12.4	26.4	16.9	18.2	27.3	10.9	10.1	09.6	08.8	11.4	89	34	79	67	-	0	W	1	SE	1
12	703.9	704.4	706.2	13.4	11.8	06.2	09.4	23.5	06.2	10.5	09.4	08.4	06.9	82	81	97	87	-	0	W	3	SW	1
13	707.5	708.9	711.0	08.9	10.2	11.0	10.3	11.2	06.0	06.5	07.1	07.8	06.8	83	84	69	79	NW	2	NE	2	-	0
14	712.0	710.3	709.2	07.4	17.0	10.0	11.1	17.6	07.2	05.7	07.0	08.6	08.1	91	59	88	79	-	0	ESE	3	E	1
15	709.0	709.2	710.0	06.4	16.2	10.6	11.0	17.7	04.8	04.5	06.8	08.5	08.1	95	62	84	80	ESE	1	NNW	1	ESE	2
16	711.8	711.5	713.2	06.9	18.0	12.2	12.3	19.8	06.0	05.0	07.1	09.4	08.2	95	61	77	78	ESE	1	WSW	2	-	0
17	713.7	712.4	712.4	09.2	21.1	12.2	13.7	21.1	08.6	07.5	08.3	09.3	09.3	95	49	87	77	-	0	W	2	-	0
18	711.5	709.2	709.5	07.0	23.6	14.2	14.8	24.0	06.1	05.0	06.9	09.5	09.3	92	44	76	71	-	0	SW	2	SE	2
19	708.4	706.5	705.9	10.7	22.2	15.2	15.8	23.0	09.5	08.5	08.2	11.0	11.9	85	55	92	77	ESE	2	WNW	1	-	0
20	708.8	710.2	712.5	09.6	07.8	17.2	08.0	15.2	07.0	09.5	08.5	07.3	05.5	95	92	72	86	-	0	ESE	1	NNE	2
21	713.2	712.6	713.4	04.4	12.0	05.8	07.0	13.2	04.0	03.1	05.9	05.0	24.9	94	47	71	71	-	0	ENE	3	-	0
22	713.3	712.4	710.9	05.0	12.8	09.0	09.0	14.5	03.1	02.0	06.0	07.2	07.0	92	65	81	79	-	0	-	0	E	3
23	708.3	707.8	709.7	08.2	15.6	12.0	12.0	16.4	07.0	05.0	07.5	08.8	09.4	93	66	89	83	ESE	2	-	0	-	0
24	711.7	711.8	712.6	10.4	18.6	14.4	14.5	19.6	10.0	08.6	09.0	09.3	09.9	95	58	80	78	-	0	SW	2	E	2
25	714.1	713.1	713.3	09.2	24.9	14.8	15.9	25.2	08.6	07.2	08.1	10.8	10.4	93	46	82	74	ESE	2	SW	1	E	3
26	712.8	710.6	709.7	10.2	25.5	14.8	16.3	26.0	09.4	08.5	08.7	11.1	10.1	93	45	80	73	ESE	2	WSW	1	ESE	3
27	708.1	705.5	704.5	11.0	18.6	14.0	14.4	19.0	10.2	09.4	08.7	10.6	11.2	89	66	94	83	ESE	2	-	0	-	0
28	701.9	701.8	702.9	09.8	08.2	06.0	07.5	14.0	05.6	09.8	08.7	07.8	06.7	95	95	96	95	SW	2	W	3	-	0
29	705.5	705.2	707.4	06.2	15.5	08.2	09.5	17.0	05.6	06.4	06.5	05.2	06.8	92	40	83	72	-	0	NW	2	-	0
30	707.7	706.7	704.8	06.8	18.6	16.0	14.4	18.7	05.0	03.8	06.1	07.2	07.7	82	45	57	61	ESE	2	S	5	S	3
MES.	RED. 708.0 707.4 707.8 09.2 17.6 12.2 12.8 19.2 07.7 07.4 08.1 08.8 08.9 92 60 82 78 0.8 1.6 1.0																						

1978 OKTOBAR

SARAJEVO

1	702.6	702.2	704.3	14.3	19.8	14.6	15.8	21.5	13.2	11.9	09.2	07.2	09.1	75	41	73	63	ESE	2	S	3	NNW	1
2	705.3	706.1	707.9	13.8	18.4	15.2	15.7	20.3	12.6	10.6	09.7	11.5	11.4	82	72	88	81	E	4	ESE	2	ESE	3
3	707.5	706.1	706.4	13.8	26.0	17.2	18.6	26.8	13.0	10.8	08.5	07.4	08.3	72	29	56	52	ESE	4	S	4	ESE	5
4	704.7	705.6	706.4	13.8	19.8	15.1	15.9	20.0	13.4	11.8	11.1	08.4	07.4	94	49	57	67	ESE	1	S	4	S	2
5	706.5	710.7	712.5	10.8	07.4	07.0	08.1	15.1	07.0	09.0	09.3	07.3	06.9	95	95	92	94	-	0	WSW	2	-	0
6	713.1	711.3	713.5	04.8	15.8	06.8	08.6	16.4	04.0	02.6	06.1	06.5	06.0	94	48	81	74	ESE	2	NE	1	ENE	2
7	714.0	713.7	714.2	06.0	12.6	11.4	10.4	12.9	04.5	03.3	06.4	07.8	08.1	92	71	80	81	-	0	SSW	1	ESE	2
8	713.5	712.8	713.2	07.8	21.0	11.8	13.1	21.7	07.0	05.4	07.1	08.7	08.8	90	47	85	74	ESE	2	W	1	-	0
9	713.4	712.3	713.3	06.6	18.6	11.0	11.8	19.0	06.0	04.2	06.4	09.0	08.7	95	56	89	80	ESF	2	SM	1	ESE	2
10	713.6	712.8	714.7	05.6	17.0	11.2	11.3	17.4	05.5	04.5	06.3	09.8	09.1	92	68	91	84	ESE	2	WNW	2	ESE	1
11	715.9	715.3	716.2	06.2	15.0	10.0	10.3	15.5	05.8	04.5	06.8	09.6	08.6	96	75	93	88	-	0	W	2	ESE	2
12	716.7	715.6	716.2	07.4	19.2	10.4	11.9	19.3	06.8	05.6	07.1	08.3	08.0	92	50	84	75	ESE	2	NW	2	E	2
13	716.3	714.3	714.5	05.2	20.0	10.6	11.6	20.2	05.0	04.0	06.4	07.5	08.5	96	43	89	76	-	0	E	4	ESE	3
14	713.5	712.1	712.6	05.4	14.4	10.8	10.4	15.5	05.2	04.0	06.4	08.9	09.1	94	73	93	87	-	0	NW	2	ESE	1
15	711.6	710.1	709.9	08.8	12.2	10.2	10.4	12.5	08.8	09.4	07.5	08.2	07.6	8									

BR. ST. 139

 $H_s = 630 \text{ m } H_b = 637.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$

Dan	Vrij.	Oblačnost N (0-10)					Intenzitet svjetlosti kraji seči km	Podzemne R mm	Snežni pokriven. h cm	Razvoj vremena w
		14	7	14	21	Sred Dnes				
1	8 10	070	04	07.0	08.6	45.6	.	0-6, =0-7 ⁰⁰ , □ 19 ⁰⁰ -24		
2	8 10*	060	01	05.7	04.9	07.2	.	□ 0-1*, 19 ⁰⁰ -24; 0-1 ⁰⁰ , =6-9		
3	8 000	010	00	00.3	09.9	03.8	.	□ 0-0, 19-24		
4	8 020	040	00	02.0	10.8	.	.	□ 0-0*, 19-24		
5	7 06	100	08	08.0	01.6	.	.	□ 0-9*, 0-13 ⁰⁰ -4 ⁰⁰		
6	7 10	100	100	10.0	00.0	00.3	.	0-7 ⁰⁰ , =0-8 ⁰⁰ , =8-11		
7	7 10*	09	10*	09.7	01.3	14.7	.	=0-8, 10-24; 0-6 ⁰⁰ , 0-23, =8-15		
8	7 10*	06	07	07.7	03.0	09.1	.	=0-11, 0-7 ⁰⁰ , 0-24 ⁰⁰		
9	8 07	08	09	08.0	06.0	01.4	.	□ 21 ⁰⁰ -24		
10	6 08	10	01	06.3	00.0	.	.	□ 0-0, 19 ⁰⁰ -24; =2 ⁰⁰ -24		
11	8 010	010	00	00.7	10.4	.	.	□ 0-0 ⁰⁰ , 10 ⁰⁰ -24; =0-6 ⁰⁰		
12	7 020	100	100	07.3	04.4	.	.	□ 0-9, 0-13 ⁰⁰ -24; 0-13 ⁰⁰ -17 ⁰⁰ , =0-1 ⁰⁰ -24		
13	7 100	100	10	10.0	00.1	37.6	.	=0-10 ⁰⁰ , =0-6 ⁰⁰ , □ 10-24		
14	8 010	09	01	03.7	05.0	02.5	.	□ 0-0, 19 ⁰⁰ -24		
15	7 05	06	00	03.7	02.9	.	.	□ 0-10 ⁰⁰ , 10 ⁰⁰ -24, =4 ⁰⁰ -10 ⁰⁰		
16	7 000	070	00	02.3	36.0	.	.	□ 0-10 ⁰⁰ , 19 ⁰⁰ -24; =6-10 ⁰⁰		
17	7 000	020	00	00.7	08.9	.	.	□ 0-0, 10-24; =5 ⁰⁰ -H		
18	8 000	030	00	00.0	09.4	.	.	□ 0-0, 10-24		
19	7 01	080	06	05.0	06.9	.	.	□ 0-0, 0-10 ⁰⁰ , 0-24 ⁰⁰ -13 ⁰⁰		
20	7 100	10	09	09.7	00.0	10.0	.	□ 0-0, 0-10 ⁰⁰ , 0-24 ⁰⁰ -13 ⁰⁰		
21	8 09	05	00	04.7	03.4	09.6	.	□ 19-24		
22	7 100	09	10	09.7	03.5	00.0	.	□ 0-5 ⁰⁰ , 19 ⁰⁰ -24; =3 ⁰⁰ -9, 0-5 ⁰⁰ -7 ⁰⁰		
23	8 10	100	10	10.0	01.2	00.0	.	□ 0-5 ⁰⁰ , 0-5 ⁰⁰ -5 ⁰⁰ , 0-5 ⁰⁰ -9 ⁰⁰ , 0-5 ⁰⁰ -16 ⁰⁰		
24	7 10	090	10	09.7	04.2	00.1	.	0-6 ⁰⁰ , =4 ⁰⁰ -10 ⁰⁰		
25	8 040	010	00	01.7	08.8	.	.	□ 0-9*, 10-24		
26	8 000	000	00	00.0	08.9	.	.	□ 0-9, 0-10 ⁰⁰		
27	8 09	10	10	09.7	00.5	.	.	□ 0-5 ⁰⁰ , 0-9 ⁰⁰ -6 ⁰⁰		
28	6 10	100	100	10.0	00.0	02.0	.	0-2 ⁰⁰ , 0-24, 0-13 ⁰⁰ -4 ⁰⁰		
29	8 08	010	00	03.0	37.7	14.7	.	0-0, =0-8, □ 13 ⁰⁰ -24		
30	8 010	090	05	05.0	07.2	.	.	□ 0-0, 10-24, =0-24		
MES.	VRED.	05.8	06.6	04.7	05.7	145.5	158.6			

1	8 09	060	10	08.3	05.2	01.3	.	0-3 ⁰⁰ , 0-14 ⁰⁰		
2	8 10	09	05	08.0	01.2	00.9	.	0-6 ⁰⁰ , 0-13 ⁰⁰		
3	8 09	030	05	05.7	04.2	00.8	.	0-5 ⁰⁰ -20 ⁰⁰ , 0-13 ⁰⁰ -24 ⁰⁰		
4	8 10	060	10	08.7	03.2	02.0	.	0-4 ⁰⁰ , 0-13 ⁰⁰ -24 ⁰⁰		
5	6 09	100	10	09.7	00.0	03.4	.	0-0 ⁰⁰ , 0-3 ⁰⁰ , 0-13 ⁰⁰ -24 ⁰⁰ , =5 ⁰⁰ -24		
6	8 01	010	00	00.7	08.4	07.4	.	=0-8 ⁰⁰ , □ 10-24		
7	6 10	09	10	09.7	00.0	.	.	□ 0-11 ⁰⁰ , 10 ⁰⁰ -24; =11 ⁰⁰ -16 ⁰⁰		
8	8 00	010	00	00.3	08.5	.	.	□ 0-9, 0-10 ⁰⁰		
9	7 00	020	00	00.7	08.2	.	.	0-10 ⁰⁰ , 20-24, =6 ⁰⁰ -13 ⁰⁰		
10	7 00	000	00	00.0	09.8	.	.	□ 0-9 ⁰⁰ , 0-13 ⁰⁰		
11	6 00	070	00	32.3	02.0	.	.	□ 0-11 ⁰⁰ , 0-10 ⁰⁰ -24; =5-24		
12	7 10	000	00	03.3	06.8	.	.	□ 0-9, 0-10 ⁰⁰ -24, =0-8		
13	6 00	000	00	00.0	08.2	.	.	□ 0-13 ⁰⁰ , 0-13 ⁰⁰ -24, =5 ⁰⁰ -24		
14	7 01	000	10	03.7	06.7	.	.	□ 0-10 ⁰⁰ , 19 ⁰⁰ -24, =0-11 ⁰⁰ , 10-24		
15	6 10	10	10	10.0	00.0	.	.	□ 0-10 ⁰⁰ , 0-10 ⁰⁰ -24, =0-24		
16	6 10	09	00	06.3	00.9	.	.	□ 0-9, 0-10 ⁰⁰ -24, =0-24		
17	7 09	07	01	05.7	06.5	.	.	□ 0-11 ⁰⁰ , =0-9 ⁰⁰		
18	8 09	07	03	06.3	03.3	00.0	.	□ 0-6 ⁰⁰ , 19 ⁰⁰ -24, 0-6 ⁰⁰ -6 ⁰⁰		
19	6 08	10	10	09.3	01.9	.	.	□ 0-9 ⁰⁰ , 10-23, =8 ⁰⁰ -24, 0-8 ⁰⁰ -24		
20	5 100	10	10	10.0	00.0	00.6	.	0-10 ⁰⁰ , 6 ⁰⁰ -9, 0-10 ⁰⁰ -24, =0-24, 0-2 ⁰⁰ -6 ⁰⁰ , 9-13 ⁰⁰		
21	6 100	100	10	10.0	03.0	04.7	.	0-10 ⁰⁰ , =0-24		
22	8 05	020	00	02.3	09.0	04.4	.	□ 0-2, 0-3 ⁰⁰ -8 ⁰⁰ , □ 17 ⁰⁰ -24		
23	6 03	09	02	04.7	14.2	.	.	□ 0-3, 18 ⁰⁰ -24, 0-3 ⁰⁰ -8 ⁰⁰ , =9 ⁰⁰ -24		
24	7 00	010	03	00.3	06.9	.	.	□ 0-9, 0-10 ⁰⁰ -24		
25	6 06	000	00	02.0	07.6	.	.	□ 0-10 ⁰⁰ , 19-24, 0-10 ⁰⁰ -8, =5 ⁰⁰ -15		
26	6 10	100	09	29.7	03.0	.	.	□ 0-9 ⁰⁰ , =9 ⁰⁰ -10, 0-12 ⁰⁰ -10		
27	7 10*	10*	09	39.7	03.4	00.8	.	* 2 ⁰⁰ 5 ⁰⁰ , =5 ⁰⁰ -11, * 5 ⁰⁰ -20		
28	8 04	050	09	06.0	17.6	04.6	.	* 0 ⁰⁰ 3 ⁰⁰ , 0-5 ⁰⁰ , □ 20 ⁰⁰ -24		
29	6 01	060	04	03.7	16.9	.	.	□ 0-0 ⁰⁰ , 20-24, 0-0 ⁰⁰ , =0 ⁰⁰ -15		
30	6 13	10	10	10.0	10.0	00.0	.	□ 0-8 ⁰⁰ , 20-24, =0-24, 0-8 ⁰⁰ -8 ⁰⁰		
31	5 10	10	10	10.0	10.0	00.0	.	□ 0-0 ⁰⁰ , 10-24, =0-24		
MES.	VRED.	36.3	75.8	35.1	35.7	127.6	31.1			

1978 NOVEMBER

SARAJEVO

 $\varphi = 43^{\circ}52' N \lambda = 18^{\circ}26' E$ Gr. $\Delta G = + 1h 14min.$

BR. ST. 139

d	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodenog parne e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0—12)					
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21			
1	716.4	716.8	718.2	05.8	13.0	08.2	08.8	13.0	05.8	05.4	06.0	05.7	05.4	86	51	66	68	-	0	NNW 2	ENE 2		
2	717.9	716.7	716.4	06.4	09.0	07.0	07.4	09.5	06.0	06.0	05.5	05.2	05.9	76	61	78	72	E	1	ESE 1	ESE 3		
3	715.7	714.9	715.7	06.0	09.2	05.2	06.4	09.2	05.2	05.0	06.1	06.5	05.8	87	74	88	83	-	0	NNW 1	ESE 3		
4	715.3	715.3	715.8	05.3	08.2	04.2	05.5	08.2	04.2	02.5	04.9	04.9	04.8	73	61	77	70	E	2	NNW 2	ESE 3		
5	716.3	716.2	717.2	03.2	10.0	05.2	05.9	10.2	01.3	-01.0	04.2	04.2	04.4	73	46	66	62	ESE 3	ESE 3	-	0		
6	717.4	716.6	718.2	04.2	10.8	01.4	04.5	10.8	01.4	03.9	04.2	04.8	04.7	68	49	93	70	ESE 3	ESE 3	ENE 2			
7	718.3	717.8	718.8	01.2	04.4	00.8	01.8	05.3	00.7	-01.0	04.7	04.3	04.7	93	69	97	86	E	1	SSW 1	-	0	
8	718.5	717.4	717.8	00.7	06.0	01.4	02.4	06.4	00.6	01.0	04.2	04.4	04.6	88	63	90	80	ENE 2	NNW 2	NNW 1			
9	717.8	717.3	717.8	-00.6	02.6	00.6	00.8	03.0	-00.6	00.2	04.1	04.5	04.3	93	81	90	88	ESE 2	SSW 1	NE 2			
10	717.2	715.6	716.0	-03.0	04.2	-00.8	-00.1	04.4	-03.0	-04.0	03.4	04.1	04.2	92	66	96	85	ESE 1	WSW 1	-	0		
11	716.1	714.7	716.1	-02.8	00.2	-01.1	-01.2	00.4	-03.2	-03.1	03.6	04.2	04.1	96	90	96	94	NW 1	NW 1	NW 1			
12	715.8	714.4	714.9	-03.8	-00.4	-01.4	-01.8	-00.3	-03.8	-03.0	03.2	03.9	03.9	92	88	95	92	SE 2	SW 1	SSE 2			
13	715.5	715.2	717.1	-03.6	00.2	-01.8	-01.8	00.5	-03.7	-03.0	03.3	04.0	03.9	93	86	96	92	SE 1	WSW 1	NNW 1			
14	719.0	720.0	721.6	-03.5	-02.0	-02.4	-02.6	00.5	-03.5	-03.2	03.4	03.5	03.6	95	89	94	93	NNW 2	NNW 1	NNW 1			
15	721.2	719.8	719.1	-05.6	01.4	-03.0	-02.6	01.5	-05.8	-06.6	02.7	03.3	03.5	90	64	95	83	ENE 1	WSW 2	-	0		
16	717.7	715.6	715.3	-05.5	02.0	-02.4	-02.1	02.2	-05.5	-06.5	02.9	03.7	03.5	95	70	92	86	-	0	WSW 1	-	0	
17	717.4	717.4	718.3	-05.0	05.0	00.0	00.0	05.0	-05.2	-06.4	03.2	03.5	04.1	100	54	89	81	-	0	NNW 1	-	0	
18	716.2	716.8	716.2	-03.2	01.6	-02.0	-01.4	02.6	-03.2	-05.0	03.2	04.4	03.8	89	86	96	90	NW 1	NNW 1	-	0		
19	717.8	715.8	715.4	-04.0	-01.4	-02.4	-02.6	-01.0	-04.0	-03.5	03.3	03.9	03.7	96	95	96	96	NM 1	WSW 1	WSW 1			
20	714.1	713.1	714.4	-05.0	01.5	-02.8	-02.3	02.2	-05.0	-05.5	03.0	03.9	03.5	95	76	93	88	-	0	WSW 1	-	0	
21	715.5	715.7	718.1	-05.0	04.8	-01.4	-00.8	05.1	-05.1	-05.5	03.0	03.8	03.4	95	59	81	78	-	0	WSW 1	-	0	
22	720.0	720.1	720.6	-03.9	07.0	01.2	01.4	07.4	-03.9	-05.0	03.2	03.8	04.7	94	50	93	79	-	0	WSW 1	-	0	
23	721.2	720.1	720.5	-04.6	01.4	-01.6	-01.6	01.6	-04.6	-06.1	03.1	04.2	03.9	96	84	96	92	-	0	WSW 1	-	0	
24	719.1	716.9	715.6	-03.0	00.6	-01.6	-01.4	00.6	-03.0	-06.0	03.5	04.1	03.9	96	87	96	93	-	0	WSW 2	-	0	
25	713.3	710.3	709.5	-03.0	02.0	-01.6	-01.1	02.2	-03.1	-02.8	03.4	05.0	04.0	93	94	98	95	WSW 1	WSW 1	-	0		
26	706.8	704.4	703.2	00.2	11.2	05.8	05.8	12.0	-02.2	-03.0	04.2	04.6	04.5	90	46	66	67	ENE 2	SE 4	ENE 1			
27	699.3	695.6	693.2	05.2	06.3	05.4	05.6	07.5	05.1	03.2	05.9	06.6	05.9	89	92	88	90	ESE 4	ENE 2	ESE 5			
28	693.5	692.5	692.9	-00.4	-00.9	-01.4	-01.0	06.1	-01.5	-00.2	04.3	03.8	03.9	96	89	95	93	WSW 2	NNW 2	-	0		
29	693.8	693.7	695.1	-02.4	-01.2	-02.6	-02.2	-01.2	-02.6	-01.9	03.6	03.9	03.7	94	93	97	95	-	0	NNW 1	NW 2		
30	697.0	698.7	702.0	-01.8	-00.2	-00.8	-00.9	-00.2	-02.6	-02.5	03.8	04.2	04.0	95	93	93	94	W 2	W 3	-	0		
MES.	VRED.			714.1	713.2	713.8	-01.0	03.9	00.5	01.0	04.5	-01.5	-01.9	03.9	04.4	04.3	90	74	90	84	1.2	1.5	1.0

1978 DECEMBER

SARAJEVO

1	704.7	705.3	706.6	-07.4	-00.4	-05.6	-04.8	00.0	-07.5	-09.5	02.4	03.4	02.9	93	76	95	88	ESE 1	-	0	SSE 2	
2	707.0	707.7	708.8	-04.8	00.8	-02.6	-02.3	00.8	-06.0	-06.4	03.1	03.6	03.6	95	75	94	88	-	0	-	0	
3	708.6	706.4	705.5	-01.8	04.0	-03.0	-01.0	04.0	-03.0	-03.4	03.8	04.0	03.0	95	66	82	81	-	0	ESE 2	ESE 3	
4	704.1	703.3	703.9	-07.7	-03.2	-02.8	-04.1	-02.8	-08.0	-09.0	02.3	03.1	03.2	90	85	86	87	-	0	SW 1	-	0
5	704.8	707.6	710.9	-01.6	-03.2	-09.4	-01.1	-09.4	-01.1	-02.8	03.0	02.0	01.4	74	56	61	64	ESE 4	NE 4	E 2		
6	712.2	710.8	711.4	-11.2	-04.2	-08.6	-08.2	-04.0	-12.5	-13.2	01.3	02.0	01.6	67	59	67	64	E	1	W 1	ENE 2	
7	707.8	708.1	708.8	-10.6	-04.0	-10.0	-08.7	-04.0	-11.0	-11.0	01.6	02.0	01.8	79	58	85	74	-	0	WSW 1	ESE 2	
8	709.4	706.6	708.8	-12.8	-06.0	-07.4	-08.4	-05.0	-13.0	-13.5	01.5	02.0	02.1	85	67	79	77	-	0	WSW 1	-	0
9	706.0	705.4	710.0	-03.8	01.2	00.8	-00.3	02.0	-07.4	-06.5	03.2	04.5	04.7	92	90	97	93	-	0	-	0	
10	710.1	710.0	710.8	00.0	01.0	00.2	00.4	01.1	-00.2	-06.4	04.4	04.8	04.5	97	97	97	97	-	0	-	0	
11	709.0	707.2	706.5	-00.2	00.2	-00.4	-00.2	00.4	-01.9	-00.3	04.4	04.6	04.4	96	98	100	98	-	0	-	0	
12	702.6	701.2	699.0	01.8	10.0	07.5	06.7	10.8	-01.0	-01.6	04.8	04.6	04.4	92	50	83	75	E	1	S 5	2	
13	697.2	696.3	696.4	06.7	08.4	07.6	07.6	10.3	04.4	03.0	06.2	06.9	05.5	85	83	71	80	E	2	-	0	
14	692.5	691.7	692.3	03.6	08.4	04.6	05.3	09.0	03.6	03.0	05.7	06.9	05.3	96	83	83	87	S 2	E 2	-	0	
15	694.7	697.5	700.9	02.4	10.4	04.2	05.3	10.4	02.3	00.8	05.1	05.2	04.6	94	55	75	75	E 1	W 2	NW 2		
16	700.7	699.3	697.3	06.6	10.2	10.9	09.7	10.9	01.7	00.0	05.1	04.9	06.4	70	52	66	63	S 3	S 4	S 5		
17	698.3	701.8	704.0	07.3	13.6	05.6	08.0	14.0	05.6	06.2	07.2	04.7	04.8	94	50</							

BR. ST. 139

 $H_s = 630 \text{ m } H_b = 637.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$

Dan	Mj.	Vrij.	Oblačnost N (0-10)					Insekti broj	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
			14	7	14	21	Sred Dnes				
1	7	09	07○	09	08.3	02.0	.	.	.	△ 0-9, = 0-12	
2	7	09	10○	09	09.3	00.0	.	.	.	△ 0-8, = 5-8, 0-12-14○	
3	7	10	09	07	08.7	00.0	00.0	.	.	△ 0-12, = 0-24; = 6-8, 0-12-24	
4	6	10	10	06	08.7	30.0	.	.	.	= 0-24, △ 0-8, 0-12-24	
5	7	07	05○	10	07.3	05.3	.	.	.	△ 0-7○, = 0-8	
6	7	09	01○	00	03.3	04.7	.	.	.	△ 10-24	
7	6	10	05	00	05.0	01.2	.	.	.	△ 0-12○, = 0-24; = 0-24	
8	6	10	00○	10	06.7	02.8	.	.	.	= 0-24, △ 0-9, 0-12-24	
9	6	10	10	10	10.0	00.0	.	.	.	= 0-12○, △ 0-9, 0-12-24	
10	4	06	00○	00	02.0	05.8	.	.	.	= 0-12○, △ 0-5○, = 5-7○, 0-24-24; = 10-24	
11	3	10	10	10	10.0	00.1	.	.	.	□ 0-12○, = 0-24	
12	4	10	10	10	10.0	00.0	.	.	.	□ 0-9, 0-12-24; = 9-12○	
13	3	10	05	10	08.3	00.0	.	.	.	□ 0-9, = 0-24; = 0-24, = 15-16○	
14	3	10	10	10	10.0	00.0	.	.	.	□ 0-24, □ 0-4	
15	5	10	00○	00	03.3	04.3	.	.	.	□ 0-5, 0-24; □ 0-9, 0-24; = 5-23	
16	3	10	00	09	06.3	02.2	.	.	.	□ 0-12○, 0-9, 0-24; V 0-12○, 0-9, 0-24; = 0-6, 0-9, 0-24; = 6-9○	
17	6	09	00○	05	04.7	02.6	.	.	.	= 0-12○, □ 0-8, □ 0-9, 0-12-24; = 10-24	
18	5	02	00○	10	04.0	00.5	.	.	.	= 0-9, □ 0-12○, □ 0-10, = 0-24; = 9-11, 0-12-24; = 11-13○	
19	3	10	10	10	10.0	00.0	.	.	.	□ 0-12○, 0-9, 0-24; V 4-9○, 0-24	
20	3	10	00	00	03.3	00.6	.	.	.	= 0-5, □ 0-12○, 0-9, 0-24; = 5-24	
21	3	10	00	00	03.3	02.7	.	.	.	□ 0-9, □ 0-10, 0-12-24; = 9-12○, = 0-24	
22	5	08	03	00	03.7	03.2	.	.	.	□ 0-5○, = 0-24	
23	5	00	00○	10	03.3	00.0	.	.	.	□ 0-12○, 0-9, 0-12-24; = 3-6, 0-12-24; = 6-11○	
24	3	10	00	10	06.7	00.0	.	.	.	□ 0-12○, 0-9, 0-12-24; = 12-16○	
25	3	10	00	10	06.7	00.0	.	.	.	□ 0-12○, 0-9, 0-12-24; = 0-12-24; = 12-16○	
26	8	01	08○	08	05.7	04.6	.	.	.	□ 0-9, = 0-12○, = 9-12○	
27	7	10	10○	10○	10.0	00.0	03.3	.	.	● 2-9○, 10○, 0-12-24; □ 0-8, 0-12-24	
28	5	10*	10*	10*	10.0	00.0	22.7	01	.	● 0-4○, □ 0-6○, * 4-9○, = 5-24, □	
29	5	10*	10*	10*	10.0	00.0	10.0	06	.	* 0-24, = 0-24, □	
30	6	10*	10	10	10.0	00.0	08.1	12	.	* 0-24, 0-12○, = 0-24, □ 0-12-16, □	
MES. VRED.			08.7	05.1	07.1	07.0	42.6	44.1			

SARAJEVO

1978 DECEMBER

1	6	00	04○	00	01.3	00.8	01.2	10	= 0-24, □	
2	5	00	09	00	03.0	00.0	.	07	= 0-24, □	
3	6	10	00○	00	03.3	02.8	.	07	= 0-24, □	
4	5	00	10*	10	06.7	00.0	.	06	= 0-24, * 12-20, □	
5	7	10	05	00	05.0	00.0	00.2	06	= 0-24, □	
6	5	08	01○	01	03.3	02.3	.	04	= 7-9○, * 8-12○, □	
7	6	10	00○	00	03.3	01.0	00.0	04	* 5-10○, = 6-12-24, □	
8	6	00	00○	10	03.3	00.2	00.0	04	= 0-24, * 21-24, □	
9	5	10*	10○	10*	10.0	00.0	06.0	13	= 0-19, 0-24, 0-30, * 6-7○, 0-7○-20○, = 19-22○, & 20-24○, □	
10	2	10	10	10	10.0	00.0	18.0	06	= 0-24, □	
11	0	10	10	10	10.0	00.0	.	06	= 0-23○, □	
12	8	04	10	09	07.7	00.2	.	05	● 4-12○, 0-14○, 0-23○	
13	7	06	10	08	08.0	00.0	00.0	.	● 0-12○, 0-14○, 0-23○	
14	8	10	07	10	09.0	00.2	17.8	.	● 0-12○, 0-14○, 0-23○	
15	4	08	00○	01	03.0	00.2	04.9	.	● 0-12○, 0-14○, 0-23○	
16	8	10	09	09○	09.3	00.0	.	.	● 0-12○, 0-14○, 0-23○, 0-24○, □	
17	6	10	08○	06	08.0	00.2	04.0	.	● 0-12○, 0-14○, 0-23○, * 17-22○, □	
18	6	10	10○	10*	10.0	00.0	00.0	.	● 0-24, 0-12○, 0-14○, 0-23○, 0-24○, □	
19	6	10	07	10○	09.0	00.0	19.3	04	● 0-24, 0-12○, 0-14○, 0-23○, 0-24○, □	
20	6	09○	00○	00	03.0	00.2	26.6	.	● 0-24, 0-12○, 0-14○, 0-23○, 0-24○, □	
21	1	00	00	10	03.3	00.0	00.5	.	● 0-10○, = 5-8○, H 0-6○, 0-12○, 0-14○, 0-24○, = 0-12○, 0-24○, = 15-20○	
22	7	10	05○	09	08.0	00.9	.	05	= 0-8, = 2-11, P 0-12○, H 0-14○, 0-17○, 0-20○, 0-23○	
23	8	08	00○	00	02.7	05.6	00.6	.	● 0-12○, 0-14○, 0-23○, = 12-22○, = 22-24○	
24	1	10	19	10	10.0	00.0	.	.	● 0-24, = 4-7○, □ 0-24○, □	
25	5	10	09	10	09.7	00.0	.	.	● 0-7○, = 0-5, = 5-9○, 0-7○-12○, H 0-19○, = 9-24	
26	4	10○	10	09	09.7	00.0	03.7	.	= 0-9○, 0-12○, 0-14○, = 9-12○, H 0-16○	
27	8	02	07	04	04.3	01.9	00.2	.	= 0-2○, ● 0-12○, 0-14○	
28	8	07	10	08	08.3	00.0	.	.	● 0-4○, 0-12○, 0-14○, 0-17○, 0-18○, P 0-14○-12○	
29	8	01	10	10	07.0	00.6	00.4	.	● 0-12○, 0-14○, 0-17○, 0-18○, P 0-14○-12○	
30	8	10○	05	00	05.0	01.4	05.5	.	● 0-12○, 0-14○, 0-17○, 0-18○, H 0-16○, P 0-14○-5○	
31	8	09	10	13○	05.7	00.0	03.2	.	● 0-12○, 0-14○, 0-17○, 0-18○, H 0-16○, P 0-14○-5○	
MES. VRED.			07.2	06.3	06.3	06.6	18.5	109.1		

1978 JANUAR

BEOGRAD

 $\varphi = 44^\circ 48' N \lambda = 20^\circ 28' E$ Gr. $\Delta G = + 1h 22 min.$

BR. ST. 169

D	Vazdušni pritek P mm			Temperatura vazduha T °C									Napon vodenе pare e mm			Relativna vlažnost U %			Pravac i jačina vetro D, I (0-12)											
				7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 8 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21							
		7	14	21																										
1	742.1	752.7	757.9	00.8	02.3	00.6	01.1	02.4	00.4	-01.0	03.8	03.5	03.7	78	65	77	73	WNW	3	NW	3	W	2							
2	760.0	758.8	756.5	-02.6	05.1	00.8	01.0	06.0	-02.7	-06.7	03.3	03.4	03.2	88	52	66	69	SSE	2	S	2	ESE	2							
3	754.2	753.7	751.4	02.7	06.2	01.7	03.1	06.8	-01.4	-04.8	03.5	03.9	04.4	63	55	85	68	SSW	2	NW	2	ESE	2							
4	747.1	749.7	750.5	05.2	05.2	01.8	03.5	07.2	01.6	-02.7	05.7	04.6	04.5	86	69	87	81	NNW	2	WSW	2	WSW	1							
5	753.5	755.5	760.0	-00.7	01.4	-01.4	-00.5	02.6	-01.5	-02.5	04.0	05.0	03.3	91	59	80	77	WSN	2	NW	3	N	2							
6	763.3	763.6	762.4	-04.9	-01.6	-04.3	-03.8	-00.9	-05.2	-06.7	02.6	02.8	02.6	82	69	77	76	N	3	NNW	2	SW	1							
7	760.5	761.8	762.7	-03.1	-02.1	-02.4	-02.5	-02.1	-04.4	-06.5	02.6	03.0	03.1	72	75	80	76	WSW	2	NNE	2	WNW	2							
8	763.8	763.3	763.0	-03.0	-02.2	-03.8	-03.2	-02.2	-03.8	-03.8	03.0	02.7	03.2	81	70	92	81	NNW	2	WSW	2	NNE	2							
9	762.0	760.0	758.5	-04.7	01.0	-02.2	-02.0	01.0	-05.2	-07.8	02.7	02.7	02.6	83	55	66	68	ESE	3	ESE	3	ESE	3							
10	757.5	756.4	756.9	-07.0	-05.1	-05.4	-05.7	-02.2	-07.6	-08.9	02.7	02.9	02.8	98	93	93	95	SW	2	WSW	2	SW	1							
11	754.6	750.6	747.9	-05.6	00.2	02.1	-00.3	02.8	-05.8	-15.8	02.9	03.2	03.2	95	70	60	75	SSE	1	E	1	ESE	3							
12	746.9	747.6	750.6	02.8	08.6	06.9	05.9	09.3	02.1	00.4	03.3	03.8	04.5	58	45	64	56	ESE	4	ESE	5	ESE	4							
13	753.4	754.6	755.0	07.2	12.0	08.4	09.0	13.7	05.2	13.6	05.3	05.8	05.6	70	54	68	64	ESE	3	ESE	3	ESE	2							
14	755.3	754.9	755.6	02.0	09.7	03.6	04.7	10.7	02.0	-11.9	05.1	05.8	05.8	97	64	98	86	SW	2	W	1	NW	1							
15	756.5	755.5	755.3	00.3	09.7	01.0	00.8	03.9	-00.3	-00.3	04.7	04.8	04.3	100	100	88	96	NNW	1	NNE	1	ESE	3							
16	753.3	753.0	752.3	01.2	05.2	02.3	02.8	05.8	00.8	-01.3	03.6	03.3	03.7	71	50	68	63	ESE	4	ESE	4	ESE	5							
17	750.2	747.3	746.8	00.0	01.4	00.0	00.4	02.4	-00.6	-00.5	03.4	03.1	03.0	75	60	66	67	ESE	3	ESE	3	ESE	6							
18	745.8	747.6	749.2	-00.6	03.6	-00.5	00.5	04.0	-00.6	-01.6	03.3	03.3	03.2	74	55	73	67	ESE	5	ESE	4	ESE	3							
19	748.2	747.0	746.1	-00.4	03.8	00.2	01.0	04.6	-00.9	-02.2	03.4	03.8	03.7	77	63	80	73	ESE	5	ESE	4	ESE	4							
20	745.2	746.1	747.2	-01.1	02.6	-01.6	-00.4	02.8	-01.6	-02.6	03.3	03.0	03.0	77	55	75	69	ESE	4	ESE	4	ESE	5							
21	746.9	747.4	748.8	-03.0	-02.0	-01.6	-02.1	-01.4	-03.1	-03.5	02.9	02.6	02.8	78	65	69	71	ESE	4	ESE	5	E	4							
22	748.9	748.9	749.5	-00.5	02.0	00.1	00.4	02.5	-01.6	-01.9	03.3	03.5	03.6	75	66	77	73	E	3	E	3	ESE	3							
23	750.1	751.2	752.3	-00.6	02.6	01.1	01.1	03.2	-00.6	-02.0	03.9	04.0	04.2	89	72	85	82	ESE	3	SE	1	WSW	2							
24	750.0	746.3	742.7	00.8	09.2	04.8	04.9	09.7	00.1	-00.7	04.1	04.4	04.4	84	51	69	68	ESE	2	ESE	3	ESE	3							
25	740.1	740.9	745.2	04.6	05.2	04.5	04.7	06.6	04.0	02.5	05.8	06.3	04.8	91	94	75	87	ESE	3	WNW	2	WNW	2							
26	747.7	747.9	749.0	00.5	08.8	04.4	04.5	10.1	-00.8	-04.5	04.2	03.7	05.9	88	44	79	70	ESE	2	WNW	1	-	0							
27	750.5	751.3	752.8	00.1	08.2	04.3	04.2	09.2	-00.2	-04.6	04.4	05.1	05.0	95	63	81	80	WNW	2	W	1	1	1							
28	753.2	750.4	747.7	00.2	08.5	05.8	05.1	09.1	-00.5	-04.5	04.3	03.8	04.2	93	45	61	66	ESE	2	SSE	3	SE	3							
29	741.5	736.5	735.1	06.2	07.8	06.3	06.7	08.8	04.9	03.2	04.1	04.6	04.8	57	58	67	61	ESE	5	ESE	5	ESE	5							
30	736.0	735.7	738.4	04.6	07.2	05.3	05.6	07.2	04.3	03.0	06.0	06.9	06.3	94	91	94	93	ESE	2	WSW	2	WSW	2							
31	742.3	743.9	746.5	02.3	06.4	04.0	04.2	07.0	02.3	02.0	05.1	04.8	04.6	95	67	76	79	WSW	2	WSW	3	W	2							
MES.	751.0			751.0			751.4			00.1			03.9			01.5			04.8			-00.6			-02.4					
																									03.9			04.0		
																									82			64		
																						77			74			2.7		
																						2.7			2.7			2.7		

MFS.	VRFDo	745.8	746.0	746.6	00.6	14.2	22.1	37.2	35.6	-01.3	-01.8	04.3	04.6	04.5	86	74	84	87	2.2	2.3	2.4						
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B.R. ST. 169

$$H_s = 132 \text{ m } H_b = 132.0 \text{ m } h_t = 2.0 \text{ m } h_f = 1.2 \text{ m}$$

Dan	Vreme 0-6 h	Oblačnost N (0-10)					Insekticid broj	Padavina R mm	Snežní pokrývad h cm	Rezervi vremena w
		14	7	14	21	Sred Dnes				
1	7	10	06	09	08.3	03.7	00.0	.	■■■■■ 0-15 ^h , * 4 ^h 6 ^h	
2	8	10	00○	09	00.0	07.9	.	.	— 5 ^h 9 ^h	
3	7	10	13	00	06.7	00.9	.	.		
4	7	10*	12	03	07.7	00.0	01.0	.	* 15 ^h 9 ^h ; ■■■ 7 ^h , — 8 ^h 2 ^h	
5	7	12	06○	05	04.3	06.3	03.4	.	— 0-10 ^h ; ■■■ 10 ^h 13 ^h	
6	7	11	02○	03	00.7	07.1	.	.	■■■ 0 ^h 5 ^h , — 7 ^h 10 ^h , 2 ^h 2 ^h , = 16 ^h 2 ^h	
7	6	10*	10	10	10.0	00.0	00.0	.	= 0-10 ^h ; — 10 ^h , * 5 ^h 0 ^h	
8	6	10	10	10	10.0	00.0	00.1	.	= 6 ^h 2 ^h	
9	7	13	04○	03	02.3	07.6	.	.	= 0-10 ^h	
10	4	10	10*	10*	10.0	03.0	.	.	* 2 ^h 4 ^h , 11 ^h 24 ^h ; = 4 ^h 11 ^h , V 1 ^h 6 ^h , 24 ^h	
11	4	10*	08○	03	06.0	02.1	00.0	.	= 0-23 ^h , V 0-4 ^h , * 5 ^h 9 ^h , ■■■ 15 ^h 24 ^h	
12	7	01	04	07	04.0	05.0	00.0	.	■■■ 0-14 ^h ; ■■■ 11 ^h 13 ^h , 20 ^h	
13	7	09	05	05	06.3	15.7	.	.	■■■ 0-14 ^h	
14	7	00	00○	00	00.4	05.7	.	.	= 4 ^h 13 ^h , 17 ^h 19 ^h ; = 1 ^h 15 ^h , = 5 ^h 24 ^h	
15	2	10	10	10	10.0	00.0	.	.	= 0-15 ^h ; = 11 ^h 15 ^h , 19 ^h 24 ^h , * 4 ^h 15 ^h , ■■■ 21 ^h 23 ^h	
16	7	10	06○	14	13.3	36.6	00.0	.	= 0-10 ^h , ■■■ 0 ^h 24 ^h , ■■■ 10 ^h 24 ^h	
17	6	04	11	10	08.3	22.0	.	.	■■■ 0-04 ^h ; ■■■ 0-14 ^h , ■■■ 11 ^h 19 ^h , 10 ^h 20 ^h ; * 1 ^h 15 ^h 15 ^h , ■■■ 18 ^h 19 ^h , ■■■ 18 ^h 19 ^h	
18	8	06	00○	06	04.0	25.1	01.5	.	■■■ 0-24 ^h , ■■■ 0-25 ^h	
19	7	03	11○	04	01.7	26.8	.	.	■■■ 0-24 ^h ; ■■■ 1 ^h 4 ^h 6 ^h , 9 ^h , ■■■ 23 ^h	
20	7	02	00○	05	02.3	06.9	.	.	■■■ 0-24 ^h ; ■■■ 2 ^h 5 ^h , 5 ^h 24 ^h , ■■■ 0 ^h 9 ^h	
21	6	06	10	10*	08.7	00.0	.	.	■■■ 0-04 ^h , ■■■ 0-23 ^h , = 13 ^h 15 ^h , * 15 ^h 24 ^h	
22	7	09	10	09	09.3	00.0	00.0	.	■■■ 0-10 ^h ; * 0-2 ^h , ■■■ 10 ^h 19 ^h ; = 2 ^h 10 ^h	
23	6	10*	10	10	10.0	03.0	03.0	.	■■■ 0-04 ^h ; ■■■ 4 ^h 14 ^h , ■■■ 14 ^h 22 ^h	
24	6	10	00○	08	06.0	07.2	00.0	.	= 5 ^h 24 ^h ; ■■■ 1 ^h 24 ^h	
25	5	10○	10○	05	08.3	00.0	02.6	.	■■■ 0-05 ^h ; = 0-24 ^h , ■■■ 1 ^h 15 ^h , 9 ^h 14 ^h 15 ^h , ■■■ 21 ^h 22 ^h	
26	7	00	07○	09	05.3	06.9	00.2	.	= 0-0 ^h 21 ^h 24 ^h ; — 1 ^h 10 ^h 9 ^h	
27	7	00	02○	09	00.7	06.8	.	.	= 0-5 ^h 23 ^h ; — 0 ^h 9 ^h	
28	7	00	10	04	04.7	23.8	.	.	■■■ 0-10 ^h ; ■■■ 4 ^h 24 ^h , ■■■ 10 ^h 24 ^h	
29	7	10	08	10○	09.3	00.5	.	.	■■■ 0-24 ^h ; ■■■ 4 ^h 20 ^h , ■■■ 1 ^h 15 ^h 24 ^h	
30	7	09	10	10○	09.7	00.1	05.1	.	■■■ 0-0 ^h ; * 0-1 ^h , ■■■ 1 ^h 15 ^h , 9 ^h 14 ^h 15 ^h ; = 24 ^h 0 ^h	
31	7	10○	06○	09	08.3	03.1	04.2	.	* 2 ^h 9 ^h ; 9 ^h 10 ^h	
MES.	VRED.	05.8	06.3	05.9	06.0	105.7	25.1			

1	7	28	09	10	09.0	01.3	00.2	.	=+15 ²⁴
2	7	32	060	05	04.3	08.0	.	.	=+0-0-24, =+20-930, F ₂₄ 12 ²⁴ , 12 ²⁴ , 23 ²⁴
3	7	17	10	10*	10.0	00.0	.	.	=+5 ²⁴ , 20 ²⁴ , 20 ²⁴ , 14 ²⁴
4	7	19*	29	08	09.0	01.9	00.3	.	=+0-0-24, *+20-10 ²⁴ , 19 ²⁴ , 23 ²⁴ , F ₂₄ 17 ²⁴ , 10 ²⁴ , 23 ²⁴ , 23 ²⁴
5	7	17	09	10	39.7	00.6	00.0	.	*+20-14 ²⁴ , 19 ²⁴ , 24 ²⁴ , F ₂₄ 4 ²⁴ , 70 ²⁴ , 14 ²⁴ , 24 ²⁴
6	4	10*	10	10*	10.0	00.0	04.3	05	*+0-12 ²⁴ , 14 ²⁴ , 24 ²⁴ , F ₂₄ 8 ²⁴ , 9 ²⁴ , 12 ²⁴ , 14 ²⁴ , [■]
7	4	10*	10*	10*	10.0	00.0	16.6	19	*+0-24, [■]
8	5	10*	10	10*	10.0	00.0	10.4	26	*+0-8 ²⁴ , 22 ²⁴ , 24 ²⁴ , =+0-8 ²⁴ , 24 ²⁴
9	5	10*	10	10	10.0	00.0	01.4	72	=+0-6 ²⁴ , 14 ²⁴ , 24 ²⁴ , *+0-9 ²⁴ , 24 ²⁴ , F ₂₄ 9 ²⁴ , 14 ²⁴ , [■]
10	6	10	000	00	33.3	32.3	01.0	21	*+0-4 ²⁴ , =+24 ²⁴ , F ₂₄ 17 ²⁴ , 24 ²⁴ , [■]
11	6	10	06	06	37.3	13.8	.	17	=+0-16 ²⁴ , F ₂₄ 0-24 ²⁴ , F ₂₄ 0-12 ²⁴ , [■]
12	7	10	10	100	10.0	03.8	.	24	F ₂₄ 0-14 ²⁴ , 0-16 ²⁴ , 24 ²⁴ , [■]
13	6	100	100	100	10.0	00.0	25.7	.	*+0-9 ²⁴ , 22 ²⁴ , =+0-9 ²⁴ , 24 ²⁴
14	4	100*	10*	10*	10.0	00.0	27.5	.	*+0-6 ²⁴ , 14 ²⁴ , 24 ²⁴ , *+0-7 ²⁴ , 23 ²⁴ , F ₂₄ 8 ²⁴ , 13 ²⁴ , 22 ²⁴ , [■]
15	5	10	10*	10	10.0	00.0	15.4	08	=+0-7 ²⁴ , 14 ²⁴ , 24 ²⁴ , F ₂₄ 17 ²⁴ , 24 ²⁴ , [■]
16	7	31	040	06	03.7	08.0	01.7	10	=+0-7 ²⁴ , [■], 10 ²⁴ , 20 ²⁴ , [■]
17	6	100	10	10	10.0	00.0	03.1	06	*+20-24 ²⁴ , 24 ²⁴ , 14 ²⁴ , 13 ²⁴ , =+0-3 ²⁴ , 24 ²⁴ , [■]
18	4	100*	10*	10	10.0	00.0	06.1	21	=+0-4 ²⁴ , 14-22 ²⁴ , *+0-4 ²⁴ , 6 ²⁴ , F ₂₄ 6 ²⁴ , 7 ²⁴ , *+7 ²⁴ , 14, R ²⁴ , 10 ²⁴ , =+22 ²⁴ , 24, [■]
19	4	02	10*	100*	07.3	00.0	12.4	11	=+0-3 ²⁴ , =+24 ²⁴ , 12 ²⁴ , *+24 ²⁴ , 13 ²⁴ , 24 ²⁴ , *+0-3 ²⁴ , 24 ²⁴ , =+24 ²⁴ , 24, [■]
20	4	10*	10*	10	10.0	00.0	21.3	23	[■], 0-0 ²⁴ , *+0-0 ²⁴ , 14 ²⁴ , 24 ²⁴ , *+24 ²⁴ , 16 ²⁴ , 24 ²⁴ , =+16 ²⁴ , 24, [■]
21	4	10	000	00	03.3	02.6	01.5	22	=+2-0-24, [■]
22	4	03	000	03	01.0	06.0	.	18	=+0-24, F ₂₄ 3 ²⁴ , =+8 ²⁴ , 9 ²⁴ , [■]
23	5	310	030	03	02.3	07.0	.	18	=+2-0-22, [■]
24	7	08	070	05	06.7	03.4	.	10	F ₂₄ 6 ²⁴ , E ₂₄ 24 ²⁴ , [■]
25	7	09	10	10	29.7	11.0	.	15	F ₂₄ 0-23 ²⁴ , *+19 ²⁴ , 19 ²⁴ , 22 ²⁴ , 24 ²⁴ , [■]
26	7	09	090	09	20.0	12.1	01.2	.	*+0-0 ²⁴ , 24 ²⁴ , F ₂₄ 0 ²⁴ , 4 ²⁴ , 10 ²⁴ , 23 ²⁴
27	8	09	09	09	19.0	16.1	01.7	.	*+0-3 ²⁴ , F ₂₄ 2 ²⁴
28	8	32	09	100	27.0	15.0	.	.	*+0-5 ²⁴ , [■]

1978 MART

BEOGRAD

 $\rho = 44^{\circ}48' N \lambda = 20^{\circ}28' E$ Gr. $\Delta G = + 1h 22 min.$

BR. ST. 169

D	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodenе pare e mm			Relativna vlažnost U %			Pravac i jačina veta D, f (0-12)					
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21			
1	745.0	746.0	748.0	09.8	15.4	10.6	11.6	17.2	08.7	05.5	07.3	08.1	07.6	80	62	79	74	SSE 1	WNW 2	SSE 2			
2	748.7	747.9	748.0	08.4	16.2	12.0	12.2	18.2	08.0	03.2	07.6	07.9	08.3	92	58	79	76	SE 2	NE 1	ESE 3			
3	747.7	746.4	746.0	08.4	18.6	10.0	11.8	16.8	08.1	06.0	06.8	07.7	07.3	82	48	79	70	ESE 3	ESE 3	ESE 3			
4	745.8	745.1	745.5	08.0	18.4	10.6	11.9	19.0	07.4	06.2	06.8	07.7	06.9	85	48	71	68	ESE 4	ESE 3	ESE 3			
5	746.2	745.8	746.4	08.7	20.2	12.8	13.6	20.5	08.6	07.1	06.6	07.9	07.4	78	44	66	63	ESE 4	ESE 3	ESE 3			
6	746.4	745.6	746.1	09.0	15.6	09.5	10.9	16.8	08.9	08.0	07.2	07.5	07.0	84	57	78	73	ESE 4	ESE 3	ESE 3			
7	747.7	751.4	752.6	08.2	22.3	02.1	03.7	09.5	02.0	02.0	07.4	05.2	05.1	91	97	95	94	SSW 2	W 3	W 3			
8	752.6	752.1	752.0	02.8	05.4	23.6	03.9	05.6	02.1	02.0	04.7	03.8	04.6	84	56	77	72	W 2	WSW 3	W 1			
9	751.2	750.0	752.2	00.4	09.0	05.6	05.2	09.0	00.0	-03.7	04.6	03.8	06.1	96	44	89	76	SSE 1	WSW 1	WSW 3			
10	752.8	753.7	754.6	04.4	03.4	04.4	04.2	06.0	02.8	03.9	05.6	05.6	05.2	90	95	82	89	WNW 3	NW 2	NW 2			
11	755.1	750.7	746.7	01.1	07.6	08.0	06.2	09.5	00.0	-32.2	04.5	04.7	05.0	91	60	63	71	WSW 1	WNW 3	WSW 3			
12	747.8	750.1	752.6	02.4	24.7	03.2	03.4	08.1	01.6	00.5	04.9	04.4	04.2	90	68	72	77	NW 2	NNE 2	WNW 2			
13	753.7	753.2	752.6	-01.0	09.0	05.6	04.8	09.5	-01.2	-04.7	03.9	04.2	04.4	92	48	64	68	W 1	SE 2	ESE 2			
14	753.2	752.8	750.9	04.3	12.8	10.5	09.5	13.8	02.6	-00.3	04.8	05.0	05.6	76	45	58	60	S 1	SSE 1	ESE 3			
15	750.3	747.8	747.2	10.2	15.0	08.8	10.7	17.0	07.5	03.0	05.4	06.6	08.1	58	52	95	68	ESE 2	S 3	NW 1			
16	749.1	747.7	746.0	06.8	16.2	12.8	12.2	17.6	06.6	03.5	06.6	05.1	04.4	89	37	40	55	WSW 3	SSW 2	WSW 3			
17	742.8	741.8	746.5	10.6	17.3	05.8	09.9	17.6	05.8	08.4	04.8	04.7	06.7	50	32	97	60	SE 3	SW 2	SSE 3			
18	746.7	747.7	749.5	05.8	07.4	07.2	06.9	07.7	05.8	05.0	06.5	06.6	07.1	94	86	93	91	S 2	SSE 1	SW 2			
19	753.2	751.6	750.6	03.1	07.6	05.8	05.6	08.3	03.1	02.2	05.5	04.9	04.0	95	62	58	72	WSW 2	WNW 2	NM 3			
20	750.3	744.8	742.4	01.0	09.5	08.6	06.9	10.1	00.9	-01.0	04.3	03.5	04.5	88	40	53	60	WSW 2	S 2	W 1			
21	735.9	735.4	739.3	06.3	13.4	06.9	08.4	13.9	05.9	05.8	06.6	07.4	05.9	92	64	79	78	SE 3	WNW 3	NW 2			
22	741.0	745.6	748.7	03.2	07.6	25.4	05.4	08.1	03.1	03.1	05.0	03.7	04.0	88	47	60	65	NM 2	N 3	NW 3			
23	741.1	749.8	747.3	-00.5	08.3	06.0	05.0	10.2	-00.6	-32.4	03.5	02.7	03.1	80	33	44	52	W 2	WSW 2	ESE 3			
24	743.1	739.9	742.0	05.2	08.8	J5.0	06.0	09.1	04.6	05.2	03.8	04.1	05.8	57	48	88	64	ESE 2	ESE 4	WSW 3			
25	745.3	747.4	750.1	02.5	06.7	05.3	05.0	07.5	02.3	02.3	05.2	05.7	05.4	95	77	80	84	NNE 2	N 3	WNW 2			
26	750.1	747.6	747.0	02.0	12.4	08.8	08.0	13.0	01.3	-02.0	04.9	03.8	04.5	93	35	54	61	SW 1	SW 2	ESE 2			
27	748.4	750.1	752.4	05.6	08.4	06.2	06.6	09.2	05.3	04.8	05.3	05.1	05.5	78	62	77	72	WNW 2	NW 2	SW 2			
28	753.1	753.8	756.0	02.5	13.0	08.2	08.0	13.8	00.8	-03.1	04.2	03.2	03.8	76	29	47	51	WSW 2	NNW 2	ESE 1			
29	755.1	753.7	752.4	06.6	18.3	12.9	12.7	18.8	04.6	-00.4	03.7	05.2	04.2	51	33	37	40	ESE 2	SE 2	ESE 2			
30	750.9	749.6	748.6	09.6	20.4	13.4	14.2	21.0	09.1	06.1	04.5	05.4	05.7	51	30	49	43	ESE 3	ESE 4	ESE 4			
31	747.9	747.0	746.8	09.2	18.2	11.6	12.7	18.7	09.0	07.0	04.3	04.7	06.0	50	30	59	46	ESE 5	ESE 4	ESE 5			
MES.	VRED.			748.3	748.2	748.6	05.3	11.8	08.0	08.3	13.0	04.3	02.8	05.4	05.4	05.6	80	52	70	68	2.3	2.4	2.5

1978 APRIL

BEOGRAD

1	746.0	745.0	741.7	08.8	19.5	14.1	14.1	19.5	08.0	06.2	06.5	06.9	06.1	77	41	50	56	ESE 3	NNE 3	ESE 2
2	740.6	739.6	740.8	09.3	17.6	12.3	12.9	18.3	08.8	06.0	06.2	06.3	06.5	70	42	61	58	ESE 3	ESE 3	ESE 3
3	742.6	741.9	741.6	09.2	19.3	11.7	13.0	19.6	08.3	J6.4	06.8	05.7	08.2	78	34	80	64	ESE 3	E 3	E 4
4	741.7	742.1	743.2	09.9	12.4	12.4	11.8	13.4	09.6	09.0	08.8	09.6	10.2	96	89	94	93	E 3	ESE 2	WSW 2
5	744.2	744.9	746.0	11.5	13.5	10.0	11.3	14.1	10.0	07.5	09.6	07.8	08.1	94	67	88	83	SW 1	WSW 2	NNW 2
6	748.4	750.8	752.4	05.6	10.2	07.8	07.9	11.4	05.6	05.5	06.1	05.8	04.6	89	62	58	70	N 2	NW 2	NNE 3
7	751.4	750.1	746.8	00.1	10.2	04.2	04.7	11.2	-00.1	-02.3	04.0	05.5	05.7	87	59	92	79	NNE 2	ENE 3	ESE 4
8	743.2	743.0	743.4	05.5	09.5	08.0	07.8	09.9	04.1	03.6	05.7	06.7	07.5	84	75	94	84	ENE 2	NNE 2	NNW 1
9	745.0	746.5	747.8	04.2	12.1	06.0	07.1	12.3	03.9	03.9	04.5	06.2	05.5	72	59	78	70	NNE 2	E 3	ESE 4
10	747.8	747.6	748.0	06.3	14.0	08.8	09.5	15.0	04.5	02.3	05.5	06.7	07.2	77	56	85	73	ESE 3	E 4	ESE 4
11	748.7	748.8	748.9	09.5	18.5	12.8	13.4	19.0	08.5	02.3	07.3	06.7	07.6	82	42	68	64	ESE 4	SE 2	ESE 3
12	749.5	748.0	746.5	12.5	24.0	17.2	17.7	25.2	11.0	05.7	06.8	06.9	07.6	62	31	51	48	ESE 3	SSW 2	ESE 4
13	743.7	740.5	737.8	15.6	16.0	17.1	16.5	19.4	07.2	06.0	07.2	07.9	07.7	54	58	53	55	SE 4	E 3	ESE 4
14	744.6	737.4	739.4	14.7	17.4	13.0	14.5	18.0	13.0	11.2	08.7	07.0	07.2	69	47	64	60	SE 3	N 1	HNE 2
15	739.7	738.2	739.8	12.3	17.4	08.6	11.7	17.6	08.6	03.8	07.0	06.3	07.3	65	42	87	65	E 3	ESE 3	SE 3
16	741.1	744.1	746.2	07.4	08.0	06.0	06.9	09.1	05.4	05.3	06.8	06.3	05.8	88	78	82	83	WNW 2	WSW 2	WSW 3
17	747.5	748.6	749.3	04.6	05.6	04.8	05.0	06.4	04.4	02.4	05.2	04.8	05.5							

BR. ST. 169

$$H_s = 132 \text{ m } H_b = 132.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$$

Dan	Vrem.	Oblačnost N (0-10)					Intenzitet sunca bez oblačnosti	Podzemna R mm	Snežni pokrivač h cm	Razvoj vremena w	
		14	7	14	21	Sred Dnes					
1	7 09	050	00	04.7	03.6	03.0	.	.	0° 6° 7° 8° 9° 10° 11° 12° 13° 14° 15° 16°		
2	7 00	060	01	02.3	06.4	00.0	.	.	Δ 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10° 11°		
3	8 00	010	00	00.3	09.6	.	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
4	8 00	000	00	00.0	09.5	.	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
5	7 03	080	09	06.7	05.4	.	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
6	7 07	070	100	08.0	02.9	.	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
7	5 100	100*	10	10.0	00.0	00.0	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
8	7 10	09	00	06.3	01.2	02.7	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
9	7 06	030	100	06.3	05.1	.	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
10	7 100	100	00	06.7	00.2	01.9	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
11	7 06	10	05	07.0	03.7	03.4	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
12	7 10	09*	00	06.3	01.2	00.0	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
13	7 00	010	00	00.3	08.0	01.4	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
14	7 10	050	05	06.7	02.4	.	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
15	7 100	100	100	10.0	02.6	00.0	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
16	7 00	000	05	01.7	09.5	06.2	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
17	8 09	09	100	09.3	00.3	.	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
18	7 10	100	100	10.0	00.3	10.6	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
19	7 07	10	09	08.7	00.8	01.5	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
20	7 00	09	07	05.3	05.7	.	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
21	7 100	060	09	08.3	02.7	06.6	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
22	7 10	10	05	08.3	00.1	04.3	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
23	7 00	000	09	03.0	10.9	.	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
24	7 10	10	100	10.0	00.2	.	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
25	7 100	100	01	07.0	00.0	10.2	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
26	7 020	000	10	04.0	09.7	00.9	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
27	7 100	10	00	06.7	01.9	00.0	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
28	7 000	070	00	02.3	10.8	00.0	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
29	8 030	000	00	01.0	11.2	.	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
30	8 000	000	00	00.0	11.3	.	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
31	8 000	000	00	00.0	08.0	.	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
MES. VRED.		05.5	06.0	04.7	05.4	144.9	53.1				

1	7 00	020	06	02.7	07.6	.	.	.	Δ 0° 3° 6° 9° 12° 15° 18° 21° 24° 27° 30° 33°		
2	8 08	080	02	06.0	07.3	.	.	.	Δ 0° 7° 10° 13° 16° 19° 22° 25° 28° 31° 34° 37°		
3	8 00	050	03	02.7	09.7	.	.	.	Δ 0° 4° 8° 12° 16° 20° 24° 28° 32° 36° 40° 44°		
4	7 100	100	100	10.0	00.0	00.0	.	.	Δ 0° 5° 10° 15° 20° 25° 30° 35° 40° 45° 50° 55°		
5	7 09	10	100	09.7	00.1	00.6	.	.	Δ 0° 5° 10° 15° 20° 25° 30° 35° 40° 45° 50° 55°		
6	7 100	060	08	08.0	02.9	05.5	.	.	Δ 0° 6° 10° 14° 18° 22° 26° 30° 34° 38° 42° 46°		
7	7 01	08	100	06.3	09.0	.	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
8	6 06	100	090	08.3	00.0	01.4	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
9	7 050	09	06	06.7	09.0	04.3	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
10	7 040	060	100	06.7	03.9	.	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
11	8 100	080	00	26.0	04.1	00.5	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
12	8 09	080	00	05.7	06.7	00.0	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
13	7 09	10	05	08.0	00.6	.	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
14	8 040	080	05	05.7	07.6	00.1	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
15	8 070	10	06	07.3	03.9	00.0	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
16	6 10	10	100	10.0	00.0	06.1	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
17	6 10	10	10	10.0	00.0	00.0	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
18	6 100	100	09	39.7	00.0	03.2	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
19	7 28	10	100	29.3	00.3	00.8	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
20	7 10	10	08	29.3	10.4	00.3	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
21	8 260	050	09	26.7	10.1	00.0	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
22	6 06	080	06	06.7	05.8	.	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
23	6 09	060	02	05.7	05.9	00.3	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
24	8 000	040	060	23.3	20.5	00.3	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
25	7 09	100	100	19.7	00.1	00.5	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
26	7 070	080	04	06.3	06.8	03.6	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
27	7 08	17	22	25.7	03.3	01.2	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
28	8 040	060	10	23.3	05.7	01.9	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
29	8 090	040	01	16.0	27.7	01.2	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
30	8 11	160	10	18.7	06.1	00.1	.	.	Δ 0° 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10°		
MES. VRED.		06.0	07.8	06.2	17.0	33.9	31.8				

1978 MAJ

BEOGRAD

 $\varphi = 44^{\circ}48'N \lambda = 20^{\circ}28'E$ Gr. $\Delta G = +1h\ 22\ min.$

BR. ST. 169

d	Vazdušni pritisk P mm			Temperatura vazduha T C°								Napon vodenе pore e mm			Relativna vlažnost u %			Provac i jačina vetro D, f (0-12)			
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21	
1	744.9	738.3	737.3	14.9	24.5	24.1	21.9	27.7	14.3	11.0	09.1	08.6	06.2	71	37	27	45	ESE 3	ESE 4	S 3	
2	736.1	732.1	737.5	15.6	26.8	19.0	12.6	25.2	10.9	10.0	09.8	12.6	09.2	74	88	93	85	E 3	SE 3	W 5	
3	744.6	746.4	749.8	11.6	19.7	13.4	14.5	20.2	10.2	08.3	08.3	08.4	10.4	81	49	90	73	WSM 2	WNW 3	WSW 2	
4	753.1	753.6	753.7	11.5	19.5	13.7	14.6	20.2	08.8	04.4	07.8	08.4	09.0	77	49	76	67	SW 1	ENE 2	ESE 2	
5	754.7	753.0	751.6	15.5	23.5	18.6	19.1	23.7	11.4	06.1	08.1	08.0	08.8	61	37	55	51	ESE 2	ESE 3	ESE 3	
6	749.6	748.4	746.9	17.6	24.1	16.7	16.8	25.0	16.2	05.6	08.4	11.1	12.5	56	49	87	64	ESE 3	ESE 2	S 1	
7	744.3	744.2	743.1	15.3	13.7	10.3	18.4	18.0	10.2	13.1	11.3	08.7	08.8	87	74	94	85	ESE 3	ESE 4	ESE 4	
8	742.5	742.1	742.1	11.7	16.4	13.4	13.7	17.7	09.8	07.0	08.9	10.3	10.3	87	73	89	83	NW 1	NW 3	WSW 2	
9	743.3	744.3	745.4	12.6	18.0	13.1	14.2	19.2	11.8	11.2	10.2	08.6	09.6	93	56	85	78	NW 2	WNW 2	WSW 2	
10	748.6	750.4	752.5	12.1	15.7	10.6	12.3	17.4	10.3	09.3	09.5	09.3	08.8	90	69	92	84	WSW 2	W 3	WSW 2	
11	752.6	752.2	753.1	08.8	12.1	38.2	09.3	12.9	07.6	05.2	06.1	05.7	04.0	72	54	49	58	N 2	N 3	NW 3	
12	752.1	750.3	749.8	03.7	09.2	04.0	05.2	10.2	03.7	03.2	04.3	04.4	05.4	71	51	88	70	W 3	NW 3	SW 1	
13	748.4	746.7	745.7	06.3	13.2	10.0	09.9	14.5	01.6	-02.2	04.6	05.4	08.1	63	48	88	66	ESE 2	SSW 2	ESE 3	
14	763.0	746.7	749.3	09.8	13.5	08.6	10.1	13.9	08.8	09.2	08.5	07.2	06.8	94	62	81	79	WSN 2	W 3	W 3	
15	750.2	748.8	747.9	08.4	15.2	11.7	11.8	15.6	05.3	01.8	06.7	06.2	07.2	81	48	69	66	SW 2	ENE 2	ENE 1	
16	748.6	749.5	751.3	10.0	17.0	10.4	12.0	17.6	06.4	02.4	07.3	06.8	07.7	79	47	81	69	SSW 1	W 3	ESE 1	
17	752.7	752.0	751.6	12.9	21.2	16.4	16.7	21.5	07.7	02.9	07.9	06.8	07.3	71	36	52	53	S 1	SE 1	ESE 3	
18	751.8	751.9	751.1	13.8	21.1	15.8	16.6	22.0	10.6	09.0	08.6	09.0	08.9	72	48	66	62	NNE 2	WNW 2	NE 2	
19	750.4	749.4	748.6	15.5	22.8	18.1	18.6	23.7	12.5	09.3	10.0	10.1	10.4	76	49	54	60	ESE 1	NNE 2	E 2	
20	748.7	749.3	749.9	17.4	19.6	15.9	17.2	23.2	14.1	11.5	10.2	12.1	11.4	68	71	84	74	SE 3	ESE 3	E 2	
21	750.4	750.1	749.5	16.7	24.0	19.6	20.0	24.2	13.5	10.4	11.2	12.5	11.4	78	56	67	67	ESE 3	ESE 3	ESE 3	
22	746.5	744.2	741.2	18.4	20.0	19.8	19.5	21.3	17.4	16.0	11.1	12.5	16.9	70	71	63	68	ESE 4	ESE 4	SE 4	
23	741.1	743.0	744.7	13.6	19.3	15.8	16.1	22.8	13.1	12.8	11.2	12.1	10.0	96	78	74	43	SW 3	W 2	SSW 2	
24	746.0	746.3	747.8	17.0	23.1	16.3	18.0	23.3	13.6	09.8	08.7	08.6	11.6	60	41	85	62	SSW 2	W 2	- 0	
25	748.5	748.2	748.7	16.4	20.8	15.2	16.9	21.9	13.4	10.1	10.4	10.8	12.3	74	59	95	76	WSW 2	NNW 3	N 2	
26	744.9	750.2	751.0	14.8	19.0	13.6	15.3	19.9	13.0	10.0	10.8	10.1	10.3	86	61	88	78	WSW 2	NNW 3	WSW 1	
27	751.3	751.3	750.7	12.1	18.0	14.4	14.7	16.8	10.7	08.2	09.0	09.1	10.2	85	59	83	76	W 2	SW 3	WSW 2	
28	750.3	750.4	750.5	11.4	16.7	14.2	14.1	18.1	11.2	11.0	09.2	10.4	10.6	91	73	88	84	W 2	N 1	WSW 1	
29	750.1	748.1	748.1	13.0	18.6	12.4	14.1	18.7	12.2	11.9	10.6	10.2	10.1	95	63	93	84	W 2	SSW 2	SSW 1	
30	749.1	750.2	751.7	13.1	19.3	14.6	15.4	20.0	10.0	06.2	10.5	09.7	10.6	92	58	85	78	WNW 2	NW 2	WSW 1	
31	752.8	752.5	753.0	14.5	23.1	18.4	18.6	23.6	11.7	08.1	10.6	10.9	12.0	86	51	76	71	SW 2	NNW 3	WSW 2	
MES.	VRFD.	748.1	747.9	748.2	13.1	18.7	14.1	15.0	20.0	10.7	38.2	09.0	09.2	09.3	79	57	77	71	2.2	2.6	2.1

1978 JUN

BEOGRAD

1	754.1	753.3	753.3	16.4	26.2	22.0	21.7	26.8	13.7	09.9	11.6	09.9	08.6	83	39	44	55	SW 2	NNW 2	N 1
2	753.6	752.1	751.3	16.4	25.8	20.4	20.8	25.8	13.4	09.2	11.0	09.0	09.6	79	36	53	56	WSW 2	NW 3	NNW 2
3	751.6	750.9	752.0	16.9	26.4	19.3	20.5	27.6	13.4	10.5	10.7	10.7	09.9	74	41	59	58	WNW 2	ENE 2	WSW 1
4	753.1	753.2	752.8	18.0	25.8	20.2	21.1	27.1	13.6	10.2	11.4	10.7	10.5	74	43	59	59	WNW 1	N 2	ESE 2
5	753.3	752.7	752.6	20.6	27.8	21.2	22.7	28.2	15.9	12.5	11.1	09.6	12.3	61	34	65	53	ESE 1	WSW 2	ESE 3
6	752.1	751.9	751.9	20.7	24.4	19.8	21.2	25.8	17.9	14.3	11.4	14.6	12.6	62	63	73	66	ESE 2	NNE 1	SE 2
7	752.0	752.0	751.2	21.0	28.0	21.9	23.2	28.4	18.3	13.9	12.4	14.5	12.4	66	51	63	63	ESE 2	SSE 2	ESE 2
8	750.5	749.8	748.9	20.6	27.1	22.7	23.3	29.4	18.1	14.6	12.7	12.7	12.5	70	42	61	58	SW 2	SH 2	WSW 1
9	750.9	750.3	750.4	18.0	25.0	20.7	21.1	25.8	17.5	17.0	13.6	11.8	10.1	88	50	55	55	WSW 3	NW 3	NNW 1
10	750.5	748.7	748.6	22.5	29.4	23.8	24.9	32.2	15.1	10.7	11.1	13.0	14.5	54	42	66	54	ESE 1	SE 3	SE 1
11	750.9	753.5	754.8	21.8	19.3	15.4	17.9	25.4	15.4	16.2	14.6	13.4	11.8	75	81	93	82	SSE 1	N 3	NNW 2
12	752.8	747.5	743.1	16.4	23.4	24.0	22.0	25.6	14.6	12.5	12.4	12.1	11.6	88	56	52	65	ESE 3	ESE 3	SSE 3
13	746.0	747.3	748.7	15.6	13.6	12.5	12.5	24.0	12.5	14.5	12.6	10.9	09.9	95	94	91	93	NNE 2	WN 4	WSH 2
14	748.1	747.2	747.6	12.4	15.8	14.4	14.3	16.2	11.9	11.6	10.1	10.0	10.3	93	74	84	84	W 1	WNW 2	WSW 2
15	748.3	747.2	745.1	12.5	18.0	15.9	15.6	18.2	12.0	11.0	10.0	10.0	11.0	92	65	81	79	SW 1	ESE 1	SE 1
16	741.0	742.6	743.5	14.3	19.1	16.5	16.6	20.7	13.7	13.7	11.8	11.3	12.4	97	68	88	86	ENE 2	NNW 2	SSW 2
17	744.7	744.7	744.8	16.0	24.6	21.3	20.8	26.6	15.0	11.3	12.7	11.3	16.4	93	49	84	75	SE 2	WSW 1	ESE 2
18	746.5	748.8	751.2	22.3																

BP. ST. 169

 $H_a = 132 \text{ m } H_b = 132.0 \text{ m } h_1 = 2.0 \text{ m } h_2 = 4.2 \text{ m}$

DNE	VRED.	Oblačnost N (0-10)					Sred Duge	Padavina R mm	Snijeli pokriven h cm	Kraće vrijeme w
		14	7	14	21	Sred Duge				
1	8	10	08	06	06.0	04.7	.	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
2	7	100	100	100	10.0	00.1	00.1	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
3	8	99	030	09	07.0	07.6	23.3	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
4	8	000	080	00	02.7	08.9	01.8	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
5	7	910	070	08	05.3	10.6	.	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
6	8	080	10	100	09.3	03.7	.	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
7	7	10	100	100	10.0	01.7	03.4	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
8	7	37	09	100	08.7	04.9	06.0	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
9	6	08	08	10	08.7	04.7	05.6	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
10	6	12	090	09	09.3	02.3	00.0	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
11	7	760	09	10	08.3	04.0	00.9	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
12	8	78	060	09	04.7	04.6	.	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
13	8	760	09	100	08.3	06.1	.	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
14	8	100	78	01	06.9	02.7	05.5	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
15	7	06	08	04	06.0	35.2	00.3	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
16	8	090	090	09	03.0	08.6	.	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
17	7	09	050	09	04.7	11.8	02.4	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
18	8	020	060	74	04.0	09.8	01.0	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
19	8	09	020	04	05.0	07.3	00.0	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
20	7	05	09	05	06.3	37.9	00.2	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
21	7	910	980	05	04.7	07.5	25.7	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
22	7	10	100	100	10.0	00.0	00.0	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
23	7	100	770	05	07.3	07.1	17.4	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
24	8	050	760	06	05.7	07.8	02.7	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
25	8	020	100	10	07.3	07.5	00.0	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
26	7	760	10	00	05.3	05.8	11.3	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
27	7	950	10	100	08.3	02.0	00.2	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
28	7	10	060	09	08.3	02.2	00.2	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
29	7	10	070	09	08.7	03.0	10.0	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
30	7	09	770	05	07.3	06.7	07.2	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
31	7	140	040	03	03.7	19.5	00.2	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
MES. VRED.		36.4	07.7	06.5	06.8	177.3	125.4			

BENGRAN

1978 JUN

1	8	010	050	05	13.3	13.3	.	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
2	8	060	940	08	03.3	12.4	.	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
3	8	770	750	09	01.7	09.8	.	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
4	8	030	740	02	03.0	12.5	00.0	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
5	8	020	720	08	04.0	11.1	.	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
6	8	260	10	00	05.3	04.7	.	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
7	8	25	730	09	02.7	08.1	00.0	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
8	8	050	770	03	05.0	08.4	.	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
9	8	360	050	00	03.7	11.4	02.8	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
10	8	250	070	05	04.0	12.1	.	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
11	8	020	10	09	07.0	12.8	00.9	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
12	8	99	10	08	09.0	77.2	.	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
13	6	100	100	100	10.0	00.0	03.5	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
14	6	100	10	10	10.0	00.0	11.4	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
15	7	10	10	08	09.3	01.0	02.1	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
16	7	130	050	05	06.7	03.2	18.8	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
17	8	98	750	06	06.3	57.8	01.4	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
18	8	99	09	06	05.0	05.4	.	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
19	8	330	790	01	04.3	07.4	01.0	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
20	8	020	710	00	10.7	12.5	01.0	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
21	7	720	1000	100	07.3	05.6	.	0° 0-10°; 10°-20°; 20°-30°; 30°-40°; 40°-50°; 50°-60°; 60°-70°; 70°-80°; 80°-90°; 90°-100°	.	.
22	7	10	260	00	25.3	75.0	03.0	0° 0-10°; 10°-20°; 20°-30°; 30°		

1978 JUL

BEOGRAD

 $\varphi = 44^{\circ}48' N \lambda = 20^{\circ}28' E$ Gr. $\Delta G = +1h\ 22\ min.$

BR. ST. 169

D	Vazdušni pritisk P mm			Temperatura vazduha T C°							Napon vodené pare ø mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0—12)				
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21	
1	752.8	751.9	751.7	17.2	26.0	18.8	20.2	26.5	11.9	0.6.7	10.0	09.8	12.0	68	39	74	60	SE	1	WSW 1	- 0
2	750.6	749.1	750.2	21.3	28.8	19.8	22.4	29.2	17.3	13.5	13.2	13.1	15.9	70	44	92	69	ESE 2	2	WSW 2	WSW 2
3	750.5	749.6	748.9	17.6	24.1	19.2	20.0	25.0	16.3	15.8	13.7	11.4	14.2	91	51	85	76	WSW 1	1	SE 2	SE 2
4	748.4	747.5	746.6	20.9	28.2	23.3	23.9	29.3	15.2	11.3	12.9	14.4	15.6	69	50	73	64	ESE 3	2	WSW 2	SE 3
5	747.2	743.9	748.7	23.2	30.3	15.5	21.2	31.1	15.5	14.0	11.7	12.3	12.3	55	38	93	62	SE 2	4	SE 4	SH 2
6	751.0	749.3	748.1	16.8	24.1	21.3	20.9	25.2	14.5	12.4	11.9	12.1	13.2	83	54	70	69	SW 1	1	E 3	E 2
7	746.6	747.8	747.8	19.6	22.0	17.3	19.1	22.3	17.3	16.5	11.2	12.3	12.4	65	62	84	70	S 3	3	WSW 2	SSW 3
8	750.5	750.9	751.6	14.7	19.1	15.8	16.4	20.3	14.4	14.3	11.5	11.3	11.6	92	68	86	82	WNW 2	3	WSW 3	WSW 3
9	751.4	748.7	746.7	15.1	22.4	16.8	17.8	23.1	12.4	10.5	10.2	10.0	10.3	79	49	72	67	SW 2	2	SSE 2	ESE 1
10	748.1	748.5	749.1	14.8	20.1	18.2	17.8	20.8	14.3	12.0	10.7	12.4	10.5	85	70	67	74	W 2	2	NNE 3	ENE 1
11	750.2	750.3	750.2	17.0	25.4	20.4	20.8	26.0	15.6	15.1	11.0	11.6	12.8	76	48	71	65	NE 2	2	ENE 1	ENE 1
12	750.9	750.7	750.8	23.1	29.4	22.8	24.5	30.0	18.8	15.6	13.4	14.1	14.6	63	46	70	60	ESE 2	2	WSW 2	E 1
13	752.2	752.5	753.2	21.1	28.2	23.3	24.0	28.4	19.0	13.0	16.0	13.8	13.3	85	48	62	65	W 2	2	WNW 2	WNW 2
14	753.6	753.1	752.0	19.5	25.8	21.5	22.1	26.4	16.3	13.4	12.6	12.2	10.5	74	49	54	59	N 2	2	NNW 2	NE 1
15	750.0	748.2	750.0	20.8	27.2	21.0	22.5	27.3	16.0	12.7	11.2	11.3	12.8	61	42	69	57	ESE 1	2	NNW 2	NNW 2
16	751.9	751.5	751.2	17.0	22.9	19.4	19.7	23.7	15.4	14.2	08.3	08.6	09.7	57	41	57	52	W 2	3	N 2	N 2
17	752.6	752.7	752.7	17.3	25.2	19.3	20.3	25.7	13.8	10.7	10.2	11.3	11.7	68	47	70	62	SSW 1	2	NNW 2	ESE 1
18	750.9	748.0	745.4	19.7	31.4	26.0	28.8	31.9	17.8	13.7	11.7	14.1	14.9	68	41	59	56	ESE 3	2	S 2	SE 3
19	742.7	739.4	745.6	23.6	32.4	18.2	23.1	32.8	18.0	16.8	13.4	12.8	14.1	61	35	90	62	ESE 2	2	S 3	W 3
20	749.2	748.5	748.0	15.8	22.8	17.6	18.5	24.2	14.2	12.7	10.6	09.0	10.6	79	43	70	64	WSW 2	2	NNW 2	NNW 1
21	747.7	746.2	747.1	18.6	26.6	17.9	20.3	26.9	14.0	10.9	10.3	09.5	09.0	64	36	59	53	ESE 1	1	ESE 1	NW 3
22	751.1	751.6	753.3	12.7	20.2	16.1	16.3	20.5	12.4	12.0	10.1	08.5	07.9	91	48	57	65	W 3	3	NNW 3	NNW 2
23	753.6	753.0	752.9	12.2	20.5	16.9	16.6	21.2	10.4	08.4	08.3	08.0	09.2	78	44	63	62	WSW 2	3	NNW 3	WSW 2
24	752.8	751.9	752.1	15.8	22.4	16.5	17.3	23.6	11.8	09.3	09.0	08.6	10.0	76	42	71	63	SW 2	2	WNW 3	NW 1
25	752.6	751.9	752.0	15.1	24.5	18.6	19.2	24.8	11.2	08.5	09.9	09.0	10.3	77	39	64	60	SW 1	2	NNW 2	SSW 1
26	752.6	752.1	751.7	17.1	25.5	18.6	20.0	26.7	12.7	10.0	10.1	08.3	11.5	69	34	72	58	SSW 1	2	NE 2	E 1
27	752.4	752.6	753.3	18.7	28.4	21.7	22.6	28.6	13.8	10.5	10.9	09.7	11.2	68	33	58	53	SE 1	3	E 2	E 2
28	754.5	755.2	752.2	20.6	27.6	22.2	23.2	28.4	17.3	13.2	10.8	11.0	12.5	59	40	62	54	ESE 4	2	E 2	E 1
29	755.4	754.1	753.3	21.4	27.3	21.2	22.8	28.6	18.7	15.2	12.6	11.9	13.3	66	44	70	60	SE 1	1	SSE 1	ESE 2
30	752.8	752.1	751.3	20.8	27.2	19.6	21.8	27.7	17.4	13.0	11.1	10.9	10.8	60	40	63	54	ESE 2	2	NNE 2	ESE 1
31	750.9	750.3	750.1	19.4	27.7	21.4	22.5	28.7	14.8	11.1	11.8	10.9	11.2	70	39	59	56	ESE 1	1	ESE 1	E 1

MES. VRED. 750.9 750.1 750.3

18.3 25.6 19.6 20.8 26.3 15.1 12.6 11.3 11.1 11.9 72 45 70 62 1.8 2.2 1.7

1978 AVGUST

BEOGRAD

1	751.1	751.5	751.9	17.9	28.1	21.2	22.1	28.5	15.2	12.3	11.7	11.8	11.0	76	41	58	58	SW 2	2	NW 2	ESE 2
2	752.5	752.0	751.4	19.6	29.5	23.5	24.0	29.9	16.4	12.5	11.2	11.2	11.3	65	36	52	51	ESE 3	3	SE 3	ESE 3
3	750.7	750.1	749.9	20.9	30.2	24.2	24.9	30.6	19.1	16.1	10.5	11.8	13.0	57	37	57	50	ESE 3	2	SE 2	ESE 3
4	750.4	750.0	750.4	21.9	28.0	22.3	23.6	30.2	17.6	15.5	14.1	15.2	15.8	72	53	78	68	SSW 1	2	WSW 3	SSE 2
5	749.8	750.1	750.2	20.3	25.4	22.5	22.7	26.4	19.8	15.7	15.7	15.8	13.3	88	65	66	73	SW 2	2	NNW 3	NNW 2
6	750.4	750.1	749.0	19.0	28.3	21.6	22.6	29.0	16.0	12.2	13.3	10.8	13.4	80	37	69	62	SW 2	2	SE 1	SE 1
7	748.1	746.5	744.2	23.3	32.7	25.8	26.9	33.3	18.0	13.5	12.2	13.8	11.7	57	37	47	47	SE 3	2	ESE 2	ESE 3
8	741.8	739.4	743.0	24.1	33.9	23.4	26.2	34.1	22.8	18.5	10.1	13.0	11.6	45	33	54	44	SE 3	4	SSE 4	NW 3
9	748.6	748.0	748.6	16.3	24.7	17.6	18.9	23.0	19.5	13.2	10.0	09.4	09.4	72	41	62	58	W 2	2	SSW 2	SE 2
10	749.3	749.7	749.8	16.4	24.1	19.2	19.7	24.7	14.8	12.0	09.4	09.2	10.2	67	41	61	56	NNE 2	2	NNW 2	NNW 2
11	751.3	750.6	750.3	15.5	18.6	16.8	16.9	23.0	13.9	12.0	11.9	09.9	10.8	90	62	76	76	SW 2	2	SSW 1	SSW 1
12	752.0	751.9	752.5	14.1	21.4	16.9	17.3	22.1	12.8	11.9	10.3	10.3	10.6	85	54	59	66	WSW 2	2	NW 3	NW 3
13	753.5	752.8	752.1	14.2	21.5	15.0	16.4	23.0	11.7	0.9.0	09.4	08.0	08.7	78	42	68	63	WSW 2	2	ESE 1	ESE 1
14	751.8	751.6	752.5	15.9	24.4	19.2	19.7	24.6	13.0	0.9.4	09.2	08.6	08.4	68	38	50	52	ESE 2	2	NNE 2	NNE 2
15	753.6	752.8	752.6	15.5	26.6	18.8	19.9	26.7	12.6	0.9.8	10.0	09.5	09.6	76	36	59	57	NW 1	1	SSE 2	ESE 2
16	753.1	752.7	751.8	18.7	29.2	22.3	23.1	30.0	15.7	11.											

БЕОГРАД

1978 JUL

8R. ST. 169

$$H_s = 132 \text{ m} \quad H_b = 132.0 \text{ m} \quad h_t = 2.0 \text{ m} \quad h_f = 1.2 \text{ m}$$

Den	V. M. O.	Oblačnost N (0-10)					Incep. 1000 hPa	Podzemí R mm	Snežní pokrývka h cm	Rozvoj vremene w
		14	7	14	21	Sred Dnes				
1	8	010	020	02	01.7	11.9	.	.	.	$\Delta^{+} 0-5^{\circ} N, 10^{\circ}-14^{\circ}$
2	8	060	050	100	07.0	10.8	.	.	.	$\Delta^{+} 0-5^{\circ} N, 10^{\circ}-14^{\circ}, \Delta^{+} 10^{\circ}-14^{\circ}, R^{+} 10^{\circ}-14^{\circ}, C^{+} 10^{\circ}-14^{\circ}$
3	7	08	050	00	04.3	09.3	03.9	.	.	$\Delta^{+} 0-5^{\circ} N, = 0^{\circ}-10^{\circ}, \Delta^{+} 10^{\circ}-14^{\circ}$
4	7	000	040	00	01.3	12.6	.	.	.	$\Delta^{+} 0-5^{\circ} N, 10^{\circ}-14^{\circ}, R^{+} 10^{\circ}-14^{\circ}, C^{+} 10^{\circ}-14^{\circ}$
5	7	000	040	100K	04.7	12.3	.	.	.	$\Delta^{+} 0-5^{\circ} N, 10^{\circ}-14^{\circ}, R^{+} 10^{\circ}-14^{\circ}, C^{+} 10^{\circ}-14^{\circ}$
6	8	030	020	06	03.7	10.9	13.5	.	.	$\Delta^{+} 0-5^{\circ} N, 10^{\circ}-14^{\circ}, R^{+} 10^{\circ}-14^{\circ}, C^{+} 10^{\circ}-14^{\circ}, \Delta^{+} 10^{\circ}-14^{\circ}, V^{+} 10^{\circ}-14^{\circ}, T^{+} 10^{\circ}-14^{\circ}, P^{+} 10^{\circ}-14^{\circ}, F^{+} 10^{\circ}-14^{\circ}, S^{+} 10^{\circ}-14^{\circ}$
7	7	100	040	100K	08.0	05.5	03.8	.	.	$\Delta^{+} 0-5^{\circ} N, 10^{\circ}-14^{\circ}, = 0^{\circ}-10^{\circ}, \Delta^{+} 10^{\circ}-14^{\circ}$
8	6	10	08	06	08.0	03.7	14.1	.	.	$\Delta^{+} 0-5^{\circ} N, 10^{\circ}-14^{\circ}, = 0^{\circ}-10^{\circ}, \Delta^{+} 10^{\circ}-14^{\circ}$
9	7	070	060	00	04.3	11.0	00.0	.	.	$\Delta^{+} 0-5^{\circ} N, 10^{\circ}-14^{\circ}, = 0^{\circ}-10^{\circ}$
10	8	100	050	09	08.0	04.1	00.1	.	.	$\Delta^{+} 0-5^{\circ} N, 10^{\circ}-14^{\circ}, = 0^{\circ}-10^{\circ}, G^{+} 10^{\circ}-14^{\circ}, R^{+} 10^{\circ}-14^{\circ}, P^{+} 10^{\circ}-14^{\circ}$
11	8	06	020	01	03.0	11.7	01.1	.	.	$\Delta^{+} 0-5^{\circ} N, \Delta^{+} 10^{\circ}-14^{\circ}$
12	7	000	000	00	00.0	12.2	.	.	.	$\Delta^{+} 0-5^{\circ} N, \Delta^{+} 10^{\circ}-14^{\circ}, R^{+} 10^{\circ}-14^{\circ}$
13	7	050	030	00	02.7	11.0	09.7	.	.	$\Delta^{+} 0-5^{\circ} N, \Delta^{+} 10^{\circ}-14^{\circ}, = 0^{\circ}-10^{\circ}, \Delta^{+} 10^{\circ}-14^{\circ}$
14	7	000	010	00	00.3	13.0	.	.	.	$\Delta^{+} 0-5^{\circ} N, = 0^{\circ}-10^{\circ}, \Delta^{+} 10^{\circ}-14^{\circ}, C^{+} 10^{\circ}-14^{\circ}$
15	7	010	030	09	04.3	08.9	.	.	.	$\Delta^{+} 0-5^{\circ} N, = 0^{\circ}-10^{\circ}, \Delta^{+} 10^{\circ}-14^{\circ}, C^{+} 10^{\circ}-14^{\circ}$
16	7	050	010	01	02.3	11.8	00.0	.	.	$= 0^{\circ}-5^{\circ} N, R^{+} 10^{\circ}-14^{\circ}, \Delta^{+} 10^{\circ}-14^{\circ}, \Delta^{+} 10^{\circ}-14^{\circ}$
17	6	010	030	00	01.3	12.3	.	.	.	$\Delta^{+} 0-5^{\circ} N, = 0^{\circ}-10^{\circ}, \Delta^{+} 10^{\circ}-14^{\circ}, R^{+} 10^{\circ}-14^{\circ}$
18	8	000	020	00	00.7	12.7	.	.	.	$\Delta^{+} 0-5^{\circ} N, \Delta^{+} 10^{\circ}-14^{\circ}, = 0^{\circ}-10^{\circ}, \Delta^{+} 10^{\circ}-14^{\circ}, R^{+} 10^{\circ}-14^{\circ}$
19	8	06	040	100K	06.7	10.3	.	.	.	$\Delta^{+} 0-5^{\circ} N, \Delta^{+} 10^{\circ}-14^{\circ}, = 0^{\circ}-10^{\circ}, \Delta^{+} 10^{\circ}-14^{\circ}, R^{+} 10^{\circ}-14^{\circ}$
20	7	00	040	00	01.3	11.5	00.4	.	.	$= 0^{\circ}-5^{\circ} N, \Delta^{+} 10^{\circ}-14^{\circ}$
21	8	000	010	06	02.3	12.2	.	.	.	$\Delta^{+} 0-5^{\circ} N, R^{+} 10^{\circ}-14^{\circ}, = 0^{\circ}-10^{\circ}, \Delta^{+} 10^{\circ}-14^{\circ}$
22	7	10	050	00	03.0	07.2	06.8	.	.	$\Delta^{+} 0-5^{\circ} N, R^{+} 10^{\circ}-14^{\circ}, = 0^{\circ}-10^{\circ}, \Delta^{+} 10^{\circ}-14^{\circ}, \Delta^{+} 10^{\circ}-14^{\circ}$
23	7	000	07	08	05.0	12.1	00.0	.	.	$\Delta^{+} 0-5^{\circ} N, = 0^{\circ}-10^{\circ}, \Delta^{+} 10^{\circ}-14^{\circ}$
24	8	030	040	00	02.3	10.2	.	.	.	$\Delta^{+} 0-5^{\circ} N, = 0^{\circ}-10^{\circ}, \Delta^{+} 10^{\circ}-14^{\circ}$
25	8	000	050	00	01.7	11.3	.	.	.	$\Delta^{+} 0-5^{\circ} N, = 0^{\circ}-10^{\circ}$
26	8	000	040	00	01.3	12.5	.	.	.	$\Delta^{+} 0-5^{\circ} N, = 0^{\circ}-10^{\circ}$
27	7	000	030	00	01.0	12.2	.	.	.	$\Delta^{+} 0-5^{\circ} N, = 0^{\circ}-10^{\circ}$
28	7	040	000	10	04.7	07.2	.	.	.	$\Delta^{+} 0-5^{\circ} N, = 0^{\circ}-10^{\circ}, \Delta^{+} 10^{\circ}-14^{\circ}$
29	8	000	05	03	02.7	10.3	.	.	.	$\Delta^{+} 0-5^{\circ} N, = 0^{\circ}-10^{\circ}, \Delta^{+} 10^{\circ}-14^{\circ}$
30	8	010	050	02	02.7	06.4	.	.	.	$\Delta^{+} 0-5^{\circ} N, = 0^{\circ}-10^{\circ}, \Delta^{+} 10^{\circ}-14^{\circ}$
31	8	000	040	00	01.3	12.6	.	.	.	$\Delta^{+} 0-5^{\circ} N, = 0^{\circ}-10^{\circ}$
MES. VRED.		03.1	03.6	03.3	03.3	323.7	53.4			

REF ID: A9

1978 AUGUST

1	8	040	020	00	02.0	11.8	.	.	$\Delta^{\text{E}} 0-7^{\circ}$, $\Delta^{\text{E}} -2^{\circ}$
2	8	000	000	00	00.0	12.8	.	.	$\Delta^{\text{E}} 0-7^{\circ}$, $\Delta^{\text{E}} 0-4^{\circ}$
3	8	000	000	00	00.0	10.7	.	.	$\Delta^{\text{E}} 0-7^{\circ}$
4	7	010	10	10	07.0	05.8	.	.	$\Delta^{\text{E}} 0-7^{\circ}$, $\Delta^{\text{E}} 0-4^{\circ}$; $\Delta^{\text{E}} 15^{\circ}$, $\Delta^{\text{E}} 10^{\circ}$, $\Delta^{\text{E}} 10^{\circ}$, $\Delta^{\text{E}} 10^{\circ}$
5	8	38	040	00	04.0	06.1	00.5	.	$\Delta^{\text{E}} 0-7^{\circ}$, $\Delta^{\text{E}} 17^{\circ}$, $\Delta^{\text{E}} 0-12^{\circ}$
6	8	000	040	00	01.3	10.9	00.0	.	$\Delta^{\text{E}} 0-7^{\circ}$, $\Delta^{\text{E}} 10^{\circ}$
7	8	200	030	00	01.0	12.6	.	.	$\Delta^{\text{E}} 0-7^{\circ}$
8	8	10	040	02	05.3	07.4	00.0	.	$\Delta^{\text{E}} 0-7^{\circ}$, $\Delta^{\text{E}} 0-4^{\circ}$
9	8	100	040	00	04.7	09.5	00.5	.	$\Delta^{\text{E}} 0-7^{\circ}$, $\Delta^{\text{E}} 0-4^{\circ}$
10	8	260	08	10	08.0	07.4	00.1	.	$\Delta^{\text{E}} 0-7^{\circ}$, $\Delta^{\text{E}} 0-4^{\circ}$
11	8	09	090	06	08.0	08.6	02.5	.	$\Delta^{\text{E}} 0-7^{\circ}$, $\Delta^{\text{E}} 0-4^{\circ}$, $\Delta^{\text{E}} 0-4^{\circ}$, $\Delta^{\text{E}} 0-4^{\circ}$, $\Delta^{\text{E}} 0-4^{\circ}$
12	7	04	06	00	03.3	09.2	00.8	.	$\Delta^{\text{E}} 0-7^{\circ}$, $\Delta^{\text{E}} 0-4^{\circ}$, $\Delta^{\text{E}} 0-4^{\circ}$, $\Delta^{\text{E}} 0-4^{\circ}$, $\Delta^{\text{E}} 0-4^{\circ}$
13	7	000	07	03	03.3	10.4	00.9	.	$\Delta^{\text{E}} 0-7^{\circ}$, $\Delta^{\text{E}} 0-4^{\circ}$, $\Delta^{\text{E}} 0-4^{\circ}$
14	8	030	000	00	01.0	10.7	.	.	$\Delta^{\text{E}} 0-7^{\circ}$, $\Delta^{\text{E}} 0-4^{\circ}$
15	7	040	000	00	01.3	10.9	.	.	$\Delta^{\text{E}} 0-7^{\circ}$, $\Delta^{\text{E}} 0-4^{\circ}$
16	8	200	000	00	10.9	12.1	.	.	$\Delta^{\text{E}} 0-7^{\circ}$
17	8	000	200	00	00.0	11.7	.	.	$\Delta^{\text{E}} 0-7^{\circ}$
18	7	020	040	20	05.3	08.0	.	.	$\Delta^{\text{E}} 0-7^{\circ}$
19	7	000	010	00	00.3	12.3	.	.	$\Delta^{\text{E}} 0-7^{\circ}$
20	7	04	10	10	08.0	05.4	.	.	$\Delta^{\text{E}} 0-7^{\circ}$, $\Delta^{\text{E}} 0-4^{\circ}$
21	7	10	060	00	05.3	08.4	<u>02.6</u>	.	$\Delta^{\text{E}} 0-7^{\circ}$, $\Delta^{\text{E}} 0-4^{\circ}$
22	7	000	220	00	00.7	11.7	.	.	$\Delta^{\text{E}} 0-7^{\circ}$, $\Delta^{\text{E}} 0-4^{\circ}$
23	7	000	020	00	00.7	11.8	.	.	$\Delta^{\text{E}} 0-7^{\circ}$, $\Delta^{\text{E}} 0-4^{\circ}$
24	7	020	040	02	02.7	08.4	.	.	$\Delta^{\text{E}} 0-7^{\circ}$
25	6	39	070	03	03.0	03.9	.	.	$\Delta^{\text{E}} 0-7^{\circ}$, $\Delta^{\text{E}} 0-4^{\circ}$
26	6	02	040	100	05.3	08.9	.	.	$\Delta^{\text{E}} 0-7^{\circ}$, $\Delta^{\text{E}} 0-4^{\circ}$, $\Delta^{\text{E}} 0-4^{\circ}$, $\Delta^{\text{E}} 0-4^{\circ}$, $\Delta^{\text{E}} 0-4^{\circ}$
27	7	250	070	10	05.7	10.5	00.4	.	$\Delta^{\text{E}} 0-7^{\circ}$, $\Delta^{\text{E}} 0-4^{\circ}$
28	7	38	10	100	09.3	00.3	01.5	.	$\Delta^{\text{E}} 0-7^{\circ}$, $\Delta^{\text{E}} 0-4^{\circ}$, $\Delta^{\text{E}} 0-4^{\circ}$
29	7	340	000	06	03.3	10.7	02.0	.	$\Delta^{\text{E}} 0-7^{\circ}$
30	7	020	380	00	03.3	06.3	.	.	$\Delta^{\text{E}} 0-7^{\circ}$, $\Delta^{\text{E}} 0-4^{\circ}$
31	6	170	100	100	10.0	00.0	01.5	.	$\Delta^{\text{E}} 0-7^{\circ}$, $\Delta^{\text{E}} 0-4^{\circ}$, $\Delta^{\text{E}} 0-4^{\circ}$, $\Delta^{\text{E}} 0-4^{\circ}$

$\varphi = 44^{\circ}48' N \lambda = 20^{\circ}28' E$ Gr. $\Delta G = + 1h 22 min.$

BR. ST. 169

d	Vazdušni pritisk P mm			Temperatura vazduha T °C								Napon vodenog pore e mm			Relativna vlažnost u %			Pravac i jačina vetro D, f (0-12)					
	7	14	21	7	14	21	Sred Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dnes	7	14	21			
1	743.9	745.0	746.2	19.8	16.7	11.7	12.5	18.0	9.5	38.9	18.9	17.3	18.2	98	52	80	73	W	3	W	4	SE	2
2	747.2	747.6	748.0	12.0	19.2	12.8	14.2	20.0	10.4	36.7	18.7	18.6	18.9	82	52	81	72	W	2	SW	3	SE	2
3	749.1	749.0	749.1	11.0	20.4	13.4	14.6	21.7	8.8	35.4	18.9	19.2	19.6	91	51	83	75	WNW	3	WNW	2	E	1
4	748.4	747.6	747.2	14.5	24.6	16.4	18.0	24.7	11.6	37.5	18.9	19.9	11.2	72	43	83	65	ESE	2	SW	3	ESE	1
5	766.1	744.8	745.0	17.8	26.1	21.5	21.2	26.8	14.5	10.6	10.7	19.4	12.6	76	41	73	60	SSE	2	S	3	SSE	2
6	743.9	743.0	742.4	18.4	24.6	17.8	19.7	25.3	17.0	15.0	11.8	13.5	14.6	74	58	95	76	ESE	2	SSE	2	ESE	1
7	741.2	741.6	742.4	17.4	18.7	17.6	17.6	20.1	17.2	16.8	14.3	14.8	14.2	96	92	94	94	WSW	2	W	2	SW	3
8	744.4	745.8	747.1	15.2	21.1	17.4	17.8	21.6	14.6	13.9	11.4	10.2	10.8	88	49	59	65	WSW	2	NW	4	WNW	2
9	749.1	749.9	751.2	13.0	17.8	14.6	15.0	17.9	12.5	11.2	09.3	09.3	10.3	83	61	83	76	W	2	NW	3	WSW	2
10	751.6	751.5	750.5	12.3	19.7	16.7	16.4	19.7	10.6	07.3	10.0	11.9	11.5	93	69	81	81	WSW	2	NW	3	SW	1
11	749.7	748.7	746.3	18.0	27.4	20.4	21.6	28.1	15.9	13.9	10.8	11.4	12.6	70	42	73	61	WSW	2	NE	1	SE	2
12	745.2	746.7	747.2	18.8	14.2	11.6	14.1	21.0	11.6	12.0	11.7	10.1	10.9	72	84	97	84	SSW	1	NW	3	WNW	3
13	749.3	751.5	754.1	11.3	18.4	13.8	14.3	19.1	11.3	10.4	08.7	06.7	08.1	86	42	67	65	NW	3	N	3	N	2
14	755.9	754.7	753.6	09.1	19.9	14.0	14.3	20.6	9.0	7.5	17.8	19.8	19.6	90	56	83	75	WSW	2	ESE	2	ESE	3
15	751.8	752.4	752.8	12.3	19.4	14.2	15.0	23.3	10.4	07.4	18.9	19.9	16.6	82	59	88	76	ESE	3	NW	1	WSW	1
16	753.4	753.7	754.6	12.7	20.8	14.6	15.7	22.3	10.6	07.0	09.7	08.8	08.4	88	48	67	68	WSW	2	NW	3	WSW	1
17	757.1	756.0	755.0	10.8	26.2	13.0	14.3	24.1	9.2	5.6	17.4	16.9	16.1	76	39	81	65	SSW	1	NNW	2	SE	2
18	753.3	752.8	752.7	11.8	25.3	18.6	18.6	25.6	10.3	9.6	08.8	10.0	11.2	84	41	63	63	ESE	1	WNW	1	E	2
19	751.9	751.2	750.6	13.8	20.7	12.9	14.9	21.5	12.6	9.3	9.6	9.7	10.3	81	42	92	72	E	1	NNE	2	E	1
20	752.3	753.8	755.4	12.1	12.6	10.2	11.3	13.4	10.2	11.4	09.9	10.2	10.7	93	66	72	77	WNW	2	NW	3	NNW	2
21	756.8	756.8	757.1	14.8	15.0	19.5	19.7	15.4	06.4	01.7	06.0	05.1	06.5	93	39	73	68	SW	2	WNW	3	WSW	1
22	756.3	754.5	753.4	10.8	16.2	11.6	12.3	17.0	10.8	34.1	17.0	17.8	18.6	77	57	84	73	WSW	3	NNW	2	SSW	2
23	753.4	749.3	751.2	12.0	18.5	14.8	15.0	29.2	11.2	18.9	09.0	10.7	11.6	66	61	84	77	SE	2	W	2	W	2
24	753.4	754.3	755.3	13.6	19.8	16.0	16.4	20.2	13.4	11.3	10.2	10.0	10.5	87	58	77	74	WSW	2	NNW	2	SSE	2
25	755.3	755.3	755.3	14.6	26.3	17.0	18.7	26.7	13.0	09.2	09.9	10.0	10.7	80	39	74	64	SE	1	SSW	2	ESE	2
26	754.5	753.5	751.8	12.9	27.6	18.4	19.3	27.6	12.0	07.7	10.3	12.8	10.7	92	46	67	68	-	0	E	1	ESE	2
27	749.4	748.3	748.7	14.8	19.1	14.5	15.7	21.4	13.8	09.7	11.1	14.3	08.3	88	86	67	80	WSW	1	WSW	2	NNW	2
28	755.0	744.6	745.1	11.6	11.1	10.2	10.8	14.5	11.2	10.6	19.7	19.5	09.0	94	94	96	95	W	3	NNW	3	SE	2
29	746.4	747.9	749.5	08.4	14.9	09.4	10.5	16.3	08.3	18.2	07.6	06.0	07.6	92	47	85	75	WNW	2	NNW	3	WNW	2
30	757.0	748.9	747.5	11.8	23.5	15.7	16.7	23.7	20.6	05.2	16.7	18.1	09.4	64	28	70	57	SE	2	WSW	3	SSE	3
MES. RED.	757.0	750.0	750.2	12.9	26.0	14.6	15.5	21.0	11.3	09.0	09.4	09.5	09.9	84	55	79	72	1.9	2.4	1.8			

1978. OKTOBAR

BEOGRAD

1	746.4	746.2	746.9	16.1	21.7	16.3	17.4	21.1	14.5	39.8	10.1	11.0	11.0	73	59	79	70	S	3	SE	3	ESE	3
2	749.6	750.4	751.5	12.0	21.0	18.2	17.6	22.5	12.4	09.6	10.6	12.1	14.2	95	65	91	84	WSW	1	ESE	2	ESE	2
3	751.2	750.3	749.3	17.6	24.7	21.5	21.3	25.1	16.8	14.5	11.4	11.5	11.9	74	49	62	62	ESE	3	ESE	4		
4	747.9	746.8	748.6	17.9	26.1	18.2	20.1	26.8	17.4	13.9	11.7	10.4	08.6	76	41	55	57	ESE	3	S	2	SW	3
5	751.3	753.5	755.5	11.9	21.1	11.2	11.4	18.2	10.1	07.6	19.5	18.4	07.6	91	85	76	84	N	3	W	2	NNW	2
6	756.8	756.4	756.5	06.6	15.4	11.4	11.2	15.5	06.0	02.2	06.8	06.5	07.6	93	50	75	73	SW	2	WSW	2	WSW	1
7	756.7	757.5	758.0	12.0	17.9	11.6	13.3	18.5	10.0	10.5	07.8	09.7	09.4	74	63	92	76	WSW	2	W	2	S	2
8	758.4	757.9	757.5	09.0	21.4	15.4	15.3	21.6	08.7	04.9	07.7	08.6	08.6	89	44	65	66	SE	2	ESE	2	ESE	3
9	757.7	757.2	757.3	12.6	21.8	13.8	15.5	21.9	12.4	09.2	09.2	09.3	08.6	84	47	72	68	ESE	3	ESE	2	ESE	2
10	757.6	757.1	757.9	11.3	21.4	13.0	14.6	21.6	10.1	04.3	07.9	08.5	09.9	81	45	88	71	ESE	2	ESE	2	ESE	2
11	759.2	759.6	760.0	08.2	19.4	12.3	13.1	19.7	07.9	03.7	07.8	09.5	10.0	96	56	93	82	WSW	1	NNW	2	SSE	2
12	761.3	759.7	759.8	09.8	20.0	13.2	14.1	20.0	09.1	04.6	08.9	09.6	10.5	98	55	92	82	S	1	NNW	2	SSE	1
13	759.9	759.5	759.4	10.8	19.5	11.9	13.5	19.5	10.1	04.5	09.4	11.3	07.8	96	67	75	79	S	2	ESE	2	ESE	4
14	758.2	757.1	757.0	10.9	18.2	11.6	13.1	18.2	09.2	07.2	06.6	06.6	06.9	67	42	67	59	ESE	3	ESE	3	ESE	2
15	755.9	754.6	753.9	07.0	18.0	19.1	18.1	17.0	07.0	02.2	06.8	07.0	07.6	91	46	88	75	SE	2	E	2	WSW	2
16	752.8	751.4	751.1	16.5																			

BR. ST. 169

$$H_s = 132 \text{ m } H_b = 132.0 \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$$

DNE	VRED.	Oblačnost N (0-10)					Srednja temperatura v °C	Podzemna voda R mm	Sněžní pokrývka h cm	Razvoj vremena w	
		14	7	14	21	Sred. Dne				7	7
1	7	07	060	04	05.7	07.8	33.9	.	.	=0-6°, 0-2°, 0-2°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
2	8	10	040	00	04.7	07.0	.	.	.	Δ-10°, 0-1°	
3	8	110	04	00	01.7	11.6	.	.	.	0-1°, 0-2°, 0-2°, 0-1°	
4	8	110	050	00	02.0	11.4	.	.	.	0-1°, 0-2°, 0-2°, 0-1°	
5	8	06	09	10	08.3	06.3	.	.	.	0-1°, 0-2°, 0-2°, 0-1°	
6	8	05	09	100	08.0	02.6	00.0	.	.	0-1°, 0-2°, 0-2°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
7	6	100	100	10	10.0	00.2	05.5	.	.	0-1°, 0-2°, 0-2°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
8	6	09	060	05	06.7	07.2	06.1	.	.	0-1°, 0-2°, 0-2°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
9	7	10	10	08	09.3	00.4	.	.	.	0-1°, 0-2°, 0-2°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
10	7	050	10	03	06.0	01.6	00.0	.	.	0-1°, 0-2°, 0-2°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
11	8	10	000	00	03.3	06.5	00.0	.	.	Δ-10°, 0-1°, 0-1°, 0-1°	
12	7	09	100	100	09.7	02.0	.	.	.	Δ-10°, 0-1°, 0-1°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
13	8	06	060	00	04.0	08.5	19.2	.	.	0-1°, 0-2°, 0-2°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
14	7	06	060	00	04.7	08.8	.	.	.	0-1°, 0-2°, 0-2°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
15	8	040	07	04	05.0	05.2	.	.	.	0-1°, 0-2°, 0-2°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
16	7	08	07	03	06.9	06.8	.	.	.	Δ-10°, 0-1°, 0-1°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
17	8	060	010	00	02.3	10.5	.	.	.	0-1°, 0-2°, 0-2°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
18	7	000	000	08	02.7	10.6	.	.	.	0-1°, 0-2°, 0-2°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
19	7	260	10	100	08.7	02.3	.	.	.	0-1°, 0-2°, 0-2°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
20	7	100	10	06	08.7	00.0	11.0	.	.	0-1°, 0-2°, 0-2°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
21	8	000	030	00	01.0	08.9	01.0	.	.	Δ-10°, 0-1°, 0-1°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
22	7	100	10	08	09.3	02.5	07.2	.	.	0-1°, 0-2°, 0-2°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
23	8	100	100	09	09.7	01.3	00.0	.	.	0-1°, 0-2°, 0-2°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
24	7	05	08	10	07.7	05.5	00.0	.	.	0-1°, 0-2°, 0-2°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
25	8	000	100	00	00.0	10.2	.	.	.	0-1°, 0-2°, 0-2°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
26	8	000	000	00	00.0	10.6	.	.	.	Δ-10°, 0-1°, 0-1°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
27	7	040	100	10	08.0	02.3	.	.	.	0-1°, 0-2°, 0-2°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
28	6	100	100	100	10.0	00.0	03.7	.	.	0-1°, 0-2°, 0-2°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
29	7	100	030	00	04.3	06.6	29.0	.	.	0-1°, 0-2°, 0-2°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
30	8	000	040	02	02.0	08.5	.	.	.	0-1°, 0-2°, 0-2°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
MES. VRED.			06.0	06.3	04.7	05.7	173.7	109.6			

BEOGRAD

1978. OKTOBAR

1	8	10	040	00	04.7	03.8	03.0	.	.	Δ-10°, 0-1°, 0-1°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
2	7	05	080	100	07.7	01.2	00.6	.	.	0-1°, 0-2°, 0-2°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
3	7	08	08	03	06.3	01.6	00.6	.	.	0-1°, 0-2°, 0-2°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
4	7	09	08	00	05.7	07.4	00.0	.	.	0-1°, 0-2°, 0-2°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
5	7	09	10	10	09.7	00.0	02.7	.	.	0-1°, 0-2°, 0-2°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
6	7	000	06	00	02.0	06.9	00.9	.	.	=0-1°, Δ-10°, 0-1°	
7	7	10	060	00	05.3	03.6	.	.	.	0-1°, 0-2°, 0-2°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
8	7	000	000	00	00.0	09.0	.	.	.	0-1°, 0-2°, 0-2°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
9	8	000	010	00	00.3	09.9	.	.	.	0-1°, 0-2°, 0-2°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
10	8	00	060	00	00.0	09.9	.	.	.	0-1°, 0-2°, 0-2°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
11	7	1000	020	02	04.7	08.3	.	.	.	Δ-10°, 0-1°, 0-1°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
12	6	01	000	00	00.3	08.0	.	.	.	0-1°, 0-2°, 0-2°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
13	5	1000	010	00	03.7	04.3	.	.	.	0-1°, 0-2°, 0-2°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
14	7	00	010	00	00.0	08.9	.	.	.	0-1°, 0-2°, 0-2°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
15	8	000	000	00	00.0	09.3	.	.	.	0-1°, 0-2°, 0-2°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
16	6	1000	06	00	05.3	03.1	.	.	.	0-1°, 0-2°, 0-2°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
17	5	00	030	00	00.0	06.4	.	.	.	0-1°, 0-2°, 0-2°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
18	7	04	020	00	02.0	08.5	.	.	.	0-1°, 0-2°, 0-2°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
19	6	09	050	00	07.3	04.4	.	.	.	0-1°, 0-2°, 0-2°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
20	7	100	10	10	10.0	00.1	00.0	.	.	0-1°, 0-2°, 0-2°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
21	6	100	100	04	08.3	00.0	05.0	.	.	0-1°, 0-2°, 0-2°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
22	8	000	07	00	02.3	07.6	27.6	.	.	0-1°, 0-2°, 0-2°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
23	8	10	09	06	08.3	03.5	.	.	.	0-1°, 0-2°, 0-2°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
24	7	000	040	00	01.1	08.1	.	.	.	0-1°, 0-2°, 0-2°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
25	6	06	010	00	02.3	08.4	.	.	.	0-1°, 0-2°, 0-2°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
26	6	100	10	05	08.3	00.0	00.2	.	.	0-1°, 0-2°, 0-2°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
27	7	06	030	00	03.0	07.1	01.5	.	.	0-1°, 0-2°, 0-2°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
28	8	04	030	00	03.7	18.3	.	.	.	0-1°, 0-2°, 0-2°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
29	7	02	060	10	06.0	16.8	.	.	.	0-1°, 0-2°, 0-2°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
30	6	10	10	10	10.0	00.0	00.0	.	.	0-1°, 0-2°, 0-2°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
31	7	10	10	10	10.0	00.0	00.1	.	.	0-1°, 0-2°, 0-2°, 0-1°, 0-1°, 0-1°, 0-1°; Δ-10°, 0-1°	
MES. VRED.			05.7	14.0	03.1	24.6	164.2	18.1			

$\phi = 44^{\circ}48' N \lambda = 20^{\circ}28' E$ Gr. $\Delta G = +1h\ 22\ min.$

BR. ST. 169

d	Vazdušni pritisak P mm			Temperatura vazduha T °C							Napon vodenih parova e mm			Relativna vlažnost v%			Pravac i jačina vetrova D, f (0—12)			
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21
1	761.6	762.3	763.3	-9.3	13.4	18.6	10.9	13.1	9.0	17.6	37.3	66.9	37.9	83	62	83	76	SSE 1	N 2	ESE 1
2	763.1	762.7	762.3	08.7	09.4	07.0	08.0	11.5	07.0	02.8	07.3	07.1	06.2	86	81	83	83	NNE 1	ESE 2	ESE 3
3	761.6	760.9	761.2	-5.8	13.4	06.9	08.2	13.5	05.6	32.9	35.6	15.9	05.8	81	52	78	70	ESE 2	ESE 2	ESE 2
4	761.4	761.2	761.8	(2.1)	11.1	05.0	05.8	11.2	02.1	-02.1	05.0	05.4	05.8	93	54	88	78	ESE 2	NNE 2	ESE 2
5	762.4	763.1	763.7	14.6	16.7	15.3	05.3	06.2	03.2	-03.5	05.8	05.6	05.5	91	79	83	84	NNW 1	N 2	NNE 2
6	764.4	764.1	764.0	04.8	05.7	03.8	04.5	06.2	03.8	04.4	05.2	05.3	05.0	81	76	83	80	NNE 2	NNE 2	NNE 2
7	764.1	764.1	764.7	03.0	13.2	13.2	03.2	13.8	02.8	02.7	05.0	14.7	04.6	87	81	84	83	NW 2	NNE 2	N 2
8	764.9	764.7	764.5	03.0	14.1	14.1	03.8	14.7	02.8	02.7	05.1	15.0	04.9	89	82	79	83	NNW 1	W 2	ESE 2
9	764.2	763.9	763.8	13.5	14.3	04.1	04.0	04.6	03.4	03.2	05.0	04.8	05.0	85	76	82	81	W 2	NNE 2	NNE 1
10	763.5	762.5	762.4	(2.6)	13.0	02.6	02.7	04.0	02.5	02.4	04.8	14.7	04.6	87	83	82	84	NNE 1	E 1	
11	762.1	761.4	762.0	01.4	02.1	01.8	01.8	02.6	01.4	01.2	04.4	14.5	04.3	87	84	82	84	SSE 2	NNE 2	W 2
12	762.0	761.6	761.6	00.5	00.8	00.6	00.6	01.8	00.5	00.2	04.2	04.3	04.2	88	88	88	88	NE 2	ENE 2	ESE 2
13	762.0	762.3	763.4	00.6	02.4	01.8	01.7	02.4	00.3	00.1	04.1	04.2	04.2	86	78	80	81	ESE 2	SSE 1	NW 2
14	765.5	766.9	768.4	00.6	00.4	-00.3	00.1	01.8	-00.3	00.2	04.0	03.9	03.8	83	82	84	83	NNW 2	NW 2	
15	767.5	766.3	764.6	-00.8	00.3	-00.6	-00.5	00.2	-00.8	-00.9	03.7	03.8	04.0	85	84	91	87	SSE 2	ESE 2	SE 2
16	762.1	760.9	760.5	-01.7	05.0	-10.8	-00.8	00.6	-01.8	-01.7	03.9	04.1	03.9	96	89	91	92	ESE 1	WSW 2	NNW 2
17	763.1	763.9	765.0	-01.8	05.6	10.1	-00.6	03.4	-02.5	-02.5	03.7	14.2	04.3	92	96	93	94	NNW 3	NW 2	NNW 2
18	764.7	764.5	764.5	00.1	02.6	-00.3	00.0	01.2	-00.3	-00.4	04.3	14.4	14.2	93	91	94	93	ESE 1	NNE 2	ESE 1
19	763.6	762.4	761.3	-00.5	00.5	00.0	00.0	01.2	-00.5	-00.5	04.3	04.3	04.4	96	89	96	94	ESE 2	E 2	ESE 2
21	758.5	758.2	759.4	-01.2	-00.7	-01.0	-00.9	00.0	-01.2	-01.2	04.0	04.2	04.1	96	93	96	95	SE 2	SSE 1	WSW 1
22	761.4	762.6	764.3	-01.3	-03.8	-31.1	-01.1	-00.6	-01.4	-01.5	03.9	04.0	04.0	94	92	94	93	WSW 2	W 2	W 1
22	765.9	767.2	767.7	01.0	01.6	01.8	01.1	02.0	-01.3	-01.5	03.9	04.3	04.7	92	83	90	88	SSW 1	WSW 1	SW 1
23	766.6	765.5	765.4	01.4	04.6	07.2	02.1	05.0	01.2	01.2	04.9	05.3	04.8	97	84	97	93	SSW 2	NNW 2	NNW 1
24	764.5	762.6	760.2	-01.6	03.9	02.2	01.9	05.4	-00.6	-00.6	04.3	05.1	05.2	98	85	97	93	SSW 1	SW 1	ESE 3
25	757.3	754.1	753.2	-02.1	01.4	00.1	02.2	-02.0	-04.4	-04.4	03.9	14.9	04.7	98	97	100	98	SSW 2	NNW 1	WSW 1
25	751.5	748.9	747.8	-00.7	12.2	07.3	06.5	12.5	-01.0	-01.3	04.4	05.8	05.0	100	55	65	73	WSW 2	E 2	ESE 2
27	744.5	740.5	738.3	07.1	10.4	05.6	07.2	11.2	04.6	00.8	05.0	05.8	05.8	66	61	85	71	ESE 3	E 3	W 2
28	738.7	738.1	738.7	01.6	03.6	00.6	00.9	05.6	00.6	01.5	04.8	14.6	14.5	93	96	95	95	W 2	W 2	WSW 2
29	739.3	739.2	738.1	01.0	04.6	00.7	03.8	01.1	00.3	-00.2	04.2	04.5	04.7	85	95	96	92	N 1	NNW 2	NNW 2
31	738.8	740.6	744.1	01.9	12.6	02.8	02.5	02.8	00.7	30.1	04.6	14.6	04.4	88	84	78	83	NNW 3	W 3	W 3
MES. RED.	759.7	759.2	759.3	01.7	13.9	02.5	02.7	04.6	01.3	30.5	04.7	14.9	04.8	89	81	87	86	1.8	1.9	1.8

1978 DECEMBAR

BEOGRAD

1	748.0	749.5	750.1	01.3	04.3	03.0	02.9	04.4	01.3	09.5	03.8	13.8	03.8	75	61	68	68	WSW 3	NNW 2	W 2
2	751.0	752.2	753.5	-00.1	00.6	00.5	00.4	03.0	-00.4	-00.2	04.5	04.6	04.7	98	96	98	97	WSW 2	WSW 3	WSW 2
3	753.8	752.5	751.1	01.2	03.0	01.5	01.8	03.0	00.5	-03.3	04.8	14.9	04.8	97	86	95	93	WSW 2	WSW 2	ESE 2
4	748.8	749.3	750.7	-02.1	-00.8	00.0	-00.7	01.6	-03.3	-03.6	03.8	04.2	04.3	96	98	93	96	WSW 2	W 2	N 2
5	753.1	755.6	757.5	-06.1	-04.8	-03.6	-04.5	00.2	-02.7	-07.3	02.1	02.2	02.8	74	70	80	75	N 2	WSW 2	WSW 2
6	750.7	750.9	750.9	-07.9	-04.8	-06.4	-06.4	-03.6	-08.0	-09.4	02.3	12.5	02.6	90	78	92	87	NH 1	NNW 2	ESE 2
7	750.2	750.3	750.1	-07.0	-03.0	-03.7	-04.4	-01.6	-03.4	-10.6	02.5	02.4	02.4	93	66	68	76	E 2	E 3	ESE 3
8	756.0	755.6	755.5	-05.0	-01.2	-04.4	-03.8	-00.8	-05.2	-06.7	02.5	32.7	32.8	80	65	85	77	ESE 3	SE 2	E 2
9	751.3	750.1	751.8	-02.2	00.2	01.0	00.0	01.2	-04.4	-05.5	03.2	04.6	04.8	83	98	98	93	ESE 4	ESE 3	W 2
10	752.7	752.9	753.5	02.2	04.4	05.1	04.2	05.2	01.0	00.6	05.3	05.9	05.3	98	94	83	91	WSW 1	WSW 2	WSW 2
11	752.9	751.4	750.1	02.8	11.6	06.4	06.8	12.2	01.8	-02.6	05.1	16.0	05.7	96	59	89	76	ESE 2	ESE 2	ESE 3
12	746.4	744.1	742.8	05.6	10.0	07.2	07.5	10.7	05.2	03.5	04.9	05.4	05.3	72	59	69	67	ESE 4	ESE 4	ESE 3
13	739.0	739.4	739.2	10.5	19.2	08.0	08.9	11.7	06.8	04.6	06.5	08.3	07.5	68	95	94	86	ESE 2	SW 2	ESE 2
14	734.0	732.3	735.6	09.9	18.5	06.2	07.7	10.8	06.2	03.7	07.7	17.5	06.3	84	90	88	88	S 3	WSW 3	WSM 3
15	737.2	740.0	742.3	02.6	19.7	16.0	06.1	19.6	02.6	-01.8	05.3	16.2	05.6	97	68	79	81	ESE 2	WSW 2	ESE 2
16	743.8	742.6	739.3	07.4	14.2	10.8	14.9	02.3	00.3	34.0	15.5	05.8	52	45	60	52	ESE 2	SSE 3	SE 3	
17	742.6	745.4	748.8	08.9	10.0	07.4	08.4	12.3	07.4	07.0	07.4	26.0	06.4	86	65	83	78	SW 2	NNW 2	NNE 2
18	750.5	753.0	754.6	03.4	11.8	-01.8	00.4	07.4	-02.0	02.0	05.7	04.9	03.7	97	93	93	94	NNE 1	N 3	N 2
19	756.9	753.1	748.5	-03.3	-06.7	-01.5	-01.8</td													

RR, ST, 169

$$H_s = 132 \text{ m} \quad H_b = 132.0 \text{ m} \quad h_t = 2.0 \text{ m} \quad h_r = 1.2 \text{ m}$$

Den	Ves - čas - 0- 6	Oblačnosť N (0-10)					Inšpiračná dĺžka sek.	Podavine R mm	Snežný pokrivač h cm	Rozvoj vremene w
		14	7	14	21	Sred Dies				
1	6	10	10	10	10	10.0	00.0	.	.	= 0°-15°, = 15°-24°
2	6	10	9	9	7	27.7	30.1	.	.	= 0°-15°, = 15°-24°; = 5°-17°, = 15°-24°, 9°-15°-15°, 0°-25°-23°
3	7	08	060	06	06	06.7	03.8	00.0	.	= 15°-24°
4	7	05	020	00	00	02.3	07.0	.	.	= 0°-25°, = 15°-24°, = 5°-15°, = 5°-11°
5	6	10	10	10	10	10.0	01.0	.	.	= 0°-15°, = 15°-24°
6	7	10	10	10	10	10.0	00.0	.	.	= 15°-24°
7	6	10*	10	10	10	10.0	00.0	00.0	.	= 0°-15°, = 15°-24°, 9°-15°-15°, 0°-25°-24°
8	6	10	10	10	10	10.0	00.0	00.1	.	= 0°-15°, = 15°-24°, 9°-15°-15°, 0°-25°-24°
9	6	10	10	10	10	10.0	00.0	00.0	.	= 0°-15°, = 15°-24°
10	7	10	10	10	10	10.0	00.0	.	.	= 0°-15°, = 15°-24°
11	7	10	10	10	10	10.0	00.0	.	.	= 0°-15°
12	7	10	10	10	10	10.0	00.0	.	.	= 0°-15°, = 15°-24°
13	6	10	00	10	06	06.7	00.0	.	.	= 0°-15°, = 15°-24°
14	6	10	10	10	10	10.0	00.0	.	.	= 0°-15°, = 15°-24°
15	7	10	10	10	10	10.0	00.0	00.0	.	= 0°-15°, = 15°-24°
16	5	10	10	10	10	10.0	00.0	.	.	= 0°-15°, = 15°-24°, 9°-15°-15°, = 15°-24°
17	4	10	10	10	10	10.0	00.0	.	.	= 0°-15°, = 15°-24°, 9°-15°-15°
18	5	10	100	10	10	10.0	00.0	00.3	.	= 0°-15°, = 15°-24°, 9°-15°-15°, = 15°-24°
19	6	10*	10	10	10	10.0	00.0	00.0	.	= 0°-15°, = 15°-24°, 9°-15°-15°, = 15°-24°
20	6	10	10	10	10	10.0	00.0	00.0	.	= 0°-15°, = 15°-24°, 9°-15°-15°
21	6	10	10	10	10	10.0	00.0	00.0	.	= 0°-15°, = 15°-24°, 9°-15°-15°, = 15°-24°, 10°-22°
22	7	10	10	10	10	10.0	00.0	00.1	.	= 0°-15°, = 15°-24°, 9°-15°-15°
23	6	10	10	00	00	06.7	00.0	.	.	= 0°-15°, = 15°-24°, 9°-15°-15°, = 15°-24°
24	6	10	000	00	03	03.3	04.1	00.0	.	= 0°-15°, = 15°-24°, 9°-15°-15°, = 15°-24°
25	3	10	10	10	10	10.0	00.0	.	.	= 0°-15°, = 15°-24°, 9°-15°-15°, = 15°-24°, 10°-22°
26	5	10	020	00	04	04.3	05.9	00.2	.	= 0°-15°, = 15°-24°, 9°-15°-15°
27	8	10	10	10	10	10.0	00.0	00.0	.	= 0°-15°, = 15°-24°, 9°-15°-15°, = 15°-24°, = 15°-24°
28	5	10	10*	10	10	10.0	00.0	00.8	.	= 0°-15°, = 15°-24°, 9°-15°-15°, = 15°-24°, = 15°-24°
29	5	10	10*	10*	10	10.0	00.0	04.8	.	= 0°-15°, = 15°-24°, 9°-15°-15°, = 15°-24°, = 15°-24°
30	6	10	10	10	10	10.0	00.0	08.7	05	= 0°-15°, = 15°-24°, = 15°-24°
MES. WRED.		09.8	08.6	08.3	08.9	20.9	15.0			

BEOGRAD

1978 DECEMBER

1	8	10	10	10	10.0	00.5	.	.	
2	5	10*	10*	10	10.0	00.0	02.6	01	$\boxed{F_0-0-10^6, X^2-23^6-24}$
3	5	10	10	03	07.7	00.3	03.9	02	$\boxed{X^2-0-10^6, 0-23^6-24}$
4	2	10**	10**	10	10.0	00.1	.	.	$\boxed{0-7-20, 0-23^6-24}$
5	7	05	08	10	07.7	00.0	.	.	$\boxed{0-0-20, 0-23^6-24}$
6	7	10	03	09	01.0	04.5	.	.	$\boxed{0-4-20, H^6}$
7	6	09	10	10	06.7	03.4	.	.	$\boxed{F^2-0-10^6, 0-23^6-24}$
8	7	10*	06○	09	05.3	00.6	07.0	.	$\boxed{0-2-20, X^2-23^6-24}$
9	7	10	10*	10	10.0	00.0	00.0	.	$\boxed{0-0-20, 0-23^6-24}$
10	6	10*	10*	10	10.0	00.0	07.7	.	$\boxed{0-0-20, 0-23^6-24}$
11	7	09	09	08	08.7	02.9	03.3	.	$\boxed{0-2-20, 0-23^6-24}$
12	8	06	03	06	05.0	05.2	.	.	$\boxed{0-5-20, 0-23^6-24}$
13	7	10	10*	08	09.3	00.0	00.3	.	$\boxed{0-3-4-20, 0-23^6-24}$
14	6	10*	10*	06	08.7	00.4	07.0	.	$\boxed{0-2-10^6, F^2-12^6-12^6}$
15	7	07	06○	02	04.3	04.7	06.5	.	$\boxed{0-3-8-20, 0-6-12-20, 0-8-9-20}$
16	8	10	08	10	08.7	13.5	00.3	.	$\boxed{0-2-20, F^2-12^6-12^6}$
17	8	10*	08*	09	09.0	03.0	05.8	.	$\boxed{0-2-20, X^2-23^6-24}$
18	5	10	10**	10*	10.1	00.0	00.4	.	$\boxed{X^2-0-10^6, 0-23^6-24}$
19	7	10	10	10	10.0	00.0	07.9	18	$\boxed{X^2-0-10^6, 0-23^6-24}$
20	7	02	10	03	14.0	17.7	01.0	14	$\boxed{0-0-8-20, 0-2-0-4-20, \boxed{0-3-9-10-20, F^2-12-20, 0-9-10-20}}$
21	7	02	06○	07	02.7	06.1	00.3	03	$\boxed{0-4-2-20, 0-5-6-20}$
22	7	18	03○	02	04.3	06.4	.	.	$\boxed{0-3-2-20, 0-2-0-2-20, F^2-7-20, 0-9-6-20}$
23	8	10	08○	06	08.0	03.6	.	.	$\boxed{0-5-2-20, F^2-0-22-22}$
24	7	05	01○	08	02.0	04.2	.	.	$\boxed{0-0-2-20, 0-2-0-2-20, F^2-0-22-22}$
25	6	19	10*	09	09.3	00.0	.	.	$\boxed{0-0-20, 0-4-8-20, \boxed{0-1-0-1-20, 0-0-4-20, 0-1-0-1-20}}$
26	6	10	09	00	06.3	00.1	00.2	.	$\boxed{0-1-0-2-20, F^2-10-20}$
27	7	15	08○	07	04.3	03.6	.	.	$\boxed{0-0-8-20, 0-5-6-20, \boxed{0-0-9-20, 0-0-4-20}}$
28	7	14	10	00*	08.0	00.8	.	.	$\boxed{0-1-0-2-20, 0-0-8-20}$
29	8	14	09	10	17.3	00.1	07.7	.	$\boxed{0-1-0-2-20, 0-0-8-20}$
30	9	10	10	05	18.3	00.8	00.9	.	$\boxed{0-0-8-20, 0-5-6-20, \boxed{0-0-9-20, 0-0-4-20}}$
31	7	02	10*	10*	07.3	02.3	02.0	.	$\boxed{0-0-2-20, F^2-0-22-22}$
MES.									
VREF.	77.3	08.2	06.7	07.2	79.7	57.2			

1978 JANUAR

TITOGRAD

 $\varphi = 42^{\circ}26' N \lambda = 19^{\circ}17' E$ Gr. $\Delta G = + 1h 17 min.$

BR. ST. 242

d	Vazdušní průtok P mm			Temperatura vzduchu T °C									Napět vodné páry e mm			Relativní vlhkost u%				Pravac i jačina větra D, I (0-12)				
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 8 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21	7	14	21	
1	755.0	758.0	763.0	03.2	07.7	04.8	05.1	08.2	-00.5	-02.6	02.9	02.9	03.0	50	37	47	45	N	3	N	4	N	4	
2	767.6	767.0	767.4	02.4	08.0	-00.8	02.2	08.8	-00.8	-01.2	02.6	03.6	03.7	47	44	85	59	N	4	SSE	2	-	0	
3	765.4	763.0	761.7	-02.6	05.4	00.0	00.7	05.8	-02.6	-05.0	03.3	03.9	04.4	88	59	96	81	-	0	-	0	-	0	
4	759.1	756.1	756.8	02.2	04.8	03.4	03.5	06.0	00.0	-05.0	04.0	05.2	05.3	74	80	91	82	-	0	-	0	W	2	
5	756.7	757.1	760.2	05.6	06.3	02.8	04.4	06.7	02.2	00.0	02.6	02.4	02.0	39	33	35	36	NNE	6	NNE	2	NNE	2	
6	762.3	764.2	764.3	00.8	04.0	02.0	02.2	04.4	00.8	-00.4	01.8	02.3	01.9	37	37	36	37	NNE	8	N	7	N	6	
7	765.8	762.8	765.5	03.6	06.0	02.4	03.6	07.0	00.0	-02.6	01.5	02.6	02.6	25	37	49	37	N	5	N	8	N	7	
8	765.1	764.4	765.4	01.4	07.0	01.2	02.7	07.0	00.6	-01.0	02.2	02.1	02.4	43	28	47	39	N	7	NNE	4	ESE	2	
9	765.7	765.0	765.2	-02.4	07.2	-00.2	00.6	07.2	-05.2	-08.0	02.7	02.6	03.8	83	34	84	67	WWW	1	S	2	-	0	
10	765.5	762.8	763.3	-03.0	07.6	-00.2	01.1	07.8	-04.0	-07.3	03.4	03.2	03.9	91	41	85	72	-	0	SSE	1	-	0	
11	762.2	760.0	758.6	01.4	01.4	01.4	01.4	02.0	-01.0	-07.2	04.5	04.9	04.9	88	97	97	94	-	0	NW	2	-	0	
12	756.5	757.2	759.1	03.0	06.0	05.0	04.8	06.8	01.6	00.2	05.7	06.8	06.4	100	97	97	98	-	0	-	0	-	0	
13	761.5	762.2	763.2	05.4	09.0	05.5	06.4	10.0	04.5	02.8	06.3	08.0	06.5	94	93	96	94	-	0	-	0	-	0	
14	763.1	762.0	761.5	01.4	14.0	05.3	06.5	14.4	01.3	-00.5	04.9	07.5	06.2	97	63	93	84	-	0	E	1	-	0	
15	760.1	759.1	758.3	04.5	12.8	07.6	08.1	13.2	02.2	-00.5	05.9	06.8	07.4	93	62	95	83	-	0	-	0	NW	1	
16	758.2	757.5	758.0	05.8	08.4	07.0	07.1	09.6	04.2	01.8	06.5	07.6	07.5	94	92	100	95	NE	2	-	0	-	0	
17	753.5	750.0	751.2	07.0	07.2	06.9	07.0	08.3	06.5	05.0	07.3	07.6	07.5	97	100	100	99	-	0	-	0	-	0	
18	753.5	754.5	754.3	07.0	11.7	05.8	07.6	12.5	05.2	05.4	07.4	07.9	06.6	99	77	96	91	-	0	-	0	-	0	
19	753.1	751.2	749.8	04.8	09.2	03.6	05.3	11.2	03.6	01.8	06.0	06.6	05.8	93	76	97	89	-	0	NW	1	NNE	1	
20	750.3	751.1	752.7	01.8	09.2	05.4	05.5	09.5	01.0	-00.8	05.0	04.6	06.3	97	53	94	81	NNE	1	-	0	-	0	
21	750.0	747.7	750.6	04.8	07.6	06.7	06.5	08.2	04.5	-01.0	04.3	07.0	06.9	97	90	93	93	-	0	-	0	-	0	
22	752.4	752.9	753.8	05.1	07.8	05.0	05.7	09.4	04.2	04.2	06.4	06.9	06.4	97	87	97	94	-	0	-	0	-	0	
23	755.2	754.8	756.0	04.7	11.0	03.8	05.8	11.4	03.2	01.7	05.9	07.0	05.8	93	71	97	87	NM	1	SSE	1	-	0	
24	756.9	756.0	755.0	-00.6	11.2	05.8	05.6	11.6	-00.6	-02.6	04.1	05.6	06.3	93	56	92	80	-	0	-	0	-	0	
25	750.6	747.3	750.0	06.2	06.6	07.8	07.1	09.4	05.1	-02.6	06.9	07.3	07.0	97	100	88	95	-	0	N	4	N	3	
26	755.3	756.2	756.6	07.0	12.0	06.8	08.2	12.5	05.3	02.1	04.0	05.9	06.4	54	56	87	66	N	2	SW	2	-	0	
27	758.8	759.3	761.3	02.2	10.4	06.4	06.4	12.0	01.8	00.2	05.3	06.8	06.6	98	72	92	87	-	0	SSE	2	NNW	1	
28	763.3	761.9	759.1	03.2	09.6	06.4	06.4	10.0	02.0	00.0	04.9	05.8	06.8	84	65	94	81	NWW	1	-	0	-	0	
29	753.4	746.0	742.0	11.4	12.4	08.8	10.4	13.2	06.5	01.5	05.7	07.3	08.1	57	68	95	73	SE	0	SSE	4	SE	6	
30	744.3	745.3	747.0	04.8	06.8	05.0	05.4	09.5	04.5	04.4	06.1	07.2	08.4	97	97	99	97	WWN	1	NW	2	NNW	3	
31	749.6	750.7	753.0	04.5	05.4	04.0	04.5	06.6	04.0	03.0	06.2	06.3	06.1	99	94	100	98	NNW	1	SSE	2	-	0	
MES.	VRF0	757.7	756.9	757.6	03.4	08.2	04.4	05.1	09.0	01.9	-00.4	04.8	05.6	05.5	80	68	86	78	1.6	1.9	1.5			

1978 FEBRUAR

TITOGRAD

1	753.8	753.0	753.5	03.5	10.0	03.4	05.1	10.6	03.2	02.4	05.8	05.4	05.1	98	59	88	82	-	0	-	0	-	0
2	752.6	748.8	747.3	02.2	07.1	04.8	04.7	07.6	00.8	-01.6	04.5	05.0	05.8	84	66	90	80	-	0	-	0	-	0
3	748.0	749.1	752.5	02.9	10.0	08.4	07.4	10.8	02.4	00.6	05.2	04.2	03.9	92	46	47	62	-	0	NNE	4	NNE	4
4	754.5	754.8	756.5	07.4	11.3	07.5	08.4	11.5	06.0	00.6	03.7	04.4	03.7	47	43	48	46	NNE	4	NNE	6	NNE	6
5	756.3	753.4	753.0	05.4	10.8	06.4	07.3	12.0	04.6	02.2	03.8	03.8	03.8	56	39	53	49	NH	3	N	8	N	3
6	750.0	748.6	749.3	05.8	08.0	06.4	06.2	09.2	03.2	01.0	03.7	04.9	04.5	61	60	63	61	-	0	SSE	2	ENE	2
7	749.3	747.7	747.5	03.8	09.2	06.2	06.4	09.5	03.5	01.0	04.7	03.9	03.4	79	44	47	57	NNW	2	N	6	N	4
8	746.3	746.5	747.4	03.8	10.2	05.4	06.2	10.6	03.0	-0.5	03.4	03.9	03.2	56	42	48	49	-	0	NNW	2	NNE	4
9	750.7	752.5	753.7	03.2	05.6	03.0	03.7	07.4	02.5	01.2	04.5	05.3	05.5	78	78	97	84	NNE	1	SSE	2	-	0
10	756.6	754.9	752.8	00.8	09.0	05.8	05.4	10.2	00.8	-00.8	04.9	05.7	06.3	100	66	92	86	-	0	-	0	-	0
11	749.3	746.5	746.6	05.8	14.4	14.2	12.2	15.8	05.3	-01.0	06.9	08.1	10.4	100	66	86	84	-	0	SSE	5	SE	4
12	749.8	751.2	751.2	13.0	14.2	09.6	11.6	15.0	09.4	06.1	08.5	08.2	08.7	76	68	98	81	E	4	WWN	2	-	0
13	747.9	746.9	744.8	09.6	10.2	09.6	09.8	11.0	09.0	04.0	08.7	09.3	08.9	98	100	99	99	WWN	3	-	0	-	0
14	738.5	742.9	747.4	09.4	08.8	07.0	08.1	10.8	07.0	04.6	08.8	08.2	07.1	100	96	95	97	-	0	S	4	N	2

BR. ST. 242

 $H_s = 49 \text{ m } H_b = 50.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$

Den	V. O. P.	Oblačnost N (0-10)					Incidenc s ke s	Padavina R mm	Snežni pokriven h cm	Krajev vremena w
		14	7	14	21	Sred Dnes				
1	8 02	030	00	01.7	08.0	00.3	.	—	—	—
2	8 00	000	00	00.0	08.8	.	.	—	—	—
3	8 04	10	00	04.7	02.6	.	.	—	—	—
4	8 10	10	10	10.0	00.0	.	.	—	—	—
5	8 02	06	00	02.7	07.0	02.2	.	—	—	—
6	8 02	000	00	00.7	08.7	.	.	—	—	—
7	8 02	000	00	00.7	08.6	.	.	—	—	—
8	8 00	000	00	00.0	08.8	.	.	—	—	—
9	8 02	000	00	00.7	08.3	.	.	—	—	—
10	8 04	000	00	01.3	07.0	.	.	—	—	—
11	7 08	10	100	09.3	00.0	.	.	—	—	—
12	7 100	100	100	10.0	00.0	04.5	.	—	—	—
13	8 1000	10	10	10.0	00.0	03.1	.	—	—	—
14	8 00	000	00	00.0	08.1	.	.	—	—	—
15	8 05	040	10	06.3	03.0	.	.	—	—	—
16	7 100	100	100	10.0	00.0	00.6	.	—	—	—
17	7 100	100	100	10.0	00.0	13.9	.	—	—	—
18	7 10	08	00	06.0	03.9	30.6	.	—	—	—
19	8 10	08	00	06.0	01.3	.	.	—	—	—
20	8 03	07	100	06.7	02.1	00.2	.	—	—	—
21	7 100	10	10	10.0	00.0	04.9	.	—	—	—
22	7 10	09	07	08.7	01.9	04.3	.	—	—	—
23	8 09	030	00	04.0	06.3	01.3	.	—	—	—
24	8 02	020	06	03.3	07.3	.	.	—	—	—
25	8 100	1000	10	10.0	00.0	05.3	.	—	—	—
MES.										
VRED.	06.0	05.9	05.3	05.7	119.0	186.6				

1	8 10	060	00	35.3	33.0	07.4	.	—	—	—
2	8 08	10	10	09.3	00.4	.	.	—	—	—
3	8 06	08	10	08.0	01.7	.	.	—	—	—
4	8 08	020	09	03.3	06.1	.	.	—	—	—
5	8 03	040	00	02.3	05.2	.	.	—	—	—
6	8 06	08	10	08.0	00.6	.	.	—	—	—
7	8 10	08	00	06.0	00.1	00.0	.	—	—	—
8	8 08	060	00	04.7	02.7	.	.	—	—	—
9	7 10	10	100	10.0	00.9	.	.	—	—	—
10	8 06	10	05	07.0	03.3	04.1	.	—	—	—
11	8 100	10	10	10.0	00.9	12.0	.	—	—	—
12	7 10	10	100	10.0	00.0	00.4	.	—	—	—
13	7 100	100	100	10.0	00.0	32.0	.	—	—	—
14	8 10	10	07	39.0	00.0	20.9	.	—	—	—
15	7 08	10	00	06.0	00.0	05.4	.	—	—	—
16	7 02	10	10	07.3	01.6	06.2	.	—	—	—
17	7 100	100	100	10.0	03.0	03.0	.	—	—	—
18	7 100	100	00	06.7	00.0	11.1	.	—	—	—
19	8 04	100	100	08.0	01.0	09.2	.	—	—	—
20	7 100	100	10	10.0	00.0	43.0	.	—	—	—
21	8 00	020	02	01.3	13.1	05.6	.	—	—	—
22	8 06	000	00	02.0	09.1	.	.	—	—	—
23	8 02	020	01	01.7	08.2	.	.	—	—	—
24	8 06	050	04	05.0	08.0	.	.	—	—	—
25	8 06	08	100	08.0	04.9	.	.	—	—	—
26	7 100	100	100	10.0	30.0	32.3	.	—	—	—
27	8 100	10	00	06.7	01.5	50.9	.	—	—	—
28	7 08	100	10	09.3	00.0	02.6	.	—	—	—
MES.										
VRED.	07.4	07.8	05.7	07.0	68.4	316.1				

1978 MART

TITOGRAĐ

 $\varphi = 42^{\circ}26' N \lambda = 19^{\circ}17' E$ Gr. $\Delta G = + 1h 17 min.$

BR. ST. 242

D	Vršački pritisk P mm			Temperatura vazduha T C°								Napon vodenog pore e mm			Relativna vlažnost u %			Pravac i jačina vetro D, f (0-12)					
	7	14	21	7	14	21	Sred. Dne	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dne	7	14	21			
1	754.3	754.7	756.6	10.2	16.3	11.4	12.3	17.2	10.0	08.2	09.1	10.6	09.8	98	76	97	90	-	0	S	3	-	0
2	756.7	754.8	755.0	07.0	19.4	10.4	11.8	20.0	07.0	04.0	07.4	07.4	08.8	99	44	93	79	-	0	WSW	1	-	0
3	753.9	751.0	751.7	09.4	21.3	13.6	14.5	21.5	08.5	04.2	06.7	08.6	07.4	76	45	63	61	NNW	1	-	0	-	0
4	752.8	752.4	753.8	09.4	21.9	12.2	13.9	22.6	08.4	05.0	06.5	08.3	09.0	74	42	85	67	-	0	E	2	-	0
5	755.3	753.4	754.7	11.1	19.2	13.6	14.4	20.2	08.6	05.4	07.8	09.6	09.2	78	58	79	72	-	0	SSE	1	-	0
6	751.9	750.8	753.9	11.2	17.8	10.0	12.3	18.2	10.0	08.4	07.7	08.1	08.8	77	53	95	75	N	1	-	0	-	0
7	754.7	755.0	755.0	09.6	17.0	10.8	12.1	18.1	09.0	06.0	08.7	08.5	08.8	98	58	91	82	-	0	0	0	-	0
8	756.0	755.6	756.9	09.6	15.6	09.0	10.8	16.0	08.2	06.3	08.1	08.2	08.4	90	62	97	83	-	0	SSE	3	NNW	2
9	756.9	756.0	756.4	08.0	14.2	10.8	11.0	15.5	07.0	05.0	07.2	07.1	07.9	90	59	82	77	-	0	S	2	-	0
10	758.9	758.0	758.4	09.6	12.6	09.2	10.2	13.6	08.7	07.5	04.2	03.9	03.9	47	36	44	42	NNW	5	N	6	N	6
11	759.7	756.9	755.6	08.3	15.0	09.2	10.4	15.6	08.0	05.7	03.5	05.0	04.8	42	39	55	45	N	3	NNE	3	NNW	2
12	752.5	753.9	757.7	09.8	10.8	06.6	08.5	12.6	06.0	02.0	04.0	02.9	03.2	44	31	43	39	NNW	4	N	6	N	6
13	760.0	760.0	761.9	04.6	13.6	07.3	08.2	14.0	04.6	02.5	02.8	04.4	05.5	44	38	72	51	N	5	S	3	-	0
14	762.7	762.8	762.8	04.8	14.0	11.2	10.3	14.4	03.0	00.9	04.5	05.7	07.7	70	47	77	65	N	2	SSE	3	-	0
15	760.9	758.6	756.3	08.8	09.8	10.8	10.1	12.0	08.6	03.0	08.1	08.4	09.0	95	93	94	94	NNW	1	SE	3	-	0
16	758.9	759.1	758.8	05.8	15.2	11.7	11.1	15.4	05.4	03.4	06.3	07.9	08.8	92	61	85	79	NNE	1	S	4	S	2
17	756.2	754.9	754.6	11.1	12.4	12.2	12.0	13.9	09.2	05.3	08.0	09.8	10.2	81	91	96	89	S	6	SSE	3	SSE	6
18	753.9	754.7	757.2	12.2	11.8	09.2	10.6	13.6	09.0	08.8	10.2	09.7	08.1	96	93	94	93	WSW	2	-	0	-	0
19	759.8	756.0	756.5	07.2	09.6	07.1	07.8	10.4	07.0	06.5	07.4	07.8	07.5	97	87	99	94	-	0	W	2	S	2
20	756.6	756.7	755.5	05.7	11.0	08.8	08.6	12.2	05.4	03.4	06.6	05.9	06.8	96	60	80	79	W	2	SSE	3	-	0
21	746.7	744.5	742.7	08.8	11.2	09.2	09.6	14.5	07.0	04.0	08.2	09.3	07.7	96	93	88	92	ESE	4	-	0	N	5
22	742.7	746.7	752.8	07.0	10.7	08.0	08.4	11.3	06.1	05.0	05.0	04.2	03.4	66	43	42	50	NE	6	NNE	2	NNW	6
23	758.9	757.6	757.3	05.8	12.4	06.4	07.8	13.0	05.4	03.6	02.4	03.2	04.7	35	30	65	43	NNW	6	SSE	3	SE	1
24	752.1	749.2	749.7	04.8	03.8	05.0	04.7	09.0	03.5	02.6	05.2	06.0	06.2	96	100	94	97	NE	2	NNW	5	-	0
25	749.7	751.8	755.6	03.8	12.3	09.2	08.6	12.7	03.4	01.0	05.5	04.0	04.2	91	37	48	59	-	0	NNE	7	NNW	4
26	756.9	755.4	755.4	07.7	14.8	09.0	10.1	15.5	06.0	05.2	04.5	03.8	06.3	57	30	73	53	NW	3	E	4	-	0
27	753.0	753.1	757.6	08.8	13.0	10.0	10.5	14.6	06.8	03.6	04.8	04.9	04.8	57	44	52	51	-	0	NNE	4	NNW	6
28	761.5	761.0	762.7	09.8	16.0	11.8	12.4	16.8	08.8	06.4	03.6	04.0	03.5	39	20	34	34	NNW	3	NNW	5	N	4
29	763.4	761.0	760.6	05.8	18.2	09.4	10.7	18.6	04.0	-0.6	05.0	05.4	06.3	73	35	71	60	-	0	SSE	2	SE	2
30	760.1	757.6	758.0	07.6	18.6	11.2	12.2	19.2	05.0	-0.6	06.4	05.4	06.2	82	33	63	59	-	0	S	4	-	0
31	756.3	755.4	755.6	07.0	17.1	13.0	12.5	17.8	06.2	01.5	06.3	06.5	08.6	84	44	77	68	-	0	S	4	-	0
MES.	RED. 756.0 755.1 756.0			08.1	14.4	09.9	10.6	15.5	06.9	04.4	06.2	06.6	07.0	76	54	75	68	1.8	3.1	1.7			

1978 APRIL

TITOGRAĐ

1	753.6	749.1	750.2	10.4	14.9	10.0	11.3	17.8	08.6	05.1	07.7	10.2	09.0	81	80	98	86	-	0	ESE	2	N	2
2	748.4	748.4	750.3	09.2	15.4	10.8	11.6	17.0	09.0	08.0	07.9	07.6	09.0	90	58	93	80	NNW	2	E	6	-	0
3	749.3	747.1	745.6	09.6	14.5	11.4	11.7	17.2	08.7	05.5	08.1	08.3	09.9	90	67	98	85	-	0	S	3	-	0
4	743.1	744.3	748.5	10.2	18.8	15.0	14.8	19.6	10.0	08.4	09.2	07.6	06.9	99	47	54	67	-	0	NNE	4	NNE	4
5	751.3	752.8	753.7	11.8	14.2	12.2	12.6	15.5	10.6	08.0	08.3	08.9	09.0	80	74	85	80	-	0	-	0	-	0
6	754.8	754.8	755.5	10.0	15.6	11.8	12.3	17.0	10.0	08.0	08.1	09.3	09.3	88	70	90	83	-	0	SSE	3	-	0
7	753.8	750.5	749.7	11.2	14.0	11.2	11.9	15.5	09.5	07.0	05.2	07.7	07.9	52	64	80	65	NNW	4	-	0	-	0
8	747.9	747.2	748.3	13.6	17.4	12.8	14.2	18.6	09.3	06.0	08.3	09.5	09.4	71	64	85	73	-	0	SSE	4	SM	2
9	749.5	751.0	752.3	12.0	15.4	12.0	12.9	16.0	10.5	10.0	09.6	09.5	09.8	91	73	93	86	-	0	-	0	-	0
10	754.1	756.0	757.4	11.2	14.6	12.8	12.9	16.0	11.0	10.5	09.7	09.9	09.2	98	80	83	87	-	0	SE	3	SE	2
11	758.7	759.4	748.0	10.4	15.6	13.2	13.1	17.5	10.0	08.0	09.0	09.2	10.4	95	69	91	85	-	0	SE	5	-	0
12	760.5	757.0	755.6	10.8	22.2	14.0	15.3	22.6	09.2	05.5	08.8	08.3	09.0	91	41	75	69	-	0	SSE	2	E	1
13	753.0	749.6	748.2	11.6	14.8	14.4	13.8	17.5	11.0	08.0	09.8	11.3	11.0	95	90	92	92	NNW	2	SSW	3	S	5
14	748.1	748.5	748.1	13.2	16.6	12.6	13.																

BR. ST. 242

 $H_s = 49 \text{ m } H_b = 50.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$

Dan	Mj.	G.	Oblačnost N (0—10)					Sred vjetra km/h	Padavina mm	Snježni pokriven. h cm	Razvoj vremena w
			14	7	14	21	Sred Dne				
1	8	10	08	00	06.0	01.1	18.0	.	0° 0-5, 0° 10; 0° 20-25	.	
2	8	02	04	00	02.0	08.6	00.4	.	0° 0-5; 0° 20-25	.	
3	8	04	06	00	03.3	09.5	.	.	0° 0-5; 0° 20-25	.	
4	8	00	00	00	00.0	-09.9	.	.	0° 0-5; 0° 20-25	.	
5	8	09	06	06	07.0	04.9	.	.	0° 0-5; 0° 20-25	.	
6	8	10	10	10	10.0	00.2	.	.	0° 0-5; 0° 20-25	.	
7	8	10	04	00	04.7	08.6	05.2	.	0° 0-5; 0° 20-25	.	
8	8	10	02	10	07.3	05.5	.	.	0° 0-5; 0° 20-25	.	
9	8	10	06	10	08.7	04.5	02.0	.	0° 0-5; 0° 20-25	.	
10	8	06	09	02	05.7	07.4	.	.	0° 0-5; 0° 20-25	.	
11	8	02	02	00	01.3	10.5	.	.	0° 0-5; 0° 20-25	.	
12	8	04	04	00	02.7	09.8	.	.	0° 0-5; 0° 20-25	.	
13	8	00	00	02	00.7	10.5	.	.	0° 0-5; 0° 20-25	.	
14	8	04	06	10	06.7	09.1	.	.	0° 0-5; 0° 20-25	.	
15	8	10	10	10	10.0	00.0	03.6	.	0° 0-5; 0° 20-25; 0° 30-35; 0° 40-45	.	
16	8	04	08	09	07.0	09.2	15.5	.	0° 0-5; 0° 20-25	.	
17	8	08	10	10	09.3	00.1	00.5	.	0° 0-5; 0° 20-25	.	
18	7	100	10	10	10.0	00.0	25.5	.	0° 0-5; 0° 20-25; 0° 30-35; 0° 40-45	.	
19	8	100	10	10	10.0	00.0	25.5	.	0° 0-5; 0° 20-25; 0° 30-35	.	
20	8	06	10	10	08.7	05.7	06.3	.	0° 0-5; 0° 20-25	.	
21	7	100	10	100	10.0	00.7	17.2	.	0° 0-5; 0° 20-25; 0° 30-35; 0° 40-45	.	
22	8	10	07	05	07.3	03.0	33.5	.	0° 0-5; 0° 20-25; 0° 30-35	.	
23	8	00	02	08	03.3	11.3	.	.	0° 0-5; 0° 20-25	.	
24	7	100	100	100	10.0	00.5	02.2	.	0° 0-5; 0° 20-25; 0° 30-35; 0° 40-45	.	
25	8	06	05	07	06.0	10.8	27.9	.	0° 0-5; 0° 20-25	.	
26	8	00	00	06	02.0	10.8	
27	8	10	10	00	06.7	01.2	
28	8	00	01	00	00.3	11.6	.	.	0° 0-5; 0° 20-25	.	
29	8	00	00	00	00.0	11.4	.	.	0° 0-5; 0° 20-25	.	
30	8	00	00	00	00.0	11.6	.	.	0° 0-5; 0° 20-25	.	
31	8	00	08	10	06.0	06.9	.	.	0° 0-5; 0° 20-25	.	
MES.	VRED.		05.6	05.7	05.3	05.6	194.9	203.4			

1	8	07	10	100	09.0	01.9	.	.	0° 0-5; 0° 10; 0° 20-25	.	
2	8	08	06	100	08.0	05.5	06.4	.	0° 0-5; 0° 10; 0° 20-25	.	
3	8	10	10	100	10.0	02.2	01.0	.	0° 0-5; 0° 10; 0° 20-25	.	
4	8	09	08	06	07.7	06.0	07.4	.	0° 0-5; 0° 10; 0° 20-25	.	
5	7	10	10	10	10.0	00.0	.	.	0° 0-5; 0° 10; 0° 20-25	.	
6	8	06	10	10	08.7	07.7	01.4	.	0° 0-5; 0° 10; 0° 20-25	.	
7	8	10	08	04	07.3	01.3	01.3	.	0° 0-5; 0° 10; 0° 20-25	.	
8	7	10	10	10	10.0	00.6	00.6	.	0° 0-5; 0° 10; 0° 20-25	.	
9	7	10	08	10	09.3	00.0	09.2	.	0° 0-5; 0° 10; 0° 20-25	.	
10	8	100	10	10	10.0	01.2	01.4	.	0° 0-5; 0° 10; 0° 20-25	.	
11	7	10	08	10	09.3	03.4	03.5	.	0° 0-5; 0° 10; 0° 20-25; 0° 30-35	.	
12	8	02	01	00	01.0	11.2	01.8	.	0° 0-5; 0° 10; 0° 20-25; 0° 30-35	.	
13	7	100	100	100	10.0	00.0	00.8	.	0° 0-5; 0° 10; 0° 20-25; 0° 30-35	.	
14	8	100	08	08	08.7	03.6	12.5	.	0° 0-5; 0° 10; 0° 20-25; 0° 30-35	.	
15	7	100	100	04	08.0	00.2	08.2	.	0° 0-5; 0° 10; 0° 20-25; 0° 30-35	.	
16	7	10	100	100	10.0	01.0	21.3	.	0° 0-5; 0° 10; 0° 20-25; 0° 30-35	.	
17	8	10	08	06	08.0	05.3	16.6	.	0° 0-5; 0° 10; 0° 20-25	.	
18	8	08	08	02	06.0	04.5	00.0	.	0° 0-5; 0° 10; 0° 20-25	.	
19	8	02	04	04	03.3	09.9	.	.	0° 0-5; 0° 10; 0° 20-25	.	
20	8	04	08	00	04.0	08.0	.	.	0° 0-5; 0° 10; 0° 20-25	.	
21	8	02	04	06	04.0	10.4	.	.	0° 0-5; 0° 10; 0° 20-25	.	
22	8	06	08	04	06.0	07.8	.	.	0° 0-5; 0° 10; 0° 20-25	.	
23	8	06	04	06	05.3	10.7	.	.	0° 0-5; 0° 10; 0° 20-25	.	
24	8	02	08	06	05.3	09.5	.	.	0° 0-5; 0° 10; 0° 20-25	.	
25	7	100	100	100	10.0	00.0	04.0	.	0° 0-5; 0° 10; 0° 20-25	.	
26	8	10	08	10	09.3	04.5	50.9	.	0° 0-5; 0° 10; 0° 20-25; 0° 30-35	.	
27	7	100	10	100	10.0	00.1	03.2	.	0° 0-5; 0° 10; 0° 20-25	.	
28	8	10	04	06	06.7	06.8	27.1	.	0° 0-5; 0° 10; 0° 20-25	.	
29	8	02	04	00	02.0	11.1	01.2	.	0° 0-5; 0° 10; 0° 20-25	.	
30	8	08	09	10	09.0	03.3	.	.	0° 0-5; 0° 10; 0° 20-25	.	
MES.	VRED.		07.7	07.8	07.1	07.5	139.7	181.8			

$\varphi = 42^{\circ}26' N \lambda = 19^{\circ}17' E$ Gr. $\Delta G = + 1h 17 min.$

BR. ST. 242

d	Vazdušni pritisk P mm			Temperatura vazduha T C°								Napon vodené pare ø mm			Relativna vlažnost u %			Pravac i jačina veta D, I (0-12)						
	7	14	21	7	14	21	Sred Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dnes	7	14	21				
1	752.5	748.5	749.5	16.6	26.4	19.4	20.5	28.2	12.5	09.2	07.5	07.1	10.6	53	27	63	48	-	0	S	6	SE	5	
2	754.7	746.1	752.1	15.0	13.7	12.0	13.1	19.6	12.0	10.0	11.5	09.4	09.8	90	83	93	89	SE	8	SE	5	SE	2	
3	756.4	758.2	760.2	12.0	17.8	12.4	13.7	18.6	10.8	09.0	09.6	10.3	08.9	91	68	83	81	WSW	1	SE	4	-	0	
4	761.5	760.8	760.6	12.8	18.6	12.8	14.3	20.0	08.8	06.0	08.0	10.2	10.1	72	63	91	75	-	0	SSE	2	-	0	
5	761.8	759.2	759.2	14.8	24.6	15.6	17.7	26.0	09.8	07.2	08.6	09.6	10.9	68	41	82	64	-	0	S	1	-	0	
6	758.7	757.7	757.0	15.6	22.4	12.8	15.9	24.4	12.6	11.2	10.2	09.8	10.7	77	48	97	74	-	0	SSW	3	NNW	2	
7	753.1	751.2	751.4	13.0	13.6	12.4	12.9	15.4	12.0	11.0	11.0	11.7	10.6	98	100	98	99	-	0	-	0	-	0	
8	751.4	751.4	752.5	11.8	11.4	11.0	11.3	14.0	10.7	10.0	10.1	10.1	09.4	98	100	95	98	-	0	S	5	-	0	
9	752.9	753.8	756.1	11.2	14.9	13.0	12.8	17.0	10.0	09.8	09.5	09.5	10.7	95	79	96	90	W	2	E	1	-	0	
10	757.4	759.2	759.3	14.0	15.0	12.8	13.7	16.0	11.5	09.0	10.5	10.5	10.6	87	82	96	88	-	0	-	0	-	0	
11	757.3	756.0	755.5	12.4	15.0	12.6	13.2	15.8	11.8	10.0	10.6	09.0	06.2	98	71	56	75	-	0	N	2	N	5	
12	755.0	754.0	756.1	10.6	15.2	10.0	11.5	16.0	10.0	97.6	05.1	05.5	04.6	53	43	50	49	N	5	N	4	NNW	3	
13	757.1	756.7	754.7	9.4	14.2	11.8	11.8	15.4	9.5	22.0	05.7	07.8	10.4	65	64	100	76	NN	2	S	4	-	0	
14	750.7	754.0	755.1	14.2	19.4	13.9	14.9	20.0	09.9	09.0	10.9	09.4	10.5	90	56	93	80	SE	5	S	4	-	0	
15	756.0	755.0	754.4	12.5	21.4	14.8	15.9	22.0	08.0	05.5	08.3	08.3	09.6	76	43	76	65	W	2	S	4	-	0	
16	756.7	756.0	759.0	14.0	19.6	14.2	15.5	21.0	14.0	06.8	08.6	09.2	09.7	72	54	80	69	-	0	SSE	5	-	0	
17	760.3	758.4	759.2	14.8	22.2	15.4	17.0	23.0	10.0	07.6	09.1	08.4	09.8	72	42	75	63	-	0	SSE	4	-	0	
18	759.6	758.1	758.5	16.8	25.0	17.4	19.2	25.6	10.9	07.0	08.6	09.8	12.0	60	41	80	60	-	0	SE	4	-	0	
19	758.6	757.3	756.6	15.0	22.8	17.2	18.1	23.5	14.0	10.5	11.5	11.4	12.0	90	55	81	75	-	0	-	0	-	0	
20	756.5	756.6	756.8	18.4	25.0	18.8	20.3	25.4	15.0	12.0	11.1	11.7	13.9	70	49	86	68	-	0	S	5	-	0	
21	757.3	757.1	756.3	19.2	23.8	19.2	20.4	25.2	16.0	13.2	13.3	14.7	14.3	80	66	86	77	N	2	SSE	2	NNW	1	
22	754.2	755.7	750.3	19.0	17.2	15.4	16.8	20.5	15.4	15.0	12.7	14.4	12.9	77	98	91	91	NNW	2	W	2	-	0	
23	753.3	754.4	755.3	16.4	20.4	15.0	16.7	21.2	14.4	13.5	11.0	12.0	12.4	79	67	97	81	SE	5	S	5	-	0	
24	755.7	755.9	756.3	17.2	21.5	16.4	17.9	22.2	13.0	11.7	12.8	09.9	11.6	87	52	83	74	-	0	SSE	3	SE	1	
25	756.2	757.0	757.2	16.6	18.0	13.6	15.5	20.6	13.6	12.0	11.2	12.4	11.7	79	80	100	86	N	1	-	0	-	0	
26	757.4	756.4	756.3	15.8	22.5	18.4	18.8	23.6	10.4	08.8	10.3	10.4	12.7	77	51	80	69	-	0	E	2	-	0	
27	756.5	754.8	754.6	17.0	22.8	19.0	19.5	24.6	18.4	16.1	11.4	11.6	10.0	78	56	61	65	-	0	WNW	2	NW	3	
28	755.3	755.2	755.7	15.4	20.4	17.0	17.5	23.6	13.6	13.0	10.8	10.4	08.7	82	58	60	67	NW	2	NE	5	N	2	
29	754.7	752.8	752.8	16.8	20.7	18.4	18.6	23.4	15.4	12.6	09.3	08.5	09.0	65	46	57	56	NW	3	N	6	NW	4	
30	752.9	754.4	756.0	19.0	22.0	18.6	19.6	23.6	14.0	09.6	08.7	08.6	08.4	53	44	52	50	WNW	3	NNE	4	NNE	3	
31	758.2	758.1	759.7	19.4	24.4	20.2	21.1	26.5	14.5	11.0	10.1	09.2	11.3	60	40	63	54	NNW	1	SE	2	-	0	
MES.	RED.	755.8	755.4	755.9	15.0	19.7	15.2	16.3	21.4	12.2	09.9	09.9	10.0	10.4	77	60	81	73	1.4	3.1	1.0			

1	761.3	760.1	760.8	19.2	27.2	18.3	20.8	28.2	14.5	11.5	11.0	09.6	12.1	66	35	77	59	-	0	S	3	-	0
2	760.1	758.1	758.7	19.2	26.2	18.2	20.5	29.0	15.0	10.7	11.8	10.2	12.5	70	40	80	63	-	0	SE	2	-	0
3	757.6	756.0	758.7	21.0	27.2	22.0	23.1	28.5	13.5	10.8	10.3	09.2	10.9	55	34	55	48	NNW	2	NW	2	SE	6
4	759.5	759.4	760.8	21.2	28.2	21.4	23.1	28.6	14.2	12.5	10.2	10.4	13.5	54	36	71	54	NN	2	SSE	3	-	0
5	761.5	760.7	760.6	20.2	25.8	21.8	22.4	27.6	16.2	15.0	11.5	13.4	12.1	65	54	62	60	NNW	2	-	0	NM	2
6	760.6	758.5	759.6	20.6	27.2	22.3	23.1	28.2	17.6	14.2	11.3	14.7	13.3	62	54	66	61	-	0	S	3	-	0
7	760.3	759.2	759.1	22.8	29.2	21.6	23.8	29.4	18.0	17.6	12.6	13.6	15.2	61	45	78	61	-	0	SSE	2	-	0
8	759.8	759.7	759.9	21.6	27.2	21.4	22.9	28.2	17.2	16.0	13.1	13.3	15.3	68	49	80	66	NW	1	SE	1	-	0
9	758.5	756.9	757.8	21.8	28.8	23.0	24.2	29.6	18.1	15.5	14.5	13.1	19.3	74	44	92	70	-	0	S	3	-	0
10	758.7	756.7	758.2	22.3	30.0	23.8	25.0	31.0	18.0	15.2	15.0	14.2	15.6	74	44	71	63	N	2	SSE	2	-	0
11	759.2	759.5	758.8	24.0	31.4	23.2	25.5	32.0	20.0	16.0	15.2	13.5	15.0	68	39	70	59	NNM	1	-	0	-	0
12	758.6	756.1	754.7	24.2	30.5	26.4	26.9	32.4	21.2	17.0	13.9	10.9	10.0	61	33	39	44	-	0	S	6	S	5
13	753.5	753.1	753.2	22.8	27.8	22.6	24.0	28.2	22.2	20.2	16.8	14.3	15.6	81	51	76	69	S	4	SSW	3	-	0
14	752.8	752.7	754.0	21.6	27.0	21.2	22.8	28.0	19.0	17.0	16.3	12.8	15.7	84	48	83	72	SSE	2	SE	6	-	0
15	754.2	754.0	751.2	20.																			

BR. ST. 242

 $H_s = 49 \text{ m } H_b = 50.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$

D S D s W O O -	V M P R -	Oblačnost N (0-10)					R R -	Podzemní R' mm	Sedmí pokriven h cm	Rozvoj vlnoviny w
		14	7	14	21	Sred Dnes				
1	8	050	060	10	07.0	07.5	.	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
2	8	100	10	10R	10.0	00.5	24.0	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
3	8	10	080	00	06.0	03.9	10.6	.	.	.
4	8	040	08	00	04.0	04.8	.	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
5	8	020	040	00	02.0	10.9	.	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
6	8	060	08	100	08.0	03.7	.	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
7	7	100	100	100	10.0	00.0	17.8	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
8	7	100	100	100	10.0	00.0	22.9	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
9	8	10	100	06	08.7	01.0	30.2	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
10	8	10	10	10	10.0	00.1	03.6	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
11	8	100	10	06	08.7	00.0	08.0	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
12	8	10	040	02	05.3	07.4	02.9	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
13	8	040	10	100	08.0	04.1	.	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
14	8	100	020	00	04.0	07.7	21.5	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
15	8	05	04	04	04.3	10.1	18.0	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
16	8	020	070	00	03.0	11.4	.	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
17	8	010	020	00	01.0	13.7	.	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
18	8	020	020	03	02.3	11.8	.	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
19	8	10	04	00	04.7	08.6	00.4	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
20	8	060	040	08	06.0	13.1	.	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
21	8	020	080	10	06.7	04.8	.	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
22	7	10	100	100	10.0	00.0	.	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
23	8	10	06	10	08.7	04.3	54.0	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
24	8	060	08	00	04.7	08.6	04.7	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
25	7	10	080	00	06.0	02.6	.	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
26	8	040	070	05	05.3	07.6	03.6	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
27	8	10	08	10	09.3	05.4	00.8	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
28	8	060	100	08	08.0	05.8	05.0	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
29	8	08	080	08	08.0	05.4	01.7	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
30	8	040	08	06	06.0	06.3	.	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
31	8	020	030	06	03.7	12.7	.	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
MES.										
WRED.		06.7	07.0	05.5	06.4	183.8	229.7			

1	8	000	060	00	02.0	10.5	.	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
2	8	000	08%	06	04.7	10.2	.	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
3	8	000	040	06	03.3	10.5	.	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
4	8	000	040	04	02.7	12.4	.	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
5	8	040	060	06	05.3	10.8	.	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
6	8	040	080	02	04.7	10.6	.	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
7	8	000	020	00	00.7	13.4	.	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
8	8	08	06	10	08.0	05.8	.	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
9	8	080	040	00	04.0	08.9	.	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
10	8	000	040	00	01.3	11.8	.	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
11	8	06	04	00	03.3	09.5	.	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
12	8	040	10	02	05.3	06.9	.	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
13	8	36	040	02	04.0	04.0	00.0	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
14	8	10	040	00	04.7	08.1	.	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
15	7	10	100	10	10.0	00.3	.	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
16	7	070	080	02	05.7	06.3	25.7	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
17	8	10	040	02	05.3	19.5	02.0	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
18	8	060	020	.10	26.0	11.4	.	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
19	8	10	020	08	06.7	08.1	.	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
20	8	000	000	00	30.0	13.2	.	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
21	8	080	070	02	05.7	04.5	.	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
22	8	110	040	06	03.7	13.1	00.3	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
23	8	060	070	00	04.3	09.8	.	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
24	8	000	040	04	22.7	13.5	.	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
25	8	080	010	00	03.0	13.0	.	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
26	8	030	020	06	03.7	13.9	.	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
27	7	160	100	100	08.7	04.6	.	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
28	8	10	08	00	26.0	26.2	.	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
29	8	030	040	00	02.3	11.4	.	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
30	8	000	020	00	00.7	13.8	.	.	.	$\text{H}_s 10^{\circ}-10^{\circ}, \text{H}_b 10^{\circ}, \text{h}_t 10^{\circ}, \text{h}_r 10^{\circ}$
MES.										
WRED.		34.6	05.1	33.3	34.3	2800.1	680.2			

1978 JUL

TITOGRAD

 $\varphi = 42^\circ 26' N \lambda = 19^\circ 17' E$ Gr. $\Delta G = + 1h 17 min.$

BR. ST. 242

S	Vodootná príčka P mm			Temperatura vzduchu T C°								Napón vodotne pote e mm			Relatívna vlhkosť U %			Pravac i jačina vetra D, f (0-12)					
				7	14	21	7	14	21	Sred. Dies	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dies	7	14	21
		7	14	21		7	14	21							7	14	21						
1	760.0	758.8	760.0	20.2	28.0	21.6	22.9	28.8	16.0	12.3	11.0	12.0	15.2	62	42	78	61	WNN	2	SSE	2	SSE	1
2	760.2	758.9	758.3	22.8	29.2	20.6	23.3	29.2	18.6	16.0	14.0	12.3	12.5	67	40	68	58	WNN	1	SE	5	-	0
3	757.0	756.0	756.3	22.0	27.7	22.0	23.4	27.8	18.2	15.5	11.5	13.7	16.4	58	49	63	63	WNN	2	SSE	5	S	3
4	757.2	755.7	755.9	21.6	28.8	22.6	23.9	29.4	19.0	16.0	14.0	14.4	16.1	72	49	78	66	NNE	2	SSE	3	SSE	1
5	756.6	755.2	755.3	23.6	29.6	26.0	26.3	30.6	18.4	15.4	13.6	12.1	11.5	62	39	46	49	WNN	1	SSE	2	SSE	5
6	757.3	756.7	755.2	24.6	30.0	25.6	26.5	31.0	18.8	17.6	16.9	13.2	15.1	73	41	61	58	S	2	SE	2	-	0
7	754.7	754.4	754.0	22.8	28.8	21.0	23.4	29.0	20.7	20.0	14.6	13.1	13.1	70	44	70	61	N	3	N	2	-	0
8	755.3	755.5	756.1	22.0	28.2	21.2	23.2	28.4	17.0	13.0	10.1	10.8	11.6	51	38	61	50	WNN	1	SE	3	NM	3
9	756.5	754.9	754.7	21.6	27.2	19.8	22.1	28.0	18.8	16.2	10.3	10.6	10.9	53	39	63	52	WNN	2	SSE	3	SSE	3
10	755.3	755.1	755.2	20.0	28.0	21.4	22.7	28.6	15.0	11.4	10.0	09.9	12.6	57	35	66	53	WNN	1	S	4	-	0
11	756.7	756.0	756.4	22.4	30.6	23.7	25.1	31.4	17.6	13.2	11.3	11.3	14.1	55	34	64	51	-	0	SSE	3	-	0
12	758.0	756.8	757.1	24.3	34.8	25.6	27.6	35.2	20.0	15.6	13.7	13.4	16.7	60	32	68	53	WNN	2	SSE	2	-	0
13	758.2	757.7	757.1	25.6	35.0	27.8	29.1	36.5	22.0	17.0	12.9	13.3	13.6	52	32	49	44	N	2	SSE	3	NNW	2
14	758.0	756.4	756.2	27.8	33.8	26.6	28.7	34.5	25.8	22.6	13.0	13.3	15.9	46	34	61	47	NM	3	SE	5	-	0
15	755.2	755.2	755.4	26.2	20.0	22.6	22.9	31.6	20.0	18.0	12.9	16.6	15.5	50	95	75	73	N	2	NNW	4	NNW	2
16	755.5	749.1	755.7	25.0	30.4	25.6	26.7	30.6	23.0	20.6	11.0	12.7	11.1	46	39	45	43	N	5	NNE	3	NNE	3
17	757.9	756.1	757.4	24.4	32.6	25.0	26.8	33.2	20.8	-	10.3	12.2	12.9	45	33	54	44	NW	3	SSE	3	S	1
18	758.6	756.4	755.8	25.0	33.4	23.6	26.4	34.0	21.4	17.0	11.4	12.8	14.5	48	33	66	49	NNW	2	S	4	-	0
19	753.6	751.3	750.2	24.4	32.6	26.4	27.5	33.5	19.5	16.5	11.4	09.8	13.6	50	27	52	43	-	0	SSE	7	ESE	4
20	753.4	752.0	752.7	23.2	30.6	24.8	25.9	31.4	22.4	21.0	10.5	10.4	13.0	49	31	55	45	N	5	NNE	3	EWE	2
21	753.2	751.9	751.5	23.4	31.2	24.0	25.7	31.6	22.5	20.0	11.3	10.4	13.2	52	30	59	47	NNW	2	SSE	3	S	1
22	754.2	756.0	757.8	20.8	23.3	20.8	21.4	25.5	19.4	17.0	08.8	07.6	07.0	48	35	38	40	S	7	NNE	2	NNW	7
23	758.6	756.1	756.8	19.8	28.2	22.0	23.0	28.8	19.0	16.8	06.4	08.4	08.0	37	29	40	35	NNW	7	NNE	6	NNW	6
24	757.8	756.4	756.5	21.2	27.4	23.2	23.8	29.0	17.8	15.0	07.6	09.1	08.2	40	33	38	37	NNW	4	SSE	3	N	5
25	757.9	756.2	756.6	22.4	28.3	25.0	25.2	29.4	21.0	18.0	08.0	08.9	08.5	40	31	36	36	N	5	SSE	5	-	0
26	758.0	756.2	757.0	23.0	30.4	23.4	25.1	31.0	20.4	15.4	08.8	09.3	11.2	42	28	52	41	NNW	4	SSE	3	WSW	1
27	757.7	756.8	757.3	23.2	32.2	25.4	26.6	33.2	22.0	20.0	10.6	11.1	10.1	50	31	41	41	NNW	3	S	3	M	2
28	758.8	758.2	759.1	26.0	31.4	27.4	28.1	34.2	22.3	20.0	10.0	10.4	09.6	40	30	35	35	NNW	3	SSE	4	NNE	5
29	760.7	757.3	758.2	25.2	31.0	26.2	27.2	33.6	23.4	21.2	09.6	12.4	10.5	40	37	41	39	N	5	NNE	3	N	3
30	756.0	755.9	756.5	24.8	32.0	26.0	27.2	33.0	22.5	16.0	10.4	10.6	09.8	44	30	39	38	NNW	3	S	3	N	3
31	756.8	755.8	756.5	24.4	32.0	25.4	26.8	32.6	22.4	18.8	09.7	10.9	13.0	42	31	53	42	N	3	SSE	2	NW	2
MES.	VRED.	757.0	755.7	756.1	23.3	29.9	23.9	25.3	31.1	20.2	17.1	11.1	11.5	12.4	52	37	56	48	2.8	3.6	2.1		

1978 AUGUST

TITOGRAD

1	758.4	756.9	757.9	23.2	31.7	24.7	26.1	32.7	20.4	17.0	11.7	14.3	16.0	55	41	68	55	NNW	2	SSE	3	WSW	2
2	758.7	757.8	756.7	25.0	34.4	27.0	28.4	35.5	21.6	17.9	13.3	12.6	16.0	56	31	60	49	NNW	2	S	3	S	0
3	758.0	757.3	757.8	26.0	34.6	25.4	27.9	34.7	22.1	18.4	13.6	13.2	18.0	54	32	74	53	N	2	SSE	5	-	0
4	758.4	757.5	756.9	24.0	33.2	23.0	25.8	33.2	20.6	18.1	15.5	15.6	16.7	69	41	79	63	ESE	2	SSE	2	NNW	3
5	756.2	754.8	756.0	25.8	31.8	24.6	26.7	33.2	22.4	19.8	14.6	14.9	18.2	59	42	78	60	NNW	2	SSE	3	SW	1
6	756.4	755.0	754.6	26.0	33.8	27.0	28.5	34.2	22.9	19.6	12.4	12.3	12.6	49	31	47	42	NNW	2	SSE	4	NNW	2
7	755.4	754.1	754.8	25.4	34.6	27.0	28.5	35.6	23.6	20.2	11.6	12.2	14.7	48	30	55	44	NNW	3	SSE	3	SE	1
8	752.7	752.5	752.9	25.0	29.6	24.2	25.8	32.4	21.0	19.0	13.8	12.1	20.5	58	39	90	62	NNW	2	SSE	2	SSE	2
9	755.4	754.4	755.3	22.4	29.0	22.7	24.2	30.4	22.0	16.2	13.3	13.0	13.1	65	43	63	57	NNE	1	ESE	5	SE	4
10	755.5	753.7	755.2	21.3	29.0	21.8	23.5	30.4	17.6	14.2	11.4	12.4	11.3	60	41	58	53	NNW	2	SSE	3	NNE	2
11	756.7	755.8	755.5	21.0	25.4	21.4	22.3	27.6	19.4	16.4	10.9	11.8	10.1	58	48	53	53	NNW	2	NNW	4	NNW	3
12	756.5	756.4	757.9	22.0	28.0	24.0	24.5	28.8	17.2	15.0	09.8	08.5	08.4	50	30	38	39	NNW	3	NNW	3	NNE	5
13																							

BR. ST. 242

 $H_s = 49 \text{ m } H_b = 50.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$

Den	Měs.	Vrh.	Občasnost N (0-10)					Světlo zdroj číslo	Podzemní R mm	Snežní pokrivení h cm	Rozvoj vremene w
			14	7	14	21	Sred Dnes				
1	8	000	000	00	00.0	13.2
2	8	06	06	00	04.0	38.8
3	8	040	020	00	02.0	10.6
4	8	000	020	03	00.7	13.4
5	8	100	010	10	03.7	13.6
.
6	8	040	060	08	06.0	09.7
7	8	19	060	00	05.3	13.4
8	8	000	040	02	02.0	07.0
9	8	020	050	00	02.3	13.8
10	8	000	020	00	00.7	14.2
11	8	000	000	00	00.0	14.1
12	8	000	200	00	00.0	14.0
13	8	000	020	00	00.7	13.8
14	8	000	020	00	00.7	13.1
15	8	000	100	10	06.7	08.9
16	8	000	020	00	00.7	12.4	05.2
17	8	000	010	00	00.3	13.9
18	8	000	000	00	00.0	13.8
19	8	020	08	02	04.0	13.3
20	8	000	020	00	00.7	13.4
21	8	000	030	01	01.3	13.2
22	8	07	07	00	04.7	08.2	00.0
23	8	000	000	00	00.0	13.9
24	8	000	020	03	00.7	13.8
25	8	000	010	00	00.3	13.6
26	8	000	020	00	00.7	13.4
27	8	000	020	04	02.0	13.2
28	8	000	070	08	05.0	10.4
29	8	000	040	00	01.3	10.8
30	8	000	070	00	02.3	11.6
31	8	030	06	00	03.0	10.2
MES.	VRED.		01.2	03.3	01.5	02.0	380.7	05.2			

1	8	000	010	00	00.3	12.8
2	8	000	010	00	00.3	13.1
3	8	000	040	00	01.3	12.7
4	8	000	060	100%	05.3	06.4
5	8	000	08	00	02.7	11.1	01.6
6	8	000	020	00	00.7	13.2
7	8	000	010	00	00.3	13.0
8	8	010	08	00	03.0	06.1
9	8	000	03	00	01.0	12.8	00.5
10	8	000	080%	00	02.7	10.9
11	8	08	07	10%	08.3	08.1	00.6
12	8	060	080	07	07.0	08.0	01.6
13	8	030	020	00	01.7	11.8
14	8	020	070	00	03.0	10.1
15	8	000	010	00	00.3	12.7
16	8	000	000	00	00.0	12.7
17	8	000	000	02	00.7	12.1
18	8	000	010	03	01.3	12.4
19	8	000	040	03	03.3	10.8
20	8	000	020	02	01.3	11.9
21	8	000	010	00	00.3	12.6
22	8	000	010	00	00.3	12.4
23	8	040	030	00	02.3	12.8
24	8	030	050	07	05.0	10.9
25	8	020	050	00	02.3	08.7
26	8	000	030	00	01.0	12.0
27	8	000	08	04	04.0	39.6
28	8	000	040	00	04.0	07.2
29	7	10	36	03	05.3	34.8
30	8	000	040	06	03.3	11.8
31	7	10	080	10	30.3	11.5	19.5
MES.	VRED.		01.9	03.3	02.1	02.6	327.1	23.8			

$\varphi = 42^{\circ}26' N$ $\lambda = 19^{\circ}17' E$ Gr. $\Delta G = + 1h 17 min.$

BR. ST. 242

D S	Vazdušni pritisak P mm			Temperatura vazduha T °C								Napon vodenе pare e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0-12)					
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21			
1	751.9	753.0	754.3	15.2	22.8	16.0	17.5	23.0	11.4	10.0	06.8	07.8	09.5	53	38	70	54	-	0	N	2	-	0
2	755.3	756.2	755.8	15.2	14.9	15.2	15.1	19.1	12.7	11.0	09.4	10.3	11.4	73	81	88	81	-	0	N	2	NNW	2
3	755.7	755.0	755.6	14.8	25.6	18.4	19.3	26.5	12.4	11.6	11.6	10.8	11.1	92	44	70	69	NNW	3	S	5	-	0
4	756.8	755.8	755.0	16.8	26.6	18.4	20.1	27.0	15.0	12.5	10.8	10.9	12.4	76	42	78	65	-	0	SSE	3	-	0
5	754.6	754.9	754.6	17.8	18.4	17.2	17.7	20.1	15.6	13.5	10.6	14.0	14.4	69	88	98	85	N	2	-	0	N	2
6	752.0	750.5	749.1	17.8	17.6	16.8	17.3	20.5	16.8	16.1	14.7	14.8	14.4	96	98	100	98	NW	3	NW	4	-	0
7	750.0	749.2	748.7	19.4	20.4	17.6	18.8	24.0	16.8	16.6	15.1	14.9	14.5	89	83	96	89	-	0	SSE	3	-	0
8	749.3	752.6	753.7	17.6	22.0	18.6	19.2	24.4	16.6	15.0	14.2	10.6	08.8	94	54	55	68	-	0	N	6	NNW	4
9	755.6	755.3	757.3	19.1	22.2	18.4	19.5	24.5	14.6	14.0	07.5	07.1	07.6	65	36	48	43	NNW	4	NW	7	NW	3
10	757.5	757.0	757.3	17.8	25.4	21.2	21.4	27.5	17.5	14.2	08.3	10.9	10.8	55	45	57	52	N	4	N	5	N	2
11	757.5	757.0	757.0	17.2	28.0	20.2	21.4	28.6	15.6	14.5	12.0	12.6	12.8	81	44	72	66	-	0	SSE	3	S	2
12	755.2	752.2	750.8	16.9	25.0	29.6	15.8	25.8	09.5	09.0	13.6	14.4	08.5	83	61	95	80	NNW	2	SE	6	NW	8
13	752.5	752.6	755.2	15.2	17.4	18.0	17.2	19.6	09.6	05.6	07.3	06.9	07.8	56	46	50	51	N	4	NW	7	N	6
14	757.2	757.1	756.8	18.6	24.2	20.0	20.7	24.5	18.0	14.0	07.5	09.7	09.1	46	43	52	47	N	6	N	7	NNE	5
15	756.0	755.9	757.9	17.0	26.2	19.8	20.7	26.4	13.5	10.4	10.2	12.3	09.3	70	48	54	57	N	4	S	2	NW	7
16	757.3	759.0	760.0	17.2	27.0	21.0	21.6	27.0	16.6	12.0	09.1	10.0	09.0	62	37	48	49	-	0	N	4	N	3
17	761.6	760.5	761.6	19.4	27.8	18.2	20.9	27.8	17.6	14.8	08.8	09.1	11.3	52	33	72	52	N	2	N	6	N	2
18	761.0	759.9	759.9	17.0	26.8	16.2	19.1	27.2	14.5	13.7	09.1	10.5	11.5	63	40	84	62	NNW	3	S	2	-	0
19	758.8	756.8	755.5	16.2	27.0	18.0	19.8	27.0	14.4	07.6	08.7	11.0	12.4	63	41	80	61	-	0	S	2	-	0
20	755.1	757.1	759.1	16.2	10.0	13.8	13.5	20.6	09.8	08.2	11.1	09.0	06.4	81	98	54	78	-	0	N	5	N	5
21	760.4	760.0	761.4	13.2	18.4	14.6	15.2	19.2	13.1	08.6	04.4	05.0	04.2	39	32	34	35	N	6	N	9	N	2
22	761.7	760.0	760.6	14.8	19.8	15.0	16.2	20.6	13.5	10.4	04.6	07.1	06.5	37	41	51	43	N	9	NW	7	NW	4
23	759.4	758.5	759.0	11.2	21.2	15.8	16.0	21.3	10.8	07.0	07.1	10.0	10.2	71	53	76	67	-	0	SSE	2	-	0
24	760.0	761.1	762.7	14.0	23.2	18.8	18.7	25.2	12.0	08.6	10.6	09.0	09.7	88	42	60	63	-	0	NNW	4	N	4
25	763.7	763.4	763.0	15.8	26.0	20.0	20.5	26.8	13.1	09.0	11.3	11.5	12.2	84	46	70	67	NNW	1	SSE	3	S	2
26	762.2	760.1	759.7	16.4	27.6	18.0	20.0	28.2	14.0	10.5	12.0	14.7	13.8	85	53	89	76	-	0	SSE	1	-	0
27	758.2	757.0	755.8	15.8	24.2	19.2	19.6	25.0	14.0	10.0	11.9	12.7	14.2	88	56	85	76	-	0	S	2	-	0
28	752.2	749.4	750.5	16.2	17.2	13.8	15.3	20.4	13.2	11.8	13.5	13.0	10.8	98	89	92	93	SSE	6	SE	4	SE	2
29	754.2	756.0	759.7	13.0	20.4	12.0	14.4	20.9	10.5	09.0	07.7	06.9	09.2	69	38	88	65	NNW	3	ESE	4	S	3
30	761.4	759.6	758.0	11.8	19.6	14.8	15.3	20.0	09.6	06.6	08.3	09.4	11.8	80	55	94	76	ENE	2	-	0	-	0

MES.
RED. 756.8 756.4 756.8 16.2 22.4 17.2 18.3 24.0 13.7 11.2 09.9 10.6 10.5 71 54 72 66 2.1 3.9 2.5

1	754.7	755.5	756.0	18.8	18.4	15.0	16.8	20.0	13.8	10.8	11.2	13.8	12.5	69	87	98	85	SE	7	SE	4	NNW	1
2	756.6	757.4	758.2	15.8	16.6	15.8	16.0	18.4	15.0	13.8	12.8	12.5	12.7	95	88	94	92	-	0	NNW	2	-	0
3	758.4	756.0	757.4	15.6	26.4	20.2	20.6	26.6	14.2	13.0	12.8	14.8	12.4	96	57	70	74	NNW	2	W	2	WNN	6
4	757.0	757.4	758.5	20.2	22.2	15.4	18.3	23.2	15.4	15.0	14.4	14.9	12.6	81	74	96	84	ESE	4	SE	6	-	0
5	757.6	758.2	760.0	15.0	17.2	11.8	14.0	18.6	11.8	10.8	11.7	12.8	09.9	92	87	95	91	N	3	-	0	NNW	3
6	760.7	759.5	761.0	14.4	20.8	16.8	17.2	21.4	11.8	10.5	06.6	09.9	06.9	53	54	48	92	NNW	5	NNE	3	NNE	3
7	762.3	761.0	762.6	16.0	23.4	17.8	18.8	23.6	13.6	12.2	07.1	09.1	07.9	52	42	51	48	NNW	4	NNE	6	NNW	4
8	763.0	761.5	762.2	12.0	23.0	13.2	15.4	23.8	11.5	07.8	08.9	10.1	10.2	84	48	89	74	ENE	2	-	0	-	0
9	762.4	761.6	762.0	15.2	24.0	16.0	17.8	25.5	13.2	09.5	08.2	10.8	10.6	63	48	78	63	N	4	S	1	NNE	2
10	762.5	761.8	763.2	14.3	24.8	17.0	18.3	25.6	12.2	08.6	08.9	13.0	10.2	73	55	70	66	NNW	2	-	0	NNE	2
11	763.6	763.3	763.9	12.4	25.3	16.6	17.7	26.7	12.0	09.0	09.6	12.1	12.5	89	50	88	76	-	0	SSE	3	-	0
12	764.1	762.5	763.2	14.0	24.8	21.4	20.4	25.2	13.5	10.6	10.5	10.9	08.3	87	46	43	59	NNW	2	SE	2	NNE	6
13	764.7	763.2	763.1	18.0	24.6	14.6	18.0	24.7	14.6	12.2	07.8	11.3	10.4	50	49	84	61	NE	4	SSE	2	ESE	1
14	763.0	760.6	761.3	13.7	22.8	15.0	16.6	24.6	13.5	09.5	09.6	10.8	10.0	81	52	78	70	NNW	2	SE	3	N	2
15	761.0	758.8	759.0	11.6	21.5	14.6	15.6	21.8	10.6	07.6	08.6	09.9	11.2	84	52	90	75	N	2	SSE	3	-	0
16	758.1	756.0	756.8	13.0	21.2	13.4	15.3	21.6	12.5	09.0	08.8	10.8	10.1	79	57	87	74	N	3	SE	2	N	2
17	755.8	754.8	754.2	11.0																			

BR. ST. 242

$$H_s = 49 \text{ m } H_b = 50.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$$

Dan	Vrij.	Običajnost N (0-10)					Intenzitet broj senz.	Podzemna R mm	Smeđi pokriven h cm	Rezervi vremena w
		14	7	14	21	Sred Dnes				
1	8	000	040	00	01.3	11.4	33.9	.	$\text{P}_{\text{max}} 0^{\circ}-10^{\circ}$	
2	8	10	10	08	09.3	00.4	.	.	$\text{G}^{\circ}-15^{\circ}-12^{\circ}, \text{P}_{\text{max}} 10^{\circ}-12$	
3	8	010	040	00	01.7	06.8	.	.		
4	8	000	010	00	00.3	11.6	.	.		
5	7	10	10E	10	10.0	00.8	.	.	$\text{G}^{\circ}-7^{\circ}-10^{\circ} \text{d}, \text{R}_{\text{max}} 15^{\circ}-16$	
6	7	06	10	10	08.7	00.0	14.1	.	$\text{G}^{\circ}-5^{\circ}-10^{\circ} \text{d}, \text{R}_{\text{max}} 15^{\circ}-16; \text{R}^{\circ} 5^{\circ}-50^{\circ}$	
7	7	10	10	10	10.0	01.3	34.4	.	$\text{G}^{\circ}-0-4^{\circ}, \text{P}_{\text{max}} 10^{\circ}-12^{\circ}$	
8	8	10	10	00	06.7	01.0	.	.	$\text{G}^{\circ}-10^{\circ}-10^{\circ}, \text{R}^{\circ} 10^{\circ}-10$	
9	7	000	06	00	02.0	08.0	.	.	$\text{G}^{\circ}-10^{\circ}-10^{\circ}, \text{R}^{\circ} 10^{\circ}-10$	
10	7	000	10	06	05.3	06.7	.	.	$\text{G}^{\circ}-10^{\circ}-10^{\circ}$	
11	8	08	010	00	03.0	09.5	.	.	$\text{G}^{\circ}-10^{\circ}-10^{\circ}$	
12	7	010	080	100	06.3	05.8	.	.	$\text{G}^{\circ}-0-5^{\circ}, \text{R}^{\circ} 10^{\circ}-10; \text{G}^{\circ} 0^{\circ}-50^{\circ}, \text{P}_{\text{max}} 10^{\circ}-10$	
13	8	10	10	07	09.0	02.0	50.4	.	$\text{G}^{\circ}-0-5^{\circ}, \text{R}^{\circ} 10^{\circ}-10$	
14	8	030	070	00	03.3	11.7	.	.	$\text{G}^{\circ}-10^{\circ}-10^{\circ}, \text{R}^{\circ} 10^{\circ}-10$	
15	8	010	040	00	01.7	11.0	.	.	$\text{G}^{\circ}-10^{\circ}-10^{\circ}, \text{R}^{\circ} 10^{\circ}-10$	
16	8	020	020	00	01.3	10.4	.	.	$\text{G}_{\text{max}} 0-10^{\circ}, \text{R}^{\circ} 10^{\circ}-10; \text{G}^{\circ}-10^{\circ}-10$	
17	8	04	050	00	03.0	11.0	.	.	$\text{G}^{\circ}-0-10^{\circ}, \text{R}^{\circ} 10^{\circ}-10$	
18	8	000	000	00	00.0	11.4	.	.	$\text{G}^{\circ}-0-10^{\circ}, \text{R}^{\circ} 10^{\circ}-10$	
19	8	000	020	00	00.7	11.0	.	.	$\text{G}^{\circ} 10^{\circ}-24, \text{G}^{\circ} 10^{\circ}-10$	
20	7	06	100	10	08.7	.	.	.	$\text{G}^{\circ} 10^{\circ}-24, \text{G}^{\circ} 10^{\circ}-10$	
21	8	020	000	00	00.7	10.0	39.4	.	$\text{G}^{\circ} 0-10^{\circ}$	
22	8	000	000	00	00.0	10.9	.	.	$\text{G}^{\circ} 0-10^{\circ}$	
23	8	08	050	09	07.3	03.6	.	.	$\text{G}^{\circ} 0-10^{\circ}$	
24	8	060	08	00	04.7	04.8	.	.	$\text{G}^{\circ} 0-10^{\circ}$	
25	8	020	010	00	00.7	10.8	.	.	$\text{G}^{\circ} 0-10^{\circ}$	
26	8	040	010	00	01.7	10.9	.	.	$\text{G}^{\circ} 0-10^{\circ}, \text{R}^{\circ} 10^{\circ}-10$	
27	8	020	060	10	06.0	11.8	.	.	$\text{G}^{\circ} 0-10^{\circ}, \text{R}^{\circ} 10^{\circ}-10; \text{G}^{\circ} 10^{\circ}-24, \text{R}^{\circ} 10^{\circ}-10; \text{G}^{\circ} 10^{\circ}-10, \text{R}^{\circ} 10^{\circ}-10; \text{G}^{\circ} 10^{\circ}-10, \text{R}^{\circ} 10^{\circ}-10; \text{G}^{\circ} 10^{\circ}-10, \text{R}^{\circ} 10^{\circ}-10$	
28	7	10E	100	08	09.3	00.0	43.0	.	$\text{G}^{\circ} 0-10^{\circ}, \text{R}^{\circ} 10^{\circ}-10; \text{G}^{\circ} 10^{\circ}-24, \text{R}^{\circ} 10^{\circ}-10; \text{G}^{\circ} 10^{\circ}-10, \text{R}^{\circ} 10^{\circ}-10; \text{G}^{\circ} 10^{\circ}-10, \text{R}^{\circ} 10^{\circ}-10; \text{G}^{\circ} 10^{\circ}-10, \text{R}^{\circ} 10^{\circ}-10$	
29	8	040	010	00	01.7	09.6	110.4	.	$\text{G}^{\circ} 0-10^{\circ}, \text{R}^{\circ} 10^{\circ}-10; \text{G}^{\circ} 10^{\circ}-24, \text{R}^{\circ} 10^{\circ}-10; \text{G}^{\circ} 10^{\circ}-10, \text{R}^{\circ} 10^{\circ}-10; \text{G}^{\circ} 10^{\circ}-10, \text{R}^{\circ} 10^{\circ}-10$	
30	8	030	080	10	07.0	04.9	.	.	$\text{G}^{\circ} 0-10^{\circ}, \text{R}^{\circ} 10^{\circ}-10; \text{G}^{\circ} 10^{\circ}-24, \text{R}^{\circ} 10^{\circ}-10$	
MES. RED.		04.1	05.4	03.6	04.4	211.1	335.6			

1	8	10	100	100	10.0	00.8	04.1	.	$\text{G}^{\circ} 0-5, \text{G}^{\circ} 10^{\circ}-10; \text{R}^{\circ} 10^{\circ}-10$	
2	7	100	100	04	08.0	09.3	14.8	.	$\text{G}^{\circ} 0-10^{\circ}$	
3	8	040	020	100	05.3	05.1	11.0	.	$\text{G}^{\circ} 10^{\circ}-24, \text{G}^{\circ} 10^{\circ}-10; \text{R}^{\circ} 10^{\circ}-10$	
4	8	090	050	00	24.7	04.8	03.8	.	$\text{G}^{\circ} 3-5, \text{G}^{\circ} 10^{\circ}-10$	
5	8	100	10	100	10.0	09.0	02.8	.	$\text{G}^{\circ} 0-10^{\circ}, \text{R}^{\circ} 10^{\circ}-10$	
6	8	08	020	00	03.3	07.0	07.8	.	$\text{G}^{\circ} 0-10^{\circ}$	
7	8	000	010	00	00.3	10.6	.	.	$\text{G}^{\circ} 0-10^{\circ}, \text{R}^{\circ} 10^{\circ}-10$	
8	8	000	000	00	00.0	10.0	.	.	$\text{G}^{\circ} 0-10^{\circ}$	
9	8	020	030	00	01.7	09.4	.	.	$\text{G}^{\circ} 0-10^{\circ}$	
10	8	000	010	00	00.3	09.9	.	.	$\text{G}^{\circ} 0-10^{\circ}, \text{R}^{\circ} 10^{\circ}-10$	
11	8	000	000	00	00.0	13.0	.	.	$\text{G}^{\circ} 0-10^{\circ}, \text{R}^{\circ} 10^{\circ}-10$	
12	8	060	020	00	02.7	07.5	.	.	$\text{G}^{\circ} 0-10^{\circ}, \text{R}^{\circ} 10^{\circ}-10$	
13	8	020	000	00	00.7	.	.	.	$\text{G}^{\circ} 0-10^{\circ}$	
14	8	030	000	00	00.0	09.4	.	.	$\text{G}^{\circ} 0-10^{\circ}, \text{R}^{\circ} 10^{\circ}-10$	
15	8	000	000	00	00.0	09.1	.	.	$\text{G}^{\circ} 0-10^{\circ}, \text{R}^{\circ} 10^{\circ}-10$	
16	8	000	000	02	00.7	09.0	.	.	$\text{G}^{\circ} 0-10^{\circ}$	
17	7	060	070	04	05.7	01.6	.	.	$\text{G}^{\circ} 0-10^{\circ}, \text{R}^{\circ} 10^{\circ}-10$	
18	8	10	10	06	08.7	00.3	01.0	.	$\text{G}^{\circ} 0-10^{\circ}, \text{R}^{\circ} 10^{\circ}-10$	
19	8	06	10	10	08.7	00.4	.	.	$\text{G}^{\circ} 0-10^{\circ}, \text{R}^{\circ} 10^{\circ}-10$	
20	6	05	100	100	08.3	00.3	.	.	$\text{G}^{\circ} 0-10^{\circ}, \text{R}^{\circ} 10^{\circ}-10$	
21	8	100	10	09	09.7	31.1	13.0	.	$\text{G}^{\circ} 0-10^{\circ}, \text{R}^{\circ} 10^{\circ}-10; \text{G}^{\circ} 10^{\circ}-24$	
22	8	050	000	00	01.7	09.8	31.5	.	$\text{G}^{\circ} 0-10^{\circ}, \text{R}^{\circ} 10^{\circ}-10$	
23	8	040	070	00	03.7	06.4	.	.	$\text{G}^{\circ} 0-10^{\circ}, \text{R}^{\circ} 10^{\circ}-10$	
24	8	000	000	00	00.0	18.8	.	.	$\text{G}^{\circ} 0-10^{\circ}$	
25	8	090	040	00	01.3	08.7	.	.	$\text{G}^{\circ} 0-10^{\circ}, \text{R}^{\circ} 10^{\circ}-10$	
26	8	16	10	10	08.7	31.4	.	.	$\text{G}^{\circ} 0-10^{\circ}, \text{R}^{\circ} 10^{\circ}-10, \text{G}^{\circ} 10^{\circ}-24$	
27	8	10	240	02	75.3	27.2	01.5	.	$\text{G}^{\circ} 0-10^{\circ}, \text{R}^{\circ} 10^{\circ}-10, \text{G}^{\circ} 10^{\circ}-24$	
28	8	10	980	00	06.0	02.6	.	.	$\text{G}^{\circ} 0-10^{\circ}$	
29	8	100	940	00	01.3	19.6	.	.	$\text{G}^{\circ} 0-10^{\circ}, \text{R}^{\circ} 10^{\circ}-10$	
30	8	000	000	00	00.0	19.6	.	.	$\text{G}^{\circ} 0-10^{\circ}, \text{R}^{\circ} 10^{\circ}-10$	
31	8	000	000	00	00.0	19.6	.	.	$\text{G}^{\circ} 0-10^{\circ}, \text{R}^{\circ} 10^{\circ}-10$	
MFS. RED.		34.3	34.2	32.8	32.8	31.1	36.3			

1978 NOVEMBER

TITOGRAD

 $\varphi = 42^{\circ}26' N$ $\lambda = 19^{\circ}17' E$ Gr. $\Delta G = + 1h 17m$

BR. ST. 242

D	Vzdušní tlak P mm			Temperatura vzduchu T C°							Napětí vodného paru e mm			Relativní vlhkost u %			Pravac i jačina větra D, I (0-12)				
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21	
1	767.0	767.6	769.1	05.5	17.8	08.0	09.8	18.5	05.0	01.6	06.7	08.1	06.6	99	53	82	78	NW	2	SSE	3
2	768.3	766.7	766.2	06.0	19.6	14.8	13.8	19.6	05.4	02.2	06.2	06.8	06.6	89	40	52	60	N	2	W	1
3	766.0	764.5	765.5	08.0	18.0	09.8	11.4	18.0	07.6	05.2	07.6	08.2	07.4	95	53	81	76	NNE	1	SSE	1
4	766.0	766.2	765.8	09.0	15.6	07.6	10.0	15.6	05.2	06.0	05.5	06.4	06.9	64	48	88	67	NNW	2	SSE	4
5	766.1	765.9	767.7	06.4	14.8	10.2	04.0	15.5	04.5	01.6	05.7	06.1	04.5	80	49	48	59	N	2	S	3
6	768.4	768.2	768.2	06.2	14.2	05.0	07.6	15.0	04.6	01.6	04.6	06.0	06.4	65	49	97	70	N	3	SSE	2
7	768.0	766.1	767.3	01.2	15.0	04.6	06.4	15.0	00.2	-02.2	05.0	06.4	05.8	100	50	91	80	SSE	1	SSE	1
8	768.1	767.0	767.2	00.0	14.5	05.0	06.1	14.5	00.0	-02.4	04.5	05.9	05.9	98	47	90	78	-	0	SSE	2
9	768.0	766.5	768.2	00.4	15.0	04.6	06.2	15.0	00.0	-03.0	04.7	06.9	06.0	100	54	94	83	-	0	SSE	2
10	768.1	765.6	766.0	00.6	16.8	05.2	07.0	17.0	00.3	-03.0	04.6	05.9	06.3	96	41	94	77	N	1	SE	1
11	766.2	764.0	764.9	01.0	15.6	05.2	06.8	16.0	01.0	-02.5	04.8	06.6	06.0	98	50	90	79	NM	1	ESE	1
12	765.2	765.0	765.0	00.4	16.2	04.5	06.4	16.2	00.0	-02.6	04.5	06.1	06.0	95	44	96	78	-	0	SSE	2
13	766.7	765.9	767.3	00.0	15.4	04.6	06.2	15.5	00.0	-03.2	04.6	06.3	05.2	96	48	82	75	-	0	SE	2
14	767.2	767.0	768.7	00.4	15.0	03.2	05.5	15.5	00.0	-03.4	03.7	04.9	05.8	79	38	100	72	N	1	SSE	1
15	770.2	769.7	770.1	-01.0	14.8	03.2	05.1	15.4	-01.6	-05.0	04.2	06.1	05.2	99	49	91	80	SSE	1	SSE	1
16	769.1	767.0	766.7	-01.4	15.7	04.0	05.6	15.7	-01.8	-05.0	04.1	05.3	05.6	98	39	88	75	-	0	-	0
17	765.1	762.8	764.4	-00.5	18.6	12.6	10.8	18.6	-01.0	-03.8	04.0	05.1	06.8	91	32	62	62	NNW	2	N	6
18	765.9	765.8	766.8	10.0	15.4	04.6	08.7	16.5	04.4	-00.6	04.4	05.4	05.9	48	41	93	61	N	5	SSE	2
19	767.8	766.2	766.2	-00.6	13.8	03.0	04.8	14.6	-01.0	-03.4	04.4	06.0	05.1	100	51	91	81	SSE	1	SSE	1
20	765.8	765.0	766.0	00.0	14.2	04.6	05.9	14.6	-00.4	-04.0	04.2	04.8	05.9	91	40	93	75	NW	1	ESE	2
21	767.0	766.8	767.5	03.4	15.0	04.0	06.6	15.0	03.4	-02.0	04.9	06.0	05.6	83	47	91	74	NM	2	NE	1
22	770.3	770.0	771.0	-00.5	15.4	13.2	10.3	16.0	-00.5	-03.5	04.2	05.6	04.4	94	43	39	59	-	0	SSE	1
23	771.0	769.2	768.9	00.9	15.0	03.8	05.9	15.6	00.4	-02.8	04.8	05.6	05.3	98	44	88	77	-	0	SSE	1
24	769.3	768.9	767.7	02.2	16.5	05.4	07.4	16.6	01.2	-02.6	04.7	05.2	06.1	87	37	90	71	NNW	1	SSE	2
25	765.7	762.7	763.2	01.0	15.0	06.4	07.2	15.0	00.8	-02.7	04.8	02.9	06.3	98	21	88	70	-	0	SSE	2
26	759.6	759.0	757.2	05.2	09.6	08.8	08.1	10.8	04.0	01.6	05.9	08.1	08.2	89	90	100	93	-	0	NNW	1
27	752.0	748.5	746.1	10.0	10.4	10.0	10.1	13.0	07.2	06.5	08.3	07.7	07.4	90	81	80	84	SSE	1	SSE	4
28	749.4	742.0	741.3	06.8	07.8	09.0	08.2	10.2	06.6	06.0	07.0	07.3	06.3	95	92	73	87	SE	2	W	2
29	741.6	749.4	741.5	05.6	08.2	07.2	07.1	09.2	04.5	03.1	06.2	07.1	03.2	92	87	42	74	WSW	2	NW	2
30	744.7	746.5	751.0	06.5	10.6	05.6	07.1	11.2	05.0	04.5	03.9	03.7	03.6	54	39	53	49	NW	6	NNW	3
MES.	RED.	764.3	763.5	763.8	03.1	14.6	06.6	07.8	15.2	02.2	-00.6	05.1	06.1	05.9	89	50	82	73	1.3	1.9	1.6

1978 DECEMBER

TITOGRAD

1	756.2	757.1	758.0	02.8	10.8	04.6	05.7	11.6	02.4	-00.5	03.4	04.8	04.2	60	50	66	59	N	2	WSW	1
2	758.0	757.9	758.7	04.0	11.8	07.0	07.5	12.1	03.6	-01.7	03.4	04.1	03.9	56	40	51	49	NNW	3	SE	2
3	759.3	757.6	757.8	01.0	10.8	03.0	04.5	11.5	01.0	-13.6	04.2	04.8	04.7	85	50	83	73	-	0	SE	3
4	756.2	755.2	755.6	03.2	07.4	04.8	05.1	07.6	03.0	-02.0	04.5	04.9	06.4	78	63	99	80	NM	3	NNW	1
5	751.2	751.8	755.0	05.4	08.2	04.4	05.6	08.4	00.4	00.0	06.0	03.4	02.7	89	42	43	58	NNW	3	NNW	7
6	757.5	757.0	758.5	01.2	36.0	01.2	02.4	06.0	00.5	-00.8	02.2	01.8	01.7	44	25	33	34	NE	6	NNE	8
7	760.2	759.3	760.2	00.3	03.6	02.0	02.0	04.0	00.4	-02.4	02.0	02.8	03.6	43	47	68	53	NE	4	NW	1
8	760.5	761.3	762.2	01.4	08.6	01.8	03.4	09.0	01.2	-01.8	03.9	04.7	04.6	77	57	88	74	-	0	SSE	1
9	761.2	760.2	758.1	03.8	23.4	04.0	03.8	04.4	01.8	-01.6	04.6	05.7	05.9	76	97	97	90	NNW	2	NNW	1
10	760.4	760.0	761.3	01.6	14.4	06.8	07.4	14.6	01.6	-01.0	05.0	06.2	06.7	97	51	91	80	SSW	1	S	2
11	760.9	759.7	759.3	01.7	13.6	04.4	06.0	15.0	01.6	-01.6	05.2	06.7	05.9	130	58	94	84	-	0	SSE	3
12	757.6	755.8	752.7	03.2	08.6	07.7	06.8	09.6	03.0	-01.0	05.6	07.1	07.8	97	85	99	94	N	2	SSE	1
13	749.0	749.2	750.1	08.8	11.8	08.8	09.6	12.8	07.6	07.0	08.5	10.1	08.3	130	98	97	98	N	1	-	0
14	741.4	743.3	743.0	12.6	17.5	12.0	13.5	17.6	08.8	05.0	10.4	09.0	07.1	97	60	68	75	SSE	4	SSE	4
15	745.3	751.2	754.5	07.0	08.8	04.4	06.2	12.5	04.4	04.0	07.3	07.4	06.1	100	88	97	95	SSE	2	NW	2
16	755.0	754.2	752.8	04.6	08.8	12.4	09.6	13.2	04.4	01.6	06.0	08.1	08.8	94	95	81	90	NW	3	SSE	4
17	750.1	753.3	755.5	13.0	16.4	11.2	13.0	17.2	11.0	10.0	10.4	09.8	09.5	92	70	95	86	SSE	3	-	0
18	754.8	750.4	755.6	10.6	12.0	12.0	11.7	13.0	10.0	08.0	09.2	10.2	09.7	96	97	92	95	NW	2	NNW	3
19	755.8	754.5	751.8	09.6	13.2	12.4	11.9	15													

BR. ST. 242

$$H_a = 49 \text{ m } H_b = 50.6 \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$$

Den	S č. d.	Obřadnost N (0-10)					S č. d.	Podkroví R cm	Sedmí pokriven h cm	Rozvoj vremene w
		14	7	14	21	Sred Dnes				
1	8 03	000	00	01.0	09.3	.	.	Δ' 0-700, Δ' 20-30	.	.
2	8 06	040	05	05.0	08.6	.	.	Δ' 0-30	.	.
3	8 04	020	00	02.0	07.9	.	.	Δ' 0-700, Δ' 20-30	.	.
4	8 02	050	02	03.0	07.7	.	.	Δ' 0-700, Δ' 20-30	.	.
5	8 04	06	00	03.3	07.6	.	.	Δ' 0-700, Δ' 20-30	.	.
6	8 04	060	00	03.3	06.0	.	.	Δ' 20-30	.	.
7	8 00	000	00	20.0	08.6	.	.	Δ' 0-30, Δ' 20-30	.	.
8	8 00	100	00	00.0	08.4	.	.	Δ' 0-30, Δ' 20-30	.	.
9	8 00	000	00	00.0	08.2	.	.	Δ' 0-30, Δ' 20-30	.	.
10	8 00	000	00	00.0	08.3	.	.	Δ' 0-30, Δ' 20-30	.	.
11	8 00	000	00	00.0	08.8	.	.	Δ' 0-30, Δ' 20-30	.	.
12	8 00	200	00	00.0	09.0	.	.	Δ' 0-30, Δ' 20-30	.	.
13	8 02	000	00	00.7	08.2	.	.	Δ' 0-30, Δ' 20-30	.	.
14	8 04	040	04	04.0	08.4	.	.	Δ' 0-30, Δ' 20-30	.	.
15	8 04	000	00	01.3	07.8	.	.	Δ' 0-30, Δ' 20-30	.	.
16	8 00	000	00	00.0	08.8	.	.	Δ' 0-30, Δ' 20-30	.	.
17	8 03	040	00	02.3	07.6	.	.	Δ' 0-30, Δ' 20-30	.	.
18	8 00	000	00	00.0	08.8	.	.	Δ' 0-30, Δ' 20-30	.	.
19	8 00	010	00	00.3	07.9	.	.	Δ' 0-30, Δ' 20-30	.	.
20	8 00	000	00	00.0	08.6	.	.	Δ' 0-30, Δ' 20-30	.	.
21	8 00	000	00	00.0	08.4	.	.	Δ' 0-30, Δ' 20-30	.	.
22	8 00	000	00	00.0	08.0	.	.	Δ' 0-30, Δ' 20-30	.	.
23	8 00	000	00	00.0	08.8	.	.	Δ' 0-30, Δ' 20-30	.	.
24	8 01	010	00	00.7	08.8	.	.	Δ' 0-30, Δ' 20-30	.	.
25	8 00	000	00	00.0	08.4	.	.	Δ' 0-30, Δ' 20-30	.	.
26	6 10	100	10	10.0	00.2	.	.	Δ' 0-30, Δ' 20-30	.	.
27	7 100	100	100	10.0	00.0	14.3	.	Δ' 0-30, Δ' 20-30, Δ' 50-50, Δ' 10-10, Δ' 20-20, Δ' 30-30	.	.
28	8 08	100	100	09.3	00.0	22.2	.	Δ' 0-30, Δ' 20-20, Δ' 30-30	.	.
29	8 10	10	05	08.3	00.0	10.9	.	Δ' 0-30, Δ' 20-20, Δ' 30-30	.	.
30	8 03	050	00	02.7	04.2	01.3	.	Δ' 0-30, Δ' 20-20, Δ' 30-30	.	.
MES. MRED.		02.6	02.6	01.5	02.2	211.3	48.7			

TITOGRAD

1978 DECEMBER

1	8 00	040	00	01.3	06.9	.	.	Δ' 20-30	.	.
2	8 08	040	00	04.0	03.0	.	.	Δ' 0-30	.	.
3	8 00	000	06	02.0	08.2	.	.	Δ' 0-30	.	.
4	8 08	10	100	09.3	00.5	.	.	Δ' 0-30	.	.
5	8 100	060	00	05.3	00.5	16.0	.	Δ' 0-30, Δ' 20-30	.	.
6	8 08	020	00	03.3	06.8	.	.	Δ' 0-30	.	.
7	7 10	10	10	10.0	00.0	.	.	Δ' 0-30	.	.
8	7 10	05	05	06.7	04.7	.	.	Δ' 0-30	.	.
9	7 100	100	100	10.0	00.0	00.0	.	Δ' 0-30	.	.
10	8 01	020	10	04.0	07.8	15.0	.	Δ' 0-30	.	.
11	8 01	040	05	03.3	06.9	.	.	Δ' 0-30, Δ' 20-30	.	.
12	8 10	10	100	10.0	00.3	.	.	Δ' 0-30, Δ' 20-30, Δ' 50-50	.	.
13	7 10	10	08	09.3	00.0	22.5	.	Δ' 0-30, Δ' 20-30, Δ' 50-50, Δ' 10-10, Δ' 20-20	.	.
14	8 100	06	100	08.7	04.4	25.8	.	Δ' 0-30, Δ' 20-30, Δ' 50-50, Δ' 10-10, Δ' 20-20	.	.
15	8 07	020	00	03.0	03.0	17.3	.	Δ' 0-30, Δ' 20-30, Δ' 50-50, Δ' 10-10, Δ' 20-20	.	.
16	7 06	100	100	08.7	03.5	08.8	.	Δ' 0-30, Δ' 20-30, Δ' 50-50, Δ' 10-10, Δ' 20-20	.	.
17	8 100	10	10	10.0	00.3	23.7	.	Δ' 0-30, Δ' 20-30, Δ' 50-50, Δ' 10-10, Δ' 20-20	.	.
18	7 100	08	08	09.3	00.0	11.6	.	Δ' 0-30, Δ' 20-30, Δ' 50-50, Δ' 10-10, Δ' 20-20	.	.
19	8 03	08	05	05.3	01.1	15.4	.	Δ' 0-30, Δ' 20-30, Δ' 50-50, Δ' 10-10, Δ' 20-20, Δ' 30-30	.	.
20	8 10	06	06	07.3	01.3	18.3	.	Δ' 0-30, Δ' 20-30, Δ' 50-50, Δ' 10-10, Δ' 20-20, Δ' 30-30	.	.
21	8 07	040	00	03.7	06.4	01.4	.	Δ' 0-30, Δ' 20-30	.	.
22	8 10	070	10	09.0	04.3	.	.	Δ' 0-30	.	.
23	8 10	10	10	10.0	00.3	14.1	.	Δ' 0-30	.	.
24	8 06	010	00	02.3	06.7	.	.	Δ' 0-30, Δ' 20-30	.	.
25	7 10	10	100	10.0	00.4	.	.	Δ' 0-30, Δ' 20-30	.	.
26	7 100	100	00	06.7	03.1	15.4	.	Δ' 0-30	.	.
27	8 02	06	10	06.0	15.6	19.4	.	Δ' 0-30, Δ' 20-30, Δ' 50-50, Δ' 10-10, Δ' 20-20	.	.
28	7 10	100	100K	10.0	00.3	.	.	Δ' 0-30, Δ' 20-30, Δ' 50-50, Δ' 10-10, Δ' 20-20	.	.
29	7 10	10	12	10.0	00.1	27.1	.	Δ' 0-30, Δ' 20-30, Δ' 50-50, Δ' 10-10, Δ' 20-20	.	.
30	8 100	10	05	09.3	02.1	05.2	.	Δ' 0-30, Δ' 20-30, Δ' 50-50, Δ' 10-10, Δ' 20-20	.	.
31	7 10	100	110	10.0	00.1	17.1	.	Δ' 0-30, Δ' 20-30, Δ' 50-50, Δ' 10-10, Δ' 20-20	.	.
MES. MRED.		17.6	06.9	06.5	17.1	82.0	228.7			

$\varphi = 41^{\circ}58' N \lambda = 21^{\circ}39' E$ Gr. $\Delta G = + 1h 27 min.$

BR. ST. 264

5	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodenog pare e mm			Relativna vlažnost v %			Pravac i jačina vetro D, f (0-12)			
	7	14	21	7	14	21	Sred. Dios	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dios	7	14	21	
1	737.7	737.7	738.9	04.9	17.2	09.2	10.1	18.6	03.7	-	06.2	07.4	07.0	96	51	81	76	-	0	N 2	- 0
2	741.5	739.2	739.9	02.2	17.8	11.2	10.6	18.9	02.1	-	05.0	07.6	06.7	93	50	67	70	-	0	NNW 2	NE 1
3	739.3	737.3	736.3	06.9	20.4	14.4	14.0	22.0	05.9	-	06.4	05.6	06.6	85	31	53	56	-	0	SSE 6	SE 3
4	737.7	736.3	737.4	04.6	22.6	11.2	12.4	23.6	03.8	-	05.8	14.9	06.4	91	53	65	70	-	0	S 1	- 0
5	739.5	737.9	739.1	04.2	19.8	13.4	12.7	21.7	03.5	-	06.0	08.3	06.6	97	48	57	67	-	0	NNW 1	SSE 2
6	739.0	737.4	737.0	05.6	15.6	11.9	11.3	17.2	04.6	-	06.2	07.3	07.5	92	55	72	73	NE 2	SE 4	SE 5	
7	738.8	737.7	738.0	06.4	16.8	09.8	10.7	19.2	05.2	-	06.8	06.0	06.1	94	42	67	68	-	0	- 0	NNE 5
8	740.5	740.9	741.2	04.8	08.0	04.0	05.2	09.8	03.4	-	05.5	05.6	05.4	85	70	88	81	NNE 3	WSW 3	NNE 3	
9	740.9	738.6	739.6	02.2	12.8	09.8	08.7	14.6	00.3	-	04.8	05.2	03.6	90	47	59	S 1	ESE 1	NNE 4		
10	742.5	741.3	742.4	06.8	08.0	06.0	06.7	09.8	05.0	-	04.2	04.3	04.2	56	53	60	56	NNW 2	N 5	N 5	
11	743.0	740.8	738.0	05.0	10.4	06.7	07.2	11.0	04.1	-	05.6	04.0	04.0	86	43	55	61	NW 3	SW 3	- 0	
12	734.5	736.5	740.0	06.2	08.0	04.8	06.0	10.4	01.4	-	04.4	02.4	03.1	63	30	48	47	N 4	NW 5	NW 3	
13	743.7	742.9	744.1	-00.6	10.6	02.6	03.8	12.1	-01.4	-	03.6	02.5	03.3	82	36	59	59	NE 2	N 2	NE 1	
14	746.3	743.9	743.9	-01.8	14.6	09.2	07.8	16.1	-04.0	-	03.2	04.0	04.1	80	32	47	53	NE 2	- 0	SE 2	
15	744.2	741.3	739.7	02.0	15.8	12.0	10.5	16.0	00.6	-	04.4	05.0	06.3	84	37	59	60	-	0	SSW 1	SSE 2
16	740.0	739.6	740.3	05.8	17.0	09.2	10.3	19.6	03.9	-	06.1	04.3	03.9	89	30	44	54	ESE 1	SSW 2	SE 2	
17	740.0	736.8	737.1	02.2	19.0	14.2	12.4	20.6	00.8	-	04.3	03.6	04.1	81	22	34	46	-	0	WSW 2	S 3
18	736.8	736.9	739.7	11.4	19.6	11.8	13.7	20.6	10.8	-	04.3	04.2	04.4	43	36	61	47	SE 3	S 4	NE 4	
19	742.1	739.5	737.9	07.4	03.2	04.6	05.5	12.6	03.9	-	04.2	04.1	04.9	80	91	77	83	NNE 3	WNW 2	N 4	
20	740.3	738.4	736.3	04.8	09.4	06.8	07.0	10.4	03.0	-	04.8	03.8	06.0	74	43	61	66	NW 3	-	NNE 2	
21	730.4	727.7	728.5	04.4	12.0	08.0	08.1	12.4	03.0	-	05.2	04.3	06.8	82	59	85	75	-	0	ESE 3	- 0
22	727.0	730.4	735.6	05.0	05.6	04.8	05.1	08.0	04.1	-	05.6	05.5	03.4	86	80	52	73	-	0	NNW 2	NNW 5
23	741.3	741.4	740.5	03.6	06.8	02.4	04.3	10.7	02.2	-	03.1	02.8	03.9	53	33	71	52	N 1	N 2	- 0	
24	737.2	732.2	731.7	00.2	08.6	05.2	04.8	12.6	-01.4	-	04.2	05.9	06.1	89	71	91	84	NNE 1	W 3	NW 1	
25	733.2	734.9	737.8	02.8	07.1	06.0	05.5	07.2	00.4	-	05.5	04.3	04.2	98	56	60	71	-	0	NW 4	W 2
26	740.1	738.1	737.7	05.8	12.0	02.8	05.9	12.6	02.8	-	04.1	04.6	04.4	59	44	78	60	-	0	NNE 3	ESE 1
27	737.9	737.5	742.0	00.8	12.2	07.1	06.8	13.6	-00.8	-	04.4	04.9	04.4	90	46	58	65	SSE 1	N 3	NNW 4	
28	744.7	745.2	746.6	06.0	11.6	04.8	06.8	12.7	04.5	-	04.4	03.8	04.2	62	37	66	55	WNW 2	NNW 3	NE 2	
29	747.2	745.0	744.7	01.0	15.8	06.0	07.2	17.6	-02.9	-	04.1	04.1	04.2	83	31	60	58	-	0	NNE 1	ESE 1
30	743.8	740.6	739.4	01.8	17.4	11.4	10.5	19.4	-01.1	-	04.4	04.2	05.7	83	28	57	56	-	0	- 0	SE 3
31	741.0	738.7	738.5	04.2	17.6	11.0	11.0	17.9	02.2	-	05.6	06.8	06.3	91	45	64	67	-	0	S 2	E 1
MES. RED.	739.7	738.5	739.0	04.1	13.5	08.1	08.5	15.1	02.4	-	05.0	05.3	05.2	81	46	63	63	1.1	2.3	2.3	

1978 APRIL

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1	738.7	734.8	735.2	07.0	15.3	07.8	09.5	16.1	03.2	-	04.3	04.0	05.5	84	46	70	67	NE 1	SSE 3	SE 3
2	733.3	732.6	733.7	07.4	12.0	09.6	09.7	13.8	06.5	-	06.9	06.0	07.5	89	57	83	76	ESE 2	S 1	ESE 1
3	734.8	732.6	731.6	06.7	15.4	10.8	10.9	16.7	01.2	-	06.2	06.3	08.5	84	48	87	73	- 0	S 3	ESE 2
4	728.8	729.0	731.5	09.8	10.8	11.2	10.8	11.8	09.0	-	08.6	09.0	07.7	95	93	77	88	NNE 2	W 1	NW 2
5	735.2	735.0	735.9	09.4	17.3	11.1	12.2	17.4	08.0	-	07.2	08.2	08.0	82	56	81	73	NE 1	N 1	SE 1
6	737.5	738.4	740.4	09.6	13.7	09.4	10.5	16.7	08.2	-	08.3	08.0	07.7	93	68	87	83	- 0	NNE 4	NNE 2
7	741.8	739.9	737.1	06.1	06.8	08.2	07.3	09.5	05.7	-	05.9	06.0	07.3	84	81	90	85	NW 2	- 0	SE 3
8	733.3	732.1	732.7	09.6	16.4	10.8	11.9	16.6	07.6	-	07.7	07.8	08.6	86	70	88	81	ESE 1	WNW 2	ENE 2
9	733.2	734.3	735.9	09.6	16.0	10.8	11.8	16.8	08.0	-	08.7	07.8	06.6	98	57	68	74	- 0	WNW 2	NNE 3
10	738.5	739.9	741.3	08.0	10.8	08.8	09.2	11.6	07.2	-	07.4	07.9	07.5	92	82	89	88	NNE 2	SE 3	SE 2
11	743.5	742.5	743.7	08.6	14.2	09.4	10.4	15.6	07.4	-	07.3	06.2	07.3	87	51	83	74	SE 3	SE 2	E 1
12	744.7	742.2	742.3	09.7	17.8	12.4	13.2	19.6	06.4	-	08.3	09.3	08.2	92	59	76	76	S 2	ESE 2	ESE 2
13	740.6	737.3	735.5	11.4	16.2	11.8	12.8	17.0	08.0	-	08.7	08.6	08.9	86	61	85	77	NE 1	SE 4	SE 6
14	732.0	729.8	730.9	13.6	16.4	12.2	13.6	18.6	11.0	-	08.1	09.3	08.3	69	66	78	71	SE 5	ESE 5	E 1
15	732.1	729.9	732.3	07.8	18.6	11.0	12.1	20.4	04.4	-	07.1	07.0	06.1	90	43	62	65	NW 1	SE 5	ESE 2
16	732.3	732.9	733.6	08.0	16.0	07.8	09.9	17.2	05.6	-	06.8	05.8	07.1	85	42	90	72	NW 1	N 3	W 4
17	736.5	737.2	738.7	07.4	11.6	07.4	08.5	12.6	06.0	-	06.1	06.5	05.9	79	63	77	73	NNE 4	NNE 3	NE 3
18	736.4	737.3	737.5	06.8	12.0	05.4	07.4	12.4	03.4	-	05.3	04.4	04.8	74	42	72	63	N 3	NW 2	N 4
19	737.9	736.8	738.3	04.1	12.2	05.8	07.													

BR. ST. 264

 $H_s = 238 \text{ m}$, $H_b = 233.3 \text{ m}$, $h_t = 2.0 \text{ m}$, $h_r = 1.3 \text{ m}$

Dan	Mj. god.	Oblačnost N (0-10)					Temperatura u m	Podzemna voda mm	Srednji pokrivenost h cm	Razvoj vremena w
		14	7	14	21	Sred. Dneš				
1	7 07	06	00	04.3	-	00.5	.	0° 0-1°, = 5°-6°, = 6-11°		
2	7 04	09	03	05.3	-	.	.	Δ° 0-3°, = 5°-7°		
3	7 09	05	03	05.7	-	.	.	Δ° 0-3°, = 5°-7°, Δ° 5°		
4	7 06	02	01	03.0	-	.	.	Δ° 3°-5°, = 5°-13°		
5	6 07	10	00	05.7	-	.	.	Δ° 3°-5°, = 5°-13°		
6	7 07	10	09	08.7	-	.	.	Δ° 4°-5°, = 5°-13°, 5°-6°		
7	7 09	04	00	04.3	-	00.0	.	5°-11°, Δ° 5°, 15°-20°, 5°-10°		
8	7 10	09	00	06.3	-	07.6	.	5°-10°, 5°-13°		
9	6 07	02	09	06.0	-	01.0	.	5°-10°, = 5°-13°, 17°-18°		
10	7 09	10	10	09.7	-	.	.	Δ° 3°-5°, = 5°-13°		
11	7 09	05	08	07.3	-	00.0	.	Δ° 2°-3°, 5°-10°, 5°-13°	.	
12	7 09	08	08	08.3	-	.	.	Δ° 2°-3°, 5°-10°, 5°-13°	.	
13	7 01	01	00	00.7	-	.	.	5°-10°, 5°-13°	.	
14	7 09	09	00	36.0	-	.	.	5°-10°, 5°-13°	.	
15	7 06	06	10	07.3	-	.	.	5°-10°, 5°-13°	.	
16	8 07	02	01	03.3	-	00.0	.	5°-10°, 5°-13°, 5°-17°	.	
17	7 07	04	03	04.7	-	.	.	5°-10°, 5°-13°, 5°-17°	.	
18	8 06	09	10	08.3	-	.	.	5°-10°, 5°-13°, 5°-17°	.	
19	6 10	10	10	10.0	-	06.4	.	5°-10°, 5°-13°, 5°-17°	.	
20	7 09	08	09	08.7	-	24.8	.	5°-10°, 5°-13°	.	
21	7 10	10	10	10.0	-	.	.	Δ° 0-7°, 5°-10°, 5°-13°, 5°-17°	.	
22	7 10	10	10	10.0	-	09.7	.	5°-10°, 5°-13°, 5°-17°	.	
23	8 04	00	00	01.3	-	02.7	.	5°-10°, 5°-13°, 5°-17°	.	
24	7 04	10	09	07.7	-	.	.	5°-10°, 5°-13°, 5°-17°	.	
25	7 10	10	10	10.0	-	04.9	.	5°-10°, 5°-13°, 5°-17°	.	
26	7 09	06	00	05.0	-	.	.	5°-10°, 5°-13°, 5°-17°	.	
27	7 09	06	05	06.7	-	.	.	5°-10°, 5°-13°, 5°-17°	.	
28	7 10	06	09	05.3	-	.	.	5°-10°, 5°-13°, 5°-17°	.	
29	7 00	01	00	00.3	-	.	.	5°-10°, 5°-13°, 5°-17°	.	
30	7 00	00	00	00.0	-	.	.	5°-10°, 5°-13°, 5°-17°	.	
31	7 02	04	09	05.0	-	.	.	5°-10°, 5°-13°, 5°-17°	.	
MES. RED.		07.0	06.2	04.7	06.0	1	-	57.6		

1	7 09	10	08	09.0	-	.	.	Δ° 1°-3°, = 5°-10°, 5°-13°		
2	7 10	08	09	09.0	-	00.2	.	Δ° 0-5°, = 5°-10°		
3	7 08	10	10	09.3	-	00.0	.	Δ° 0-5°, = 5°-10°, 5°-13°		
4	6 10	10	10	10.0	-	14.9	.	Δ° 0-5°, = 5°-10°, 5°-13°		
5	7 04	06	02	04.0	-	09.5	.	Δ° 0-5°, = 5°-10°, 5°-13°		
6	7 10	10	10	10.0	-	00.5	.	= 5°-10°, 5°-13°, 5°-17°, 5°-20°, 5°-24°		
7	6 10	10	10	10.0	-	07.2	.	5°-10°, 5°-13°, 5°-17°, 5°-20°, 5°-24°		
8	7 10	06	09	08.3	-	04.3	.	5°-10°, 5°-13°, 5°-17°, 5°-20°, 5°-24°		
9	7 10	07	13	09.0	-	09.7	.	5°-10°, 5°-13°, 5°-17°, 5°-20°, 5°-24°		
10	7 10	10	10	10.0	-	09.0	.	5°-10°, 5°-13°, 5°-17°, 5°-20°, 5°-24°		
11	7 09	08	01	36.0	-	02.0	.	Δ° 1°-3°, = 5°-10°, 5°-13°		
12	6 09	01	00	03.3	-	.	.	Δ° 0-5°, = 5°-10°, 5°-13°		
13	7 08	10	10	09.3	-	.	.	Δ° 0-5°, = 5°-10°, 5°-13°, 5°-17°, 5°-20°, 5°-24°		
14	7 06	07	02	05.0	-	00.1	.	Δ° 0-5°, = 5°-10°, 5°-13°, 5°-17°, 5°-20°, 5°-24°		
15	8 01	08	01	03.3	-	01.0	.	Δ° 0-5°, = 5°-10°, 5°-13°, 5°-17°, 5°-20°, 5°-24°		
16	8 10	03	10	27.7	-	01.0	.	5°-10°, 5°-13°, 5°-17°, 5°-20°, 5°-24°		
17	7 09	08	07	26.3	-	06.6	.	5°-10°, 5°-13°, 5°-17°, 5°-20°, 5°-24°		
18	7 29	06	03	06.0	-	.	.	5°-10°, 5°-13°, 5°-17°, 5°-20°, 5°-24°		
19	7 05	04	01	03.3	-	.	.	5°-10°, 5°-13°, 5°-17°, 5°-20°, 5°-24°		
20	7 10	25	06	37.0	-	.	.	5°-10°, 5°-13°, 5°-17°, 5°-20°, 5°-24°		
21	7 24	04	10	06.7	-	.	.	Δ° 0-5°, = 5°-10°, 5°-13°, 5°-17°, 5°-20°, 5°-24°		
22	7 24	10	09	27.7	-	.	.	5°-10°, 5°-13°, 5°-17°, 5°-20°, 5°-24°		
23	8 26	06	23	05.0	-	01.3	.	Δ° 0-5°, = 5°-10°, 5°-13°, 5°-17°, 5°-20°, 5°-24°		
24	7 24	07	13	25.7	-	.	.	Δ° 0-5°, = 5°-10°, 5°-13°, 5°-17°, 5°-20°, 5°-24°		
25	7 24	10	10	08.0	-	00.0	.	Δ° 0-5°, = 5°-10°, 5°-13°, 5°-17°, 5°-20°, 5°-24°		
26	7 12	05	00	05.0	-	00.1	.	5°-10°, 5°-13°, 5°-17°, 5°-20°, 5°-24°, 5°-28°, 5°-32°		
27	7 09	09	09	09.0	-	02.1	.	5°-10°, 5°-13°, 5°-17°, 5°-20°, 5°-24°		
28	8 13	03	04	05.7	-	01.6	.	5°-10°, 5°-13°, 5°-17°, 5°-20°, 5°-24°		
29	8 02	03	04	03.0	-	00.0	.	5°-10°, 5°-13°, 5°-17°, 5°-20°, 5°-24°		
30	7 10	09	08	09.0	-	.	.	5°-10°, 5°-13°, 5°-17°, 5°-20°, 5°-24°		
MES. VRFD.		37.6	37.1	26.4	17.7	-	.	52.1		

1978 MAJ

SKOPJE - PETROVAC

 $\varphi = 41^{\circ}38' N \lambda = 21^{\circ}39' E$ Gr. $\Delta G = + 1h 27 min.$

BR. ST. 264

D S	Vazdušni pritisk P mm			Temperatura vazduha T C°									Napon vodene pare e mm			Relativna vlažnost u %			Pravac i jačina vjetra D, I (0—12)				
	7	14	21	7	14	21	Sred. Dne	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dne	7	14	21			
1	738.2	739.0	732.3	11.4	27.2	23.7	21.5	27.8	09.4	-	08.5	09.2	07.1	84	34	32	50	-	0	SE	4	NNW 2	
2	729.8	727.5	732.7	14.6	20.0	14.4	15.9	23.8	13.9	-	10.7	09.0	06.6	86	51	53	63	S	2	W	3	WSM 3	
3	737.1	736.1	740.5	13.6	23.4	15.0	16.8	23.7	06.9	-	07.2	06.8	06.7	62	31	52	48	SE	1	NNW	4	NNW 3	
4	744.6	743.1	743.2	10.2	20.9	14.8	15.2	21.6	04.6	-	07.6	07.0	07.9	81	58	63	61	-	0	-	0	-	
5	745.6	743.7	743.1	11.4	24.9	18.0	18.1	25.6	05.7	-	07.6	09.6	07.5	75	41	49	55	-	0	ESE	2	SE 3	
6	744.3	740.8	739.8	15.0	23.8	18.2	18.8	24.4	08.9	-	09.0	09.7	07.3	71	44	47	54	W	1	SE	3	S 2	
7	738.8	736.3	735.0	12.6	15.6	14.0	14.1	18.4	11.4	-	09.7	10.9	08.8	89	82	73	81	-	0	S	2	SE 3	
8	735.4	732.3	734.6	12.4	16.0	11.8	13.0	18.4	10.2	-	08.9	09.7	09.2	83	71	89	81	SSE	1	SM	3	ESE 1	
9	735.4	736.3	737.4	10.2	18.2	14.6	14.4	18.4	07.1	-	08.7	09.5	09.9	93	61	80	78	-	0	NNE	3	-	
10	740.0	740.1	740.7	11.8	20.4	14.4	15.3	21.1	07.9	-	09.2	09.8	09.6	89	55	78	74	-	0	SSW	3	NNE 2	
11	741.2	739.9	740.7	11.0	11.8	09.6	10.5	14.6	09.6	-	09.0	09.2	06.0	92	89	67	83	N	2	NNW	1	N 3	
12	739.7	738.0	739.8	08.0	11.4	06.6	08.2	12.6	06.6	-	04.3	05.5	04.6	53	55	63	57	NNW	4	N	5	NNE 5	
13	740.5	738.1	737.4	02.2	16.0	11.0	10.3	16.4	-01.2	-	04.7	05.5	07.3	81	41	74	65	-	0	NE	2	NNE 1	
14	736.4	736.0	738.1	12.0	18.8	14.0	14.7	21.6	06.8	-	07.8	09.1	08.8	74	56	73	68	SE	4	NNE	5	NNE 3	
15	739.6	736.8	736.8	13.0	21.8	15.0	16.2	22.4	10.4	-	09.1	10.5	10.7	81	53	84	73	NNE	1	SSE	2	S 1	
16	738.5	738.0	741.2	14.2	22.4	14.6	16.5	23.0	10.8	-	10.1	06.5	06.9	84	32	55	57	N	1	NNW	2	NNE 3	
17	742.6	742.9	742.2	11.4	22.4	17.1	17.0	23.7	06.0	-	07.8	08.0	10.1	78	40	69	62	-	0	ENE	2	-	
18	743.1	741.3	741.1	14.2	24.4	18.8	19.1	26.0	08.0	-	08.9	08.1	08.7	74	35	53	54	-	0	NE	1	NE 2	
19	741.9	740.5	739.7	16.6	19.8	14.2	16.2	22.0	08.8	-	08.9	10.4	09.4	63	60	78	67	-	0	N	3	-	
20	740.4	737.9	741.0	14.0	26.6	16.8	18.6	27.7	08.4	-	10.7	10.9	09.7	90	42	68	67	-	0	SE	2	SE 2	
21	741.7	741.0	741.9	14.2	24.8	19.4	19.5	25.0	11.0	-	10.6	11.8	13.1	88	50	77	72	SW	1	SE	2	ESE 2	
22	741.6	740.0	736.2	16.4	21.4	19.0	19.0	22.4	09.6	-	10.5	11.5	09.5	75	60	58	64	-	0	S	3	ESE 5	
23	734.9	735.2	737.2	20.4	25.6	17.8	20.4	26.4	12.1	-	07.5	07.6	08.8	42	31	58	44	NNW	3	WSW	4	WSW 1	
24	738.7	737.7	737.9	15.0	24.6	17.0	18.4	26.0	09.9	-	09.0	08.3	07.3	71	36	50	52	-	0	S	3	NNE 2	
25	739.5	737.7	739.4	14.1	21.3	15.0	16.4	24.4	08.3	-	07.8	11.1	09.0	65	59	71	65	-	0	SSW	3	ESE 2	
26	740.5	739.6	739.6	15.2	22.2	18.0	18.4	23.1	10.7	-	09.8	10.0	09.7	75	50	63	63	-	0	NNE	3	-	
27	741.0	739.9	739.8	16.2	18.6	16.0	16.7	21.6	13.4	-	10.9	11.3	10.5	79	70	77	75	-	0	N	2	NE 3	
28	738.8	739.1	739.7	15.6	19.0	14.2	15.3	19.0	12.3	-	10.9	10.0	09.2	94	61	76	77	NW	2	NW	4	NNE 1	
29	738.6	737.0	736.6	14.0	18.6	15.8	16.1	19.0	12.1	-	10.0	08.9	09.1	83	56	68	69	NNW	2	NNW	4	NNW 1	
30	737.4	738.8	740.6	13.1	19.8	14.2	14.3	16.9	11.8	-	10.5	10.3	08.9	92	77	74	81	-	0	WSW	3	N 1	
31	742.4	741.7	743.8	15.4	22.7	13.6	16.3	23.6	09.4	-	10.3	11.1	10.6	78	54	90	74	NNE	1	NNW	2	NNE 1	
MES.	RED.			739.6	738.3	739.0	13.2	20.6	15.4	16.2	22.0	09.0	-	08.9	09.2	08.7	78	52	66	66	0.8	2.7	1.9

1978 JUN

SKOPJE - PETROVAC

1	745.0	743.4	744.5	14.4	24.6	17.2	18.4	24.6	07.8	-	10.3	10.5	10.1	84	45	69	66	-	0	N	2	NE 2
2	744.8	741.8	742.1	12.4	23.4	16.3	17.6	25.0	09.6	-	10.3	11.2	09.7	84	52	70	69	-	0	NN	4	NNE 3
3	741.5	739.8	741.9	15.0	25.6	15.4	17.9	26.2	10.8	-	10.4	08.8	11.3	81	36	86	68	-	0	NNE	3	W 1
4	744.3	743.5	744.3	14.8	25.4	17.4	18.8	25.7	10.0	-	10.8	09.4	10.8	86	38	72	65	-	0	NW	1	S 1
5	745.4	743.3	743.7	14.8	26.8	20.0	20.4	27.6	09.6	-	10.3	08.5	10.6	82	32	60	58	-	0	SW	2	E 1
6	744.6	742.3	743.2	16.2	26.6	18.8	20.1	27.2	11.0	-	10.9	10.6	13.1	79	41	80	67	-	0	NNE	2	SSW 1
7	744.8	743.1	743.4	16.8	26.8	19.2	20.5	27.6	11.6	-	11.9	11.4	12.3	83	43	74	67	-	0	SSE	2	-
8	743.2	740.9	740.6	17.4	26.8	23.0	23.1	29.8	12.4	-	11.6	12.8	11.8	78	43	56	59	-	0	N	1	SE 2
9	741.0	740.8	741.3	19.0	25.4	20.2	21.2	26.4	16.3	-	13.5	13.0	12.7	82	53	71	69	SSW	1	SSW	2	NNE 2
10	742.4	741.0	741.1	19.0	29.2	22.3	23.2	30.8	14.3	-	11.9	11.4	12.5	72	37	62	57	-	0	NE	2	ESE 1
11	742.9	741.7	742.6	21.8	30.2	23.6	24.8	31.8	16.0	-	12.1	12.4	13.3	62	39	61	54	NNE	1	W	2	NNE 6
12	743.2	739.2	736.7	19.8	32.4	24.6	25.4	34.4	16.1	-	14.1	14.3	13.4	62	39	58	60	-	0	SE	3	NNE 2
13	737.1	734.7	735.9	20.8	33.4	22.4	24.8	35.0	16.0	-	12.1	09.5	09.4	65	24	46	45	-	0	ESE	2	E 1
14	736.2	734.5	735.9	19.2	30.4	22.8	23.8	31.7	15.4	-	12.0	10.5	10.7	72	32	51	52	S	1	SW	2	NNE 3
15	737.8	736.1	735.3	17.6	26.4	18.7	20.4	27.0	12.0	-	11.5	11.3	10.4	76	44	64	61	-	0	W	3	NE 2
16	730.3	730.7	733.9	16.2	28.7	19.2	20.8	29.0	11.7	-	10.9	10.4	11.8	79	35	70	61	NNW	1	NNW	3	NNE 4
17	736.9	737.0	737.1	16.8	29.8	23.2	23.3															

BR. ST. 264

$$H_s = 238 \text{ m } H_b = 233.3 \text{ m } h_t = 2.0 \text{ m } h_r = 1.3 \text{ m}$$

1	7	010	06%	06	04.3	-	.	.	$\Delta^{\circ} 0-9^{\circ} = 4-8^{\circ}, T 16^{\circ}-14^{\circ}$
2	7	010	07	01	03.0	-	.	.	$\Delta^{\circ} 0-9^{\circ}$
3	7	040	070	05	05.3	-	.	.	$T 14^{\circ}-15^{\circ}, 6^{\circ} 14^{\circ}-16^{\circ}, R 15^{\circ}-16^{\circ}, 3^{\circ} 15^{\circ}-16^{\circ}, 6^{\circ} 15^{\circ}-16^{\circ}$
4	7	030	030	00	02.0	-	02.4	.	$\Delta^{\circ} 0-9^{\circ} = 3^{\circ}-7^{\circ}$
5	7	030	040	05	04.0	-	.	.	$\Delta^{\circ} 0-9^{\circ}$
6	7	000	08%	04	04.0	-	.	.	$\Delta^{\circ} 0-9^{\circ} 16^{\circ}-24^{\circ} = 4^{\circ} 14^{\circ}-7^{\circ}, T 13^{\circ}-6^{\circ}, 6^{\circ} 14^{\circ}-14^{\circ}$
7	7	030	060	04	04.3	-	00.2	.	$\Delta^{\circ} 0-9^{\circ}, 2^{\circ}-14^{\circ} = 3^{\circ}-9^{\circ}, 5^{\circ} 15^{\circ}-15^{\circ}, T 17^{\circ}-15^{\circ}, 6^{\circ} 17^{\circ}-15^{\circ}$
8	7	010	030	10	04.7	-	00.7	.	$\Delta^{\circ} 0-9^{\circ} = 3^{\circ}-9^{\circ}$
9	7	07	07%	05	06.3	-	.	.	$6^{\circ} 15^{\circ}-12^{\circ}, T 15^{\circ}-14^{\circ}$
10	7	390	010	03	04.3	-	00.0	.	$\Delta^{\circ} 3^{\circ}-6^{\circ}$
11	8	050	070	04	05.3	-	.	.	$\Delta^{\circ} 19^{\circ}-20^{\circ}, 6^{\circ} 15^{\circ}-15^{\circ}, T 25^{\circ}-21^{\circ}$
12	7	360	040	09	06.3	-	.	.	$\Delta^{\circ} 3-6^{\circ}$
13	8	040	030	04	03.7	-	.	.	$\Delta^{\circ} 17-17^{\circ}$
14	7	090	020	06	05.7	-	.	.	$\Delta^{\circ} 6^{\circ}-7^{\circ}, 6^{\circ} 14^{\circ}-5^{\circ}$
15	7	070	09	08	08.0	-	.	.	$\Delta^{\circ} 7^{\circ}-8^{\circ}$
16	7	05	050	02	04.0	-	00.0	.	00 7^{\circ}-8^{\circ}
17	8	000	030	01	01.3	-	.	.	$\Delta^{\circ} 4^{\circ}-6^{\circ}$
18	8	030	030	02	01.7	-	.	.	$\Delta^{\circ} 17^{\circ}-20^{\circ}$
19	8	340	020	05	03.7	-	.	.	$\Delta^{\circ} 17^{\circ}-20^{\circ}$
20	8	020	010	01	00.7	-	.	.	$\Delta^{\circ} 17^{\circ}-20^{\circ}$
21	7	09	060	06	07.0	-	.	.	$\Delta^{\circ} 4^{\circ}-4^{\circ}$
22	8	36	09	02	05.7	-	00.0	.	$\Delta^{\circ} 4^{\circ}-2^{\circ}$
23	7	300	050	02	02.3	-	00.4	.	$\Delta^{\circ} 2^{\circ}-6^{\circ} = 3^{\circ}-10^{\circ}$
24	7	300	020	00	00.7	-	.	.	$\Delta^{\circ} 2^{\circ}-6^{\circ}$
25	8	020	010	00	01.0	-	.	.	$\Delta^{\circ} 2^{\circ}-6^{\circ}$
26	8	000	010	01	00.7	-	.	.	$6^{\circ} 14^{\circ}-5^{\circ}, T 14^{\circ}-5^{\circ}, \Delta^{\circ} 17^{\circ}-15^{\circ}, 6^{\circ} 15^{\circ}-15^{\circ}$
27	7	330	08	05	04.3	-	.	.	$\Delta^{\circ} 3^{\circ}-10^{\circ}, 12^{\circ}-10^{\circ}, 6^{\circ} 14^{\circ}-14^{\circ}$
28	8	36	08	10	08.0	-	00.0	.	$\Delta^{\circ} 9^{\circ}-16^{\circ}$
29	8	38	08	09	08.3	-	00.1	.	$\Delta^{\circ} 9^{\circ}-16^{\circ}$
30	7	050	04	02	05.3	-	.	.	$\Delta^{\circ} 9^{\circ}-16^{\circ}$

1978 JULI

SKOPJE - PETROVAC

$\varphi = 41^{\circ} 58' N$ $\lambda = 21^{\circ} 39' E$ Gr. $\Delta G = + 1h 27 min.$

BR. ST. 264

d	Vazdušni pritisak P mm			Temperatura vazduha T C°								Napon vodenе pare e mm			Relativna vlažnost u %			Pravac i jačina vetro D, f (0-12)				
				7	14	21	7	14	21	Sred Dnes	Max				7	14	21	Sred Dnes	7	14	21	
	7	14	21	7	14	21	Sred Dnes	Max	Min	Min 5 cm	7	8	9	10	11	12	13	14	15	16	17	
1	744.1	742.2	742.7	17.2	28.0	22.8	22.7	30.4	09.3	-	08.9	09.3	09.2	60	33	46	46	-	0	N	2	SE 1
2	743.5	740.5	739.8	19.9	32.2	25.8	25.9	34.2	13.6	-	12.0	11.4	07.9	69	32	32	44	-	0	S	2	N 1
3	739.8	738.4	738.3	21.0	31.4	24.4	25.3	32.1	15.3	-	08.5	08.5	12.3	46	25	54	42	-	0	NE	2	NNE 3
4	740.3	738.3	737.8	19.8	31.0	25.4	25.4	32.8	15.2	-	11.7	10.8	10.3	68	32	42	47	-	0	S	2	E 1
5	740.1	737.3	736.5	21.2	34.4	28.8	28.3	36.6	14.4	-	10.5	08.5	10.1	56	21	34	37	-	0	SE	4	SSE 4
6	740.4	738.4	738.7	24.0	35.4	26.6	28.2	37.6	17.3	-	11.6	11.1	09.7	52	26	37	38	-	0	NNE	2	ESE 2
7	738.2	734.7	734.9	22.2	36.2	25.4	27.3	37.7	18.0	-	10.5	05.2	11.5	52	12	47	37	-	0	W	5	NNE 4
8	738.9	738.4	740.0	21.0	26.4	19.4	21.6	27.0	17.3	-	09.8	08.7	09.3	52	34	55	47	N	3	N	3	N 3
9	741.2	738.3	737.0	17.6	26.6	23.2	22.7	28.4	14.9	-	08.9	08.3	08.7	59	32	41	44	NN	2	W	2	- 0
10	738.2	737.4	737.4	18.4	28.6	23.4	23.5	31.4	12.4	-	11.1	08.7	07.8	70	30	36	45	-	0	SW	2	SE 2
11	740.0	739.0	739.7	19.0	31.8	26.2	25.8	33.6	13.1	-	09.2	08.3	12.0	56	23	47	42	-	0	SW	2	N 2
12	742.4	740.4	740.4	21.0	34.2	29.7	28.7	36.4	16.6	-	11.7	12.4	14.3	63	31	46	47	-	0	WSW	2	ENE 2
13	742.5	740.1	741.5	23.0	34.6	28.2	28.7	36.1	18.0	-	11.7	12.2	13.1	53	30	46	43	-	0	WSW	2	N 4
14	743.4	741.5	741.3	25.0	32.4	25.2	27.0	32.7	20.9	-	13.5	09.8	10.2	57	27	42	42	W	2	NE	4	N 3
15	740.7	736.9	738.8	21.8	32.6	19.0	23.1	33.3	14.6	-	10.7	10.3	15.0	55	28	91	58	NE	1	SSW	3	NNE 1
16	740.6	740.4	740.9	19.4	24.6	19.4	20.7	26.2	17.6	-	14.2	12.8	11.1	84	55	66	68	WWN	3	WSW	2	NNE 3
17	743.5	742.4	742.7	16.0	29.0	22.2	22.4	30.0	10.4	-	09.1	08.0	09.5	67	27	47	47	E	1	NE	3	- 0
18	743.2	740.6	738.6	17.2	32.0	25.4	25.2	34.0	12.1	-	10.9	09.6	08.4	74	26	34	45	-	0	SSW	2	SW 1
19	738.3	733.7	732.2	20.8	34.4	31.4	29.5	37.4	16.0	-	11.2	09.7	06.5	61	24	19	35	-	0	S	3	W 4
20	738.5	737.7	737.8	19.4	26.0	21.8	22.3	31.4	16.4	-	09.3	09.2	09.4	55	36	48	46	NNE	5	NNE	5	N 5
21	738.4	735.8	735.5	18.2	29.4	23.8	23.8	30.2	16.0	-	09.1	09.5	12.3	58	31	56	48	NNE	2	NW	2	SSE 5
22	738.1	741.8	742.8	19.0	18.0	14.0	16.3	20.2	13.6	-	12.1	08.5	07.7	74	55	64	64	N	5	NNW	4	NE 3
23	743.9	741.5	742.3	14.6	23.6	17.0	18.4	24.4	21.4	-	07.1	07.4	06.8	57	34	45	45	-	0	NE	3	N 3
24	742.9	741.4	741.7	15.4	25.6	17.0	18.8	25.6	08.1	-	07.4	06.4	07.5	57	26	52	45	-	0	N	4	W 2
25	742.5	740.7	741.7	18.0	26.0	22.0	22.0	27.0	10.0	-	08.7	06.8	07.7	56	27	39	41	NW	1	N	4	N 3
26	743.2	741.5	741.7	17.6	27.8	21.8	22.3	29.2	10.1	-	08.4	07.5	08.6	56	27	44	42	-	0	WWN	3	N 1
27	742.8	741.4	741.9	17.0	29.8	23.2	23.3	30.7	11.4	-	09.0	09.0	08.2	62	29	38	43	-	0	-	0	NNE 3
28	744.2	743.0	743.7	18.0	29.4	23.8	23.8	31.0	14.6	-	09.5	06.4	08.4	61	21	38	40	-	0	NE	3	NNE 3
29	744.2	742.3	742.7	22.2	27.2	22.4	23.6	28.2	19.0	-	10.0	07.2	09.1	50	27	45	41	N	1	NE	3	NNE 3
30	742.2	740.8	741.1	17.0	27.6	20.0	21.2	28.6	10.4	-	08.5	07.8	07.7	58	28	44	43	NE	1	N	3	NNE 2
31	742.0	739.9	740.5	15.3	28.6	22.4	22.2	30.4	10.4	-	08.2	07.9	06.5	63	27	32	41	S	1	WWN	3	- 0
MES.	FRED.	741.4	739.6	739.8	19.3	29.5	23.3	23.9	31.1	14.1	-	10.1	08.9	09.6	60	30	45	45	0.9	2.8	2.4	

1978 AVGUST

SKOPJE - PETROVAC

1	742.2	741.2	742.2	16.8	32.0	23.8	24.1	32.4	11.2	-	07.9	08.8	09.2	55	25	42	41	-	0	N	3	W 1
2	743.9	741.8	741.4	19.0	30.6	21.6	23.2	32.7	14.6	-	10.0	09.8	14.6	61	30	75	55	-	0	WWN	2	NE 3
3	742.8	740.5	740.1	21.0	33.2	25.8	26.5	33.8	12.9	-	12.8	12.2	11.6	69	32	46	49	-	0	S	2	SE 2
4	742.2	740.0	741.3	21.4	34.5	26.1	27.0	34.8	17.4	-	12.6	11.3	15.3	66	27	60	51	-	0	W	2	ENE 2
5	740.1	738.2	740.2	22.8	32.0	24.8	26.1	33.2	19.4	-	12.8	12.5	11.5	61	35	49	48	-	0	NHE	3	N 4
6	741.2	739.8	740.3	20.4	30.8	23.0	24.3	32.3	16.0	-	13.4	08.8	09.1	75	26	43	48	-	0	N	3	NNE 2
7	740.9	738.5	737.8	20.8	30.0	27.8	27.2	34.6	14.0	-	10.3	08.6	13.6	59	23	49	44	-	0	S	3	SSE 3
8	738.8	734.0	734.7	20.0	37.1	27.4	28.0	37.2	16.8	-	11.5	11.6	11.4	66	25	42	44	NN	1	SE	5	ESE 1
9	736.9	736.9	737.8	25.7	32.4	23.6	26.3	32.4	20.6	-	11.2	08.9	12.7	45	24	58	42	SW	2	NNE	3	N 4
10	738.9	736.6	739.4	18.8	30.6	21.8	23.3	31.2	13.0	-	09.6	11.0	09.1	59	33	47	46	-	0	N	2	W 2
11	740.5	739.3	739.5	19.2	25.6	20.8	21.6	27.0	14.4	-	09.6	09.4	10.2	58	38	55	50	N	1	NNE	4	NNE 5
12	740.7	741.2	742.5	15.8	18.0	17.2	17.1	22.4	14.6	-	12.4	11.6	10.6	92	75	72	80	-	0	WWN	2	WW 3
13	743.7	742.4	742.2	15.1	25.1	19.0	19.6	26.1	10.7	-	07.9	08.5	08.5	61	36	51	49	-	0	W	2	NE 2
14	742.8	740.4	741.6	13.8	26.7	20.8	20.5	28.1	10.8	-	08.8	08.3	09.4	74	32	51	52	-	0	E	2	WWN 2
15	743.9	742.8	742.9	16.2	27.4	21.1	21.5	28.4	11.6	-	10.1	08.5	07.2	73	31	38	47	-	0	SW	3	ESE 1
16	745.5	743.3	743.0	15.2	28.6	21.6	21.8	30.7														

BR. ST. 264

 $H_s = 238 \text{ m } H_b = 233.3 \text{ m } h_t = 2.0 \text{ m } h_r = 1.3 \text{ m}$

Dan	Vreme O. G.	Oblačnost N (0—10)					Indeks zračne vrućine broj	Padavina R mm	Snežni pokrivač h cm	Rezervi vremena w
		14	7	14	21	Sred Dnev				
1	7	000	000	00	00.0	-
2	7	060	020	03	03.7	-
3	8	020	020	00	01.3	-
4	7	000	040	00	01.3	-	.	.	= 39.4°	.
5	7	000	000	00	00.0	-
6	8	000	000	04	01.3	-
7	7	060	050	01	04.0	-
8	8	020	030	01	02.0	-	.	.	P 100°-H 0°	.
9	7	060	010	03	03.3	-
10	7	000	010	00	00.3	-
11	8	000	010	00	00.3	-
12	7	000	020	00	00.7	-
13	7	000	010	02	01.0	-	.	.	P 100°-H 0°	.
14	7	040	020	01	02.3	-
15	8	000	040	04	02.7	-	.	.	0° 14°-15°, T 15°-17°, 3 15°-16°, P 15°-16°, R 15°-16°	.
16	7	10	090	00	06.3	-	05.8	.	P 0°-12°, 5°-14°, 0°-14°, = 4°-14°, H 0°-10°	.
17	7	000	010	00	00.3	-	.	.	0° 10°-10°, = 4°-9°	.
18	7	000	000	00	00.0	-	.	.	P 10°-3°	.
19	7	020	020	00	01.3	-
20	8	05	030	04	04.0	-
21	7	06	010	07	04.7	-	.	.	P 0°-10°	.
22	8	04	08	01	04.3	-
23	7	030	020	00	01.7	-
24	7	020	050	02	03.0	-
25	7	000	040	04	02.7	-
26	7	000	020	00	00.7	-
27	7	000	040	02	02.0	-
28	7	09	040	05	06.0	-
29	7	08	09	04	07.0	-
30	7	030	060	01	03.3	-
31	7	000	030	00	01.0	-
MES. VRFD.		02.5	02.9	01.6	02.3	-	05.8			

1	8	010	020	00	01.0	-
2	7	020	020	01	01.7	-
3	7	000	010	00	00.3	-
4	7	000	040	08	04.0	-	.	.	P 0°-17°, T 10°-10°, L 21°-23°	.
5	8	010	030	10	04.7	-	.	.	P 0°-17°	.
6	7	000	010	00	00.3	-
7	7	000	000	00	00.0	-
8	7	060	020	00	02.7	-
9	8	000	020	00	00.7	-
10	8	030	030	00	02.0	-
11	7	000	08	09	05.7	-	.	.	0° 17°-18°, L 17°-24°, L 20°-20°, T 20°-21°, R 21°-21°, 3 21°-21°	.
12	7	10	100	03	07.7	-	1.0.0	.	0° 0°-20°, 4°-14°, 4°-14°	.
13	7	000	040	01	01.7	-	0.0.4	.	L 0°-10°, = 14°-9°	.
14	7	030	050	01	03.0	-
15	7	000	000	00	00.0	-
16	7	000	010	00	00.3	-
17	7	000	020	00	00.7	-
18	7	000	010	00	00.3	-
19	7	09	020	06	05.7	-
20	7	09	010	01	03.7	-
21	7	040	050	00	03.0	-
22	7	030	010	01	00.7	-
23	7	15	020	03	02.3	-
24	7	010	020	00	01.0	-
25	7	080	030	00	03.7	-
26	7	18	020	09	06.3	-
27	7	050	000	00	00.0	-
28	7	100	08	08	05.3	-	.	.	0° 15°-6°	.
29	7	040	050	02	03.7	-	1.0.0	.	.	.
30	7	090	060	02	02.7	-	.	.	0° 14°-12°, 10°-24°, T 10°-25°, R 15°-21°, L 21°-21°	.
31	7	18	19	190R	19.0	-
MES. VRFD.		12.5	03.1	02.3	02.7	-	18.4			

1978 SEPTEMBAR

SKOPJE - PETROVAC

 $\varphi = 41^{\circ}58' N \lambda = 21^{\circ}39' E$ Gr. $\Delta G = + 1h 27 min.$

BR. ST. 264

D	Vazdušni pritisk P mm			Temperatura vazduha T °C								Napon vodenе pare e mm			Relativna vlažnost v %			Pravac i jačina veta D, I (0-12)					
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm		7	14	21	7	14	21	Sred. Dnes	7	14	21		
1	733.9	735.5	737.7	12.4	20.4	13.2	14.8	21.4	10.1	-	08.0	06.1	07.2	74	34	63	57	-	0	NW	4	NE	3
2	740.0	737.9	738.7	09.4	21.3	16.0	15.7	23.1	05.1	-	07.1	07.1	09.0	81	37	66	61	-	0	NE	2	NNW	3
3	739.7	738.6	739.4	13.2	25.3	17.6	16.4	25.7	10.8	-	09.4	09.0	08.9	83	37	59	60	-	0	N	1	S	1
4	740.4	738.6	738.3	12.2	26.6	21.0	20.3	26.1	08.6	-	09.0	08.8	09.8	85	32	52	57	-	0	NNE	1	SE	1
5	739.6	738.7	738.0	15.0	20.2	16.8	17.2	21.0	11.4	-	10.2	12.1	13.5	80	68	94	81	-	0	WNW	2	NE	2
6	737.2	734.7	734.3	16.2	25.0	19.4	20.0	25.5	14.4	-	12.7	13.8	14.2	92	58	84	78	N	1	NW	3	NE	3
7	733.0	731.1	732.5	16.0	26.4	17.2	19.2	27.1	14.6	-	13.6	14.8	12.8	100	57	87	81	S	1	NW	2	SW	1
8	733.2	735.4	737.6	17.2	20.0	16.4	17.5	21.2	15.9	-	12.6	11.1	09.8	86	63	70	73	NNW	3	N	3	N	2
9	738.7	739.3	740.6	16.1	17.8	15.4	16.2	18.2	13.3	-	08.7	07.6	09.5	63	50	73	62	NNE	2	WNW	4	NNE	1
10	741.2	740.6	741.7	16.2	22.4	18.2	18.8	23.6	14.0	-	09.1	08.6	10.7	66	42	68	59	-	0	N	3	-	0
11	741.3	741.0	740.1	17.2	25.6	18.2	19.8	26.6	15.1	-	19.6	10.5	12.5	72	43	80	65	-	0	NE	2	-	0
12	738.4	734.3	731.8	14.6	28.0	19.8	20.6	28.1	12.3	-	11.6	12.9	11.7	92	46	68	69	-	0	S	1	NNE	5
13	735.8	736.1	738.8	10.2	13.2	15.4	13.6	19.8	06.1	-	08.0	08.7	07.6	86	77	58	74	NW	2	N	5	NNW	5
14	741.9	743.2	742.8	13.9	17.4	16.2	15.9	19.6	12.2	-	08.2	10.3	10.1	69	69	73	70	WSM	3	WSM	3	NNM	1
15	741.2	740.8	741.8	13.6	20.2	16.8	16.9	20.5	10.5	-	09.7	10.7	10.8	83	60	76	73	-	0	W	1	-	0
16	742.9	743.5	744.7	16.0	21.4	14.0	16.4	22.7	14.0	-	10.5	08.5	09.8	77	45	81	68	-	0	N	3	NNE	3
17	745.5	744.7	746.3	14.4	21.6	14.4	16.3	22.1	10.7	-	09.1	07.8	08.1	74	40	66	60	NNE	2	ESE	4	ESE	1
18	746.0	743.8	742.9	10.8	23.8	14.4	15.9	25.6	06.2	-	08.1	10.2	09.8	84	46	80	70	-	0	-	0	-	0
19	742.6	740.0	739.1	11.0	25.6	16.6	17.5	26.4	07.8	-	08.7	08.8	09.9	88	36	70	65	-	0	SSE	3	SSE	1
20	739.3	740.3	744.1	12.2	16.2	11.6	12.9	20.0	09.3	-	09.5	08.4	07.5	89	61	73	74	-	0	N	4	N	3
21	745.5	745.3	745.3	10.0	14.8	11.6	12.0	15.8	07.1	-	07.0	05.7	05.2	77	45	51	58	NNW	2	N	4	NW	4
22	746.7	744.6	744.7	08.0	16.6	10.0	11.2	17.1	04.2	-	06.8	05.9	07.0	85	42	77	68	N	2	N	3	NE	2
23	743.6	741.3	741.7	08.3	19.2	14.6	13.7	20.4	03.2	-	06.5	07.2	09.2	90	43	74	69	-	0	SW	1	-	0
24	743.6	744.6	746.3	16.0	21.2	15.8	17.2	21.4	13.2	-	10.2	09.2	08.9	75	49	66	63	-	0	NNE	3	-	0
25	746.2	746.7	746.8	10.2	25.2	15.9	16.8	25.7	07.6	-	08.7	10.2	10.9	93	42	81	72	S	1	W	1	-	0
26	747.0	744.3	743.6	11.6	26.8	15.8	17.5	28.0	08.6	-	09.3	09.4	09.8	91	35	73	66	-	0	ENE	1	-	0
27	741.8	737.9	737.5	12.2	26.0	19.0	19.1	26.8	08.4	-	09.2	11.9	14.1	87	47	86	73	-	0	WNW	1	NE	1
28	736.6	733.5	732.7	13.6	23.6	15.4	17.1	25.0	12.9	-	11.3	11.5	11.0	96	53	84	78	-	0	NW	3	WNW	5
29	736.8	738.8	740.7	09.4	18.2	09.6	11.7	18.3	09.2	-	08.2	05.6	06.8	93	35	76	68	WSM	3	NNW	4	-	0
30	744.9	742.4	741.7	07.0	21.4	13.0	13.6	22.7	03.2	-	06.7	07.5	07.9	89	39	71	66	-	0	SE	2	-	0

MES.
VRED. 740.9 739.9 740.4 12.8 21.7 15.6 16.5 22.9 10.1 - 09.3 09.3 09.8 83 48 73 68 0.7 2.5 1.6

1	741.2	739.6	740.3	09.8	19.2	16.0	15.3	20.4	07.0	-	08.2	09.9	10.7	90	59	79	76	NNE	1	WNW	2	-	0
2	741.8	743.1	742.3	12.6	20.3	16.0	16.2	22.0	11.0	-	10.0	10.8	11.5	91	62	84	79	W	1	WNW	1	-	0
3	745.3	743.0	742.5	12.4	27.4	20.6	20.3	28.0	10.2	-	10.3	11.1	11.1	96	40	61	66	-	0	SE	3	ESE	2
4	741.5	739.1	739.9	13.6	26.7	18.9	19.5	27.6	12.2	-	10.0	09.4	10.1	85	36	61	61	-	0	SE	4	NNE	3
5	740.7	739.5	742.3	10.2	22.9	14.2	15.4	24.3	09.8	-	08.7	09.1	07.3	93	43	60	65	-	0	N	4	NNE	4
6	745.7	745.8	746.3	12.0	16.0	11.2	12.6	16.8	10.8	-	06.9	06.2	06.7	66	46	67	60	S	1	SW	1	-	0
7	747.5	746.6	748.2	08.4	18.3	10.6	12.0	19.0	05.6	-	06.8	08.1	07.6	82	51	79	71	S	1	N	3	-	0
8	749.2	747.4	747.0	07.6	20.9	14.4	14.1	21.8	05.0	-	06.8	08.0	08.1	87	46	66	66	-	0	WNW	1	-	0
9	747.2	746.4	746.7	08.0	21.6	13.6	14.2	22.4	05.3	-	07.0	08.2	07.9	87	42	67	65	-	0	ESE	1	ENE	1
10	748.2	746.7	747.9	09.8	21.4	11.4	13.5	22.4	07.3	-	07.6	08.8	07.8	83	46	78	69	-	0	S	1	-	0
11	749.2	747.9	748.4	08.0	23.0	15.2	15.4	23.4	06.0	-	07.4	09.3	09.4	92	44	73	70	-	0	S	1	S	1
12	749.5	747.9	748.9	10.0	21.8	12.4	14.2	22.1	08.4	-	08.5	09.9	08.5	93	51	78	74	NE	1	W	1	-	0
13	750.3	748.5	748.1	06.4	21.3	11.6	12.7	22.4	06.0	-	06.2	08.3	07.3	86	44	71	67	-	0	E	2	ESE	1
14	748.6	746.2	746.4	07.4	18.4	08.8	10.9	19.1	05.2	-	07.1	08.5	07.4	92	54	88	78	-	0	-	0	ESE	1
15	746.1	743.6	743.4	03.6	19.2	08.8	10.1	20.2	02.1	-	05.4	07.6	07.2	91	46	85	74	-	0	-	0	-	0
16	743.1	741.1	740.4	03.2	18.8	08.8	09.9	19.6	02.2	-	05.6	07.1	07.0	97	44	83	75	-	0	WSM			

BR. ST. 264

 $H_s = 238 \text{ m } H_b = 233.3 \text{ m } h_t = 2.0 \text{ m } h_x = 1.3 \text{ m}$

D	M	G	Oblačnost N (0-10)					Padavina R mm	Snežni pokriveni h cm	Rezervi vremena w
			14	7	14	21	Sred Dnes			
1	8	10	02	03	04.0	-	15.2	.	T 0°-1°, 0°-3°-4°	
2	7	310	040	10	05.0	-	.	.	D 0°-7°, 0°-2°-10°	
3	7	320	030	00	01.7	-	00.0	.	D 1°-3°-5°	
4	7	000	030	00	01.0	-	.	.	D 1°-3°-5°	
5	7	09	100	10	09.7	-	.	.	D 0°-3°-5°, 0°-10°-10°	
6	6	00	08	09	05.7	-	05.4	.	= 0°-10°, 0°-2°-5°-10°-14°; T 0°-5°	
7	7	04	06	100	06.7	-	07.3	.	0°-10°, 0°-2°-5°-10°-14°; = 5°-6°, = 6°-9°, T 0°-10°; R 10°-10	
8	7	10	09	09	09.3	-	15.6	.	0°-10°, 0°-2°-5°-10°-14°	
9	7	08	09	10	09.0	-	00.0	.	.	
10	7	10	10	10	10.0	-	.	.	.	
11	7	09	040	00	04.3	-	.	.	.	
12	7	010	230	120	04.7	-	.	.	D 1°-0°-5°, 0°-2°-5°-10°-14°	
13	7	130	100	08	09.3	-	15.7	.	0°-10°, 0°-2°-5°-10°-14°; = 5°-6°, = 6°-9°, T 0°-10°; R 10°-10	
14	7	10	09	09	09.3	-	01.3	.	0°-10°, 0°-2°-5°-10°-14°	
15	7	05	29	10	08.0	-	00.4	.	D 0°-7°, = 5°-10°, 0°-10°	
16	7	06	060	00	04.0	-	00.5	.	.	
17	7	05	040	00	03.0	-	.	.	D 0°-7°	
18	7	000	000	00	00.0	-	.	.	D 0°-10°, 0°-2°-5°-10°-14°	
19	7	030	010	01	00.3	-	.	.	D 0°-8°, = 5°-10°, 0°-10°-14°	
20	7	010	10	100	07.0	-	.	.	D 0°-8°, = 5°-10°, 0°-10°-14°	
21	7	10	06	00	05.3	-	05.4	.	0°-4°	
22	7	010	05	05	03.7	-	.	.	D 0°-7°	
23	7	01	090	100	06.7	-	.	.	D 1°-9°, = 15°-18°, 0°-10°-14°	
24	7	06	09	04	06.3	-	00.0	.	D 0°-6°, = 7°-10°	
25	7	09	010	00	03.3	-	.	.	D 0°-6°, = 7°-10°	
26	8	030	010	00	01.3	-	.	.	D 0°-9°, = 5°-8°	
27	7	00	03	10	04.3	-	.	.	D 1°-8°, = 6°-10°, 0°-10°-14°; T 0°-10°, 0°-10°-14°	
28	7	03	09R	100R	07.3	-	01.3	.	D 0°-8°, = 5°-10°, 0°-10°-14°	
29	8	100	02	00	04.0	-	05.2	.	D 0°-8°, = 5°-10°, 0°-10°-14°	
30	8	30	03	00	01.0	-	00.0	.	D 0°-8°, = 5°-10°, = 5°-6°	
MES.										
MED.			04.8	05.6	05.1	05.2	1	-	76.5	

1	7	08	070	07	07.3	-	00.0	.	D 0°-8°, = 5°-10°, 0°-10°-14°	
2	7	07	10	06	07.7	-	.	.	D 0°-8°, = 5°-10°, 0°-10°-14°	
3	7	020	020	03	02.3	-	.	.	D 0°-8°, = 5°-10°, 0°-10°-14°	
4	7	010	07	00	02.7	-	.	.	D 0°-8°, = 5°-10°, 0°-10°-14°	
5	7	040	060	10	06.7	-	.	.	D 0°-8°, = 5°-10°, 0°-10°-14°	
6	7	10	060	00	05.3	-	.	.	.	
7	7	010	030	00	01.3	-	.	.	D 0°-8°, = 5°-10°	
8	7	39	010	05	05.0	-	.	.	D 0°-8°, = 5°-10°	
9	7	000	010	01	00.7	-	.	.	D 0°-8°, = 5°-10°	
10	7	000	010	00	00.3	-	.	.	D 0°-8°, = 5°-10°	
11	7	000	000	00	00.0	-	.	.	D 0°-8°, = 5°-10°	
12	6	37	020	00	03.0	-	.	.	D 0°-8°, = 5°-10°	
13	7	00	010	00	00.3	-	.	.	D 0°-8°, = 5°-10°	
14	6	10	020	03	04.0	-	.	.	D 0°-8°, = 5°-10°, 0°-10°-14°	
15	7	000	000	00	00.0	-	.	.	D 0°-8°, = 5°-10°	
16	6	000	000	00	00.0	-	.	.	D 0°-9°, = 5°-8°	
17	7	020	020	07	03.7	-	.	.	D 0°-9°, = 5°-8°, 0°-10°-14°	
18	7	05	09	09	07.7	-	00.0	.	D 0°-10°, = 5°-10°	
19	6	34	09	10	07.7	-	.	.	D 0°-10°, = 5°-10°	
20	6	10	070	100	09.0	-	00.0	.	D 0°-8°, = 5°-10°	
21	7	09	10	10	09.7	-	04.6	.	= 3°-9°, 0°-6°-12°, 0°-10°-14°; P 0°-10°-14°	
22	8	340	020	03	02.0	-	11.1	.	P 0°-10°	
23	7	330	09	08	06.7	-	.	.	D 0°-9°	
24	7	14	020	00	02.0	-	.	.	D 0°-9°	
25	7	000	030	01	01.0	-	.	.	D 0°-7°, = 4°-7°	
26	6	340	080	10	07.3	-	.	.	D 0°-8°-8°, = 5°-10°, P 0°-10°-14°	
27	7	13	100	170	10.0	-	.	.	D 0°-8°	
28	7	100	100	100	10.0	-	01.6	.	D 0°-10°, P 0°-10°-14°	
29	7	10	010	00	03.7	-	03.2	.	D 0°-3°-3-4°	
30	7	10	10	10	10.0	-	.	.	D 0°-8°	
31	5	09	09	10	09.3	-	.	.	= 0°-8°-Kv	
MES.										
MED.			34.9	34.8	34.4	34.7	-	23.5		

$\varphi = 41^{\circ}58' N$ $\lambda = 21^{\circ}39' E$ Gr. $\Delta G = + 1h 27 min.$

BR. ST. 264

d	Vazdušni pritisk P mm			Temperatura vazduha T C°								Napon vodenе pare e mm			Relativna vlažnost u %			Pravac i jačina veta D, f (0-12)				
	7	14	21	7	14	21	Sred. Dnes	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dnes	7	14	21		
1	752.3	751.9	752.9	04.2	14.2	05.0	07.1	15.0	02.4	-	05.8	06.0	05.8	94	49	88	77	-	0	-	0	ENE 1
2	753.1	751.2	751.1	02.2	11.0	08.2	07.4	11.0	00.2	-	04.8	05.3	07.3	90	54	90	78	-	0	-	0	-
3	750.5	750.1	750.3	06.6	12.6	07.0	08.3	12.6	06.3	-	05.9	05.7	05.7	81	53	76	70	NE	3	NNN	3	-
4	751.3	749.9	750.7	01.8	11.7	02.2	04.5	12.6	00.7	-	04.7	05.4	04.5	90	52	84	75	NE	1	-	0	-
5	751.1	751.5	752.2	02.2	08.4	04.2	04.8	08.6	-01.0	-	05.0	05.4	05.3	93	66	85	81	-	0	-	0	NNW 2
6	753.5	751.9	752.6	-00.8	11.0	04.2	04.7	11.0	-01.1	-	04.1	05.1	05.3	96	52	85	78	-	0	NNE	2	NW 2
7	751.9	751.3	753.7	04.4	09.4	03.0	05.0	09.4	-01.4	-	04.8	04.5	04.6	77	51	84	71	NNE	1	NE	4	NNE 3
8	754.6	753.5	753.4	03.2	05.6	02.2	03.3	05.8	-00.4	-	04.5	04.6	04.3	78	67	81	75	-	0	-	0	-
9	753.6	753.3	753.5	02.8	04.8	04.4	04.1	04.8	01.6	-	04.9	04.6	05.0	87	71	79	79	-	0	WNW	2	-
10	753.2	751.6	751.9	02.2	04.6	-02.0	00.7	04.8	-02.7	-	04.5	04.0	03.5	84	63	88	78	NNE	2	W	2	-
11	751.6	750.2	751.2	00.2	01.0	01.4	01.0	01.4	-05.1	-	04.5	04.4	04.6	96	90	90	92	-	0	NNW	1	-
12	751.6	750.6	751.4	00.2	02.7	-03.0	-00.8	04.2	-04.0	-	04.0	05.6	03.1	86	100	83	90	NE	2	NNW	2	-
13	752.5	751.7	751.9	-02.4	-00.4	-00.6	-01.0	00.4	-05.0	-	03.7	04.1	04.0	96	93	92	94	NE	2	-	0	-
14	753.6	754.0	755.3	-00.2	04.0	00.0	01.0	04.4	-01.4	-	03.9	03.9	03.6	86	65	79	77	NNW	2	W	1	NNW 2
15	757.0	756.3	755.9	00.6	02.4	-03.6	-01.1	03.3	-03.6	-	03.8	03.9	03.2	79	71	91	90	-	0	NNW	1	-
16	757.4	752.0	751.0	-03.2	-01.2	-02.4	-02.3	-01.0	-0.4.1	-	03.4	04.0	03.6	93	96	94	94	-	0	-	0	-
17	750.1	748.6	751.3	-02.2	11.4	02.0	03.3	11.4	-03.2	-	03.7	04.7	04.1	94	51	77	73	-	0	NNE	3	NNE 4
18	753.4	752.6	753.7	01.2	0.6	-01.0	01.3	06.7	-01.2	-	03.5	04.2	03.8	70	60	89	73	N	2	NNE	3	NE 1
19	754.1	752.7	752.2	-01.0	01.6	01.6	01.0	02.1	-04.4	-	03.8	04.1	04.3	89	80	83	84	-	0	-	0	NNE 1
20	751.1	749.9	750.3	-00.2	00.7	-00.8	-00.3	01.6	-00.9	-	04.2	04.2	04.2	93	88	96	92	-	0	WSW	1	-
21	750.7	750.4	752.1	-01.6	02.6	-03.6	-01.4	03.6	-03.8	-	03.9	04.1	03.3	96	75	92	88	NNE	2	S	1	-
22	754.9	754.2	756.2	-06.1	03.0	02.4	00.3	04.2	-07.4	-	02.6	04.8	04.4	94	84	81	86	-	0	-	0	NW 2
23	756.3	754.2	754.8	-00.6	08.2	01.4	02.6	08.6	-02.1	-	04.2	04.9	04.5	96	61	88	82	-	0	-	0	-
24	754.3	752.7	751.8	-04.8	11.4	-00.4	01.5	12.7	-05.4	-	02.9	05.3	04.0	91	53	89	78	-	0	N	2	-
25	750.1	747.0	746.0	-04.8	00.6	-02.4	-02.3	00.6	-06.3	-	03.1	04.3	03.8	95	89	100	95	-	0	-	0	-
26	745.5	743.0	742.9	-03.2	-00.8	-04.4	-03.2	00.1	-04.7	-	03.4	04.2	03.2	93	96	95	95	-	0	-	0	-
27	739.5	736.0	732.8	-02.6	04.4	02.8	01.9	05.4	-04.4	-	03.5	06.1	05.4	94	97	97	96	-	0	-	0	NW 1
28	727.8	726.5	727.6	08.4	10.2	03.6	06.5	12.6	00.1	-	06.8	07.6	05.5	82	81	92	85	SE	1	NNW	3	NNE 2
29	727.7	724.2	723.8	00.8	04.8	01.4	02.1	06.1	00.4	-	04.9	06.1	04.9	100	94	97	97	-	0	-	0	W 3
30	727.3	729.9	734.0	00.8	02.4	02.2	01.9	03.4	00.0	-	04.7	04.9	04.0	97	90	74	87	E	1	NNE	2	SE 2
MES.	VRED.	749.7	748.5	749.0	00.2	05.6	01.2	02.0	06.2	-02.1	-	04.2	04.9	04.4	90	73	87	83	0.6	1.1	0.9	0.9

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SKOPJE - PETROVAC

1	738.9	740.0	740.6	-02.8	04.4	-02.6	-00.7	03.6	-03.6	-	03.1	03.9	03.2	83	62	84	76	-	0	NE	1	0
2	741.8	741.8	743.1	-04.4	02.2	-00.8	-01.0	05.4	-04.0	-	02.8	04.3	04.3	87	81	99	89	-	0	-	0	SSE 2
3	743.6	742.7	742.2	-00.2	03.4	01.4	02.0	05.8	-02.0	-	04.0	04.1	04.6	89	61	90	80	-	0	NE	1	E 1
4	741.1	739.7	739.6	00.0	04.6	02.4	02.4	05.2	-00.4	-	04.1	04.2	04.4	89	66	81	79	-	0	-	0	-
5	738.4	740.1	743.2	00.2	00.7	-00.6	-00.1	03.3	-01.0	-	04.5	04.4	03.4	96	91	78	88	-	0	N	1	-
6	745.6	745.8	746.7	-03.6	-01.0	-02.0	-02.2	-00.6	-04.0	-	03.1	03.0	02.7	88	70	68	75	NM	2	NM	1	NM 2
7	746.3	745.4	745.7	-04.6	-02.8	-04.0	-03.9	-01.9	-05.6	-	02.4	02.8	02.4	87	79	74	76	NE	3	-	0	-
8	745.6	745.2	746.1	-04.0	00.6	-02.0	-01.9	01.2	-05.4	-	02.7	03.6	03.3	80	76	84	80	-	0	-	0	-
9	745.1	743.4	743.0	-01.4	01.0	00.4	00.1	01.5	-02.0	-	03.8	04.3	04.6	91	86	96	91	-	0	-	0	-
10	744.1	743.6	744.3	00.0	03.6	01.2	01.5	03.6	-00.4	-	04.4	05.0	04.7	96	85	93	91	-	0	-	0	-
11	744.5	743.5	743.7	-00.8	01.8	-00.4	00.1	03.0	-01.7	-	04.2	04.9	04.1	96	93	93	94	-	0	-	0	-
12	742.2	740.4	738.3	-00.4	01.8	02.0	01.4	02.3	-02.0	-	04.5	04.9	04.9	100	93	93	95	-	0	W	1	-
13	735.6	733.5	733.7	02.0	04.8	05.4	04.4	05.6	01.4	-	05.1	05.7	06.3	97	88	94	93	-	0	ESE	1	-
14	728.4	726.3	726.9	04.8	09.0	06.8	06.9	10.4	04.0	-	06.3	08.0	06.2	97	93	84	91	-	0	NE	2	ESE 1
15	728.9	731.4	736.3	07.2	10.2	02.4	05.6	10.5	02.2	-	06.4	06.5	04.9	84	70	90	81	NE	1	-	0	-
16	738.9	737.7	736.7	-01.8	04.8	01.2	01.4	03.6	-02.2	-	03.9	05.7	04.8	98	88	97	94	-	0	-	0	-
17	733.6	735.0	738.5	04.3	10.1	10.6	10.9	10.6	-01.0	-	05.4	07.2	08.2	87	46	86	73	NE	3	W	5	SSW 1
18	739.9	739.4	742.1	08.4	10.4	07.8	09.6	10.6	07.8	-	07.4	08.2	06.5	90	69	82	80	E	1	-		

BR. ST. 264

 $H_s = 238 \text{ m } H_b = 233.3 \text{ m } h_t = 2.0 \text{ m } h_r = 1.3 \text{ m}$

Dan	Mj.	Oblačnost N (0-10)					Intenzitet sunca	Podzemna voda mm	Snežni pokrivač h cm	Razvoj vremena w
		14	7	14	21	Sred Dnev				
1	7	10	02	02	04.7	-	.	.	.	$\equiv 0^{\circ} 4^{\circ}, \Delta 1^{\circ} 15^{\circ} 24^{\circ}$
2	6	07	10	10	09.0	-	.	.	.	$\equiv 0^{\circ} 3^{\circ}, \Delta 1^{\circ} 34^{\circ} 0^{\circ}, \equiv 4^{\circ} 19^{\circ}$
3	7	10	08	06	08.0	-	.	.	.	$\equiv 0^{\circ} 2^{\circ}, \Delta 1^{\circ} 34^{\circ} 24^{\circ}$
4	7	00	00	03	01.0	-	.	.	.	$\equiv 0^{\circ} 1^{\circ}, \Delta 1^{\circ} 34^{\circ} 0^{\circ}, \equiv 4^{\circ} 10^{\circ}$
5	7	10	10	06	08.7	-	.	.	.	$\equiv 0^{\circ} 1^{\circ}, \Delta 1^{\circ} 34^{\circ} 24^{\circ}, \equiv 4^{\circ} 15^{\circ}$
6	7	03	03	00	02.0	-	.	.	.	$\equiv 0^{\circ} 7^{\circ}, \equiv 5^{\circ} 24^{\circ}$
7	7	10	05	00	05.0	-	.	.	.	$\equiv 0^{\circ} 8^{\circ}, \equiv 5^{\circ} 24^{\circ}$
8	6	10	10	09	09.7	-	.	.	.	$\equiv 0^{\circ} 2^{\circ}, \equiv 5^{\circ} 24^{\circ}$
9	5	10	10	10	10.0	-	.	.	.	$\equiv 0^{\circ} 2^{\circ}, \Delta 1^{\circ} 34^{\circ} 24^{\circ}$
10	6	10	04	00	04.7	-	.	.	.	$\equiv 0^{\circ} 2^{\circ}, \Delta 1^{\circ} 34^{\circ} 24^{\circ}$
11	4	10	10	10	10.0	-	00.0	.	.	$\equiv 0^{\circ} 2^{\circ}, \Delta 1^{\circ} 34^{\circ} 24^{\circ}, \Delta 1^{\circ} 40^{\circ} 0^{\circ}$
12	6	10	03	00	04.3	-	.	.	.	$\equiv 0^{\circ} 2^{\circ}, \Delta 1^{\circ} 34^{\circ} 24^{\circ}$
13	5	10	10	10	10.0	-	00.0	.	.	$\equiv 0^{\circ} 2^{\circ}, \Delta 1^{\circ} 34^{\circ} 24^{\circ}, \equiv 6^{\circ} 24^{\circ}$
14	5	10	04	00	04.7	-	00.0	.	.	$\equiv 0^{\circ} 2^{\circ}, \Delta 1^{\circ} 34^{\circ} 24^{\circ}$
15	6	10	05	00	05.0	-	.	.	.	$\equiv 0^{\circ} 2^{\circ}, \Delta 1^{\circ} 34^{\circ} 24^{\circ}$
16	3	10	10	10	10.0	-	.	.	.	$\equiv 0^{\circ} 6^{\circ}, \Delta 1^{\circ} 34^{\circ} 24^{\circ}, \Delta 1^{\circ} 40^{\circ} 0^{\circ}, \Delta 1^{\circ} 40^{\circ} 15^{\circ}, \Delta 1^{\circ} 40^{\circ} 24^{\circ}, \Delta 1^{\circ} 40^{\circ} 30^{\circ}, \Delta 1^{\circ} 40^{\circ} 34^{\circ}, \Delta 1^{\circ} 40^{\circ} 40^{\circ}$
17	7	10	09	09	09.3	-	.	.	.	$\equiv 0^{\circ} 1^{\circ}, \Delta 1^{\circ} 34^{\circ} 24^{\circ}$
18	7	07	00	00	02.3	-	.	.	.	$\equiv 0^{\circ} 1^{\circ}, \Delta 1^{\circ} 34^{\circ} 24^{\circ}, \equiv 5^{\circ} 24^{\circ}$
19	5	10	10	10	10.0	-	.	.	.	$\equiv 0^{\circ} 2^{\circ}, \Delta 1^{\circ} 34^{\circ} 24^{\circ}$
20	4	10	10	10	10.0	-	.	.	.	$\equiv 0^{\circ} 2^{\circ}, \Delta 1^{\circ} 34^{\circ} 24^{\circ}$
21	4	10	00	00	03.3	-	.	.	.	$\equiv 0^{\circ} 22^{\circ}, \Delta 1^{\circ} 34^{\circ} 24^{\circ}, \Delta 1^{\circ} 40^{\circ} 0^{\circ}$
22	5	10	00	00	03.3	-	.	.	.	$\equiv 0^{\circ} 2^{\circ}, \Delta 1^{\circ} 34^{\circ} 24^{\circ}, \Delta 1^{\circ} 40^{\circ} 0^{\circ}, \Delta 1^{\circ} 40^{\circ} 15^{\circ}, \Delta 1^{\circ} 40^{\circ} 24^{\circ}, \Delta 1^{\circ} 40^{\circ} 30^{\circ}, \Delta 1^{\circ} 40^{\circ} 34^{\circ}, \Delta 1^{\circ} 40^{\circ} 40^{\circ}$
23	6	10	00	00	03.3	-	.	.	.	$\equiv 0^{\circ} 2^{\circ}, \Delta 1^{\circ} 34^{\circ} 24^{\circ}$
24	6	01	01	00	00.7	-	.	.	.	$\equiv 0^{\circ} 2^{\circ}, \Delta 1^{\circ} 34^{\circ} 24^{\circ}$
25	3	00	10	10	06.7	-	.	.	.	$\equiv 0^{\circ} 2^{\circ}, \Delta 1^{\circ} 34^{\circ} 24^{\circ}, \equiv 6^{\circ} 24^{\circ}, \equiv 16^{\circ} 24^{\circ}$
26	3	10	10	10	10.0	-	.	.	.	$\equiv 0^{\circ} 13^{\circ}, \Delta 1^{\circ} 34^{\circ} 24^{\circ}, \Delta 1^{\circ} 40^{\circ} 0^{\circ}, \Delta 1^{\circ} 40^{\circ} 15^{\circ}, \Delta 1^{\circ} 40^{\circ} 24^{\circ}, \Delta 1^{\circ} 40^{\circ} 30^{\circ}, \Delta 1^{\circ} 40^{\circ} 34^{\circ}, \Delta 1^{\circ} 40^{\circ} 40^{\circ}$
27	2	10	10	00	06.7	-	00.4	.	.	$\equiv 0^{\circ} 1^{\circ}, \Delta 1^{\circ} 34^{\circ} 24^{\circ}, \Delta 1^{\circ} 40^{\circ} 0^{\circ}, \Delta 1^{\circ} 40^{\circ} 15^{\circ}, \Delta 1^{\circ} 40^{\circ} 24^{\circ}, \Delta 1^{\circ} 40^{\circ} 30^{\circ}, \Delta 1^{\circ} 40^{\circ} 34^{\circ}, \Delta 1^{\circ} 40^{\circ} 40^{\circ}$
28	7	10	09	04	07.7	-	.	.	.	$\equiv 0^{\circ} 1^{\circ}, \Delta 1^{\circ} 34^{\circ} 24^{\circ}, \Delta 1^{\circ} 40^{\circ} 0^{\circ}, \Delta 1^{\circ} 40^{\circ} 15^{\circ}, \Delta 1^{\circ} 40^{\circ} 24^{\circ}, \Delta 1^{\circ} 40^{\circ} 30^{\circ}, \Delta 1^{\circ} 40^{\circ} 34^{\circ}, \Delta 1^{\circ} 40^{\circ} 40^{\circ}$
29	7	10	10	10	10.0	-	02.0	.	.	$\equiv 0^{\circ} 2^{\circ}, \Delta 1^{\circ} 34^{\circ} 24^{\circ}, \Delta 1^{\circ} 40^{\circ} 0^{\circ}, \Delta 1^{\circ} 40^{\circ} 15^{\circ}, \Delta 1^{\circ} 40^{\circ} 24^{\circ}, \Delta 1^{\circ} 40^{\circ} 30^{\circ}, \Delta 1^{\circ} 40^{\circ} 34^{\circ}, \Delta 1^{\circ} 40^{\circ} 40^{\circ}$
30	7	09	09	10	09.3	-	16.0	05	.	$\times 0^{\circ} 2^{\circ}, \equiv 1^{\circ} 24^{\circ}, \square$
MES. VRED.		08.6	06.4	05.0	06.6	-	21.2			

SKOPJE - PETROVAC

1978 DECEMBAR

1	8	00	03	00	01.0	-	.	03	\square
2	6	04	09	00	04.3	-	.	01	$\equiv 0^{\circ} 15^{\circ}, \square$
3	6	10	06	10	08.7	-	.	.	$\equiv 0^{\circ} 15^{\circ}, \square$
4	6	06	06	10*	07.3	-	.	.	$\equiv 0^{\circ} 24^{\circ}, \Delta 1^{\circ} 23^{\circ} 45^{\circ}, \times 1^{\circ} 24^{\circ} 24^{\circ}$
5	4	10*	10*	10*	10.0	-	11.3	07	$\times 0^{\circ} 24^{\circ}, \square$
6	4	10*	10	10	10.0	-	10.8	13	$\times 0^{\circ} 15^{\circ}, \square$
7	7	10	10	10	10.0	-	01.8	10	$\equiv 0^{\circ} 15^{\circ}, \square$
8	6	10	07	10	09.0	-	.	09	$\equiv 0^{\circ} 24^{\circ}, \times 1^{\circ} 14^{\circ}, \square$
9	5	10	10	10*	10.0	-	00.0	08	$\equiv 0^{\circ} 24^{\circ}, \times 0^{\circ} 24^{\circ}, \times 1^{\circ} 24^{\circ}, \square$
10	4	10	09	06	08.3	-	02.2	07	$\equiv 0^{\circ} 24^{\circ}, \times 0^{\circ} 24^{\circ}, \times 1^{\circ} 24^{\circ}, \equiv 4^{\circ} 5^{\circ}, \equiv 6^{\circ} 8^{\circ}, \square$
11	1	10	07	07	08.0	-	.	36	$\equiv 0^{\circ} 15^{\circ}, \equiv 4^{\circ} 5^{\circ}, \Delta 1^{\circ} 22^{\circ} 24^{\circ}, \equiv 5^{\circ} 12^{\circ}, \square$
12	3	10	10	10	10.0	-	.	34	$\equiv 0^{\circ} 15^{\circ}, \equiv 4^{\circ} 5^{\circ}, \Delta 1^{\circ} 22^{\circ} 24^{\circ}, \square$
13	4	10	10	10	10.0	-	.	.	$\equiv 0^{\circ} 15^{\circ}, \equiv 4^{\circ} 5^{\circ}, \square$
14	5	10	06	07	07.7	-	.	.	$\equiv 0^{\circ} 15^{\circ}, \equiv 4^{\circ} 5^{\circ}, \Delta 1^{\circ} 22^{\circ} 24^{\circ}, \equiv 5^{\circ} 10^{\circ}, \equiv 6^{\circ} 15^{\circ}, \equiv 7^{\circ} 10^{\circ}, \square$
15	7	10	09	00	06.3	-	23.2	.	$\equiv 0^{\circ} 4^{\circ}, \Delta 1^{\circ} 22^{\circ} 24^{\circ}, \square$
16	6	00	09	06	05.0	-	.	.	$\equiv 0^{\circ} 11^{\circ}, \Delta 1^{\circ} 22^{\circ} 24^{\circ}, \equiv 4^{\circ} 5^{\circ}, \Delta 1^{\circ} 22^{\circ} 24^{\circ}, \equiv 5^{\circ} 11^{\circ}, \equiv 5^{\circ} 14^{\circ}, \square$
17	8	07	09	10	08.7	-	.	.	$\equiv 0^{\circ} 2^{\circ}, \Delta 1^{\circ} 22^{\circ} 24^{\circ}, \square$
18	6	07	03	25	05.0	-	01.0	.	$\bullet 0^{\circ} 4^{\circ}, \square$
19	6	10	10	05	08.3	-	.	.	$\equiv 0^{\circ} 15^{\circ}, \equiv 4^{\circ} 5^{\circ}, \square$
20	7	09	08	06	07.7	-	03.1	.	$\equiv 0^{\circ} 15^{\circ}, \equiv 4^{\circ} 5^{\circ}, \square$
21	4	10	10	10	10.0	-	.	.	$\equiv 0^{\circ} 15^{\circ}, \equiv 4^{\circ} 7^{\circ}, \square$
22	6	28	09	10	09.0	-	11.0	.	$\equiv 0^{\circ} 15^{\circ}, \square$
23	7	29	10	10	09.7	-	10.0	.	$\bullet 0^{\circ} 4^{\circ}, \square$
24	6	07	27	10	08.0	-	02.7	.	$\equiv 0^{\circ} 15^{\circ}, \square$
25	6	10	09	06	08.3	-	.	.	$\equiv 0^{\circ} 15^{\circ}, \square$
26	6	10	10	10	10.0	-	10.7	.	$\equiv 0^{\circ} 15^{\circ}, \square$
27	7	01	08	02	02.7	-	18.9	.	$\equiv 0^{\circ} 15^{\circ}, \square$
28	4	10	10	10	10.0	-	.	.	$\equiv 0^{\circ} 15^{\circ}, \square$
29	1	10	10	10	10.0	-	.	.	$\equiv 0^{\circ} 15^{\circ}, \square$
30	8	05	03	00	02.7	-	.	.	$\equiv 0^{\circ} 15^{\circ}, \square$
31	8	01	10	11	07.0	-	.	.	$\equiv 0^{\circ} 15^{\circ}, \square$
MES. VRED.		37.9	28.3	07.6	07.9	-	72.7		

**B) Mesečni i godišnji
pregled**

S	M	J	J	A	S	O	N	D	Temperatura vazduha °C			Coetina pravaca i srednja jačina veta m/s, Fm (0-12)																
									7	14	21	Sred. (m/s)	8	15	22	29	8	15	22	Dati.	N	NE	E	SE	S	SW	W	NW
SR SLOVENIJA																												
									Ψ = 46°20' N λ = 13°33' E Gr. ΔG = + 34 min.																			
I	-	-01.2	02.8	00.0	00.4	04.1	-02.8	08.1	01	-07.8	09	04	01.0	13	02.2	04	03.0	03	01.3	04	01.0	03	01.7	03	01.0	01.0	06	
II	-	-02.1	02.5	-00.2	00.6	03.6	-03.9	09.0	28	-11.3	21	07	01.3	16	03.0	01	04.0	03	01.0	01	01.0	04	01.3	03	01.7	04	01.5	06
III	-	02.8	09.6	04.8	05.5	10.9	01.1	17.0	30	-02.2	23	02	01.0	28	02.6	04	01.2	04	02.0	02	02.5	12	02.2	05	01.6	02	01.0	28
IV	-	09.2	11.1	07.0	07.6	12.4	03.2	17.0	28	-01.5	17	04	01.8	18	02.7	16	03.5	05	02.0	01	01.0	05	01.8	05	02.4	.	.	36
V	-	09.9	15.1	10.9	11.7	16.4	07.1	21.6	31	-01.5	12	32	01.5	18	02.6	09	02.6	04	01.5	02	01.0	16	01.7	05	01.8	03	02.0	24
VI	-	13.2	20.9	14.7	15.7	21.7	09.9	26.7	03	04.9	29	02	01.5	14	01.9	05	01.4	02	01.5	05	01.4	12	01.6	18	02.3	04	02.5	28
VII	-	14.2	21.5	16.1	17.0	22.2	11.4	28.0	13	25.4	06	04	01.3	09	01.2	05	01.6	02	01.5	02	01.5	13	01.7	09	02.1	11	01.8	38
VIII	-	13.8	21.7	15.4	16.6	21.3	11.3	27.9	31	03	01.5	15	16	07	01.9	01	01.0	02	02.0	07	02.0	16	02.3	03	02.3	39		
IX	-	10.2	19.5	13.0	14.0	20.4	08.5	25.3	11	01.9	21	01	01.0	23	02.0	05	01.6	02	02.0	02	01.0	06	01.5	10	02.1	06	01.8	35
X	-	05.6	15.3	08.2	09.4	16.3	04.3	21.9	07	-01.0	28	02	01.0	12	01.8	08	01.8	.	05	01.6	14	01.6	11	01.5	02	02.0	39	
XI	-	-00.1	09.3	01.8	03.2	09.9	-01.6	14.6	01	-05.5	11	04	01.3	23	02.2	05	04.4	06	01.7	09	01.6	05	01.4	02	01.0	01	01.0	26
XII	-	-01.6	02.0	-00.2	00.0	02.8	-03.1	07.0	13	-13.5	08	04	01.3	16	01.6	03	01.0	09	01.1	01	01.0	01	01.0	05	01.4	03	01.7	51
GOD.	-	03.8	12.4	07.6	08.4	13.6	03.6	28.0	15	W-N -12.5	08.XII	39	01.3	207	02.2	74	02.4	41	01.5	36	01.5	98	01.7	96	02.0	42	01.8	462
VEDRIJAN																											BR. ST. 1	
									Ψ = 46°01' N λ = 13°33' E Gr. ΔG = + 54 min.																			
I	-	02.9	04.4	02.6	04.2	07.2	02.0	11.5	04	-02.5	06	01	.	21	02.8	51	01.9	11	01.8	05	01.2	01	01.0	03	01.3	.	.	01
II	-	01.9	05.7	03.2	03.5	06.6	01.2	10.5	28	-04.0	09	01	01.0	18	02.9	44	01.8	08	01.6	05	01.4	01	01.0	02	01.0	05	01.7	09
III	-	06.3	11.5	07.7	08.3	12.5	03.4	17.6	12	01.5	23	01	01.0	24	02.0	29	01.2	12	01.3	08	01.6	06	01.2	03	01.3	02	01.0	26
IV	-	08.4	13.7	09.5	10.3	14.5	07.3	19.0	23	03.0	17	0.	.	18	02.9	40	01.7	04	01.0	07	02.0	05	01.4	14	01.0	02	01.0	.
V	-	12.0	15.8	12.5	13.2	17.0	10.5	25.8	29	03.5	12	05	01.0	18	02.3	34	01.4	16	01.3	10	01.2	03	01.3	04	01.3	03	01.3	01
VI	-	16.6	22.2	17.3	18.6	23.1	14.6	25.5	03	10.0	29	0.	.	16	02.2	35	01.5	14	01.7	15	01.6	04	01.8	02	01.5	03	01.7	01
VII	-	17.4	23.6	19.1	19.8	24.7	15.5	30.2	29	10.5	08	02	01.0	26	02.0	25	01.6	14	01.3	11	01.8	06	01.3	04	01.0	01	05.0	04
VIII	-	17.3	23.7	18.6	19.6	24.8	15.8	29.5	06	01.5	09	0.	.	16	02.0	38	01.6	17	01.3	04	01.5	06	01.0	01	01.0	03	01.3	01
IX	-	14.3	20.9	16.8	16.9	21.9	13.0	24.8	15	04.8	28	0.	.	21	01.7	29	01.3	13	01.6	05	01.0	08	01.4	07	01.0	04	01.0	03
X	-	11.1	17.9	12.8	13.7	18.9	10.4	24.5	11	05.0	28	01	01.0	23	02.6	34	02.0	10	01.2	02	01.0	05	01.4	06	01.3	04	01.0	.
XI	-	05.7	13.1	07.3	08.4	13.6	04.9	19.5	15	01.0	18	02	01.0	25	02.6	38	01.7	08	01.1	05	01.2	01	01.0	01	03.0	.	.	01
XII	-	02.9	03.0	03.2	03.6	06.0	01.6	10.5	26	-04.5	08	01	01.0	18	03.1	42	01.7	23	01.3	03	01.3	02	01.0	.	.	01		
GOD.	-	09.7	15.0	10.9	11.7	15.9	08.5	30.2	29	W-N -06.5	08.XII	13	01.0	264	02.4	439	01.6	150	01.4	80	01.5	53	01.3	52	01.1	24	01.4	20
PATECE-PLANICA																											BR. ST. 2	
									Ψ = 46°30' N λ = 13°43' E Gr. ΔG = + 54 min.																			
I	689.4	-06.3	-00.8	-04.9	-04.2	00.0	-07.7	05.0	25	-17.8	06	0.	.	04	02.3	01	02.0	08	01.6	.	.	01	01.0	09	01.4	01	01.0	69
II	681.3	-06.8	00.2	-04.6	-04.0	01.1	-07.9	09.1	28	-17.1	15	0.	.	07	01.4	07	01.9	05	02.2	.	.	01	01.0	05	01.6	.	.	59
III	684.9	-02.0	06.9	00.2	01.4	06.1	-02.9	14.4	28	-09.2	27	01	02.0	06	01.8	02	01.5	02	02.5	16	02.0	01	02.0	01	02.0	61		
IV	682.5	00.4	08.4	02.0	03.2	09.7	-01.1	15.4	25	-07.4	17	21	03.0	02	01.5	08	02.1	10	01.7	01	02.0	04	01.8	01	01.0	57		
V	685.7	05.9	12.7	07.4	08.6	13.9	03.5	18.0	20	-02.3	12	0.	.	11	02.3	05	01.2	.	.	08	01.0	03	01.7	.	.	.	66	
VI	687.2	10.3	17.8	11.3	12.7	19.2	06.2	24.5	07	06.6	29	0.	.	01	31.3	09	02.0	10	02.3	.	.	08	02.0	04	01.3	03	01.7	66
VII	688.9	10.9	18.7	13.0	14.0	20.0	08.1	25.0	13	01.4	06	0.	.	07	01.3	07	01.4	09	01.9	.	.	03	01.3	05	01.6	02	01.5	60
VIII	689.4	10.1	18.0	13.1	12.5	20.5	07.6	26.7	03	03.0	11	0.	.	05	01.6	11	02.1	11	01.9	.	.	03	01.0	02	01.0	01	01.0	60
IX	686.6	06.2	17.3	08.7	10.2	18.3	03.9	24.6	11	-01.7	21	0.	.	03	02.3	07	01.6	05	01.4	02	01.0	04	01.3	04	01.0	67		
X	691.2	02.3	12.2	09.5	05.4	13.2	00.8	18.8	10	-01.8	28	0.	.	04	02.0	05	01.4	05	01.0	01	02.0	03	01.0	01	01.0	67		
XI	692.8	-05.8	06.3	-03.5	-01.1	07.7	-05.5	12.5	16	-12.8	30	0.	.	01	91.3	03	01.3	07	01.6	.	.	03	01.7	01	01.0	75		
XII	692.9	-05.6	-01.0	-04.8	-04.1	00.1	-07.5	07.0	29	-21.2	08	0.	.	01	02.0	01	02.0	03	01.3	02	01.0	03	01.0	04	01.3	.		
GOD.	-	06.3	14.8	09.1	09.8	19.8	04.8	31.0	15	W-N -06.2	08.XII	07	01.6	57	02.1	34	01.5	67	02.1	26	01.1	43	31.6	20	01.2	07	01.4	834
TOLMIN																											BR. ST. 4	
									Ψ = 46°11' N λ = 13°44' E Gr. ΔG = + 55 min.																			
I	-	-00.5	04.4	01.0	01.5	05.4	-02.0	10.6	04	-07.9	10	01	01.0	14	02.2	01	03.0	06	01.7	.	.	01	01.0	08	01.4	01	01.0	70
II	-	-01.1	04.1	00.9	01.2	05.0	-02.4	09.5	14	-08.2	22	0.	.	09	02.3	04	01.3	08	02.3	03	01.3	01	01.0	05	01.6	.	.	59
III	-	02.7	12.3	06.7	07.1	11.0	01.5	19.8	31	-03.5	23	01	01.0	21	03.0	04	01.0	01	01.0	06	01.7	33	01.0	.	.	.	61	
IV	-	06.0	14.0	09.4	09.7	15.2	04.1	19.7	23	-02.5	18	0.	.	05	02.0	05	01.4	10	03.4	01	01.0	06	02.0	01	01.0	01	01	

Mesec	Oblaknost mm (0-10)				Vlažnost vzdušja %	Temperatura vzdušja °C	Vlažnost vzdušja			Padavine R mm	Broj dana na sat:																														
							Tn	Tx	Tn	Tx	Tx	F(0-12)	Rm(0-10)	R mm	•	*	•	Δ	▲	▲	R																				
	7	14	21	Sred. (Dien.)	7	14	21	Vzdušna temperatura °C	Mesec	Σ	M	N	N.	<	<	IV	IV	IV	M	M	<	>	M	M	M	P	•	Δ	▲	▲	R										
BUVEC																										SR SLOVENIJA															
BR. ST. 1																										H_a = 425 m H_b = - m h = 2.0 m h = 1.3 m															
I	6.5	6.6	5.7	6.3	978.0	J3.8	85	69	83	79	25	431	121.8	29	•	•	28	•	•	01	•	06	16	13	10	08	09	11	04	01	02	01	02	05	18						
II	7.4	7.6	6.9	7.3	980.0	03.5	94	87	80	77	32	264	077.8	26	01	03	23	•	•	01	•	01	16	14	11	08	09	09	01	01	01	03	01	05	25						
III	5.9	7.3	5.8	6.4	156.3	94.3	77	51	71	66	18	149	107.0	17	•	•	25	•	•	04	•	05	13	13	12	02	12	04	01	01	01	02	03	03	10						
IV	7.1	8.2	7.0	7.4	131.6	05.4	79	55	73	69	24	324	120.5	13	•	•	03	•	•	04	•	03	15	13	11	05	13	03	03	•	•	04	02	02	02	09					
V	6.9	8.8	7.9	7.9	121.5	07.6	81	60	82	74	33	310	086.1	23	•	•	01	•	•	01	•	16	24	17	07	24	•	•	•	01	•	13	01	•	•	•	•				
VI	5.7	6.9	6.4	6.3	186.8	09.7	82	56	79	72	33	220	039.9	18	•	•	08	•	•	02	•	01	09	14	08	09	14	•	•	01	01	13	•	•	•	•					
VII	6.3	6.9	6.7	6.6	176.2	11.6	91	61	88	80	43	301	070.8	06	•	•	39	•	•	01	10	21	20	05	21	•	•	•	01	01	16	03	•	•	•	•					
VIII	5.9	5.9	4.8	6.9	228.1	11.1	85	86	78	75	35	137	022.6	05	•	•	09	•	•	02	02	03	04	15	13	06	19	•	•	12	01	•	•	•	•						
IX	6.0	5.5	5.4	5.6	186.9	09.3	91	56	86	78	26	062	038.5	28	•	•	01	02	•	02	01	04	07	10	05	01	10	•	•	•	01	06	01	•	•	•	•				
X	4.3	4.1	2.5	3.6	175.1	07.0	82	57	87	79	31	274	106.4	01	•	•	01	•	•	14	05	08	07	06	08	•	•	•	03	01	01	•	•	•	•						
XI	2.5	1.9	1.5	2.0	181.0	04.0	84	47	77	70	33	070	050.4	27	•	•	23	•	•	03	02	21	03	03	02	03	02	02	02	02	02	04	04	04	04	04	04	04			
XII	7.2	7.0	7.0	7.1	059.0	04.1	93	80	88	87	44	254	077.7	30	02	04	21	•	•	04	18	20	16	06	15	09	03	01	•	•	10	20	09	09	09	09	09				
GOD.	5.8	6.4	5.6	6.0	1700.5	06.8	85	60	81	73	18	2802	121.8	29	03	07	110	28	•	20	05	67	132	168	194	62	153	38	15	04	02	08	05	73	35	09					
VEDRIJAN																										H_a = 238 m H_b = - m h = 2.0 m h = 1.3 m															
BR. ST. 2																										H_a = 238 m H_b = - m h = 2.0 m h = 1.3 m															
I	6.6	6.3	5.2	6.1	986.3	04.8	78	70	77	75	27	204	047.7	30	•	•	04	•	•	00	14	13	12	06	12	04	01	•	•	•	01	01	01	01	01	01	01				
II	6.8	5.9	5.1	6.0	935.7	04.6	79	71	79	76	27	146	031.8	26	•	•	10	•	•	07	12	13	10	04	12	03	•	•	•	01	01	01	02	01	01	01					
III	6.8	6.6	4.2	6.5	159.3	05.5	69	60	71	67	20	068	028.6	24	•	•	26	•	•	01	02	09	12	07	02	13	•	•	01	04	04	04	04	04	04						
IV	6.4	5.2	6.0	5.9	141.4	06.3	72	54	70	66	27	226	104.0	13	•	•	03	•	•	01	02	09	11	09	03	11	•	•	01	01	01	01	01	01	01						
V	6.3	6.9	7.1	6.8	122.9	08.7	79	68	79	75	31	260	051.5	24	•	•	01	•	•	01	01	14	24	20	09	24	•	•	03	02	03	03	03	03	03						
VI	4.8	6.7	5.0	6.9	211.1	10.4	72	53	69	65	35	179	061.9	18	•	•	09	•	•	04	05	12	09	05	12	09	•	•	09	09	09	09	09	09	09						
VII	5.6	6.9	5.1	5.2	210.5	11.8	73	57	72	67	30	213	058.6	16	•	•	16	01	01	03	06	17	15	07	17	•	•	02	02	02	02	02	02	02							
VIII	5.7	4.2	3.5	5.8	245.6	11.8	73	57	74	68	39	144	037.2	27	•	•	15	•	•	01	04	14	10	03	14	•	•	03	03	03	03	03	03	03							
IX	5.5	6.1	3.6	6.4	187.5	10.5	79	60	76	72	31	160	100.9	28	•	•	05	•	•	01	03	08	05	02	08	•	•	01	01	01	01	01	01	01							
X	3.4	2.5	2.0	2.6	221.7	07.9	73	56	70	66	34	106	039.8	03	•	•	05	•	•	19	03	04	06	03	04	03	•	•	01	01	01	01	01	01	01						
XI	2.4	1.7	1.6	1.9	209.1	05.0	65	69	62	59	26	071	029.7	27	•	02	03	30	•	•	02	02	23	02	03	02	03	02	02	02	02	02	02	02	02						
XII	7.0	7.0	7.1	7.2	355.2	05.1	83	79	84	82	49	224	034.9	29	•	01	00	•	•	02	02	04	17	16	12	08	15	03	•	•	12	02	02	02	02	02	02				
GOD.	5.3	4.9	4.6	4.9	1945.1	07.7	74	61	73	69	23	1981	106.0	04X	34	40	176	06	•	02	04	101	95	152	118	58	147	10	01	•	•	02	23	19	09	09	09	09	09	09	09
RATECE-PLANICA																										H_a = 864 m H_b = 865,1 m h = 2,2 m h = 1,3 m															
BR. ST. 3																										H_a = 864 m H_b = 865,1 m h = 2,2 m h = 1,3 m															
I	7.3	7.2	6.2	6.9	056.8	03.0	92	79	91	87	44	177	041.2	12	12	13	31	•	•	03	16	14	11	04	02	14	•	•	01	02	01	01	01	01	01						
II	8.0	7.8	7.8	8.1	046.4	03.0	92	75	90	86	46	125	045.0	12	10	12	24	•	•	02	17	12	08	04	04	08	•	•	01	02	01	02	01	02	01						
III	6.3	6.7	5.0	6.0	162.8	03.0	93	53	83	76	27	096	048.4	17	•	•	26	•	•	04	11	13	09	02	06	01	•	•	01	01	01	01	01	01	01						
IV	6.9	8.3	6.9	7.4	128.7	24.5	93	53	86	78	25	165	060.3	13	•	03	•	•	•	02	15	16	13	04	10	07	•	•	02	03	03	03	03	03	03						
V	7.5	8.5	8.1	8.0	127.2	06.7	93	81	86	80	38	190	055.4	22	•	•	03	•	•	01	16	19	15	05	18	32	•	•	04	02	02	02	02	02	02						
VI	6.0	7.4	6.5	6.6	168.6	08.4	89	57	83	76	32	189	066.0	25	•	•	01	01	01	01	09	17	14	06	17	17	05	•	•	08	08	08	08	08	08	08					
VII	6.5	6.7	6.4	6.5	211.0	09.8	94	64	87	82	40	241	069.1	19	•	•	18	01	01	01	19	20	14	06	20	14	06	20	•	•	09	09	09	09	09	09	09				
VIII	5.8	6.0	5.1	5.6	231.7	09.5	93	65	89	83	45	137	037.5	08	•	•	03	•	•	01	02	05	14	09	06	14	06	14	06	07	07	07	07	07	07	07					
IX	5.4	5.2	4.4	5.0	204.3	07.9	94	60	81	82	33	099	043.9	28	•	•	05</td																								

M	Mj.	Vrijeme u Hr. min.	Temperatura vazduha °C								Cestina pravaca i srednja jačina vatra nD, fm (0-12)																	
			Tm				RH				N		NE		E		SE		S		SW		W		NW			
			7	14	21	Srednja Srednja RH	RH	RH	RH	RH	Dst.	Mis.	Dst.		E.	J.	E.	J.	E.	J.	S.	J.	E.	J.	C			
$\varphi = 46^{\circ}23' N \lambda = 13^{\circ}51' E$ Gr. $\Delta G = + 55$ min.																												
I	555.3	-09.0	-07.9	-08.7	-06.2	-11.1	03.2	02	-19.9	05	35	05.7	01	32.0	05	03.2	36	05.0	05	06.4	.	.	31	34.0	35	05.0	05	
II	551.9	-09.3	-08.0	-08.6	-08.7	-05.5	-11.6	05.3	23	-18.8	15	32	06.0	02	04.5	05	04.8	22	04.7	38	05.6	37	05.1	08
III	556.4	-06.5	-05.4	-06.8	-06.4	-03.7	-09.3	04.0	29	-15.4	19	36	04.8	04	04.5	04	03.5	18	06.4	10	06.0	45	06.0	06
IV	555.1	-06.3	-04.2	-06.1	-05.7	-03.1	-08.0	01.2	28	-14.2	07	36	04.5	05	03.2	05	03.2	34	03.7	01	04.0	.	.	01	01.0	21	03.4	17
V	559.5	-02.4	-01.2	-02.2	-02.0	00.3	-04.1	04.6	20	-12.7	12	02	03.0	02	02.5	01	03.0	21	04.8	04	02.5	.	.	32	04.0	53	03.7	08
VI	562.8	01.8	03.2	02.0	02.3	04.9	00.2	11.1	08	-7.5	26	04	02.8	01	03.3	04	02.5	22	02.5	01	02.0	.	.	38	02.9	31	03.4	19
VII	564.8	03.4	05.0	04.0	04.1	07.3	01.8	11.4	18	-02.9	08	05	03.2	04	03.8	06	03.5	20	09.7	04	02.8	41	03.5	13
VIII	565.4	03.9	05.8	04.2	04.5	08.0	02.2	13.1	03	-05.4	31	04	03.8	01	04.0	03	03.0	18	03.6	04	03.0	45	03.6	18
IX	563.8	02.0	04.0	02.9	02.9	04.2	00.0	14.6	11	-06.6	28	33	05.7	12	03.3	04	04.0	65	04.3	06
X	564.5	00.1	02.0	00.3	00.7	03.8	-02.2	12.4	11	-11.7	27	03	05.7	01	02.0	02	02.0	32	03.9	07	04.0	37	04.3	11
XI	565.3	-02.1	00.0	-02.4	-01.7	01.6	-04.1	07.4	08	-16.3	28	.	.	01	04.0	05	02.8	15	03.3	01	02.0	.	.	04	03.8	42	03.4	22
XII	564.6	-05.9	-04.9	-05.9	-05.7	-03.1	-06.3	06.2	11	-13.7	06	03	04.7	03	04.0	05	04.2	21	04.0	11	05.6	37	04.4	13
GOD.	560.0	-02.5	-01.0	-02.3	-02.0	00.9	-04.5	14.6	44	-19.9	05.1	43	04.4	25	03.7	45	03.4	271	04.1	12	04.2	.	.	64	04.5	489	04.2	146
$\varphi = 46^{\circ}01' N \lambda = 13^{\circ}55' E$ Gr. $\Delta G = + 56$ min.																												
I	-	-02.8	-01.2	-02.8	-02.4	-00.3	-04.7	04.3	14	-09.5	09	02	01.0	02	02.5	33	01.6	15	01.7	01	01.0	04	01.5	36
II	-	-04.0	-01.9	-03.5	-03.2	-00.7	-05.4	07.3	27	-13.0	21	01	01.0	.	.	39	01.8	17	02.1	.	.	01	03.0	26
III	-	01.0	04.6	01.7	02.3	05.9	-06.6	10.5	30	-09.0	08	.	.	20	01.6	.	.	37	02.1	02	02.0	07	02.7	27				
IV	-	02.3	05.7	03.2	03.6	06.9	00.7	11.7	29	-04.9	07	02	01.5	02	02.0	32	02.3	01	03.0	.	.	09	02.0	05	01.2	03	01.7	36
V	-	07.2	09.4	06.9	07.6	11.0	06.9	14.5	29	-04.5	12	.	.	14	03.7	20	02.0	25	02.1	05	01.4	04	02.0	25
VI	-	12.2	15.4	11.4	12.7	16.8	09.1	20.7	02	04.0	14	.	.	01	03.0	25	02.2	31	02.5	08	01.8	05	02.2	20
VII	-	17.8	16.6	12.6	13.7	17.6	06.9	22.7	13	05.0	08	01	01.0	.	.	32	01.6	17	02.3	03	01.7	08	02.5	32
VIII	-	12.3	15.9	12.1	13.1	17.5	06.7	22.7	02	05.9	31	03	02.3	.	.	35	02.0	19	02.3	01	01.0	.	.	35
IX	-	10.0	14.3	10.0	11.1	15.3	07.3	21.3	11	01.0	21	.	.	03	02.7	24	02.2	25	02.2	02	01.5	09	02.2	27
X	-	05.0	06.9	05.9	06.5	10.3	03.9	15.1	10	-02.7	28	01	01.0	01	03.0	67	02.2	03	01.3	01	04.0	01	01.0	19
XI	-	00.8	04.0	01.0	01.7	05.3	-00.6	10.7	10	-07.5	29	.	.	06	03.3	54	01.8	09	01.6	.	.	05	02.2	16
XII	-	-01.9	-00.8	-01.4	-01.4	01.2	-03.8	06.3	10	-15.7	08	01	01.0	09	03.6	15	02.8	34	01.9	09	01.2	01	01.0	24
GOD.	-	04.6	07.6	04.6	05.4	08.9	02.5	22.7	03/VII	-19.7	08/XI	11	01.4	38	03.3	396	02.0	01	03.0	.	.	241	02.1	37	01.5	48	02.2	323
$\varphi = 46^{\circ}21' N \lambda = 14^{\circ}11' E$ Gr. $\Delta G = + 57$ min.																												
I	-	-02.4	01.7	-01.1	-00.7	03.0	-03.6	08.1	03	-09.0	28	22	01.7	11	02.2	.	.	09	02.0	06	01.8	06	01.3	.	.	17	02.0	22
II	-	-03.3	02.1	-01.1	-00.8	-	-04.4	-	-12.9	16	14	01.4	10	02.0	.	.	13	02.5	14	01.7	06	02.3	.	.	05	01.2	22	
III	-	01.7	10.4	05.6	05.8	-	00.7	-	-04.5	20	20	01.8	15	02.7	.	.	04	03.3	10	02.2	09	02.7	.	.	20	03.7	15	
IV	-	04.0	11.2	07.0	07.4	12.2	02.4	18.9	29	-02.9	07	12	01.9	11	02.5	.	.	07	02.0	08	01.5	05	02.2	.	.	20	02.4	27
V	-	09.1	14.6	10.6	11.2	16.2	06.9	20.9	26	00.3	13	09	01.9	17	01.9	.	.	21	02.4	10	01.9	06	01.7	.	.	08	02.4	22
VI	-	13.2	20.2	14.6	15.7	21.2	10.1	27.1	07	06.0	29	09	01.9	17	02.1	.	.	14	01.9	10	01.7	12	02.0	.	.	08	02.9	20
VII	-	14.0	20.9	15.8	16.7	22.0	11.3	24.5	12	05.7	06	14	01.3	14	02.0	.	.	12	02.3	09	02.3	07	01.6	.	.	13	01.6	24
VIII	-	13.4	21.0	15.3	16.3	22.1	11.2	28.4	03	06.5	09	14	01.3	12	02.4	.	.	13	02.5	09	02.0	06	02.0	.	.	17	01.8	22
IX	-	08.5	19.0	12.3	13.3	19.9	07.7	24.5	11	01.6	21	15	01.4	15	02.3	.	.	12	01.8	03	01.7	05	01.6	01.0	01.0	12	02.2	27
X	-	05.5	13.1	07.7	08.5	14.0	06.4	19.4	07	00.0	29	14	01.2	18	02.2	.	.	12	02.4	09	01.7	06	01.8	.	.	08	01.1	26
XI	-	-01.3	05.9	00.0	01.1	06.6	-02.4	12.7	01	-05.8	20	09	02.2	21	01.7	.	.	10	02.5	07	01.9	07	01.9	.	.	18	01.7	18
XII	-	-03.1	01.5	-01.9	-01.3	02.6	-04.5	08.4	29	-11.5	04	16	01.5	21	01.9	.	.	08	02.3	04	01.8	04	02.3	.	.	17	01.7	23
GOD.	-	05.0	11.8	07.1	07.8	-	-03.3	-	-12.5	16.0	01.6	182	02.1	100</td														

Mesec	Oblačnost Nm (0-10)			Vlažnost vazduha U m s	Padavine R mm			Broj dana na sat																																	
	7	14	21		Sred. (Dien.)	Broj sati	Sred. (Dien.)	Min.	Max.	Dat.	Tn	Tx	Tn	Tx	Tn	Tx	F(0-12)	Nm(O-10)	R mm	•	*	‡	▲	▲	R	T	≡														
											≤	<	<	≥	≤	≥	≤	≥	≤	≥	≤	≥	≤	≥	•	‡	▲	▲	R	T	≡										
KREDARICA																																									
BR. ST. 6																																									
I	6.7	7.3	6.2	6.7	377.4	01.8	80	82	83	82	23	245	055.4	12	20	29	31	.	.	.	23	12	03	13	18	14	08	.	18	19	31						
II	7.8	7.1	5.6	6.8	373.0	01.9	82	82	80	81	13	150	052.7	12	18	26	28	.	.	.	19	10	02	12	15	09	04	.	15	22	28						
III	6.4	6.1	5.4	6.0	165.9	02.0	73	73	73	73	19	179	111.2	17	15	25	31	.	.	.	23	19	04	05	16	14	03	.	16	.	01	.	.	31	31						
IV	6.7	7.8	6.6	7.1	104.0	02.6	87	88	90	88	29	232	071.4	13	08	26	30	.	.	.	10	03	02	12	22	14	04	.	22	.	02	.	.	01	24	30					
V	5.8	6.8	6.4	8.3	080.9	03.6	85	92	94	91	38	200	046.9	23	02	14	31	.	.	.	16	06	.	21	25	21	04	06	24	02	03	01	03	.	06	29	31				
VI	5.8	8.8	5.7	6.8	151.1	04.5	82	86	81	83	26	227	039.4	11	.	02	14	.	.	.	13	05	05	11	15	07	14	15	03	02	01	04	.	08	20	30					
VII	6.2	8.5	7.3	7.4	157.8	05.2	81	87	86	85	39	236	043.8	36	.	10	.	.	.	14	05	01	12	20	19	08	16	14	06	04	03	.	12	25	25						
VIII	5.4	6.9	4.4	5.6	180.1	05.2	79	81	85	82	18	158	029.6	08	.	01	09	.	.	.	12	04	03	06	17	15	06	14	06	04	03	.	02	09	19	03					
IX	5.8	6.4	4.3	5.5	151.7	04.2	76	75	74	75	21	042	010.9	12	.	02	12	.	.	.	20	08	03	07	13	08	01	08	06	01	02	.	01	17	04						
X	4.6	4.8	3.7	4.2	160.8	03.2	67	72	70	70	14	216	096.0	01	02	35	20	.	.	.	15	24	13	05	08	06	05	04	08	03	.	02	.	.	11	31					
XI	2.5	2.3	1.7	2.2	192.0	01.6	46	45	47	47	14	063	039.2	27	04	06	23	.	.	.	11	02	20	03	05	04	02	05	05	05							
XII	5.9	5.0	4.2	5.3	101.3	02.0	69	67	69	68	18	167	037.8	20	07	28	31	.	.	.	25	16	07	08	18	15	05	02	17	.	02	01	.	02	18	31					
GOD.	5.9	6.7	5.3	6.0	1596.0	03.2	75	77	77	77	13	2095	111.2	47	m	76	164	270	.	.	.	201	96	58	119	199	156	57	67	162	17	19	03	17	.	41	220	280			
VOJSKO																																									
BR. ST. 7																																									
I	7.4	7.7	7.4	7.5	-	-	-	-	-	-	-	379	127.3	29	.	17	29	.	.	.	01	.	01	20	14	13	09	05	14	02	03	.	02	.	.	19	31				
II	6.4	8.8	8.1	8.2	-	-	-	-	-	-	-	177	036.6	11	03	19	23	.	.	.	03	20	15	13	05	05	10	.	01	.	.	.	03	28							
III	6.5	6.9	4.9	6.1	-	-	-	-	-	-	-	164	069.8	17	.	15	.	.	.	03	12	10	10	05	07	07	02	.	02	.	.	03	31								
IV	7.4	8.1	7.4	7.7	-	-	-	-	-	-	-	289	112.5	13	.	10	.	.	.	01	01	17	17	15	05	15	06	01	01	03	.	03	04	25							
V	5.7	8.7	7.5	7.8	-	-	-	-	-	-	-	292	042.0	22	.	04	.	.	.	01	.	17	24	19	08	22	03	.	02	.	.	09	08	04							
VI	6.7	7.0	5.6	6.4	-	-	-	-	-	-	-	214	075.2	13	.	04	.	.	.	02	09	12	12	05	12	.	01	13	06	06							
VII	5.8	6.9	6.4	6.4	-	-	-	-	-	-	-	261	046.3	19	.	04	.	.	.	01	11	19	16	09	19	.	03	02	11	06	.	.	.	06							
VIII	5.8	6.3	5.3	5.5	-	-	-	-	-	-	-	172	040.5	27	.	04	.	.	.	02	04	15	11	06	15	.	02	.	.	09	06	.	.	.	06						
IX	6.2	4.1	4.3	5.6	-	-	-	-	-	-	-	171	113.5	28	.	04	.	.	.	01	.	02	04	07	06	03	07	.	01	.	.	08	07								
X	7.6	5.1	5.3	6.0	-	-	-	-	-	-	-	185	059.1	03	.	04	.	.	.	02	09	06	04	05	04	01	01	01	.	01	16	01									
XI	5.1	2.9	3.1	3.7	-	-	-	-	-	-	-	094	059.3	27	.	03	12	.	.	.	13	05	04	04	03	32	04	01	01	01	.	09	05								
XII	8.4	7.9	7.7	8.0	-	-	-	-	-	-	-	254	067.7	30	05	10	19	.	.	.	01	.	02	20	18	14	09	11	09	01	02	.	.	13	31						
GOD.	6.4	6.8	6.1	6.4	-	-	-	-	-	-	-	2652	127.3	29	01	08	49	116	.	.	.	05	.	32	150	161	137	72	126	54	07	08	02	16	02	54	106	156			
RADOVLIJICA																																									
BR. ST. 8																																									
I	7.8	6.9	7.0	7.2	-	-	-	-	-	-	-	03.7	87	75	88	83	34	267	068.1	29	.	03	28	.	.	.	01	.	03	17	14	10	07	05	11	01	.	.	.	02	18
II	8.6	7.3	7.5	7.8	-	-	-	-	-	-	-	33.7	87	72	87	82	35	129	036.6	27	01	08	23	.	.	.	03	.	03	19	14	11	04	04	10	01	27
III	6.4	6.7	4.3	5.8	-	-	-	-	-	-	-	04.5	83	54	69	69	26	112	052.2	17	.	09	.	.	.	04	.	04	02	07	11	15	09	03	12	04	.	.	04	05	
IV	7.0	8.3	5.8	7.0	-	-	-	-	-	-	-	05.7	86	61	76	74	34	142	060.5	13	.	04	.	.	.	02	.	12	13	11	03	13	03	.	.	01	02	01	04		
V	5.5																																								

Mjesec	Godina	Geografske koordinate	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta m/s (0-12)																									
			Ta			Hg			M			D			N			NE			E			SE			S			SW			W			NW		
			7	14	21	Ta 50°C	Hg 50°C	M 50°C	M 50°C	M 50°C	M 50°C	D 50°C	N 50°C	N 50°C	N 50°C	N 50°C	E 50°C	E 50°C	E 50°C	E 50°C	S 50°C	S 50°C	S 50°C	S 50°C	S 50°C	SW 50°C	SW 50°C	W 50°C	W 50°C	NW 50°C	NW 50°C	C 50°C						
$\varphi = 46^{\circ}13' N \lambda = 14^{\circ}29' E$ Gr. $\Delta G = + 58$ min.																												BRNIK-LETALISTE		BR. ST. 11								
I	729.5	-02.7	01.5	-01.4	-01.0	32.7	-04.2	09.6	04	-13.7	28	05	01.6	02	01.0	07	01.3	05	01.6	02	01.5	06	01.2	13	01.2	12	01.7	41										
II	729.7	-03.6	01.7	-01.6	-01.4	32.8	-05.0	13.6	28	-17.1	21	01	01.0	01	01.0	08	01.5	07	02.0	.	.	03	02.0	12	01.5	14	01.6	38										
III	729.2	00.5	10.7	03.3	04.5	12.1	-01.4	19.0	31	-07.5	23	06	02.7	05	01.2	10	01.8	04	01.8	02	01.0	04	02.5	20	01.7	09	01.8	33										
IV	729.6	03.5	11.8	05.3	06.5	13.4	00.7	19.1	29	-05.6	09	05	01.6	03	01.7	10	02.4	06	01.7	02	01.5	15	01.3	10	01.6	31												
V	729.5	09.9	14.7	09.6	10.7	17.0	05.3	22.0	29	-00.6	15	06	02.2	02	01.0	08	01.9	12	01.7	03	01.3	04	01.3	12	01.8	10	01.6	36										
VI	729.3	13.3	20.8	14.1	15.6	22.4	08.3	27.9	04	01.9	29	06	02.2	03	01.3	08	01.8	07	01.9	05	01.8	08	02.0	15	02.0	01	01.0	37										
VII	729.1	14.2	22.1	17.0	17.6	23.4	11.7	29.0	12	05.5	06	02	01.5	01	02.0	17	01.8	05	01.8	05	01.4	13	01.5	05	01.6	40												
VIII	729.7	13.6	22.2	16.0	17.0	23.6	12.0	30.6	02	07.0	11	03	01.0	02	02.0	09	01.8	13	01.8	04	02.0	06	01.3	07	01.4	45												
IX	729.0	09.9	19.9	13.0	14.0	21.3	08.4	29.0	11	01.7	21	06	02.0	02	01.0	08	01.4	09	01.6	11	01.5	05	01.8	09	01.2	11	01.5	29										
X	732.7	05.6	14.1	08.1	09.0	15.4	04.8	20.9	07	-00.6	28	04	01.3	04	01.3	09	01.4	10	01.6	07	01.6	06	01.0	11	01.4	11	01.6	36										
XI	730.6	-01.5	04.1	-00.5	00.4	04.9	-02.6	14.1	01	-08.4	36	02	01.0	07	01.1	07	01.0	03	01.0	10	01.1	04	01.0	12	01.0	07	01.1	38										
XII	729.6	-02.6	00.8	-01.7	-01.4	01.8	-04.0	08.8	17	-12.2	03	07	01.1	06	01.0	08	01.1	10	01.8	03	01.0	01	02.0	20	01.3	11	01.4	27										
GOD.	729.1	04.9	12.0	08.8	07.6	13.4	02.8	30.6	02.VII	-17.1	24.II	53	01.7	38	01.2	109	01.6	93	01.8	58	01.5	47	01.7	158	01.5	108	01.5	431										
$\varphi = 46^{\circ}24' N \lambda = 14^{\circ}30' E$ Gr. $\Delta G = + 58$ min.																																	JEZERSKO		BR. ST. 12			
I	-	-03.6	05.6	-02.1	01.7	07.7	-05.8	05.6	25	-12.1	06	.	.	.	06	01.5	05	01.6	.	.	.	07	04.1	02	05.0	15	03.7	38										
II	-	-04.3	06.4	-02.8	-02.4	01.6	-06.2	09.7	26	-15.6	16	01	02.0	01	02.3	01	01.0	11	03.7	10	03.0	11	02.6	37										
III	-	-06.1	07.2	01.8	02.7	08.1	-01.8	14.8	11	-07.7	20	.	.	11	02.2	07	03.1	06	02.8	.	.	10	04.0	11	03.7	13	02.6	35										
IV	-	00.9	07.6	02.8	03.6	09.1	-00.4	15.3	29	-05.7	19	.	.	16	02.5	05	02.6	03	01.7	01	04.0	10	03.4	06	02	01.5	47											
V	-	04.8	11.6	07.4	08.3	13.1	04.0	16.8	19	-02.7	12	01	02.0	11	02.3	03	01.7	01	03.0	.	.	14	03.5	12	02.3	08	02.6	63										
VI	-	10.1	17.4	11.2	12.5	18.5	0.4	24.6	07	02.1	15	.	.	03	01.3	05	02.4	01	01.0	.	.	08	04.3	09	03.2	10	03.7	54										
VII	-	10.9	18.2	12.9	13.7	19.6	0.7	25.0	13	01.9	06	.	.	04	02.8	02	02.5	03	02.0	.	.	11	03.5	12	03.0	12	03.0	49										
VIII	-	09.9	18.7	11.9	13.1	20.0	0.7	26.3	03	03.4	29	.	.	05	02.8	.	03	02.7	.	.	07	03.9	07	02.7	07	02.4	64											
IX	-	07.3	14.3	09.3	10.6	17.5	05.2	25.3	11	-02.1	21	.	.	04	02.8	06	02.7	02	02.0	.	.	08	03.3	06	02.7	13	02.5	51										
X	-	02.9	12.3	04.9	06.3	13.3	01.6	19.1	07	-02.7	22	.	.	10	03.0	04	02.3	04	03.0	.	.	02	04.5	03	02.7	11	02.1	59										
XI	-	-03.4	06.5	-02.5	-00.4	07.6	-04.6	12.7	01	-06.6	30	.	.	04	02.5	03	03.0	03	02.3	.	.	01	04.0	01	05.0	01	02.0	77										
XII	-	-03.3	00.5	-02.2	-01.8	01.9	-05.5	07.7	29	-21.1	08	.	.	06	02.7	01	03.0	02	04.0	.	.	08	03.9	11	02.8	13	03.5	52										
GOD.	-	02.8	09.8	04.3	05.3	11.0	00.7	26.3	03.VII	-21.1	08.XI	02	02.0	93	02.4	42	02.5	28	02.5	01	04.0	97	03.7	90	03.0	116	02.8	626										
$\varphi = 46^{\circ}04' N \lambda = 14^{\circ}31' E$ Gr. $\Delta G = + 58$ min.																																	LJUBLJANA-BEZIGRAD		BR. ST. 13			
I	730.8	-01.0	02.0	00.2	00.3	03.0	-02.3	09.3	04	-08.6	06	.	.	08	01.8	.	.	06	01.8	06	02.3	20	02.1	12	02.2	06	03.0	35										
II	730.0	-01.2	02.2	00.5	00.4	02.9	-02.0	12.3	28	-16.6	21	01	01.0	12	01.0	01	02.0	04	02.0	13	01.8	18	01.6	05	01.2	01	.	.										
III	732.4	02.5	11.6	06.8	06.9	12.7	01.0	19.6	31	-02.9	23	15	01.5	07	01.0	11	01.5	10	01.7	14	02.4	21	02.4	09	01.7	06	01.0	0.										
IV	729.4	04.6	12.7	08.4	08.5	13.1	03.0	19.7	28	-01.6	09	04	01.0	19	04	01.0	19	04	01.9	14	02.3	20	02.5	09	01.3	02	0.5	0.										
V	-	732.5	09.7	16.1	11.8	12.4	17.7	07.9	23.0	20	-00.4	12	09	01.2	15	01.3	10	01.7	11	01.8	16	01.8	18	02.0	07	01.6	06	01.2	01									
VI	-	733.4	13.5	21.8	16.6	21.0	23.0	10.8	28.8	03	06.0	29	06	01.4	15	01.3	17	01.5	15	01.4	18	01.8	18	02.2	07	02.0	06	01.3	.									
VII	-	735.4	14.2	22.4	17.3	17.8	23.9	12.2	29.1	13	08.5	23	04	01.8	22	01.3	23	01.4	11	01.6</																		

M	D	P	M	Temperatura vazduha °C								Čestina pravaca i srednja jačina vetrova m/s, Fm (0-12)												W		NW		C									
				Tm				Hm				Rm				Dm				Nm				Se				S				SW		W		NW	
				7	14	21	Broj (Broj)	1M	15	25	35	1M	15	25	35	1M	15	25	35	1M	15	25	35	1M	15	25	35	1M	15	25	35	1M	15	25	35		
$\psi = 46^{\circ}37' N \lambda = 15^{\circ}13' E$ Gr. AG = + 1h 01 min.																												RADLJE OB DRAVI		BR. ST. 16							
I	-	-02.4	02.3	-00.3	-00.2	03.2	-03.9	08.3	25	-13.0	06	02	01.5	01	01.0	01	01.0	03	01.0	01	01.0	03	01.0	02	01.0	06	01.5	74									
II	-	-02.2	04.1	00.2	00.6	04.8	-04.0	16.0	28	-15.5	21	01	01.0	02	02.0	01	01.0	02	01.0	01	01.0	09	01.4	.	02.	05	01.6	63									
III	-	02.0	12.1	03.7	06.6	13.0	00.5	20.5	30	-05.1	23	09	02.1	04	01.3	02	01.5	01	01.0	07	01.7	05	02.2	03	03.3	62											
IV	-	04.1	12.2	07.0	07.6	13.6	01.2	21.0	29	-05.3	19	01	01.0	01	01.0	07	01.4	03	01.7	04	02.0	04	01.5	05	02.2	64											
V	-	09.6	16.3	11.2	12.1	17.4	06.9	21.1	05	-00.3	12	.	.	03	01.0	.	.	04	01.0	.	.	10	01.2	03	02.3	06	01.5	67									
VI	-	12.7	21.4	15.2	16.1	22.5	09.8	29.4	07	02.8	29	01	02.0	01	01.0	01	02.0	04	01.5	08	01.6	01	01.0	10	01.6	66											
VII	-	13.8	21.9	16.5	17.2	23.3	11.3	28.0	29	06.9	06	03	01.0	.	.	03	01.0	11	01.5	.	.	07	01.1	02	01.0	06	01.3	61									
VIII	-	13.4	22.4	15.1	16.5	23.4	11.5	30.2	03	07.1	31	.	.	02	01.5	01	02.0	07	01.0	02	01.5	06	01.2	02	01.0	04	01.5	69									
IX	-	09.7	20.6	12.7	13.9	21.2	08.0	30.2	11	01.0	21	02	01.5	.	.	04	01.0	02	02.0	04	01.0	05	01.4	07	01.4	66											
X	-	06.2	15.4	08.3	09.5	16.6	04.6	22.5	07	-01.6	22	03	01.3	.	.	04	01.3	01	01.0	01	01.0	03	01.5	02	01.2	05	01.4	71									
XI	-	-00.6	04.9	-00.5	01.8	07.2	-01.0	14.3	01	-08.8	30	04	01.0	01	01.0	.	02	01.5	01	01.3	01	01.0	.	04	02.0	07	01.4	70									
XII	-	-03.1	01.5	-01.9	-01.4	02.3	-05.1	10.0	12	-19.8	07	06	01.3	.	.	02	01.0	03	01.3	01	01.0	.	.	04	02.0	07	01.4	70									
GOD.	-	05.2	13.1	07.5	08.3	14.0	03.3	30.2	44.1X	-15.8	07.31	32	01.5	15	01.3	15	01.2	47	01.2	17	01.5	62	01.4	33	01.6	68	01.6	806									
$\psi = 46^{\circ}15' N \lambda = 15^{\circ}15' E$ Gr. AG = + 1h 01 min.																											CELJЕ		BR. ST. 17								
I	-	-01.9	02.4	-00.5	-00.1	03.3	-03.3	09.6	03	-10.8	06	.	.	25	01.0	07	01.0	07	01.0	01	01.0	10	01.4	03	02.3	19	01.3	21									
II	-	-01.6	03.7	00.8	00.9	04.5	-02.6	15.4	28	-16.7	21	01	01.0	28	01.0	09	01.0	06	01.0	01	01.0	09	01.7	05	02.2	11	01.0	14									
III	-	02.2	11.9	06.2	06.6	12.9	00.8	20.2	30	-05.7	23	.	.	14	01.1	09	01.4	01	01.0	.	.	15	02.1	07	02.0	24	01.3	23									
IV	-	04.4	12.3	07.4	07.9	13.6	02.5	20.0	29	-04.5	09	03	01.0	18	01.2	07	02.1	08	01.4	01	03.0	10	01.9	08	01.1	13	01.3	22									
V	-	10.1	16.0	11.3	12.2	17.8	07.6	21.8	19	-00.7	12	03	02.0	10	01.3	06	01.8	11	01.1	02	01.5	20	01.7	13	01.5	14	01.1	14									
VI	-	14.4	22.1	16.2	17.2	23.4	10.6	28.6	07	05.0	29	04	01.0	10	01.1	07	01.3	12	01.3	04	01.5	19	01.3	18	01.3	12	01.3	23									
VII	-	14.6	22.4	17.3	17.9	24.2	11.7	29.0	12	07.6	09	03	01.3	11	01.4	07	01.4	13	01.4	05	01.8	24	01.5	10	01.6	14	01.1	11									
VIII	-	13.6	22.4	15.8	16.9	23.4	11.3	30.2	03	07.0	15	05	01.0	13	01.3	10	01.2	08	01.5	05	01.8	12	01.6	20	01.3	10	01.0	10									
IX	-	09.7	20.2	13.0	14.0	21.3	07.9	28.8	11	00.2	21	04	01.0	20	01.1	05	01.4	09	01.6	04	01.3	19	01.4	07	01.4	15	01.1	07									
X	-	05.8	14.0	07.6	08.9	15.4	04.6	20.9	07	-06.4	25	03	01.0	25	02.1	07	01.1	07	01.4	05	01.7	01	01.0	09	01.0	04	01.0	09	01.1	18							
XI	-	-00.6	03.8	-00.2	00.7	04.2	-01.5	13.6	01	-10.2	30	01	01.0	30	01.1	10	01.0	08	01.1	01	01.0	09	01.0	04	01.0	09	01.1	18									
XII	-	-02.0	02.9	-01.6	-00.4	03.6	-04.2	12.1	30	-15.4	01	01	12	01.1	10	01.2	06	01.2	05	01.0	14	01.4	16	01.6	17	01.1	12										
GOD.	-	05.7	12.9	07.8	08.6	14.0	03.8	30.2	03.VM	-16.7	24.II	28	01.1	216	01.1	94	01.3	96	01.3	24	01.4	175	01.5	118	01.4	170	01.2	174									
$\psi = 46^{\circ}06' N \lambda = 15^{\circ}24' E$ Gr. AG = + 1h 02 min.																											SELA PRI PLANINI NAD SEVNICO		BR. ST. 18								
I	-	-01.5	00.6	-00.9	-00.6	02.1	-02.9	08.0	03	-09.4	06	02	02.0	03	02.3	21	03.0	16	03.1	.	.	02	03.5	13	04.5	08	02.5	28									
II	-	-01.8	01.4	-00.3	00.3	02.1	-02.6	12.2	28	-11.1	21	02	03.0	03	02.7	29	03.4	14	02.9	.	.	02	03.0	15	04.4	03	02.7	16									
III	-	03.4	09.3	03.5	05.9	10.7	02.1	17.9	30	-02.6	08	01	02.0	02	02.0	12	04.0	17	03.2	02	03.0	10	04.3	31	04.3	02	02.5	16									
IV	-	05.0	09.1	06.4	06.9	11.1	02.9	17.8	29	-02.8	09	.	.	32	04.0	09	03.9	03	03.0	.	.	18	03.8	06	02.2	22	02.2	22									
V	-	09.6	13.6	10.1	10.9	15.3	07.6	19.3	19	-02.7	12	03	02.0	03	02.7	17	03.6	01	04.0	04	03.0	22	03.4	15	02.1	22											
VI	-	13.9	19.1	14.8	15.7	20.6	11.0	26.0	08	04.8	29	02	02.0	02	02.5	17	03.0	17	03.8	.	.	04	03.5	23	03.6	02	02.7	22									
VII	-	14.8	20.0	15.7	16.6	21.6	12.0	26.5	12	06.0	22	03	01.7	03	03.7	16	03.0	16	04.0	04	02.8	03	04.3	17	03.6	17	02.3	17									
VIII	-	13.9	20.1	15.2	16.1	21.4	12.1	27.4	07	07.0	27	.	.	02	03.5	14	03.2	24	03.5	02	03.0	05	03.0	15	03.1	08	02.4	23									
IX	-	11.3	17.7	13.1	13.8	19.7	09.6	29.4	11	02.4	21	08	01.1	03	03.3	12	02.7	18	03.8	07	03.0	04	03.0	15	03.9	05	02.2	28									
X	-	06.6	12.3	08.4	09.0	13.3	04.0	18.4	07	00.3	22	01	02.0	04	02.5	24	03.3	17	03.4	.	.	03	02.7	06	02.6	22	02.0	28									
XI	-	-00.1	04.7	00.2	01.3	05.0	-01.6	12.9	16	-06.4	19	31	02.0	01	03.0	18	03.2	20	03.1	01	03.0	01	03.0	07	02.9	02	02.5	39									
XII	-	00.3	02.4	01.0	01.2	04.0	-01.5	10.7	30	-11.0	06	02	02.0	05	02.8	17	03.9	06	03.2	01	04.0	07	03.3	28	04.5	09	02.4	48									
GOD.	-	06.3	10.9	07.4	08.0	13.0	04.7	20.0	03.VM	-15.4	24.II	95	02.5	71	02.4	38	02.2	102	02.8	144	03.2	40	02.6	65	02.4	109	02.8	431									
$\psi = 46^{\circ}24' N \lambda = 15^{\circ}39' E$ Gr. AG = + 1h 03 min.																											PRAGERSKO		BR. ST. 20								
I	-	-02.1	02.1	-00.6	-00.3	02.0	-03.5	10.0	03	-11.4	04	06	01.0	20	01.9	.	.	.	07	01.1	58								
II	-	-01.8	03.5	00.2	00.6	04.2	-03.1	16.0	28	-19.4	21	0																									

Mjesec	Vremenski period Pm	Temperatura vazduha °C										Cestina pravaca i srednja jačina vетра ND, Pm (0-12)																	
		Tm			Sred. (Dne)				Dat.			N			NE		E		SE		S		SW		W		NW		C
		7	14	21	Min	Max	Min	Max	Min	Max	Min	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.		
$\varphi = 46^{\circ}38' N \lambda = 16^{\circ}11' E$ Gr. AG = + 1h 05 min.																													
I	745.3	-02.4	01.7	-00.9	-00.6	02.5	-04.1	08.6	27	-12.4	06	05	01.6	11	02.0	04	02.8	13	02.2	05	03.0	04	01.3	03	02.0	21	01.5	27	
II	741.2	-02.1	03.1	-00.5	00.0	04.0	-03.9	17.2	26	-23.6	21	07	02.6	21	02.2	05	01.6	11	02.1	07	02.6	05	04.4	03	01.3	10	01.2	15	
III	743.0	02.5	11.5	05.6	06.3	12.4	00.4	21.3	30	-0.6	20	12	02.6	09	02.3	05	01.4	05	02.0	09	03.6	12	04.0	04	01.5	04	02.0	33	
IV	740.8	04.6	12.9	07.3	08.1	14.0	02.1	21.4	30	-0.3	08	09	15	03.1	14	02.6	06	02.0	08	01.9	06	03.5	09	03.0	02	02.0	09	01.9	21
V	743.2	10.8	16.9	11.8	12.8	18.0	07.2	23.2	31	-0.4	12	15	02.4	13	01.9	03	01.7	05	02.2	09	02.4	05	04.6	08	09	01.8	34		
VI	743.9	14.0	22.4	15.6	16.9	23.0	10.3	27.9	27	05.0	15	05	02.6	09	01.6	03	01.0	10	01.4	08	02.4	09	02.1	07	01.7	13	01.6	26	
VII	745.7	14.5	22.4	15.8	17.1	23.6	10.9	27.8	29	05.1	23	06	02.0	07	01.7	02	01.0	13	01.5	11	01.9	07	02.3	02	01.5	16	01.4	31	
VIII	746.3	13.3	22.5	14.9	16.5	23.2	10.1	29.4	27	02.1	27	05	01.6	03	02.3	04	01.0	08	02.1	05	02.3	10	02.7	03	01.7	11	01.5	44	
IX	745.5	09.3	19.5	12.5	13.5	20.5	07.0	29.3	11	-0.6	21	06	03.0	01	01.0	06	01.5	07	01.3	08	01.8	04	02.3	05	01.8	16	01.4	37	
X	749.8	05.5	14.2	07.2	08.5	15.0	03.7	26.7	27	-0.3	28	05	02.0	09	01.9	01	01.0	26	01.7	08	02.3	04	01.5	08	01.3	50			
XI	754.3	-00.6	02.3	00.3	00.6	02.8	-01.3	13.1	01	-10.0	20	05	02.2	03	01.3	07	01.1	12	01.6	09	01.2	07	01.3	03	01.7	14	01.4	30	
XII	742.5	-02.6	02.4	-01.2	-00.7	03.3	-03.3	13.0	30	-15.7	08	04	02.0	09	02.0	02	01.0	13	03.4	08	03.2	02	02.0	14	01.3	41			
GOD.	745.1	05.6	12.6	07.4	08.2	13.5	03.1	29.4	07.VIII	-23.6	21.II	88	02.5	109	32.0	48	01.5	100	01.8	98	02.5	82	02.8	34	01.7	147	01.5	389	
$\varphi = 46^{\circ}28' N \lambda = 16^{\circ}12' E$ Gr. AG = + 1h 05 min.																										JERUZALEM		BR, ST. 22	
I	-	-01.3	01.5	-00.4	-00.2	02.6	-02.6	08.5	04	-0.5	06	01	02.0	32	02.3	0.	0.	23	02.5	0.	0.	29	02.1	04	01.5	04	01.8	.	
II	-	-01.2	02.4	00.3	00.5	03.6	-02.1	15.5	26	-11.5	22	01	01.0	37	02.6	01	01.0	13	02.3	0.	0.	26	02.9	0.	0.	06	01.5	.	
III	-	04.1	10.9	06.1	06.9	12.2	02.7	20.5	29	-0.2	07	0.	0.	38	02.5	01	03.0	08	02.6	0.	0.	43	02.6	01	01.0	02	02.0	.	
IV	-	05.9	12.0	08.2	08.6	13.4	04.6	21.5	30	-0.5	07	0.	0.	47	02.6	0.	0.	10	01.5	0.	0.	26	02.6	05	01.2	02	01.5	.	
V	-	11.6	15.9	11.9	12.9	17.9	09.1	22.0	31	-0.1	12	0.	0.	31	02.7	05	02.0	15	02.4	03	01.0	35	01.7	01	01.0	03	02.0	.	
VI	-	15.0	21.6	16.3	17.3	22.6	12.5	28.5	27	04.0	13	0.	0.	23	02.2	01	02.0	16	01.8	01	02.0	44	02.2	04	01.5	01	02.0	.	
VII	-	15.9	21.7	17.6	18.3	23.5	13.6	27.5	29	07.5	22	03	01.0	23	02.0	02	01.0	11	02.1	01	03.0	46	01.9	02	02.0	05	02.0	.	
VIII	-	15.4	22.2	16.4	17.7	23.4	13.9	29.5	27	09.5	28	01	01.0	23	02.2	03	02.3	11	01.9	01	01.0	34	01.8	03	01.7	02	01.5	.	
IX	-	11.9	19.2	14.5	15.1	20.4	10.5	20.0	11	05.0	21	0.	0.	21	02.1	0.	0.	11	01.9	02	01.5	49	02.1	02	01.5	05	02.0	.	
X	-	07.5	13.7	09.9	10.3	14.4	06.7	20.0	07	00.6	28	05	01.0	32	01.9	01	01.0	12	01.3	03	01.0	28	02.0	01	01.0	11	01.5	.	
XI	-	-00.7	01.7	00.3	00.4	02.2	-00.7	11.5	01	-03.5	23	02	01.0	19	01.7	02	01.5	25	01.4	02	01.0	32	01.1	04	01.0	04	01.3	.	
XII	-	-00.2	02.6	01.0	01.1	03.9	-01.6	12.0	13	-10.5	06	04	01.3	22	02.1	01	01.0	10	01.3	01	01.0	53	02.3	01	02.0	01	01.0	.	
GOD.	-	07.0	12.1	08.5	09.1	13.3	05.5	20.0	MIX	-11.5	22.II	17	01.1	348	02.3	17	01.8	165	01.9	14	01.3	460	02.1	28	01.4	46	01.7	.	
$\varphi = 46^{\circ}30' N \lambda = 16^{\circ}17' E$ Gr. AG = + 1h 05 min.																										VELIKI DOLENCI		BR, ST. 23	
I	-	-01.8	01.4	-00.4	-00.3	02.4	-02.8	07.5	25	-11.5	06	13	01.7	12	01.8	03	01.7	25	02.0	05	01.6	09	02.0	14	01.6	12	02.2	.	
II	-	-02.2	02.4	-00.9	-00.4	03.1	-03.2	16.0	26	-14.5	22	01	01.9	18	02.4	04	01.3	16	01.7	05	01.4	15	01.9	05	01.2	06	01.5	.	
III	-	02.0	10.3	05.5	06.1	11.2	01.7	20.0	30	-0.2	13	17	02.0	07	01.9	01	01.0	17	01.5	09	02.1	09	01.2	13	02.6	.			
IV	-	03.7	11.7	07.3	08.1	12.8	09.9	21.0	30	-0.6	07	17	02.1	20	03.1	02	01.0	20	01.8	09	02.1	08	01.2	06	01.8	08	01.0	.	
V	-	11.0	15.7	11.3	12.3	17.1	08.4	22.2	31	-0.8	12	14	02.6	15	02.6	04	02.0	20	01.6	10	01.8	18	01.8	08	09	01.8	12	01.8	.
VI	-	14.8	20.8	15.1	16.5	21.8	11.8	27.0	24	07.5	15	15	01.9	07	02.1	05	01.6	17	01.6	10	02.0	15	01.9	03	01.7	18	01.9	.	
VII	-	15.6	21.3	16.3	17.4	22.7	12.6	27.6	29	08.6	22	09	01.0	16	06	07	01.4	15	01.8	16	01.8	21	02.0	04	01.5	11	01.7	.	
VIII	-	14.9	21.1	15.7	16.9	22.4	12.7	26.8	27	08.0	27	11	01.2	12	02.3	04	01.8	11	02.0	14	01.7	06	01.7	15	02.1	02	02.1	.	
IX	-	12.1	18.6	13.5	14.4	19.9	10.0	29.5	11	04.0	21	09	01.9	10	02.0	06	01.8	06	01.8	05	01.6	28	01.7	08	01.5	18	01.8	.	
X	-	06.9	13.9	09.3	09.9	14.6	06.1	20.0	07	-0.5	28																		

Mjesec	Vremenski interval m	Temperatura vazduha °C										Čestina pravaca i srednja jačina vjetra m/s, fm (0-12)																	
		Tm			Det.							N	NE	E	SE	S	SW	W	NW	C									
		7	14	21	Sred. (Dnev.)	M	H	M	N	S	D	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.						
$\varphi = 45^{\circ} 51' N \lambda = 13^{\circ} 40' E$ Gr. AG = + 55 min.																													
I	-	02.8	05.9	03.3	03.8	06.8	01.4	12.4	14	-0.4	0	03	03.7	05	01.4	44	03.6	03	02.7	06	03.7	01	02.0	.	01	01.0	30		
II	-	02.0	05.0	02.7	03.2	05.7	02.8	11.5	28	-0.4	4	21	01	02.0	07	02.6	33	02.8	01	02.0	.	02	02.0	.	01	01.7	40		
III	-	06.1	10.6	06.4	07.4	11.5	06.6	16.0	12	01.6	19	31	01.0	17	03.2	05	01.6	07	02.9	06	02.3	02	01.5	03	01.7	47			
IV	-	08.3	12.3	08.9	09.6	13.3	06.9	17.3	23	02.8	18	.	.	09	02.3	30	03.7	03	01.7	34	02.5	08	02.4	03	02.0	.	33		
V	-	12.5	15.1	11.9	12.9	16.3	10.0	23.0	29	02.2	12	03	03.0	04	02.5	25	02.9	07	01.7	07	02.1	03	03.0	02	02.0	02	02.5	40	
VI	-	17.2	21.1	16.4	17.8	21.8	13.7	24.4	03	09.5	14	01	02.0	03	01.7	25	03.0	06	02.3	16	02.7	05	03.2	.	01	03.0	33		
VII	-	16.3	23.1	18.5	19.6	23.9	15.3	29.0	29	10.4	22	02	03.0	02	01.5	31	02.8	04	02.0	11	02.5	03	02.4	.	01	02.0	37		
VIII	-	16.0	22.8	17.5	19.0	23.6	14.3	28.2	06	09.0	31	05	02.2	04	01.8	33	03.0	02	03.5	08	02.4	05	02.8	01	03.0	01	02.0	34	
IX	-	15.0	19.9	15.1	16.3	20.7	12.0	25.0	16	05.6	28	03	02.3	09	02.6	22	02.8	02	01.5	07	02.6	07	02.4	03	02.3	01	01.0	36	
X	-	11.1	16.7	12.0	13.0	17.4	09.1	22.6	11	03.2	27	01	02.0	06	02.8	20	03.1	01	01.0	01	02.0	02	01.5	01	02.0	09			
XI	-	06.2	12.1	07.3	08.2	12.7	03.5	19.3	15	-0.4	0	30	01	02.0	05	02.8	46	03.6	34	02.5	01	01.0	02	01.0	01	01.0	29		
XII	-	03.2	04.7	03.2	03.6	05.8	01.0	10.4	24	-0.7	8	.	.	03	03.0	29	04.2	01	01.0	08	02.1	.	.	.	01	01.0	51		
GOD.	-	10.1	14.1	10.3	11.2	15.0	07.7	29.0	29	VM -07.8	07.XII	21	02.5	60	02.3	405	03.2	39	02.0	76	02.6	48	02.4	14	02.1	13	01.8	419	
$\varphi = 45^{\circ} 31' N \lambda = 13^{\circ} 52' E$ Gr. G = Δ ± 55 min.																													
I	-	02.3	07.0	02.9	03.8	08.5	00.4	15.0	14	-0.6	0	07	02	02.5	10	02.2	10	03.3	04	02.5	43	02.3	11	01.9	07	01.6	06	02.2	
II	-	01.9	06.5	03.2	03.7	07.7	00.4	13.0	25	-0.7	5	21	02	02.0	14	02.1	19	03.0	09	02.4	32	02.3	07	01.9	01	02.0	.	.	
III	-	04.5	11.3	05.9	06.9	12.6	02.9	18.0	30	-0.2	0	11	08	02.1	08	02.8	13	03.0	05	03.0	26	02.3	15	02.1	08	01.8	10	02.1	
IV	-	07.0	12.9	08.0	09.2	14.4	05.1	18.0	03	-0.5	9	19	05	03.0	06	01.8	20	03.6	04	02.5	34	02.2	09	01.9	05	01.6	07	02.4	
V	-	12.2	15.8	11.0	12.9	17.8	08.8	23.5	29	03.5	16	01	02.0	07	02.3	11	03.2	04	02.8	36	02.1	18	02.2	06	01.8	10	01.8	.	
VI	-	17.0	22.0	15.7	17.6	23.5	11.5	27.6	09	05.5	29	04	02.5	04	01.5	06	02.5	03	02.7	17	02.5	23	01.8	22	02.1	13	01.7	.	
VII	-	18.1	24.3	17.3	19.3	25.4	13.5	30.0	29	09.0	08	12	02.6	06	02.7	06	03.2	05	02.0	20	01.9	16	01.8	25	01.8	03	01.7	.	
VIII	-	16.4	23.5	16.4	18.3	24.9	13.0	29.0	02	08.0	29	06	02.5	06	03.0	12	02.8	07	02.1	29	01.6	17	01.5	12	02.2	04	02.5	.	
IX	-	13.3	20.5	14.0	15.3	21.8	10.2	24.0	16	05.0	22	01	03.0	10	02.7	10	03.1	06	02.7	26	01.8	20	01.6	11	01.7	06	02.3	.	
X	-	06.3	17.7	09.7	11.4	18.8	06.5	24.5	12	02.0	31	08	02.6	20	02.3	11	03.2	09	02.4	14	02.0	10	01.7	09	01.6	12	02.0	.	
XI	-	01.7	12.6	03.2	03.2	13.6	06.3	20.0	15	-0.5	9	30	16	01.9	15	02.7	11	03.6	02	01.0	13	01.8	15	01.7	09	01.9	09	01.6	.
XII	-	03.5	06.7	03.8	04.4	07.7	01.2	11.5	29	-10.5	08	04	01.8	06	03.0	07	04.4	03	02.7	55	01.9	12	01.5	02	02.5	04	01.8	.	
GOD.	-	09.0	15.1	09.3	10.7	16.4	06.2	30.0	29	VM -10.5	08.XII	69	02.3	112	02.4	134	03.2	61	02.4	345	02.1	173	01.8	117	01.9	84	02.0	.	
$\varphi = 45^{\circ} 52' N \lambda = 12^{\circ} 04' E$ Gr. AG = + 54 min.																													
I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
IV	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
V	-	12.6	16.6	12.8	13.6	18.1	09.0	24.0	29	02.2	16	11	03.2	06	04.7	15	02.6	03	02.0	10	02.3	02	03.0	10	02.7	01	03.0	35	
VI	-	16.5	23.2	16.4	18.1	24.3	11.7	26.6	03	04.3	29	08	01.9	09	04.2	12	03.6	03	02.7	06	01.8	03	03.0	13	02.5	05	02.4	31	
VII	-	16.6	25.3	19.4	20.7	26.3	14.0	31.1	14	07.8	09	15	02.3	09	03.4	15	02.5	05	01.5	08	01.9	04	02.3	11	02.3	09	01.7	16	
VIII	-	17.7	25.1	18.7	20.0	26.1	14.7	31.0	06	07.9	15	01	04.1	13	03.3	21	03.0	05	02.0	07	01.4	13	01.8	05	01.6	11	01.6	11	
IX	-	12.8	21.7	14.4	15.9	22.5	10.1	27.1	16	04.1	22	05	02.2	07	04.0	14	02.9	03	01.7	03	02.3	02	02.5	13	02.1	04	01.8	39	
X	-	11.5	18.0	13.3	14.1	19.0	10.0	24.1	07	01.8	25	05	05.0	23	05.0	21	04.8	08	02.5	10	02.8	05	02.0	06	01.7	01	01.0	14	
XI	-	04.7	13.8	06.5	07.9	14.3	02.5	19.4	15	-0.5	1	20	05	02.2	13	05.1	23	04.4	11	03.0	09	02.3	01	02.0	04	02.0	03	02.3	20
XII	-	03.1	05.5	03.8	04.1	06.5	01.0	11.3	26	-0.8	1	08	04	02.5	13	05.2	21	04.3	10	02.4	05	03.6	03	02.0	07	02.0	01	02.0	29
GOD.	-	05.2	11.4	07.0	07.6	12.4	03.3	27.5																					

Meseč Broj	Oblačnost Nm (0-10)			Temperatura broj sati (Dnevi)	Vlažnost vazduha			Padavine R mm			Brodj dana na sat																										
	7	14	21		7	14	21	Tm (Dnevi) MIN	Tm (Dnevi) MAX	Dan.	Tn	Tn	Tn	Tn	Tn	Tn	P(0-12)	Nm(0-10)	R mm	•	*	Δ	▲	▲	R	T	≡										
					7	14	21	MIN	MAX	Dan.	≤	<	=	≥	≥	≥	≤	≥	<	>	≥	≤	≥	Δ	▲	▲											
NAVELO PRI TEMNICI																																					
BR. ST. 26																																					
I	7.1	6.3	6.3	6.6	88.6	4.5	75	67	75	73	26	155	045.3	29	•	•	06	•	•	04	•	06	14	12	11	06	12	02									
II	6.9	6.4	6.4	6.6	97.5	24.5	73	70	79	74	33	146	030.0	26	•	•	12	•	•	01	•	04	13	11	11	06	10	05	•								
III	5.1	5.7	5.0	5.3	151.2	05.3	68	60	74	68	25	071	034.7	24	•	•	•	•	•	01	•	09	09	09	08	02	02	02	06								
IV	7.2	6.4	6.9	6.9	137.2	36.1	70	58	72	67	33	206	100.0	13	•	•	•	•	•	04	•	11	09	05	09	•	•	•	01								
V	6.7	7.5	8.1	7.5	132.1	08.4	74	70	79	74	40	222	042.4	14	•	•	•	•	•	01	•	17	24	19	09	24	•	•	01								
VI	4.9	4.6	4.5	4.6	247.8	10.4	69	58	73	67	40	142	054.0	13	•	•	05	•	•	07	05	10	09	03	10	•	•	01									
VII	5.4	6.4	6.9	5.3	251.2	11.7	71	59	72	67	37	114	031.2	19	•	•	13	•	•	02	•	05	04	14	11	05	14	•	02								
VIII	3.5	4.5	4.7	4.2	248.7	11.5	73	59	75	68	42	241	108.7	05	•	•	13	•	•	04	•	03	13	12	04	13	•	•	01								
IX	6.0	4.9	4.8	5.2	200.4	10.3	75	63	77	72	40	173	135.0	28	•	•	01	•	•	01	•	04	05	09	06	02	09	•	•	05							
X	3.2	2.6	2.2	2.7	219.7	37.8	74	59	72	68	38	106	048.7	05	•	•	01	•	•	01	•	18	03	06	03	36	•	•	•	•							
XI	2.3	2.1	1.9	2.1	176.6	04.8	62	50	61	57	28	048	049.7	27	•	•	02	•	•	02	•	21	04	03	03	02	02	01	•	•							
XII	7.9	7.9	7.5	7.8	044.4	05.2	85	80	84	83	30	211	034.0	29	•	03	11	•	•	04	01	04	20	16	15	08	14	03	•	14							
GOD.	5.5	5.3	5.3	5.4	1992.0	37.5	72	62	74	69	25	1855	135.0	28.IX	•	03	31	32	•	02	19	01	84	108	136	119	55	132	11	•	01						
KUBEDO																																					
BR. ST. 27																																					
I	7.1	5.0	5.5	6.6	-	-	-	-	-	-	-	155	036.5	30	•	•	13	•	•	01	•	07	14	12	12	05	12	02	•	01							
II	6.8	6.4	5.5	6.2	-	-	-	-	-	-	-	085	018.5	20	•	•	13	•	•	05	•	11	11	10	06	10	05	02	•	01							
III	5.7	6.3	4.4	5.5	-	-	-	-	-	-	-	066	023.0	24	•	•	05	•	•	08	•	10	12	10	01	12	01	01	•	01							
IV	6.8	8.2	5.6	6.9	-	-	-	-	-	-	-	109	027.5	13	•	•	01	•	•	01	•	15	13	10	04	13	•	•	03	•	03						
V	7.0	8.3	6.5	7.3	-	-	-	-	-	-	-	129	025.1	14	•	•	08	•	•	03	•	14	16	16	05	14	•	•	04	01	•						
VI	4.3	6.0	4.1	4.8	-	-	-	-	-	-	-	082	026.5	13	•	•	09	•	•	08	•	03	11	08	04	11	•	01	04	•	•						
VII	4.7	5.5	2.5	4.2	-	13.2	82	61	86	76	42	079	026.2	20	•	•	17	01	•	05	•	01	11	03	11	•	02	05	•	03	•						
VIII	3.3	5.2	2.4	3.7	-	13.0	86	64	89	80	47	149	098.4	31	•	•	16	•	•	11	03	08	07	03	08	•	•	01	03	•							
IX	5.1	5.2	2.6	4.3	-	11.0	86	66	90	81	36	145	097.0	28	•	•	02	•	•	06	06	07	07	03	07	•	•	04	•	•							
X	3.2	3.2	1.8	2.8	-	08.0	67	57	86	77	40	085	027.1	32	•	•	•	•	•	17	04	06	06	03	06	•	•	02	•	•							
XI	2.8	2.2	2.2	2.4	-	05.1	85	53	86	75	38	078	041.4	27	•	•	11	•	•	02	•	17	03	05	03	03	01	01	•	02	•						
XII	7.7	7.7	6.9	7.5	-	05.7	90	78	88	86	42	157	020.0	09	01	•	12	•	04	•	05	20	17	15	08	14	02	01	•	10	03						
GOD.	5.4	5.0	4.2	5.2	-	-	-	-	-	-	-	1319	097.0	28.IX	01	•	55	44	01	•	10	•	94	104	127	114	46	125	11	05	•	01	03	01	26	16	05
AJDOVŠČINA																																					
BR. ST. 28																																					
I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-					
II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-					
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-					
IV	-	-	-	-	-	-	-	-	-	-	-	187	076.0	13	•	•	•	•	•	07	06	•	•	11	10	05	11	•	•	02	•	02	-				
V	7.5	8.3	7.5	7.8	123.2	08.6	81	62	78	76	33	230	033.0	24	•	•	•	•	•	09	06	01	18	23	20	08	23	•	•	09	03	•	•				
VI	4.6	5.2	4.5	4.8	228.5	10.0	75	44	73	64	25	109	040.6	18	•	•	14	•	•	08	02	04	07	13	10	03	13	•	•	09	•	•	•				
VII	5.7	5.7	4.7	5.4	238.5	11.2	70	46	69	62	30	222	109.4	05	•	•	19	03	02	10	04	04	07	14	13	05	14	•	•	11	•	•	11				
VIII	6.6	4.5	3.7	4.3	253.1	11.0	72	47	69	62	33	131	028.7	31	•	•	21	04	•	13	01	03	03	12	04	12	04	•	•	09	02	•	02				
IX	6.0	5.3	4.4	5.2	195.4	09.5	81	50	7																												

Meseč	Vremenski period	Temperatura vazduha °C										Čestina pravaca i srednja jačina veta nD, fm (0-12)																					
		Tm		Sred. (Dnev.)		Max.		Min.		Dat.		Min.		Dat.		W		NE		E		SE		S		SW		W		NW		C	
		7	14	21	Sred. (Dnev.)	Max.	Min.	Max.	Min.	Dat.	Min.	Dat.	Min.	Dat.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.					
$\varphi = 45^{\circ}38' N \lambda = 14^{\circ}22' E$ Gr. AG = + 57 min.															MARLN												BR. ST. 31						
I	-	-03.1	00.1	-02.9	-02.2	01.2	-05.2	06.4	14	-11.1	09	-	-	-	08	31.3	25	01.8	12	01.5	02	02.0	21	01.7	03	01.0	13	01.2	-				
II	-	-04.3	-01.2	-03.3	-03.3	00.1	-06.2	07.4	23	-15.6	16	-	-	-	08	31.3	25	01.8	12	01.5	02	02.0	21	01.7	03	01.0	13	01.2	-				
III	-	-00.2	05.1	00.3	01.4	06.2	-02.2	12.2	04	-09.5	20	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-					
IV	-	01.7	06.0	02.1	03.0	07.1	-00.2	11.9	30	-06.7	17	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-					
V	-	04.7	09.6	04.2	07.2	11.5	03.7	16.2	31	-04.8	12	01	01.0	12	01.2	18	01.4	08	01.0	04	01.3	17	01.4	28	01.3	05	01.0	-					
VI	-	11.5	15.9	10.1	11.9	17.2	06.7	23.5	07	00.6	29	06	11.2	08	04.1	14	01.1	11	01.4	-	26	01.7	07	01.3	18	01.2	-						
VII	-	12.2	17.5	11.3	13.1	18.8	07.8	24.3	13	02.4	09	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
VIII	-	10.6	17.3	10.6	12.3	18.4	07.5	23.2	06	02.9	31	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
IX	-	07.0	14.7	08.0	09.4	15.7	04.5	21.7	11	-00.7	01	-	-	-	07	01.3	66	01.6	07	01.1	03	01.0	05	01.4	-	-	-	-					
X	-	03.7	11.1	04.8	06.1	11.8	02.6	17.7	10	-02.3	28	-	-	-	07	01.3	66	01.6	07	01.1	03	01.0	05	01.8	-	-	-	-					
XI	-	-01.9	06.2	-01.4	00.4	07.4	-03.5	13.0	11	-09.3	30	-	-	-	07	01.3	66	01.6	07	01.0	03	01.0	05	01.8	-	-	-	-					
XII	-	-01.8	06.5	-01.7	-01.2	01.8	-04.5	08.2	11	-16.6	08	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
GOD.	-	03.5	08.6	03.7	04.9	09.8	00.9	24.3	15.VII	-16.6	08.XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-					
$\varphi = 45^{\circ}53' N \lambda = 14^{\circ}26' E$ Gr. AG = + 58 min.															RAKITNA												BR. ST. 32						
I	-	-02.3	00.5	-02.3	-01.7	01.5	-05.4	08.1	14	-12.8	09	05	02.1	14	02.2	19	02.4	07	02.0	12	01.4	09	02.0	16	01.3	08	02.4	01					
II	-	-03.8	-00.4	-02.0	-02.5	00.9	-06.7	08.3	23	-19.3	21	07	01.6	07	02.7	17	02.6	19	02.2	10	01.5	02	02.5	06	01.2	10	02.7	06					
III	-	00.7	07.3	02.3	03.1	08.2	-01.7	14.5	31	-11.7	20	04	01.5	19	03.1	04	02.5	11	02.2	09	02.3	11	02.6	12	02.1	20	02.4	33					
IV	-	02.2	07.8	04.1	04.6	08.9	00.3	14.1	01	-10.3	17	14	01.6	12	02.2	08	02.5	18	02.4	15	01.7	03	02.3	11	02.0	07	02.6	02					
V	-	08.3	11.4	08.2	09.1	13.2	04.8	18.8	20	-03.6	15	09	01.8	21	02.1	12	02.3	09	02.1	07	01.1	12	02.1	13	01.6	09	02.3	01					
VI	-	12.7	17.3	13.6	13.8	18.5	07.3	22.6	03	-00.5	29	07	02.3	07	03.0	15	02.4	13	02.2	07	02.3	08	01.8	15	02.1	16	02.9	02					
VII	-	13.3	18.3	13.9	14.3	19.8	08.1	24.3	13	-01.0	09	07	02.0	19	02.2	11	02.4	08	01.8	09	01.1	16	01.9	04	01.5	14	02.1	33					
VIII	-	11.8	16.4	12.1	13.1	19.5	07.5	24.8	01	-02.4	20	13	01.3	09	01.4	23	02.3	12	02.2	09	01.2	11	01.0	08	01.9	06	01.7	02					
IX	-	09.0	16.2	10.4	11.5	17.1	09.5	22.4	11	-01.6	21	08	01.5	16	07.4	02	01.0	10	02.1	08	01.6	23	01.9	38	02.6	13	02.1	02					
X	-	03.8	11.3	04.7	06.1	12.2	01.9	16.8	10	-04.7	30	12	01.7	14	01.9	12	02.4	07	02.4	20	01.7	07	01.6	10	01.5	09	01.7	02					
XI	-	-03.1	05.0	-02.0	-00.5	05.8	-05.0	11.0	16	-13.7	30	06	01.5	03	01.0	15	01.7	21	02.0	07	01.9	15	01.6	10	01.8	04	01.0	09					
XII	-	-01.9	01.1	-01.4	-01.0	02.5	-04.7	09.3	29	-20.6	01	-	-	33	02.5	-	-	01	02.0	-	13	03.5	05	02.6	20	02.2	07	02.6	22				
GOD.	-	04.2	09.5	04.8	05.9	10.7	01.0	24.8	04.VIII	-20.1	03.XI	108	01.7	151	02.3	153	02.3	147	02.2	131	01.7	124	02.0	120	01.8	126	02.3	35					
$\varphi = 45^{\circ}46' N \lambda = 14^{\circ}31' E$ Gr. AG = + 58 min.															NOVA VAS NA BLOKAMA												BR. ST. 33						
I	-	-02.5	01.3	-01.9	-01.3	02.3	-05.1	08.3	14	-13.0	28	-	-	43	02.0	01	02.0	02	01.5	-	-	07	02.7	04	04.3	16	02.1	-					
II	-	-04.3	00.7	-02.2	-02.0	01.7	-06.4	09.2	23	-19.3	21	-	-	40	02.0	02	02.5	-	-	03	03.3	01	03.0	19	02.1	-	-	-					
III	-	00.4	08.1	02.6	03.6	08.9	-01.8	15.5	31	-10.4	25	-	-	24	01.9	01	01.0	02	04.0	01	04.0	08	02.0	03	04.7	31	03.0	23	-				
IV	-	02.0	08.6	04.5	04.9	09.7	00.5	15.6	30	-06.5	17	-	-	36	02.4	01	01.0	04	01.3	-	07	02.6	-	-	18	02.3	24	-	-				
V	-	08.4	12.2	08.2	09.3	14.0	05.0	18.6	20	-03.2	12	-	-	29	01.8	01	01.0	03	02.0	02	02.3	02	03.0	31	02.1	21	-	-					
VI	-	12.0	16.1	12.5	13.0	19.4	07.1	23.8	03	00.4	29	-	-	24	01.7	-	-	04	03.3	-	-	12	02.9	-	-	29	02.2	-	-				
VII	-	12.5	19.6	13.5	14.8	20.7	08.1	25.8	13	02.0	09	01	03.0	41	01.9	02	02.5	03	04.0	-	-	04	02.3	01	02.0	22	02.3	19	-				
VIII	-	10.8	16.5	12.5	13.0	20.6	07.6	25.6	02	00.6	12	05	02.8	12	01.8	20	01.8	01.0	01.8	-	03.0	02	03.5	32	02.5	22	02.2	27					
IX	-	07.4	16.8	09.9	11.0	17.9	04.9	23.1	11	-01.3	21	-	-	28	02.0	04	02.0	01	04.0	-	-	05	02.6	-	-	24	02.4	28	-	-			
X	-	04.0	12.2	04.9	06.5	12.8	02.2	17.8	10	-05.4	30	-	-	45	02.1	-	-	01	01.0	01	02.0	-	04	02.0	02	03.0	14	01.8	28	-	-		
XI	-	-03.1																															

Mjesec	Vremenski prstenski red Broj	Temperatura vazduha °C										Cestina pravaca i srednja jačina vjetra m/s, fm (0-12)																									
		Im			Sred. (Dnev.)				Max.			Min.		Dat.		N			NE		E		SE		S			SW		W		NW					
		7	14	21	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Max.	Min.	Max.	Min.	E.	J.	E.	J.	E.	J.																
$\varphi = 45^{\circ}48' N \lambda = 15^{\circ}11' E$ Gr. AG = 1h 01 min.																																					
I	743.3	-01.4	01.5	-00.4	-00.2	02.7	-02.4	10.3	29	-10.0	06	36	01.0	13	01.7	21	01.7	05	01.0	15	01.6	06	01.5	14	01.4	04	01.0	09	01.4	03	01.7	04					
II	739.4	-01.6	02.6	00.3	00.4	03.5	-02.5	12.6	25	-14.7	21	35	01.0	12	01.5	23	01.6	02	01.0	11	01.3	11	01.1	13	01.4	03	01.7	03	01.4	03	01.7	04					
III	741.5	02.1	11.4	06.9	06.9	13.2	01.4	20.5	29	-03.0	23	33	01.7	08	01.6	14	02.0	02	01.0	15	01.9	22	01.8	03	02.0				
IV	738.9	04.6	12.4	08.3	08.4	13.7	03.5	20.3	29	-02.0	17	33	02.0	12	02.3	21	02.3	02	01.0	11	01.7	18	01.5	17	01.4	06	01.3				
V	741.6	09.2	15.2	11.6	11.9	17.6	07.7	21.9	31	-06.6	12	36	01.8	05	01.8	09	01.7	06	01.3	19	01.6	15	01.4	26	01.4	07	02.0				
VI	742.3	13.5	21.5	14.5	17.0	23.1	09.6	28.8	05	03.7	15	34	02.0	11	01.8	14	01.4	03	02.0	20	01.6	15	01.5	21	01.3	02	01.5				
VII	743.9	14.1	22.1	17.5	17.8	24.1	12.0	29.8	18	07.3	09	33	02.0	06	01.8	15	01.9	05	01.6	23	01.7	14	01.4	16	01.2	04	01.0				
VIII	744.6	13.5	22.0	14.4	17.1	23.4	12.0	31.0	07	08.3	20	34	01.3	13	01.0	17	01.7	03	01.7	17	01.5	15	01.4	23	01.3	08	01.1				
GOD.	743.4	05.7	12.3	08.3	08.6	13.7	04.3	31.0	07VII	-16.7	24.II	60	01.5	122	01.7	201	01.8	41	01.3	216	01.6	184	01.5	212	01.4	46	01.4	13			
$\varphi = 45^{\circ}34' N \lambda = 15^{\circ}32' E$ Gr. AG = + 1h 01 min.																																					
CRNCMEJ																																					
BR. ST. 37	
I	-	-01.3	02.0	00.0	00.2	02.9	-02.2	11.1	02	-10.6	06	29	01.1	22	01.2	03	02.0	05	01.6	08	01.1	11	01.5	08	01.0	01	02.0	15			
II	-	-01.9	03.3	00.7	00.7	03.8	-02.5	12.7	25	-17.7	21	31	01.1	19	01.3	04	01.3	03	02.0	04	01.5	20	01.9	08	01.3	01	01.0	14			
III	-	02.6	12.0	07.0	07.2	13.3	01.5	21.1	31	-04.5	20	31	01.5	14	01.5	05	01.6	07	01.4	07	01.7	29	02.6	06	01.5	01	02.0	13			
IV	-	05.6	13.5	08.7	09.1	14.6	04.5	21.7	29	-01.8	17	31	01.6	25	01.9	07	01.9	02	02.0	06	01.3	13	01.8	05	02.8	03	01.3	12			
V	-	10.4	16.5	12.4	13.0	18.3	08.3	22.6	05	-01.6	12	39	02.1	22	02.0	05	01.0	06	01.5	08	01.4	23	02.0	04	01.5	03	01.3	13			
VI	-	14.7	22.6	17.1	17.9	23.7	11.6	29.8	06	05.9	20	36	01.3	15	01.7	14	01.7	07	01.4	06	01.7	24	02.3	08	01.4	05	01.6	05			
VII	-	14.8	23.0	17.9	18.6	24.6	12.4	30.2	12	06.9	09	32	01.5	16	01.4	05	02.0	17	01.8	06	01.2	13	01.8	03	01.0	01	02.0	30			
VIII	-	13.7	23.3	17.1	17.8	24.0	12.0	32.7	07	07.5	20	39	01.7	20	01.7	05	01.6	12	01.6	07	01.4	05	01.6	08	01.4	05	01.6	05	01.6	22	
IX	-	09.9	20.5	13.8	14.5	21.3	08.2	29.9	11	01.4	21	31	01.5	16	01.9	12	01.4	06	01.8	05	01.8	09	02.7	09	01.4	05	01.2	17			
X	-	06.3	14.8	08.8	09.7	15.3	05.6	20.7	07	-00.2	23	31	01.1	15	02.0	08	01.9	06	01.7	04	01.5	11	01.6	11	01.0	04	01.3	22			
XI	-	-00.3	02.6	00.6	00.9	03.0	-00.6	14.0	01	-04.6	15	36	01.0	21	01.4	11	01.3	11	01.3	04	01.0	14	01.2	08	01.1	02	01.0	13			
XII	-	-00.2	03.0	00.9	01.1	04.3	-02.2	14.9	29	-14.0	06	39	01.7	17	01.1	04	02.5	02	02.0	18	03.2	09	01.1	04	01.0	21					
GOD.	-	06.2	13.2	08.8	09.2	14.1	04.7	32.7	07VII	-17.7	24.II	61	123	01.4	222	01.6	90	01.6	82	01.6	67	01.4	190	02.1	87	01.3	37	01.3	197		
$\varphi = 45^{\circ}36' N \lambda = 15^{\circ}34' E$ Gr. AG = + 1h 02 min.																																					
GORNJI LENART																																					
BR. ST. 38
I	-	-01.6	02.1	-00.1	00.1	03.0	-03.1	10.4	04	-11.8	06	32	01.4	38	01.6	08	01.0	06	01.0	07	01.1	01	01.0	11	01.0	08	01.0	08	01.0	08	01.0	08	01.0	08	01.0	08	
II	-	-02.0	03.3	00.5	00.6	03.7	-03.7	15.5	26	-21.5	21	30	01.4	02	01.0	12	01.3	01	01.0	23	01.2	03	01.3	05	01.0	08	01.0	08	01.0	08	01.0	08	01.0	08	01.0	08	
III	-	02.1	12.4	04.8	07.0	13.2	00.5	22.0	30	-04.0	08	30	01.0	24	01.3	03	01.0	07	01.3	03	01.0	07	01.3	03	01.0	10	01.3	03	01.0	12	01.3	03	01.0	12	01.3	03	
IV	-	03.6	13.2	08.6	09.0	14.2	02.2	21.2	30	-04.0	09	30	02.0	35	01.8	05	01.4	05	01.4	05	01.4	05	01.4	05	01.4	05	01.4	05	01.4	05	01.4	05	01.4	05	01.4	05	
V	-	10.6	17.0	11.8	12.8	18.3	06.7	23.0	31	-06.8	12	36	01.4	24	01																						

Mesec	Oblačnost Nm (0-10)				Vlažnost vazduha % Sred. (Giese) Inzolacij broj sati	Padavine R mm Sred. (Giese) Min Max Dat.	Broj dana na sat																														
	7	14	21	Sred. (Giese)			Tn	Tx	Tn	Tx	Tn	Tx	Tn	P(0-12)	Nm(0-10)	R mm	•	*	•	Δ	•	▲	■														
	■	■	■	■			≤	<	≤	<	≤	<	≤	≥	≤	≥	•	*	•	Δ	•	▲	■														
NOVO MESTO																																					
BR. ST. 36																																					
I	9.1	8.4	8.1	8.5	042.8	04.1	94	84	91	90	32	039	013.0	18	01	07	25	.	.	01	.	23	18	10	01	12	12	01	04	02	.	.	11	16			
II	9.1	8.4	8.0	8.5	046.6	04.2	95	79	86	84	34	042	012.2	12	02	08	22	.	.	02	.	21	16	09	01	11	11	01	02	.	.	04	20				
III	6.8	6.8	4.0	5.9	157.7	05.1	93	52	72	72	28	096	025.3	06	.	.	11	.	.	05	.	05	10	12	11	03	11	05	01	.	.	02	07	02			
IV	6.5	6.5	2.7	7.9	7.5	141.7	06.0	90	55	75	73	36	084	027.8	16	.	.	04	.	.	01	.	15	15	10	02	14	04	03	.	.	01	.	03	03	01	
V	8.0	8.5	6.1	7.6	139.9	08.6	94	67	86	82	37	110	019.9	14	.	.	01	.	.	14	20	17	04	20	13	08						
VI	5.4	6.7	5.8	6.0	249.3	10.3	87	54	78	73	34	124	026.4	12	.	.	11	.	.	02	01	03	09	12	10	06	12	.	.	06	04						
VII	5.9	6.0	4.7	5.6	260.9	11.7	92	59	84	78	40	085	028.7	22	.	.	16	.	.	01	05	07	12	11	03	12	.	.	10	11							
VIII	6.3	6.3	4.5	5.5	234.6	11.5	94	58	86	79	44	074	031.7	31	.	.	11	02	.	03	04	10	07	03	10	06	10						
IX	6.4	5.9	4.5	5.6	210.2	09.9	95	59	91	82	39	098	035.0	13	.	.	02	.	.	01	04	07	10	07	03	10	.	.	.	06	12						
X	8.3	5.1	5.3	6.2	138.7	07.5	96	65	92	84	36	095	036.1	01	.	.	01	.	.	01	08	10	05	04	08	.	.	01	.	16							
XI	9.8	8.9	9.1	9.2	027.1	04.4	93	87	93	91	60	033	016.1	28	.	03	21	.	.	25	07	03	02	07	.	.	01	01	.	17	04						
XII	6.8	7.6	8.1	8.2	041.3	04.4	94	62	92	89	53	068	012.4	30	03	08	22	.	.	16	19	10	02	12	34	.	.	01	.	.	17	21					
GOD.	7.5	7.2	6.3	7.0	1690.8	07.3	93	66	85	81	28	948	036.1	DAX	06	26	106	40	02	.	11	01	23	159	161	110	34	131	48	05	01	08	04	.	47	120	64
ČRNOSELJ																																					
BR. ST. 37																																					
I	8.6	8.6	8.6	8.6	-	04.1	94	83	90	89	38	088	029.3	18	01	06	25	.	.	02	25	20	12	03	14	11	01	03	.	.	13	17					
II	9.0	8.0	8.5	8.6	-	04.3	95	75	90	86	40	077	018.5	12	02	05	20	.	.	01	02	23	19	13	02	08	14	02	.	02	07	24					
III	6.2	6.4	4.4	5.7	-	05.4	91	55	75	74	26	121	030.6	06	.	.	14	.	.	04	07	09	15	12	05	14	05	02	.	.	02	08	03				
IV	6.7	8.3	7.4	7.5	-	06.2	89	55	76	73	35	076	016.8	14	.	.	03	.	.	15	18	12	03	18	02	01	.	.	01	04	01						
V	8.1	8.3	7.7	8.1	-	08.9	91	63	83	79	42	113	021.6	14	.	.	01	.	.	02	01	16	21	15	04	21	.	.	.	01	07	04					
VI	5.2	5.6	5.6	5.5	-	10.7	84	56	76	71	29	103	021.9	14	.	.	13	.	.	01	04	08	15	10	02	19	.	.	08	02							
VII	5.1	5.0	4.2	4.8	-	12.3	91	59	82	77	39	104	031.5	22	.	.	17	02	.	01	09	07	13	10	04	13	.	.	08	03							
VIII	4.6	4.7	3.4	4.2	-	12.0	94	60	84	79	40	168	060.2	31	.	.	14	03	.	04	03	09	06	04	09	.	.	07	04								
IX	4.9	4.7	3.9	4.5	-	10.4	95	64	90	83	40	121	030.8	28	.	.	05	.	.	01	09	06	11	08	04	11	.	.	.	03	11						
X	8.1	5.2	6.7	6.7	-	07.9	96	68	94	86	37	083	039.0	02	.	.	01	.	.	01	01	13	10	06	03	09	.	.	02	18							
XI	9.9	8.8	9.1	9.3	-	04.6	98	88	95	93	65	034	017.6	28	.	08	20	.	.	06	08	04	02	03	04	01	01	01	01	18							
XII	8.6	8.8	7.9	8.2	-	04.6	91	84	91	85	55	083	018.5	19	01	08	21	.	.	02	20	22	11	03	14	09	01	01	01	01	.	20	21				
GOD.	7.1	6.8	6.4	6.8	-	07.6	92	67	85	81	26	1151	060.2	31.VIII	04	27	100	49	05	.	13	.	43	171	181	119	39	149	45	05	07	01	03	02	44	111	69
GORNJI LENART																																					
BR. ST. 38																																					
I	8.5	8.1	7.4	8.0	-	04.0	91	81	89	87	30	047	018.7	18	01	05	26	.	.	01	21	14	08	02	09	07	01	.	.	.	09	18					
II	8.6	8.2	7.7	8.2	-	04.2	89	71	87	82	42	053	013.3	12	05	06	22	.	.	02	20	14	10	01	04	10	.	.	08	16							
III	5.6	5.0	4.0	4.8	-	05.3	92	51	75	73	30	116	025.8	06	.	.	14	.	.	01	13	08	17	12	03	16	04	.	.	01	02						
IV	5.7	5.5	5.0	6.1	-	06.3	89	55	76	73	31	071	021.9	16	.	.	04	.	.	01	05	10	15	11	02	15	.	.	01	.	01						
V	6.6	7.7	5.6	6.6	-	08.9	91	60	87	79	32	117	019.8	14	.	.	01	.	.	01	36	21	17	05	21	.	.	.	02	.	02						
VI	4.7	4.1	4.1	4.6	-	10.7	86	50	84	73	29	144	031.6	12	.	.	10	.	.	01	06	11	10	04	11	.	.	02	.	.	02						
VII	5.4	4.6	3.6	4.9	-	11.8	90	56	86	77	36	107	024.6	22	.	.	16	.	.	04	04	04	19	09	04	14	.	.	02	06							
VIII	4.7	4.0	3.5	4.1	-	11.8	94	54	89	79	28	094	048.9	31	.	.	15	02	.	01	10	04	11	08	03	11	.	.	01	09							
IX	5.0	4.8	3.0	4.3	-	10.2	96	56	95	82	36	080	027.9	28	.	.	03	.	.	01	09	11	06	03	11	.	.	03	05								
X	5.3	3.3	1.9	4.6	-	07.6	96	66	93	85	36	079	029.0	01	.	.	02	.	.	06	06	08	05</														

Mjesec	Vrstdinski prsticnik pm	Temperatura vazduha °C										Čestina pravaca i srednja jačina vjetra m/s, pm (0-12)																			
		Im		Sred. (Dnev.)		Kl. 00-06		Kl. 06-12		Kl. 12-18		Kl. 18-24		N		NE		E		SE		S		SW		W		NW		C	
		7	14	21	Sred.	Kl. 00-06	Kl. 06-12	Kl. 12-18	Kl. 18-24	Dnev.	Kl. 00-06	Kl. 06-12	Kl. 12-18	Kl. 18-24	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.			
$\varphi = 40^{\circ}02' N \lambda = 16^{\circ}33' E$ Gr. $\Delta G = + 1h 07 min.$														KRIZEVCI												BR. ST. 41					
I	749.4	-01.3	J1.9	-00.2	00.0	02.8	-02.5	10.8	29 -08.2	06	14	03.1	24	02.8	05	02.0	07	02.3	14	02.4	13	02.2	06	02.0	10	02.1	.				
II	749.4	-01.9	J3.3	00.4	00.5	04.0	-03.3	17.7	26 -20.1	21	14	02.9	29	02.7	04	03.0	05	02.2	10	02.3	11	02.5	03	03.0	08	02.0	.				
III	747.4	03.3	J1.2	06.4	06.8	12.3	01.6	20.6	30 -04.3	13	22	03.6	13	02.9	06	02.5	19	02.5	19	03.1	03	02.0	07	02.0	.						
IV	744.6	06.5	J2.8	08.7	09.2	14.2	04.1	21.6	30 -00.5	07	24	03.4	21	03.3	03	02.3	11	02.6	11	02.3	06	02.5	09	02.3	.						
V	747.2	11.1	J6.8	12.0	12.9	17.9	08.1	23.0	31 -02.2	12	23	02.9	12	02.6	06	02.3	05	02.2	17	02.3	15	02.4	09	02.0	06	02.0	.				
VI	747.9	15.0	J2.1	16.5	17.5	23.4	11.3	26.5	08 -07.2	29	12	02.9	16	03.0	11	02.4	02	02.5	17	02.7	13	02.8	04	02.2	15	02.5	.				
VII	749.5	15.5	J2.6	16.9	18.0	23.9	12.3	26.5	13 -06.8	09	25	02.3	11	02.4	07	01.9	08	02.0	16	02.3	15	02.8	08	02.2	13	01.9	.				
VIII	750.1	14.1	J2.7	16.1	17.3	23.4	11.1	30.0	07 -05.5	29	22	02.5	09	02.1	09	02.0	04	02.0	19	02.3	09	03.0	02	02.0	19	02.2	.				
IX	749.5	10.6	J9.6	13.3	14.2	20.4	08.5	28.0	11 -00.7	21	14	02.9	08	02.8	08	02.0	04	02.0	24	02.3	10	02.6	08	02.2	14	01.9	.				
X	753.7	06.3	J4.3	08.4	09.4	14.9	04.8	20.5	10 -01.1	28	30	02.5	22	02.4	06	02.3	04	02.2	09	02.7	05	02.2	03	02.3	14	02.1	.				
XI	756.5	-00.5	J2.6	01.2	01.4	03.0	-00.3	15.0	01 -03.6	30	15	02.6	10	02.8	09	02.2	06	02.0	22	02.0	11	02.1	12	02.1	05	02.0	.				
XII	746.7	-00.4	J2.8	00.8	00.7	03.4	-02.5	13.0	29 -12.5	07	13	03.0	15	02.6	02	03.0	05	02.6	25	02.2	26	02.6	05	02.0	02	02.0	.				
GOD.	749.2	06.6	J2.7	08.4	09.0	13.6	04.4	30.0	07.VII -20.0	24.II	226	02.9	190	02.7	76	02.2	61	02.2	203	02.3	148	02.6	69	02.2	122	02.1	.				
$\varphi = 46^{\circ}11' N \lambda = 16^{\circ}49' E$ Gr. $\Delta G = + 1h 07 min.$														KOPRIVNICA												BR. ST. 42					
I	-	-01.2	J0.1	00.3	00.4	02.8	-01.7	09.4	29 -06.3	11	11	01.2	12	01.7	12	01.8	07	02.0	15	01.7	25	02.3	02	01.0	09	01.4	.				
II	-	-01.6	J3.9	00.6	00.4	04.4	-03.0	17.8	26 -20.0	21	15	02.1	15	02.0	02	01.5	12	01.4	17	01.1	10	02.4	03	01.3	10	01.7	.				
III	-	04.1	J1.8	06.3	07.1	12.5	02.8	26.7	30 -29.9	13	13	02.4	21	02.1	02	01.0	05	01.6	12	03.2	31	02.6	04	02.8	05	02.0	.				
IV	-	06.4	J3.5	08.1	09.0	14.4	04.6	22.3	30 -01.5	07	21	02.7	14	02.1	03	02.7	03	01.3	12	02.1	03	01.7	18	01.9	.						
V	-	11.6	J7.8	12.1	13.4	18.8	09.5	23.8	01 -00.4	12	14	02.2	12	02.6	03	03.0	10	02.2	12	01.8	28	02.2	02	02.0	12	02.0	.				
VI	-	15.5	J2.9	16.3	17.8	23.8	12.8	26.4	07 -08.3	15	11	01.8	12	02.3	02	02.5	06	02.2	12	01.6	24	02.6	12	02.6	11	02.2	.				
VII	-	16.1	J2.5	16.5	18.2	24.5	13.3	26.2	29 -08.4	24	05	02.0	06	02.5	09	02.0	02	02.0	19	02.1	30	02.1	08	02.0	14	01.8	.				
VIII	-	15.1	J2.5	15.8	17.6	24.3	12.0	30.2	07 -06.4	29	07	02.4	23	01.9	01	03.0	05	02.2	11	01.8	27	02.1	05	01.6	14	02.1	.				
IX	-	11.6	J20.2	13.4	14.6	21.2	10.0	28.6	11 -03.2	21	10	01.5	14	01.9	04	01.8	01	02.0	10	01.7	34	02.2	08	02.2	09	02.1	.				
X	-	06.9	J15.2	08.4	09.7	15.8	05.8	21.4	09 -00.7	28	12	01.5	13	01.8	04	02.0	04	01.2	16	01.6	18	01.8	11	01.5	15	01.4	.				
XI	-	00.6	J2.9	01.2	01.5	03.4	00.1	16.0	01 -03.5	30	10	01.8	15	01.6	02	01.5	10	01.3	18	01.7	23	01.3	05	01.0	07	01.3	.				
XII	-	-00.2	J2.9	01.3	01.3	03.9	-01.6	13.8	29 -14.4	07	05	01.8	13	01.6	01	01.0	02	01.0	13	02.1	41	02.8	05	02.0	13	01.8	.				
GOD.	-	07.1	J3.4	08.3	09.3	14.2	05.4	30.2	07.VII -20.0	24.II	128	02.0	170	02.0	45	02.0	67	01.7	167	01.8	313	02.2	68	01.9	137	01.8	.				
$\varphi = 45^{\circ}14' N \lambda = 12^{\circ}36' E$ Gr. $\Delta G = + 54 min.$														POREČ												BR. ST. 43					
I	-	04.7	J8.6	05.2	05.9	09.8	02.0	15.2	14 -04.3	06	03	01.7	10	01.6	40	01.3	17	02.5	06	03.5	03	02.0	07	01.6	07	02.4	.				
II	-	03.6	J0.3	04.7	05.3	09.4	00.8	13.7	25 -25.5	09	11	02.1	06	01.8	29	01.3	20	02.4	06	02.8	01	02.0	08	01.8	03	02.0	.				
III	-	06.8	J11.8	07.5	08.4	13.0	03.6	17.6	31 -00.0	20	02	01.5	09	01.6	29	01.3	19	01.9	09	03.0	04	02.5	12	01.9	09	02.9	.				
IV	-	10.0	J3.8	09.8	10.9	15.2	06.7	19.5	04 -02.4	09	01	01.0	11	02.0	18	01.1	28	02.0	09	02.1	04	07.8	08	02.1	13	01.8	.				
V	-	13.9	J16.7	13.1	14.2	18.4	09.6	23.0	28 -00.0	12	08	01.6	10	01.9	17	01.2	29	01.9	06	02.5	06	02.2	10	02.2	07	01.9	.				
VI	-	16.6	J22.1	17.2	18.8	23.4	13.2	27.1	11 -07.5	29	04	01.7	08	01.1	23	01.3	20	01.8	09	02.7	06	02.3	11	02.4	09	01.8	.				
VII	-	20.6	J25.0	18.2	21.0	26.3	15.0	31.2	29 -08.0	22	10	02.0	07	01.4	25	01.2	20	01.6	07	02.7	10	02.6	08	02.4	14	02.1	.				
VIII	-	19.1	J24.4	18.5	20.1	25.4	14.6	32.3	07 -10.6	31	01	01.1	19	01.5	09	01.0	16	02.1	02	03.3	02	03.0	13	02.0</td							

Mesto	Oblačnost Nm (0-10)			Insolacija hroj sati	Vlažnost vazduha			Padavine R mm			Broj dana na sat																						
	7	14	21		Sred. (Dnev.)	7	14	21	Spored.	Min	Σ	Max	Dat.	Tx mm	Tx mm	Tx mm	Tx mm	Tx mm	F(0-12)	Nm(0-10)	R mm	•	*	•	Δ	▲	▲	T	≡	■			
						7	14	21	Spored.	Min	Σ	Max	Dat.	<	<	≥	≥	≥	≥	≥	≥	≥	≥	≥	≥	≥	≥	≥					
KRIŽEVCI																																	
BR. ST. 41																																	
I 9.0 7.5 8.7 8.4	041.6	34.0	89	79	87	85	48	023	004.8	30	.	03	27	.	.	.	03	.	01	23	11	06	.	03	07	.	.	36	11				
II 9.4 7.3 7.7 8.1	066.4	04.1	87	70	84	80	44	038	009.2	20	05	05	23	.	.	.	02	.	17	12	07	.	06	08	01	.	01	.	09	12			
III 6.1 5.6 3.8 5.0	157.1	05.3	87	56	74	72	31	061	018.5	24	.	09	.	.	.	06	01	08	05	12	09	02	10	03	01	.	03	01	.	03	01		
IV 7.2 5.6 7.8 6.9	141.4	06.2	83	56	73	71	37	082	019.8	16	.	01	.	.	.	05	01	08	14	11	04	14	01	01	.	01	04	03	.	03	03		
V 7.0 6.3 7.4 6.9	133.9	09.1	87	64	87	79	42	110	019.9	09	.	.	01	.	.	.	05	.	01	12	20	14	04	20	09	02	.	.	.
VI 4.5 3.8 6.0 4.8	237.1	10.7	83	53	80	72	35	053	021.8	12	.	.	13	.	.	05	.	08	05	11	07	02	11	06	01	.	.	.	
VII 5.3 4.1 4.7 4.7	244.7	12.0	89	58	87	78	39	089	019.4	06	.	.	14	.	.	07	07	11	10	04	11	01	07	03	.	.	.		
VIII 5.2 3.6 4.5 4.5	253.1	11.8	92	57	89	79	43	060	027.3	31	.	.	12	01	.	03	01	09	05	11	08	02	11	06	01	.	.	.	
IX 5.1 3.3 4.7 4.4	197.0	10.0	95	61	90	82	37	058	015.2	28	.	.	03	.	.	01	.	08	05	12	10	02	12	02	03	.	.	.	
X 6.8 4.8 5.1 5.6	135.2	06.4	94	45	85	75	22	055	024.9	01	.	.	02	.	.	05	07	12	04	02	07	03	06	.	.	.			
XI 9.7 9.2 9.3 9.4	015.1	34.6	93	86	91	90	53	016	007.7	27	.	04	19	.	.	01	28	08	02	01	03	03	11	03	.	.	.		
XII 8.5 8.2 7.7 8.1	029.8	04.5	92	94	91	89	60	061	013.4	30	02	09	21	.	.	01	20	16	12	01	10	05	.	.	.	01	01	16	15	.	.		
GOD. 7.0 5.7 6.4 6.4	1652.4	07.4	89	64	84	79	22	706	027.3	54.VII	07	21	103	42	01	.	31	32	50	142	150	104	23	118	27	03	.	01	03	38	64	42	
KOPRIVNICA																																	
BR. ST. 42																																	
I 9.1 7.7 7.7 8.2	-	039.4	84	78	81	81	49	030	004.9	18	.	05	24	.	.	.	02	17	11	07	.	09	04	.	02	.	01	11	11				
II 7.8 7.0 6.5 7.1	-	04.1	81	75	81	79	43	044	016.0	20	04	02	22	.	.	.	01	05	15	12	09	01	07	06	.	.	14	12	.	.	.		
III 6.7 6.5 4.5 5.9	-	05.6	85	53	83	74	31	071	024.3	24	.	03	.	.	.	02	02	07	14	09	02	12	02	.	.	02	02	.	.	.			
IV 7.1 7.3 6.0 6.8	-	26.2	83	56	76	72	35	084	028.3	16	.	01	.	.	.	01	10	15	10	02	15	01	.	.	02	03	01	.	.	.			
V 7.3 8.0 6.2 7.2	-	09.0	87	61	81	76	35	114	020.1	14	.	.	14	.	.	.	07	21	15	05	21	01	04	01	.	.	.		
VI 5.0 6.6 5.3 5.7	-	10.8	80	52	80	70	28	093	027.9	12	.	.	14	.	.	.	02	08	12	10	04	12	.	.	.	02	01		
VII 5.0 6.2 4.6 5.3	-	11.9	87	55	86	76	35	073	023.6	04	.	.	15	.	.	01	06	15	11	03	15	.	.	.	05	04			
VIII 5.1 5.9 4.6 5.2	-	11.5	88	52	85	75	39	096	022.1	31	.	04	14	02	.	01	03	04	12	08	02	12	.	.	01	02	05	04	.	.			
IX 5.9 5.8 4.3 5.3	-	09.7	91	57	84	77	30	077	041.2	07	.	01	.	03	.	.	05	07	09	07	02	09	.	.	.	02	07		
X 7.6 4.9 4.4 5.6	-	07.5	92	63	88	81	37	048	021.2	01	.	01	.	.	.	01	09	09	06	01	29	.	.	.	01	15			
XII 0.0 8.9 9.1 9.3	-	04.6	92	84	90	89	53	035	020.3	26	.	01	.	19	.	.	12	05	02	02	03	02	.	.	.	14	06		
XII 8.3 7.6 7.3 7.7	-	34.5	84	81	84	83	50	061	015.2	20	02	07	16	.	.	01	01	14	14	14	02	11	05	.	.	.	11	02	.	.	.		
GOD. 7.1 6.9 5.9 6.6	-	07.4	86	63	83	77	28	786	041.2	07.IX	06	14	86	48	02	.	05	.	23	130	149	108	26	135	20	.	.	.	03	03	22	93	50
POREČ																																	
BR. ST. 43																																	
I 6.6 7.2 6.2 6.7	-	05.8	82	74	86	81	32	170	029.6	14	.	09	05	13	15	14	07	15	.	01	01	
II 7.0 6.7 6.4 6.7	-	05.4	79	68	82	76	41	068	024.6	20	.	14	03	12	10	08	02	10	01	01
III 5.9 5.1 5.0 5.3	-	36.5	81	70	80	77	51	077	020.4	24	05	07	10	08	04	10	.	.	.	01	02		
IV 6.6 6.8 7.0 6.8	-	37.7	80	67	83	77	40	062	022.5	14	01	11	10	09	04	10		
V 6.6 6.8 6.6 6.7	-	10.1	84	73	88	81	49	099	020.2	14	02	10	18	13	04	18	.	.	.	05		
VII 3.8 4.9 4.1 4.3	-	12.7	78	66	83	76	50	044	014.3	18	.	.	10	.	.	.	09	04	07	04	02	07	.	.	.	04	
VIII 3.9 3.1 2.9 3.3	-	13.5	73	57	82	70	42	031	017.6	20	.	.	21	02	.	01	12	01	06	04	02	06	.	.	.	04	
VIII 2.0 3.4 3.3 3.4	-	13.8	79	63	83	76	42	099	051.2	14	.	01	.	19	01	.</																	

Mjesec	Vremenski period	Temperatura vazduha °C								Cestina pravaca i srednja jačina veta m/s, fm (0-12)																			
		Tm			NW	NE	S	SW	W	NW	C	N		NE		E		SE		S		SW		W		NW			
		7	14	21	Sred. (dane)	NW	NE	S	SW	W	NW	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.						
RIJEKA																													
VIII	45°20' N λ = 14°27' E Gr. AG = + 58 min.	I	749.9	05.3	08.1	05.5	06.1	09.2	03.4	13.6	14 -03.3	06	09	01.9	33	02.4	10	02.3	08	02.6	09	04.1	09	01.8	.	04	01.0	11	
IX	746.2	04.2	07.0	05.2	05.4	08.1	02.6	12.7	26	-03.6	21	09	02.1	29	02.5	08	02.6	06	02.3	02	01.0	06	01.5	01	02.0	03	01.7	20	
X	749.6	07.2	11.5	08.7	09.0	12.4	05.8	16.6	30	01.5	20	13	02.1	25	02.6	06	02.5	39	02.2	09	02.3	09	01.8	01	03.0	04	01.2	17	
XI	746.1	10.0	13.7	10.7	11.3	14.7	08.2	19.1	23	04.4	17.0	08	02.6	23	03.2	07	02.9	04	02.8	07	02.1	10	02.1	01	01.0	03	01.3	27	
VI	749.3	14.0	16.4	14.1	14.8	16.1	11.3	23.2	31	02.1	12	08	02.6	20	01.9	05	02.4	12	01.8	04	02.0	08	01.8	04	01.2	05	01.6	27	
VII	749.8	18.6	22.6	18.3	19.5	23.5	15.4	27.7	03	10.4	15	15	01.9	16	02.6	02	02.3	33	02.7	10	01.9	11	01.5	01	01.0	07	01.6	25	
VIII	751.1	20.5	24.6	20.4	21.5	25.9	17.0	31.2	12	01.9	21	01.9	08	01.6	02	02.0	13	01.9	16	01.9	02	01.5	20	01.0	02	01.0	20		
VII	751.5	19.4	24.5	19.8	20.9	25.5	16.8	29.6	03	13.4	31.29	20	02.2	18	03.0	02	03.5	.	05	02.0	13	01.9	05	02.8	01	01.0	29		
IX	751.3	15.5	21.3	16.7	17.6	22.3	13.1	26.3	16	07.1	21	11	02.3	31	02.6	02	02.0	35	02.6	09	01.9	08	01.5	02	01.5	.	32		
X	750.0	11.8	18.2	13.2	14.1	19.0	10.2	23.4	11	05.6	26	21	01.8	32	02.8	08	02.6	.	04	01.5	11	01.6	02	02.0	04	01.5	11		
XI	757.7	07.0	13.5	07.7	08.9	14.1	05.3	20.2	15	01.8	27	24	01.6	27	03.3	08	03.1	02	02.0	04	01.8	11	01.5	01	03.0	.	13		
XII	748.0	05.9	07.9	06.0	06.5	08.9	03.7	12.3	29	-06.8	08	11	02.1	27	02.9	03	02.3	09	02.7	12	02.1	06	01.3	.	02	01.5	29		
GOD.	750.4	11.6	19.8	12.2	13.0	16.8	09.4	31.2	29.VII	06.8	08.XII	61	02.1	292	02.7	69	02.5	54	02.3	85	02.2	118	01.7	20	01.9	35	01.4	261	
PAG																													
VIII	45°36' N λ = 14°38' E Gr. AG = + 59 min.	I	685.6	-01.8	00.3	-01.8	-01.3	01.9	-04.3	08.1	14 -09.6	09.06	04	01.8	08	01.5	06	01.3	36	01.5	22	01.9	12	02.3	.	03	01.7	02	
IX	682.4	-03.4	-00.4	-02.5	-02.2	01.2	-05.3	10.1	25	-13.3	21	05	01.2	04	01.8	03	02.0	38	01.4	22	01.6	11	03.0	.	01	02.0	.		
X	685.8	0.9	06.6	02.1	02.9	07.9	-01.1	16.4	31	-06.4	20	05	01.4	.	01	04.0	03.0	30	01.5	17	02.1	29	02.4	.	01	01.5	.		
XI	683.3	02.2	07.2	03.7	04.2	08.8	00.4	15.2	01	-03.6	17	04	01.5	14	02.0	03	02.3	28	02.1	70	02.0	18	02.1	.	05	01.6	.		
V	686.9	07.6	10.7	08.3	08.7	13.1	05.0	18.2	05	-03.9	12	05	02.2	10	02.7	06	02.3	41	02.0	18	01.7	06	01.8	.	07	02.3	.		
VI	685.3	12.2	16.6	12.8	13.6	18.7	05.4	24.2	04	03.2	15	07	01.6	06	07	04	01.2	34	01.6	22	01.7	10	02.1	.	04	02.2	03		
VII	690.1	13.3	19.1	14.3	15.3	20.7	09.7	24.9	13	04.2	22	24	01.0	05	01.0	02	01.5	44	01.3	27	01.3	10	02.2	.	01	01.0	.		
VIII	690.3	11.7	18.4	12.5	13.8	20.2	08.6	26.2	02	04.9	15	04	01.2	01	02.0	03	01.0	39	01.1	31	01.4	10	02.7	.	03	01.3	02		
IX	689.5	09.1	15.7	10.0	11.2	17.4	06.0	25.3	11	00.2	21	03	01.0	05	01.2	02	01.5	32	01.3	25	01.3	16	01.6	.	05	01.0	02		
X	692.3	05.1	10.5	04.3	07.1	11.6	03.7	16.4	10	-02.3	28	02	01.0	05	01.4	03	01.7	37	01.4	36	01.3	09	01.4	.	01	02.0	.		
XI	694.0	-00.9	03.4	-00.3	00.6	04.5	-02.6	13.4	16	-07.9	19	02	01.5	05	01.8	03	02.0	41	01.4	23	01.3	11	01.7	.	01	02.0	04		
XII	683.7	-01.1	01.3	-00.4	-00.1	02.9	-03.5	11.1	10	-04.3	08	03	02.0	05	01.6	.	03	35	01.6	26	01.4	20	02.6	.	04	01.3	.		
GOD.	687.7	0.7	04.6	09.2	05.4	06.2	10.7	02.1	26.2	02.VII	-14.3	08.XII	48	01.5	66	01.8	36	01.8	435	01.5	289	01.5	162	02.2	.	46	01.7	12	
CRKVENICA																													
VIII	45°10' N λ = 14°42' E Gr. AG = + 59 min.	I	-	06.0	09.1	06.4	07.0	10.2	02.8	14.9	13 -02.2	06	05	02.2	24	01.9	04	02.0	07	02.6	10	04.0	05	02.0	01	03.0	08	02.5	27
IX	5.5	05.3	08.1	06.1	06.4	09.3	03.9	14.6	26	-01.8	16	10	02.9	26	03.5	.	10	03.2	04	03.5	01	02.0	12	01.8	20				
X	07.6	12.2	09.2	09.5	13.3	06.1	18.5	30	01.1	20	10	01.9	14	02.5	01	04.0	13	02.9	07	04.0	04	03.0	05	03.0	11	02.2	28		
XI	10.8	14.1	11.7	12.1	15.3	09.0	19.5	23	03.5	19	05	03.4	21	03.2	03	05.3	16	02.4	01	01.0	02	01.0	09	01.8	30				
V	-	14.2	16.5	14.4	14.9	18.7	12.1	24.0	31.29	06.8	15	02	01.0	20	02.4	02	03.0	18	02.4	02	03.0	03	02.3	01	02.0	13	01.5	32	
VI	-	18.8	22.3	18.9	19.7	23.9	15.5	27.2	10	11.7	15	24	01.2	17	02.2	03	01.3	13	02.7	05	03.2	03	02.7	01	03.0	07	01.4	37	
VII	-	21.4	25.3	21.8	22.6	24.9	18.0	31.3	14	13.6	09	01	01.0	20	02.0	03	01.0	20	02.3	07	02.3	02	01.5	12	01.8	28			
VIII	-	20.3	25.0	21.1	21.9	26.6	17.5	32.6	07	14.2	31	02	02.0	22	02.7	.	14	02.3	02	02.0	04	01.8	.	08	02.1	41			
IX	-	15.7	21.4	17.4	18.0	22.5	12.4	29.5	11	07.1	21	03	01.3	23	01.9	01	01.0	18	02.2	01	05.0	.	07	01.7	37				
X	-	13.1	18.7	13.7	14.8	20.1	09.2	26.6	03	05.2	30	31	01.0	02	01.0	19	02.4	02	02.0	04	01.8	03	02.7	04	01.7	24			
XI	-	06.4	13.6	08.0	09.0	14.8	02.3	20.9	14	-03.6	20	03																	

Mjesec	Oblačnost Nm (0-10)				Vlažnost broj sati h mm	Padavine R mm	Broj dana na m:																														
	7	14	21	Sred. (Dnev.)			Tn	Tn	Tn	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	▲	■	□	■																
							=	<	<	IV	IV	IV	6	8	2,0	8,0	0,1	1,0	0,0	0,0	0,0																
RIJEKA																																					
$H_a = 120 \text{ m } H_b = 108,3 \text{ m } h_t = 2,0 \text{ m } h_r = 1,0 \text{ m}$																																					
I	7,4	7,3	6,4	7,0	089,0	J5,0	71	63	69	68	29	196	069,2	25	•	•	04	•	•	03	02	03	19	14	05	19	•	•	01	•	03	•					
II	7,8	7,0	6,7	7,2	J88,7	04,8	68	62	71	67	30	226	083,4	11	•	•	06	•	•	31	•	02	16	13	11	07	13	02	•	•	01	•	02	•			
III	6,3	7,0	5,9	6,4	157,2	05,5	68	57	67	64	29	201	042,8	24	•	•	•	•	•	04	10	15	13	09	15	•	•	•	•	01	04	03					
IV	7,4	8,0	7,4	7,6	149,3	06,5	69	55	68	64	35	115	034,6	14	•	•	•	•	•	08	03	•	15	11	08	03	11	•	•	•	•	02	•				
V	7,6	8,4	7,8	7,9	149,1	08,7	71	62	74	69	38	186	043,4	07	•	•	•	•	•	•	•	•	16	20	15	05	20	•	•	•	•	08	•				
VI	5,2	6,8	5,6	5,9	223,3	10,8	66	51	71	63	30	118	043,6	18	•	•	•	11	•	02	07	09	06	05	09	•	•	•	•	06	•						
VII	4,5	5,1	3,0	4,2	271,4	11,5	63	50	63	59	33	054	027,7	20	•	•	•	17	03	04	01	01	08	04	11	08	02	11	•	•	09	•					
VIII	3,9	5,4	3,6	4,3	251,8	11,3	64	49	66	60	31	109	042,1	31	•	•	•	18	•	03	04	08	03	10	08	04	10	•	•	08	•						
IX	5,7	6,2	4,6	5,5	204,6	09,8	70	53	69	64	27	097	052,4	13	•	•	•	07	•	•	02	•	04	11	08	07	02	08	•	•	06	•					
X	4,2	3,5	3,1	3,6	222,3	07,5	69	47	68	61	25	160	074,1	01	•	•	•	01	•	01	14	05	06	03	06	03	06	•	•	02	•						
XI	3,6	2,8	1,8	2,7	190,6	05,1	63	49	64	58	26	108	056,0	27	•	•	•	•	17	03	04	01	01	08	04	11	08	02	11	•	•	09	•				
XII	8,2	8,2	7,4	8,0	050,6	05,9	72	77	76	77	37	199	029,8	20	•	•	•	04	•	02	04	22	18	14	09	18	03	02	•	•	01	01	03	02			
GOD.	6,0	6,3	5,3	5,9	2047,9	07,7	68	55	68	64	25	1769	083,4	41,11	•	•	14	54	03	07	28	10	64	130	143	113	56	143	05	02	•	01	01	02	53	08	02
PARG																																					
$H_a = 863 \text{ m } H_b = 863,4 \text{ m } h_t = 2,0 \text{ m } h_r = 2,0 \text{ m}$																																					
I	7,9	7,7	6,8	7,5	065,2	03,7	87	83	89	86	31	185	040,3	29	•	08	28	•	•	02	•	04	21	21	16	06	07	17	01	02	13	23					
II	8,7	8,4	8,5	8,5	040,4	03,6	89	83	91	87	46	112	023,6	11	03	13	23	•	•	01	22	20	14	05	03	17	02	01	•	01	11	27					
III	6,4	7,0	5,2	6,2	145,5	04,3	81	63	84	76	29	175	038,6	17	•	•	17	•	•	04	12	16	13	05	12	08	01	•	•	03	02	10					
IV	7,0	6,5	5,8	7,9	087,1	05,0	88	84	85	80	39	171	035,4	14	•	•	12	•	•	01	01	16	18	14	06	13	08	01	01	02	09	09					
V	7,9	8,7	7,1	7,9	085,5	03,0	84	75	85	81	53	170	028,0	14	•	•	05	•	•	•	15	21	18	07	20	03	02	•	•	02	09	06	02				
VI	4,9	7,2	4,3	5,5	173,5	08,7	79	65	79	74	41	286	111,7	18	•	•	•	•	•	03	08	19	15	35	19	•	•	•	•	06	05	02					
VII	4,7	5,8	4,4	5,0	240,1	10,0	83	64	81	76	43	112	033,2	20	•	•	•	•	•	06	07	16	11	05	16	•	•	•	•	01	10	03					
VIII	4,8	6,2	3,5	4,8	212,2	09,6	88	66	86	80	39	148	071,1	31	•	•	04	•	•	01	04	05	13	11	03	13	•	•	•	•	12	02	02				
IX	6,0	5,1	3,7	4,9	190,7	08,0	85	64	86	79	39	119	059,7	28	•	•	01	•	•	06	06	12	10	33	12	•	•	•	•	03	02	02					
X	6,7	4,4	3,6	4,9	132,0	06,4	90	70	89	83	42	232	108,5	01	•	•	03	09	11	06	09	11	09	35	11	•	•	•	•	02	06	04					
XI	5,1	4,7	4,0	4,6	130,3	03,8	84	72	84	80	23	086	057,5	27	•	07	25	•	•	01	12	11	05	03	32	32	04	01	•	•	01	08	04				
XII	7,8	7,8	7,5	7,7	042,2	-	-	-	-	-	51	178	036,2	20	06	08	19	•	•	01	01	17	22	13	05	13	10	•	•	•	•	09	23				
GOD.	6,5	6,8	5,6	6,3	1544,7	-	-	-	-	-	23	1974	111,7	46,VI	09	36	132	05	•	05	•	48	149	194	147	17	143	47	08	04	•	01	04	51	71	98	
CRIKVENICA																																					
$H_a = 2 \text{ m } H_b = - \text{ m } h_t = 2,0 \text{ m } h_r = 1,5 \text{ m}$																																					
I	6,9	6,2	6,1	6,4	-	05,9	79	72	78	76	45	107	033,0	27	•	•	03	•	•	02	•	05	11	18	03	03	03	•	•	02	01	•					
II	7,1	6,4	6,5	6,7	-	05,6	75	71	78	74	40	121	033,7	20	•	•	04	•	•	04	•	01	13	10	09	34	10	•	•	02	•	02					
III	5,4	5,3	5,6	5,4	-	06,4	77	73	77	76	43	097	021,0	24	•	•	•	•	•	03	08	13	13	04	13	•	•	•	•	01	02	01					
IV	6,0	6,2	6,8	6,3	-	08,1	77	73	77	75	45	124	044,1	12	•	•	•	•	•	02	•	04	10	10	03	10	•	•	02	02	02						
V	6,4	6,9	6,5	6,6	-	10,2	80	77	80	79	47	179	037,4	24	•	•	•	•	•	•	06	18	14	26	18	•	•	•	•	05	05						
VI	4,2	5,1	4,5	4,8	-	12,6	74	67	74	72	42	076	025,0	14	•	•	02	•	•	13	06	07	02	10	10	33	10	•	•	04	04						
VII	3,8	4,0	4,2	4,0	-	13,7	70	62	66	66	39	035	013,6	22	•	•	•	21	06	07	01	01	02	01	06	05	01	04	04	04							
VIII	3,9	4,2</td																																			

Mjesec	Vremenski priredak PM	Temperatura vazduha °C										Cestina pravaca i srednja jačina vatre nD, PM (0-12)																				
		Ta		Max				Min				Det.		N			NE		E		SE		S		SW		W		NW		C	
		7	14	21	Sred. (Dnev.)	Max	Max	Max	Max	Min	Min	Det.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.						
$\varphi = 45^{\circ}16' N \lambda = 15^{\circ}14' E$ Gr. $\Delta G = + 1h\ 01\ min.$														OGULIN												BR. ST. 51						
I	732.9 -00.9	02.1	00.0	00.3	03.6	-02.5	11.2	29	-09.7	06	13	01.5	16	01.8	11	01.2	11	01.9	13	02.3	03	03.7	07	01.7	09	01.6	10					
II	729.0 -01.3	02.5	00.3	00.5	03.6	-02.9	13.4	25	-15.3	21	06	02.0	16	02.3	04	02.5	10	02.1	10	01.8	.	.	15	02.2	11	01.5	12					
III	731.6 03.3	10.6	05.8	06.4	12.0	01.6	19.4	03	-03.7	13	06	01.7	07	02.6	04	02.2	09	01.9	11	03.3	12	03.3	24	02.5	14	01.9	06					
IV	728.8 05.7	11.6	07.7	08.2	12.8	04.1	19.2	30	-01.5	17	13	02.0	09	02.8	07	01.7	05	02.4	10	01.8	08	03.1	16	02.1	17	01.7	05					
V	731.6 10.7	15.4	11.9	12.5	17.0	08.2	22.4	05	-02.7	12	05	01.6	11	02.0	09	01.8	05	02.4	07	02.9	09	03.6	23	02.1	17	01.7	07					
VI	732.9 14.6	20.6	16.0	16.8	21.9	11.2	28.6	05	05.4	29	05	01.8	09	01.7	07	01.4	05	02.2	06	02.8	18	03.1	20	01.6	17	01.4	03					
VII	734.1 14.7	22.3	16.9	17.7	23.2	11.8	27.7	12	04.5	09	24	01.2	17	01.8	08	02.0	06	01.8	04	02.2	04	03.5	26	01.7	21	01.6	03					
VIII	734.7 13.2	21.9	15.7	16.6	23.0	11.4	31.3	07	07.4	31	10	01.6	09	01.9	04	02.2	04	01.8	07	02.6	06	03.2	27	01.5	21	01.6	03					
IX	734.0 10.5	19.3	12.6	13.8	20.4	08.0	28.0	11	00.8	21	05	01.8	09	01.7	10	01.8	03	01.7	03	02.3	10	02.9	22	01.7	27	01.6	01					
X	737.8 06.7	12.9	07.8	08.8	13.9	05.4	19.3	10	00.0	22	08	01.5	12	02.2	06	01.5	09	01.7	03	01.7	04	01.2	24	01.3	17	01.4	10					
XI	741.8 -01.1	03.7	00.3	00.8	04.7	-01.7	16.2	16	-06.9	36	02	01.0	16	01.8	08	01.5	12	01.4	08	01.2	10	01.4	11	01.5	12	01.3	11					
XII	730.9 00.8	03.8	01.7	02.0	05.4	-01.6	14.1	30	-12.6	04	07	01.4	13	01.5	05	01.4	08	01.1	12	03.6	17	03.5	17	02.6	05	01.4	09					
GOD.	733.3 06.4	12.2	08.1	08.7	13.5	04.4	31.3	07VII -15.3	24.II	01	01.6	144	01.9	83	01.7	89	01.8	94	02.5	101	03.0	232	01.8	188	01.6	80						
$\varphi = 45^{\circ}30' N \lambda = 15^{\circ}33' E$ Gr. $\Delta G = + 1h\ 02\ min.$														KARLOVAC												BR. ST. 52						
I	752.1 -00.7	02.1	00.6	00.3	03.1	-01.7	17.4	02	-07.5	04	03	01.3	33	01.2	01	01.0	01	01.7	06	01.7	.	.	01	01.0	49							
II	748.2 -01.1	03.5	01.2	01.7	04.2	-01.9	11.9	26	-15.0	21	04	01.2	32	01.2	01	01.0	01	01.2	03	01.3	38											
III	750.2 03.5	12.7	08.1	08.1	14.1	02.8	21.8	31.30	-01.6	23	04	01.5	26	01.4	07	03	01.7	20	02.1	.	.	02	01.5	38								
IV	747.2 06.1	14.4	09.7	10.0	15.9	05.0	23.0	29	-00.3	17	04	01.2	27	01.7	15	01.0	19	01.5	07	03	01.0	36										
V	749.8 10.6	18.3	13.4	13.7	19.3	08.9	24.0	31	-00.7	12	01	01.0	22	01.3	04	01.0	01	01.0	14	02.0	.	.	51									
VI	750.4 14.8	23.4	18.2	18.6	24.7	12.4	30.5	06	07.0	15	07	01.0	23	01.4	01	01.0	01	01.0	23	01.6	.	.	01	01.0	34							
VII	752.0 15.2	26.4	19.5	19.7	25.9	13.9	31.3	12	08.0	09	05	01.0	24	01.3	07	03	01.0	20	01.7	03	01.0	05	01.2	39								
VIII	752.6 14.5	23.9	18.4	18.8	25.0	13.2	33.7	07	04.5	11	02	01.0	28	01.2	07	01.0	01	01.0	10	01.7	.	.	03	01.3	48							
IX	752.1 10.6	20.9	14.8	15.3	22.2	09.6	31.6	11	02.6	21	04	01.2	17	01.5	01	01.0	01	01.0	09	02.0	01	01.0	02	01.0	56							
X	756.2 07.5	14.6	09.9	10.4	15.5	06.8	21.4	07	00.9	22	09	01.1	26	01.4	04	01.2	02	01.0	01	01.0	02	01.5	49									
XI	761.0 00.7	02.9	01.4	01.6	03.4	00.2	14.0	01	-04.4	15	03	01.0	38	01.1	01	01.0	02	01.0	04	01.0	01	01.0	01	01.0	61							
XII	749.5 -00.3	02.8	00.5	00.9	03.8	-02.2	14.7	30	-13.2	04	06	*	20	01.4	*	*	*	*	19	02.0	*	*	*	*	54							
GOD.	751.8 06.8	13.7	09.6	09.9	14.7	05.6	33.7	07VII -15.0	24.II	04	01.1	316	01.3	12	01.1	09	01.0	07	01.3	145	01.8	04	01.0	23	01.2	533						
$\varphi = 45^{\circ}07' N \lambda = 15^{\circ}35' E$ Gr. $\Delta G = + 1h\ 02\ min.$															SLUNJ												BR. ST. 53					
I	-01.3	01.9	00.3	00.3	03.2	-02.3	12.5	12	-08.9	06	09	01.3	13	01.3	05	01.6	21	01.9	05	02.4	06	01.7	03	01.0	26	01.2	05					
II	-01.2	02.8	00.6	00.7	03.4	-02.4	14.2	24	-14.0	21	07	01.3	12	01.4	10	01.6	25	01.6	02	02.5	01	31.0	01	03.0	19	01.5	07					
III	03.4	11.4	06.7	07.0	12.8	02.0	21.0	30	-02.3	13	07	01.9	12	02.0	09	01.9	29	01.9	05	01.8	11	01.9	04	02.5	11	01.5	05					
IV	06.4	12.3	07.0	08.7	13.6	04.5	23.2	30	-01.4	17	09	01.7	15	01.7	14	01.9	25	01.7	02	01.0	06	02.2	09	01.8	07	01.3	03					
V	-	10.7	16.7	11.8	17.7	08.1	23.0	05	00.5	12	15	01.3	18	01.8	13	01.5	15	01.7	02	02.0	04	02.5	05	01.6	14	01.4	07					
VI	-	14.7	21.3	16.4	17.2	22.5	11.8	26.8	05	06.0	29	08	01.5	13	01.6	15	01.6	17	01.8	07	02.1	12	02.2	05	10	01.3	03					
VII	-	15.0	23.1	17.2	18.1	24.2	12.0	30.5	18	07.0	23	10	01.9	22	01.8	19	01.8	19	01.8	01	02.0	03	03.0	18	01.4	01	01					
VIII	-	14.1	22.8	16.7	17.4	23.7	12.1	33.2	07	08.0	11	19	01.7	15	01.9	22	01.9	26	01.7	03	01.3	02	03.5	05	01.0	09						
IX	-	10.8	19.8	13.3	14.3	20.8	08.8	30.0	11	01.5	21	09	01.7	11	01.6	13	02.0	29	01.9	02	02.0	03	03.0	05	02.8	13	01.5	05				
X	-	07.4	12.8	08.4	09.2	13.5	06.1	18.5	10	-06.1	20	07	01																			

Mjesec	Oblačnost Nm (0-10)			Vlažnost vazduha %	Padavine R mm	Broj dana na sat																																										
	7	14	21			Sred. (Dnev.)	Inzolatija broj sati			Vlažnost vazduha			Padavine R mm			Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	≤	<	<	IV	IV	≥	<	>	N	N	N	•	*	*	Δ	Δ	▲	▲	R	T	≡	■		
							mm	7	14	21	Sred. (Dnev.)	Min	Max	Dat.	30.00.0	0.0250.0	30.020.0	6	8	2.0	8.0	0.1	1.000.0	9	Δ	*	Δ	Δ	▲	▲	R	T	≡	■														
OGULIN																													H = 328 m H_b = 328.2 m h = 2.0 m h = 1.5 m																			
BR. ST. 51																																																
I	8.4	8.5	7.5	8.1	047.0	04.2	91	82	89	87	46	148	024.1	30	.	09	25	.	.	.	07	31	04	23	22	17	06	18	12	01	02	01	01	04	10	18												
II	8.5	8.3	8.4	8.4	053.6	04.2	89	77	89	85	46	124	027.1	20	03	06	22	.	.	.	04	01	21	20	18	12	16	03	01	03	02	03	23															
III	6.9	6.7	5.3	6.3	166.0	05.2	86	57	78	76	32	208	032.2	06	.	.	10	.	.	.	13	03	02	12	18	15	08	16	09	06	01	01	02	06														
IV	7.3	8.8	6.8	7.6	131.6	06.0	86	59	78	75	38	132	046.5	16	.	.	02	.	.	.	09	31	01	17	18	13	04	17	05	04	03	04	01	01														
V	8.2	8.4	7.2	7.9	130.9	08.3	84	64	80	76	37	141	023.8	14	.	.	01	.	.	.	05	01	01	20	21	14	07	21	01	01	.	.	01	08	01													
VI	5.6	5.8	6.1	6.1	227.6	09.9	80	56	76	71	32	102	032.4	14	.	.	07	.	.	.	08	01	10	14	11	04	14	06	02															
VII	5.0	5.7	4.0	4.9	284.5	11.4	88	58	80	75	37	089	028.3	22	.	.	07	.	.	.	06	08	07	10	07	04	10	05	03															
VIII	4.7	5.4	3.2	4.4	255.8	11.0	91	58	85	78	36	090	031.5	31	.	.	11	01	.	.	32	31	09	04	10	08	02	10	07	02														
IX	5.6	6.1	3.4	5.0	198.2	09.4	90	59	89	79	38	112	038.3	28	.	.	02	.	.	.	05	05	08	12	10	03	12	03	01															
X	6.4	6.4	5.5	6.8	101.4	07.5	94	66	93	85	42	070	028.1	02	.	.	07	.	.	.	03	03	12	09	08	04	09	02	07															
XI	7.9	7.0	6.5	7.8	057.9	04.4	94	81	93	89	30	050	019.0	28	.	04	21	.	.	.	01	02	19	06	05	03	03	04	.	.	01	01	17	04														
XII	6.8	8.8	7.6	8.4	049.3	04.7	88	77	87	84	49	141	028.4	19	05	07	17	.	.	.	13	03	01	21	23	15	05	18	12	03	.	.	01	03	11	20												
GOD.	7.1	7.3	6.1	6.8	1713.8	07.2	88	66	84	79	30	1407	046.5	46.IV	08	26	98	27	01	.	.	76	10	36	176	183	143	53	160	59	18	03	03	09	02	46	59	72										
KARLOVAC																																H = 112 m H_b = 122.6 m h = 2.0 m h = 1.0 m																
BR. ST. 52																																																
I	8.6	8.7	8.5	8.6	031.6	04.3	93	83	89	88	45	068	016.2	18	.	06	23	.	.	.	02	23	17	11	02	13	08	01	.	.	.	02	10	15														
II	9.2	7.9	7.6	8.2	042.3	04.4	93	76	87	85	46	063	015.0	12	02	04	18	.	.	.	02	19	16	10	02	11	10	02	.	.	01	10	13															
III	6.1	6.1	4.4	5.5	156.7	06.7	93	57	74	75	32	135	023.0	06	.	.	08	.	.	.	06	09	15	13	07	15	04	01	.	.	01	03	02															
IV	6.8	7.5	6.5	7.0	149.9	06.7	92	56	76	75	37	080	017.2	16	.	.	01	.	.	.	02	14	17	13	03	17	.	.	.	03	01																	
V	8.0	7.7	5.5	7.1	141.9	09.0	93	57	79	76	34	104	023.2	14	.	.	01	.	.	.	01	11	18	14	03	18	.	.	.	01	01	02																
VI	4.8	5.8	4.3	5.0	242.4	11.1	88	52	75	72	30	052	017.6	14	.	.	16	03	.	.	05	05	12	08	02	12	.	.	.	02	01																	
VII	5.2	4.9	3.1	4.5	276.5	12.2	92	52	76	73	36	136	043.2	08	.	.	22	02	.	.	11	05	11	09	04	11	.	.	.	05	03	03																
VIII	4.3	4.6	3.2	4.0	261.7	12.1	93	53	82	76	33	078	027.0	31	.	.	17	04	.	.	02	15	07	09	03	03	09	.	.	02	03																	
IX	5.8	5.0	3.0	4.7	196.4	10.3	95	56	89	80	30	113	030.2	28	.	.	07	01	.	.	08	07	11	09	03	11	.	.	.	03	06																	
X	8.2	5.2	5.1	6.2	121.9	07.9	94	65	89	83	35	074	027.8	02	.	.	01	.	.	.	03	10	07	05	02	07	.	.	.	02	12																	
XI	9.9	8.8	9.3	9.4	015.9	04.7	93	87	92	91	66	037	021.0	28	.	02	18	.	.	.	25	07	04	01	03	04	02	.	.	12	04																	
XII	9.4	8.3	7.7	8.4	027.1	04.7	94	84	93	90	47	087	023.3	19	02	07	19	.	.	.	21	12	11	92	10	03	.	.	.	18	23																	
GOD.	7.2	6.7	5.7	6.5	1664.3	07.8	82	64	83	80	30	1019	043.2	08.VII	04	19	88	62	10	.	02	55	158	152	112	36	139	31	06	.	01	01	23	80	57													
SLUNJ																															H = 258 m H_b = 2.0 m h = 2.0 m h = 2.0 m																	
BR. ST. 53																																																
I	8.5	8.3	7.3	8.0	-	04.0	09	80	86	85	38	105	018.0	21	.	10	25	.	.	.	03	20	17	14	05	10	10	.	.	.	01	13	14															
II	9.2	8.3	7.6	8.4	-	04.1	08	73	86	82	42	082	017.7	20	02	07	22	.	.	.	21	19	20	16	02	09	16	.	.	02	01	08	20															
III	6.2	6.5	4.5	5.7	-	05.0	05	32	71	69	24	153	029.0	07	.	.	06	.	.	.	06	08	18	13	06	14	07	01	.	.	03	03																
IV	7.8	8.6	7.1	7.0	-	06.1	03	81	85	82	32	088	033.6	16	.	.	02	.	.	.	01																											

Mjesec	Vremenska perioda m	Temperatura vazduha °C								Čestina pravaca i srednja jačina vjetra m/s, Fm (0-12)																		
		km				km				Čestina pravaca i srednja jačina vjetra m/s, Fm (0-12)																		
		7	14	21	Sred. (plus)	km	km	km	km	Dst.	Mis	Dst.		N	NE	E	SE	S	SW	W	NW	C						
$\varphi = 45^{\circ}49' N \lambda = 15^{\circ}59' E$ Gr. $\Delta G = + 1h 04 min.$																												
I	747.9	00.6	02.2	01.4	01.4	03.2	-00.5	10.0	29 -05.1	11	07	01.6	10	02.3	34	01.6	05	01.4	10	01.3	12	01.4	11	01.5	04	01.5		
II	743.9	00.3	03.6	02.2	02.1	04.4	-00.3	15.1	26 -10.3	21	01	01.0	13	01.7	37	01.6	02	01.5	07	01.4	05	01.4	14	01.9	02	01.5	01	
III	746.1	05.3	11.5	08.5	06.4	12.6	04.6	20.8	30 -01.1	20	04	02.0	11	02.2	22	01.5	03	08.3	06	01.6	17	02.6	18	02.2	11	01.6	01	
IV	743.2	08.2	13.6	10.2	10.6	14.5	06.8	21.3	30 01.5	17	06	01.8	19	02.2	22	02.1	04	02.2	07	01.6	14	02.3	15	01.9	09	01.8	.	
V	745.9	12.2	17.0	13.4	14.0	18.2	10.1	22.1	31 29 01.9	12	09	02.0	26	01.7	10	01.9	02	01.0	12	01.7	09	01.8	11	01.5	11	01.7	03	
VI	746.6	16.2	22.3	16.3	18.6	23.0	13.9	28.4	08 08.5	13	09	02.1	21	01.7	06	01.3	09	01.7	09	01.6	17	01.9	08	01.9	02	.		
VII	748.2	16.8	22.8	19.3	19.6	26.4	14.7	28.7	12 10.1	22	07	01.6	24	01.5	06	01.7	14	01.7	09	02.0	10	01.6	09	01.6	03	.		
VIII	748.6	16.4	22.5	18.5	19.0	23.4	14.8	30.6	07 11.1	29.27	06	01.7	25	01.5	19	01.4	05	01.8	09	01.9	11	02.0	11	01.4	05	01.2	02	
IX	748.2	12.8	19.2	15.6	15.8	20.2	11.7	27.2	11	06.3	29	05	01.4	20	01.7	12	01.3	04	01.8	06	01.8	13	01.8	13	01.5	13	01.5	04
X	752.4	08.8	13.9	10.8	11.1	14.5	08.2	19.1	09 03.8	28	08	01.1	20	31.6	18	01.4	08	01.5	15	01.5	09	01.3	06	01.0	03	01.0	06	
XI	757.0	01.4	03.2	02.1	02.2	03.5	01.0	12.7	01 -02.6	25	06	02.0	08	01.5	18	01.3	04	01.5	20	02.1	13	01.1	11	01.2	01	03.0	01	
XII	745.3	01.2	03.3	02.0	02.1	04.1	-00.2	13.4	31 -06.8	06	02	01.5	15	01.7	16	01.4	06	01.2	10	01.1	10	01.7	26	01.9	03	01.3	05	
GOD.	747.8	08.4	12.9	10.2	10.4	13.9	07.1	30.6	07.VII-18.3	24.II	70	01.7	216	01.7	220	01.6	68	01.6	122	01.5	129	01.7	163	01.7	79	01.6	28	
$\varphi = 45^{\circ}18' N \lambda = 15^{\circ}59' E$ Gr. $\Delta G = + 1h 04 min.$																												
TOPUSKO																												
BR. ST. 57																												
I	-	-01.1	02.9	00.1	00.5	03.7	-03.9	13.5	29 -10.0	06	14	02.8	11	02.2	08	01.6	11	02.3	12	02.1	11	02.5	11	01.9	14	01.5	01	
II	-	-01.2	04.2	00.2	00.9	04.8	-03.7	17.0	26 -18.0	21	26	02.8	06	02.5	06	02.2	05	01.2	09	02.7	02	03.5	16	01.7	14	01.7	.	
III	-	03.7	12.7	07.0	07.6	13.7	06.8	22.0	30 -05.0	13	23	02.9	04	02.7	04	01.8	07	02.3	16	02.5	10	02.9	10	02.4	07	01.6	.	
IV	-	06.9	14.6	08.6	09.7	15.1	03.2	23.5	30 -02.0	19.17	17	02.8	11	03.4	08	02.5	05	01.4	18	02.6	15	02.3	10	01.6	04	02.3	.	
V	-	11.5	18.4	12.5	13.7	19.2	07.1	24.5	20 19 -00.8	12	12	02.8	08	01.8	04	01.8	06	02.3	11	02.1	26	02.0	12	01.6	14	01.6	.	
VI	-	15.4	23.5	16.5	17.9	24.2	10.6	30.0	06 04.5	30.29	19	01.9	06	03.0	02	01.5	03	02.3	06	02.7	32	02.2	15	01.7	07	02.1	.	
VII	-	15.2	24.9	17.2	18.6	23.9	10.9	31.4	18 05.5	24	18	02.7	13	02.3	04	01.8	04	01.2	06	01.7	18	02.0	16	01.6	12	01.4	02	
VIII	-	14.6	24.8	16.9	18.3	23.2	10.7	33.0	07 05.5	20	19	01.9	14	01.8	06	02.2	07	01.9	12	01.9	15	02.1	11	01.3	09	01.4	.	
IX	-	11.2	21.1	13.7	14.9	22.2	07.3	31.5	11 -06.2	21	21	01.9	10	01.9	02	01.0	12	01.4	05	02.4	23	02.1	04	02.0	13	01.4	.	
X	-	07.8	14.5	08.7	09.9	14.9	05.3	20.6	04 -05.0	28	28	01.6	11	01.5	04	02.2	03	01.0	10	01.6	11	01.5	09	01.4	17	01.2	.	
XI	-	00.7	03.5	01.5	01.6	03.7	-00.9	14.0	01 -07.5	30	20	01.7	06	02.0	03	01.3	14	01.8	16	01.6	08	01.6	11	02.1	14	01.8	.	
XII	-	-00.3	04.1	00.6	01.2	04.8	-03.4	15.0	29 -19.0	06	16	01.4	16	02.5	09	01.3	15	02.2	18	02.4	17	01.5	02	01.3	.			
GOD.	-	07.0	14.1	08.6	09.6	14.8	03.6	33.0	07.VII-18.0	24.II	233	02.2	118	02.3	60	01.8	77	01.8	144	02.2	142	01.7	129	01.6	03	.		
$\varphi = 45^{\circ}49' N \lambda = 16^{\circ}02' E$ Gr. $\Delta G = + 1h 04 min.$																												
ZAGREB-MAKSIMIR																												
BR. ST. 58																												
I	751.2	-00.7	01.9	00.5	00.5	03.4	-02.0	10.3	03 -07.0	06	27	01.7	13	02.0	17	01.4	10	01.2	14	01.2	05	01.6	05	01.0	02	01.0	.	
II	747.2	-01.2	03.8	00.6	00.9	04.5	-02.7	16.2	26 -19.0	21	27	01.6	21	01.8	11	01.5	03	01.0	03	01.7	10	01.9	05	01.4	04	01.0	.	
III	749.1	03.4	11.8	04.6	07.1	13.2	01.5	21.8	30 -03.3	13	30	01.6	14	02.1	03	01.7	04	01.8	05	02.0	13	02.5	28	02.0	04	01.8	02	
IV	746.3	07.1	13.5	06.7	09.5	14.8	04.0	22.0	30 -01.2	17	38	02.0	18	02.4	09	01.6	03	01.7	04	01.5	12	01.9	06	02.2	.			
V	748.9	11.7	17.1	12.0	13.2	18.5	07.8	22.9	31 -01.5	12	35	01.7	09	02.0	08	02.0	06	01.3	12	01.6	10	02.0	07	01.6	06	01.5	.	
VI	749.5	15.9	22.4	16.2	17.7	24.0	11.3	29.1	07 05.0	15	33	01.5	08	02.0	10	01.7	07	01.6	08	02.1	11	02.1	08	02.0	05	01.6	.	
VII	751.1	16.3	23.0	17.2	18.4	24.8	12.4	29.7	12 07.6	09	39	01.5	09	02.7	08	01.8	09	01.3	08	01.8	09	02.2	04	01.8	04	01.2	03	
VIII	751.7	15.5	22.8	16.0	17.6	24.0	12.0	31.6	07 07.5	29	44	01.4	09	01.6	05	02.0	13	01.9	03	02.3	03	01.0	02	01.0	01	01.0	.	
IX	751.2	11.4	19.9	13.4	14.6	21.2	09.0	29.6	11 02.																			

Meseč	Oblačnost Nm (0-10)				Inzolacija broj sati Sred. (Dnev.)	Vlažnost vazduha				Padavine R mm		Broj dana na sat:																								
	7	14	21			U	n	s		Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	Δ	Δ	Δ	Δ	R	T	≡	█						
	mm	mm	mm	mm		7	14	21	T _{min}	T _{max}	T _{min}	T _{max}	T _{min}	T _{max}	6	8	2.0	8.0	0.1	1.0	20.0	9	Δ	*	Δ	Δ	Δ	Δ	R	T	≡	█				
ZAGREB-GRIC																																				
BR. ST. 56																																				
I	8.8	8.9	8.1	8.6	033.9	04.2	83	80	82	82	40	046	017.9	16	.	04	21	.	.	01	.	01	24	15	07	02	12	09	04	02	.	12	18			
II	9.1	9.3	7.0	8.1	053.4	04.2	80	70	77	75	47	045	010.4	20	01	04	15	.	.	01	.	18	05	01	09	02	01	01	01	01	01	10	07			
III	6.6	7.5	4.7	6.3	145.4	05.4	79	55	66	66	32	069	023.4	24	.	02	.	.	.	05	01	02	11	18	10	02	17	04	02	.	.	04	02			
IV	7.3	8.2	6.8	7.5	137.6	06.0	72	52	66	63	29	054	018.6	14	03	.	01	13	14	09	01	14	.	.	.	02	03	.			
V	7.9	8.5	7.4	7.9	138.0	08.0	81	62	76	73	42	114	023.3	23	02	.	18	10	03	25	09	.				
VI	5.4	6.6	5.5	5.8	233.3	10.4	74	52	67	65	29	062	016.6	12	.	.	12	.	.	07	.	02	05	12	10	01	12	.	.	.	04	06	.			
VII	5.0	6.7	4.7	5.5	251.1	11.6	81	57	69	69	35	115	048.9	16	.	.	15	.	.	01	01	04	06	11	09	04	11	.	.	01	08	.				
VIII	4.2	5.6	4.8	4.9	239.1	11.5	81	57	71	70	37	070	031.2	31	.	.	12	02	01	01	.	06	06	10	08	02	10	.	.	.	04	.				
IX	6.2	5.4	5.1	5.6	188.9	09.9	85	60	76	74	37	075	021.5	13	.	.	.	01	.	.	01	.	05	06	11	07	03	11	.	.	.	05	02	.		
X	6.1	5.4	6.3	5.9	134.8	07.6	86	66	80	77	38	052	020.5	02	02	.	04	08	08	05	02	08	.	.	.	01	06	.			
XI	9.0	9.4	9.6	9.3	014.3	04.6	87	82	86	85	51	017	011.3	28	.	01	15	.	.	01	.	27	04	02	01	02	03	02	.	.	.	16	04	.		
XII	8.4	7.5	6.6	7.5	034.8	04.8	85	79	85	83	00	061	019.0	20	.	05	18	.	.	02	.	01	17	14	12	01	14	03	01	.	.	01	.	14	21	
GOD.	7.0	7.3	6.4	6.9	1604.6	07.4	81	64	75	73	00	780	048.8	46.VII	01	14	71	40	02	01	21	02	27	157	157	105	23	145	28	11	02	01	04	34	64	52
TOPUSKO																																				
BR. ST. 57																																				
I	7.3	8.0	6.1	7.1	-	04.4	90	89	89	89	44	076	025.0	18	01	03	26	04	16	12	10	02	08	05	.	.	.	03	12			
II	6.2	7.5	5.5	7.4	-	04.5	88	82	86	86	39	068	019.0	20	03	03	24	02	17	09	09	02	05	05	.	.	.	01	11			
III	4.1	5.2	3.8	4.4	-	06.1	89	64	79	77	27	106	023.2	25	.	01	11	.	.	01	.	11	05	11	11	05	11	03	02	.	.	.	02			
IV	6.4	7.1	4.4	5.9	-	07.2	88	65	80	78	34	119	039.6	16	.	03	.	.	.	05	09	09	09	04	09					
V	6.2	6.2	5.1	5.9	-	09.7	90	67	84	80	43	144	029.6	14	.	01	.	.	.	01	06	16	16	07	16					
VI	5.0	4.4	4.1	4.5	-	11.6	89	55	82	75	23	045	016.2	14	.	.	15	01	.	.	01	05	09	01	01	09	01	.	.	.	01	.				
VII	3.8	4.2	2.8	3.6	-	12.1	92	53	81	75	09	092	036.1	08	.	01	21	03	.	.	01	15	05	07	07	04	07	.	.	.	06	.				
VIII	3.8	3.6	3.1	3.5	-	12.3	92	55	83	77	35	084	043.5	31	.	01	17	05	.	01	16	06	07	05	03	07	.	.	.	03	.					
IX	3.8	3.9	2.0	3.2	-	10.9	95	67	90	84	41	127	031.7	13	.	01	07	01	.	.	10	03	11	10	05	11	.	.	.	02	.					
X	8.4	5.1	4.2	5.9	-	08.5	94	81	91	88	49	052	023.2	02	.	05	.	.	.	01	12	07	07	02	07	.	.	.	13	.						
XI	9.7	9.3	9.0	9.3	-	04.6	82	87	91	90	62	040	021.0	29	.	01	21	.	.	.	01	27	05	04	02	04	03	02	.	.	11	03				
XII	8.7	8.9	5.5	7.0	-	04.7	90	83	88	87	49	101	033.2	20	04	06	22	.	.	.	02	14	14	12	03	09	05	.	.	.	05	11				
GOD.	6.3	6.0	4.7	5.6	-	08.1	90	70	85	82	09	1054	045.5	34.VIII	08	12	114	60	10	.	01	81	125	117	106	40	103	21	04	.	.	.	45	37		
ZAGREB-MAKSIMIR																																				
BR. ST. 58																																				
H = 123 m H _b = 127.6 m h = 2.0 m h = 2.0 m																																				
I	8.8	8.9	7.6	8.4	-	032.0	04.1	88	80	86	85	43	036	012.4	16	.	04	25	.	.	02	24	14	09	01	08	09	02	.	01	.	11	14			
II	9.4	8.0	7.2	8.2	-	051.0	04.2	86	87	89	86	42	036	009.9	12	04	04	20	.	.	02	18	14	06	04	38	10	01	01	01	01	10	07			
III	6.6	7.2	4.0	5.9	-	154.3	05.4	87	54	76	73	28	065	017.6	24	.	01	11	.	.	04	23	09	16	12	02	15	03	02	.	02	02				
IV	6.8	7.6	6.3	5.9	-	148.3	06.2	82	81	53	74	69	28	058	016.0	14	.	03	.	.	02	01	10	16	10	02	14	.	.	.	03	.				
V	7.3	8.5	5.5	7.2	-	140.1	09.0	86	61	85	77	41	117	027.5	23	.	01	.	.	03	.	06	23	18	04	23	.	.	.	08	03	.				
VI	5.2																																			

Mjesec	Vremenski interval h	Temperatura vazduha °C										Čestina pravaca i srednja jačina vетра m/s, fm (0-12)																							
		Z		S		W		NE		NW		fm		N		S		SW		SE		E		W		NW		C							
		7	14	21	Sred. Građ.	H	H	M	M	D	D	8.	9.	10.	11.	12.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	25.	26.	27.	28.	29.	30.	31.
$\varphi = 45^{\circ}45' N \lambda = 16^{\circ}38' E$ Gr. $\Delta G = + 1h 06 min.$																																			
I	-00.9	02.4	01.1	00.9	03.2	-02.1	12.4	29	-09.0	06	19	02.1	32	01.6	06	01.8	11	01.6	13	02.1	10	01.8	04	01.8	08	01.8		
II	-00.8	04.3	01.7	01.7	04.8	-02.5	18.0	26	-22.5	21	24	01.7	24	01.8	05	01.6	02	02.5	04	01.2	09	01.7	02	01.0	14	01.4		
III	-04.2	11.7	08.7	08.3	12.8	02.5	21.4	30	-02.9	13	12	02.2	11	01.5	05	02.0	06	01.5	11	02.3	32	02.1	37	01.4	09	01.6		
IV	-06.7	13.4	10.2	10.2	14.4	04.0	22.3	30	00.6	18.07	18	1.8	25	01.9	13	02.2	02	02.5	06	02.3	05	02.0	11	02.1	10	01.6		
V	-11.3	17.7	14.4	14.5	18.9	08.7	23.4	31	-02.3	12	13	02.1	16	02.1	06	02.0	09	02.0	13	01.9	11	02.1	07	02.0	20	01.6		
VI	-15.3	22.9	19.3	19.2	23.9	12.1	28.9	06	07.0	15	27	01.7	15	01.5	04	01.6	04	02.0	08	02.1	33	01.9	27	02.1	10	01.5		
VII	-16.6	23.7	20.0	20.0	25.0	12.8	30.5	29	07.2	23.04	14	04.6	19	01.6	06	01.8	05	01.8	15	01.7	09	01.4	14	01.3				
VIII	-19.3	23.9	19.2	19.4	25.2	11.8	31.4	07	06.5	29	19	01.4	19	01.6	05	01.2	12	01.8	06	01.4	12	01.8	07	01.1	11	01.4		
IX	-11.6	20.9	16.8	16.5	21.9	09.6	29.8	11	01.0	21	13	01.5	15	01.8	05	02.2	32	01.0	04	02.2	22	01.8	08	01.9	21	01.5		
X	-06.9	14.6	10.9	10.8	15.1	05.6	21.3	07	-02.0	28	31	01.6	06	01.7	03	01.7	08	01.5	12	01.9	06	01.3	09	01.1				
XI	-00.6	02.9	01.6	01.7	03.4	-00.1	16.5	01	-04.5	16	14	01.8	16	01.9	06	02.0	30	01.2	09	01.8	29	01.6	04	01.3	06	01.2		
XII	-00.3	03.5	01.7	01.7	04.3	-01.8	14.2	30	-12.5	07	06	02.0	20	01.8	06	01.7	04	01.0	12	02.0	32	02.1	06	01.0	07	01.6		
GOD.	-	07.2	13.9	10.5	10.4	14.4	05.1	31.4	07VM	-22.0	21.II	180	01.7	228	01.7	78	01.9	71	01.7	101	01.9	222	01.9	78	01.6	137	01.5	
$\varphi = 45^{\circ}54' N \lambda = 16^{\circ}51' E$ Gr. $\Delta G = + 1h 07 min.$																																			
I	749.7	-01.3	02.9	00.3	00.5	03.4	-02.1	12.0	29	-09.5	06	35	02.2	25	01.1	17	01.9	16	01.1	09	01.1	09	01.2	07	01.0	05	01.0	
II	749.6	-01.8	04.3	00.4	00.8	04.9	-03.7	19.0	26	-22.5	21	16	01.9	29	01.4	12	01.0	06	01.0	02	01.0	09	01.8	05	01.0		
III	747.6	03.0	11.9	06.3	06.9	13.1	01.2	22.0	30	-04.2	13	10	03.1	18	01.5	14	01.1	16	01.0	07	02.6	23	01.7	02	01.0	03	01.0	
IV	744.8	06.3	13.8	08.9	09.5	14.9	03.9	23.5	30	-00.5	07	11	02.0	29	01.3	10	01.0	08	01.0	02	01.0	04	01.4	06	01.0	14	01.4	
V	747.5	11.3	18.1	12.3	13.5	18.9	08.1	24.3	01	-03.0	12	11	01.8	23	01.2	05	01.4	14	01.1	06	01.7	17	01.4	05	01.2	12	01.1	
VI	748.2	15.6	22.9	17.0	18.1	24.0	11.1	29.2	08	04.6	15	29	02.0	12	01.3	08	01.1	16	01.0	08	01.1	15	01.4	20	01.2	08	01.2	
VII	749.7	16.2	24.1	18.0	19.1	25.3	12.2	30.8	29	06.4	24	25	01.4	15	01.1	10	01.0	17	01.0	03	01.7	25	01.2	06	01.0	12	01.1	
VIII	750.4	15.3	24.2	17.0	18.4	25.0	11.5	31.6	07	06.0	29	33	01.7	18	01.0	13	01.0	20	01.0	01	01.0	22	01.3	06	01.0	23	01.0	
IX	749.8	10.8	21.0	13.9	14.7	21.8	08.2	30.5	11	02.0	29	07	01.7	17	01.3	12	01.0	06	01.0	04	01.0	19	01.3	21	01.0	04	01.0	
X	750.4	06.6	15.2	08.6	09.7	15.9	04.6	22.2	10.4	-02.0	28	10	02.4	37	01.2	15	01.3	01	01.0	06	01.0	06	01.7	10	01.0	07	01.1	01
XI	758.6	00.6	03.0	01.5	01.7	03.4	-0.4	15.6	01	-06.0	16	02	01.5	18	01.1	10	01.0	17	01.0	16	02.0	10	01.0	07	01.0			
XII	746.9	00.2	03.6	01.0	01.4	04.6	-02.3	15.5	30	-13.2	07	07	01.0	20	01.0	09	01.0	04	02.0	31	01.5	04	01.0	09	01.0			
GOD.	-	07.6	13.8	08.7	09.5	14.6	04.3	31.8	07VM	-22.5	24.II	89	01.8	266	01.3	72	01.4	264	01.5	73	01.4	88	01.5	36	01.7	190	01.5	17
$\varphi = 45^{\circ}22' N \lambda = 16^{\circ}38' E$ Gr. $\Delta G = + 1h 08 min.$																																			
I	-00.4	02.4	00.7	00.9	03.3	-01.7	13.0	29	-08.5	09	36	01.2	20	01.1	08	01.2	07	01.1	01	01.2	07	02.0	07	02.0	18	02.1	
II	-00.7	03.6	01.2	01.3	04.3	-02.5	16.5	26	-20.0	21	16	02.3	27	01.4	06	01.2	20	01.6	05	01.4	03	01.3	02	01.5	14	01.2	01	
III	-04.4	11.7	07.6	07.8	13.2	02.7	21.7	30	-03.0	23	11	02.2	25	01.2	02	01.0	26	01.5	07	01.4	05	02.6	02	01.0	15	01.7		
IV	-07.0	13.7	09.4	10.1	14.7	05.0	23.0	30	-06.7	18	06	02.5	72	01.3	04	02.5	21	01.4	08	01.9	02	01.5	08	02.0	08	02.1	19	01.6
V	-11.7	17.8	12.7	13.7	19.0	08.9	25.0	01	-01.5	12	11	01.5	18	01.6	06	02.0	22	01.6	06	01.5	14	01.8													

Mjesec	Oblačnost Nm (0-10)				Vlažnost vazduha %	Padavine R mm	Broj dana na sat												•	*	*	Δ	▲	▲	R	≡	
	Insolacija broj sati			Srednji broj (Dnev.)			Tn	Tx	Tn	Tx	Tn	F(0-12)	Nm (0-10)	R mm	•	*	*	Δ	▲	▲	R	≡					
	7	14	21	mm	7	14	21	Max.	Dat.	≤	<	<	≥	≥	≥	<	>	≥	≥	≥	≥						
CAZMA																					$H_a = 144 \text{ m } H_b = - \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$						
BR. ST. 61																						$H_a = 144 \text{ m } H_b = - \text{ m } h_t = 2.0 \text{ m } h_r = 1.2 \text{ m}$					
I 8.9 8.6 9.2 8.9	-	04.7 93 95 94 94 78	028 006.5	30	.	04	25	01	24	11	09	.	06	06	.	.	.	01	08	14		
II 9.0 8.4 8.2 9.5	-	05.0 92 90 93 91 45	051 011.0	18	02	02	23	01	21	08	38	01	03	06	01	.	.	.	06	11		
III 6.4 7.0 6.6 6.6	-	07.9 94 91 92 92 65	085 029.3	23	.	.	08	02	12	15	14	03	13	04	02	.	.	.	01	.		
IV 8.3 8.0 8.1 8.1	-	08.9 93 91 91 92 60	071 029.1	16	18	10	10	02	10	01	.		
V 8.0 8.7 8.6 8.5	-	11.7 93 89 91 91 72	120 021.6	14	.	.	01	18	22	17	05	22	03	03		
VI 4.1 5.6 5.6 5.1	-	15.7 92 89 91 91 80	050 014.7	13	.	.	.	14	05	07	08	09	02	08	01	01		
VII 4.5 5.4 4.8 4.9	-	16.6 92 90 93 92 66	055 015.6	22	.	.	.	16	01	.	.	.	07	07	10	09	02	10	03	05		
VIII 4.4 4.6 4.5 4.5	-	16.3 92 92 92 92 30	049 027.5	31	.	.	.	18	03	.	.	.	08	07	09	04	02	08	02	02		
IX 5.6 5.0 5.1 5.2	-	13.5 94 92 93 93 87	042 025.5	13	.	.	04	04	07	08	02	02	08	05	.		
X 7.9 5.3 4.6 5.9	-	09.5 95 93 94 94 87	049 020.1	05	.	.	02	02	09	06	05	02	06	11	.		
XII 10.0 8.5 8.3 8.9	-	05.0 95 96 95 95 88	017 012.1	28	.	01	19	25	05	02	01	01	03	11	04		
XII 9.2 7.7 7.4 8.1	-	03.2 93 93 93 93 65	040 010.4	20	02	04	22	01	18	12	08	01	11	04	02	.	.	.	04	19		
GOD. 7.7 6.9 6.8 6.9	-	10.0 93 91 92 92 30	657 029.3	23	III	04	17	100	52	04	.	.	.	31	175	124	96	23	107	23	05	.	.	.	10	57	49
BJELOVAR																					$H_a = 141 \text{ m } H_b = 142.4 \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$						
BR. ST. 62																						$H_a = 141 \text{ m } H_b = 142.4 \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$					
I 8.8 8.1 8.3 8.4	-	04.3 95 81 90 88 48	031 006.8	30	.	04	26	02	21	14	10	.	08	09	03	.	.	01	07	12		
II 8.2 7.5 6.1 7.3	-	04.4 92 89 89 84 50	045 011.2	18	05	03	23	03	15	12	07	01	04	09	02	.	.	.	04	11		
III 6.2 6.6 6.4 5.7	-	05.6 93 57 79 77 36	069 017.0	24	.	.	09	01	.	05	08	14	10	03	13	03	01	.	.	04	01		
IV 7.0 6.8 6.5 6.8	-	06.7 90 60 76 76 39	045 013.2	16	.	.	01	04	14	12	08	02	11	03	01			
V 7.2 7.8 7.3 6.8	-	09.5 93 61 85 80 39	126 024.6	29	.	.	01	06	21	14	05	21	03	02			
VI 4.3 5.2 3.7 4.6	-	11.7 86 55 88 74 35	104 031.8	13	.	.	.	15	09	06	12	09	04	12	04	01	.	.	01	01			
VII 4.5 5.1 2.5 4.0	-	12.7 88 57 85 77 40	076 020.4	06	.	.	18	02	.	.	.	09	04	10	08	03	10	04	02			
VIII 4.2 4.6 2.8 3.9	-	12.4 92 54 88 78 38	059 024.6	31	.	.	18	03	.	01	.	09	04	10	08	02	10	03	03			
IX 5.5 5.0 2.5 4.4	-	10.4 94 59 91 82 40	046 017.8	13	.	.	03	01	.	.	.	08	06	09	06	02	07	03	07			
X 7.4 4.6 4.6 5.6	-	07.9 96 67 92 83 34	040 012.0	02	.	03	04	08	06	04	02	06	01	13			
XI 9.7 9.1 9.0 9.3	-	04.8 95 90 93 93 58	022 011.2	27	.	01	20	01	26	03	03	02	01	03	01	13	04		
XII 9.0 7.8 7.3 8.0	-	04.9 94 84 93 93 58	050 009.8	20	02	05	21	01	18	14	13	13	03	01	01	13	19		
GOD. 6.8 6.5 5.2 6.2	-	07.9 92 66 86 82 34	721 031.8	45	VI	07	13	104	54	06	.	02	.	55	136	137	101	26	120	27	07	.	.	05	28	47	
BRESTACA-NOVSKA																					$H_a = 152 \text{ m } H_b = - \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$						
BR. ST. 63																						$H_a = 152 \text{ m } H_b = - \text{ m } h_t = 2.0 \text{ m } h_r = 1.0 \text{ m}$					
I 9.6 8.3 8.9 8.9	-	04.4 88 83 88 87 50	042 010.2	18	02	04	21	24	14	12	01	10	08	03	01	.	.	01	14	87		
II 9.3 7.9 7.0 8.1	-	04.4 87 76 86 83 52	045 029.4	20	02	05	19	01	17	16	11	01	10	10	04	.	.	.	08	13		
III 6.4 6.4 6.4 6.3	-	05.7 84 61 71 72 33	060 015.6	24	.	.	06	02	03	12	12	11	02	11	01	.	.	.	04	01			
IV 7.3 7.3 7.6 7.4	-	06.8 83 61 78 74 34	037 012.5	14	.	.	01	01	14	15	09	01	15	04	.			
V 8.1 7.2 6.6 7.2	-	09.5 90 63 84 79 36	145 036.2	07	.	.	01	01	.	.	.	01	01	09	18	15	05	18	03	05		
VI 6.1 5.4 3.7 5.1	-	11.7 84 61 78 74 37	064 019.6	12	.	.	15	05	07	10	10	03	10	04	02			
VII 4.9 4.1 3.1 4.0	-	12.7 90 60 70 74 42	067 014.0	22	.	.	19	02	.	01	01	12	04	09	08	03	08	03	03			
VIII 5.3 3.9 2.8 4.0	-	11.9 87 53 78 73 38	042 032.5	31	.	.	16	04	.	.	.	10	04	04	01	06	04	01	06	.	.	.	01	06			
IX 5.2 4.4 3.8 4.4	-	10.3 91 60 86 79 36	099 030.4	20	.	.	06	01	.	.	.	08	10	11	08	03	11	04	.			
X 8.6 6.6 5.6 6.9	-	08.1 92 72 87 84 43	038 010.6	27	.	.	01	03	13	13	05	01	06	18	.			
XII 10.0 9.9 9.0 9.6	-	04.8 94 89 93 92 63	025 010.2	28	.	.	17	27	05	04	01	04	03	26	03			
XII 9.8 8.2 7.7 8.6	-	05.0 90 80 89 95 55	063 022.0	19	02	04	20	20	17	11	03	12	05	01	10	18		
GOD. 7.6 6.6 5.9 6.7	-	07.9 88 68 83 80 33	767 032.6	07.V	07	13	99	52	06	.	04	01	31	186	152	110	24	133	31	03	01	02	34	72	38		

Mjesec	Vrijednost mm	Temperatura vazduha °C								Cestina pravaca i srednja jačina veta m/s (0-12)																				
		Ta			Sred. (Dnev.)		N		H		Max.		Min.		Dat.		8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.
		7	14	21																										
$\varphi = 45^{\circ}20' N \lambda = 17^{\circ}41' E$ Gr. $\Delta G = + 1h 11 min.$																														
I	-01.6	02.7	00.7	00.6	03.5	-02.6	10.9	29 -08.9	06	26	01.4	15	01.7	08	01.4	05	01.2	07	01.1	06	01.0	12	01.2	14	01.0	.				
II	-02.6	03.2	00.9	00.6	04.2	-04.0	15.5	27 -24.5	21	20	01.1	14	01.1	08	01.4	02	01.0	01	01.0	05	01.0	15	01.0	19	01.1	.				
III	-03.2	11.9	08.1	07.8	13.5	01.7	23.0	30 -03.6	13	26	01.6	05	01.8	03	01.6	.	11	01.3	05	01.2	27	01.2	14	01.1	.					
IV	-06.4	14.0	10.4	10.4	15.3	04.6	24.4	30 -00.2	07	16	01.4	16	01.7	07	01.1	08	01.8	09	01.4	11	01.1	12	01.2	.						
V	-11.9	18.0	13.7	14.3	19.3	08.5	24.4	01 -06.8	12	21	01.3	14	01.5	04	01.5	04	01.0	16	01.1	13	01.1	12	01.2	09	01.1	.				
VI	-16.0	23.1	18.0	18.8	21.1	11.6	30.2	10 -06.6	15	16	01.4	07	01.3	05	01.4	06	01.3	13	01.2	09	01.4	14	01.2	20	01.4	.				
VII	-16.3	25.1	19.6	20.2	26.0	11.8	31.7	18 -07.0	24	09	01.2	15	01.3	09	01.6	01	02.0	09	01.6	18	01.1	22	01.2	10	01.0	.				
VIII	-15.5	25.9	18.0	19.2	26.2	11.7	34.0	07 -07.5	20	08	01.5	09	01.1	10	01.3	04	01.8	04	01.0	21	01.1	21	01.2	16	01.1	.				
IX	-11.8	21.2	19.7	16.1	22.2	09.0	30.8	11 -01.9	21	22	01.6	01	03.0	03	01.0	03	01.0	08	01.0	20	01.0	17	01.1	16	01.2	.				
X	-07.3	15.6	11.6	11.5	16.5	05.4	25.3	04 -03.2	28	22	01.5	04	01.0	12	01.2	07	01.0	10	01.1	12	01.1	12	01.2	.						
XI	-00.7	03.3	02.1	02.0	03.9	-00.3	14.0	01 -05.6	26	23	01.1	11	01.1	14	01.1	09	01.0	10	01.0	02	01.0	06	01.0	15	01.0	.				
XII	-00.9	04.6	02.7	02.4	06.0	-01.8	15.4	29 -12.4	07	10	01.0	09	01.2	12	01.4	07	01.0	09	01.3	16	01.1	15	01.1	15	01.1	.				
GOD.	-	07.0	14.0	10.1	10.3	15.1	04.6	34.0	07VII -26.5	24.II	221	01.4	120	01.3	99	01.4	55	01.1	106	01.2	136	01.1	186	01.1	172	01.1	.			
$\varphi = 45^{\circ}10' N \lambda = 18^{\circ}00' E$ Gr. $\Delta G = + 1h 12 min.$																														
SLAVONSKA POLEGA																														
BR. ST. 66																														
I	755.1 -01.2	02.4	-00.3	00.2	03.2	-03.3	10.4	29 -10.7	09	07	03.3	23	02.2	19	02.4	03	01.7	04	01.2	12	01.7	15	01.3	06	02.2	04	.			
II	750.9 -01.7	03.1	00.0	00.3	03.8	-04.1	13.6	26 -15.6	21	03	02.0	27	01.8	11	02.0	03	01.3	10	01.7	11	01.4	08	01.5	08	.					
III	752.9 03.2	11.8	07.3	07.4	13.5	01.2	22.2	30 -04.0	20	16	03.4	19	02.3	02	02.0	09	01.4	02	01.5	20	02.0	16	01.7	08	01.8	01				
IV	749.7 06.3	14.3	09.2	09.7	15.4	04.6	24.6	12 -00.3	18	06	02.2	19	02.6	11	02.5	04	02.2	01	02.0	16	02.6	19	02.2	07	02.7	.				
V	752.3 11.4	18.1	13.0	13.9	19.2	08.5	24.6	01 -00.2	12	11	02.4	21	01.9	05	02.6	05	01.8	07	01.4	15	02.0	17	02.0	08	01.2	04				
VI	753.0 15.3	22.4	17.3	18.1	21.1	11.6	29.6	10 -07.9	15	05	03.0	17	01.9	08	02.0	03	01.3	16	01.6	20	01.8	10	02.1	08	.					
VII	754.6 15.4	24.6	18.3	19.1	25.9	11.4	32.2	18 -06.2	24	09	02.3	13	01.5	11	01.7	08	02.0	04	01.8	21	01.5	08	01.2	09	01.6	19				
VIII	755.0 14.8	24.8	19.0	19.2	26.0	11.3	32.8	07 -08.1	15	12	01.8	16	01.5	12	01.8	05	02.2	05	01.4	19	01.9	15	01.5	05	01.6	14				
IX	754.7 10.9	20.5	13.8	14.7	21.7	08.6	31.0	11 -01.5	21	07	03.7	13	01.8	03	02.0	.	07	02.3	18	01.8	23	01.7	06	01.5	13	.				
X	758.0 07.1	14.6	08.8	09.8	15.6	05.1	25.2	04 -03.3	29	12	02.3	17	01.7	07	01.9	06	01.7	04	02.0	16	01.7	15	01.3	04	01.2	12				
XI	763.0 01.2	03.1	01.7	01.9	03.5	00.4	13.4	01 -06.7	16	03	01.0	15	01.5	23	01.7	08	01.2	04	01.5	12	01.5	17	01.5	03	01.0	05				
XII	752.3 -00.9	04.2	01.1	01.4	05.1	-02.5	15.2	30 -12.1	06	03	01.0	24	01.0	09	01.5	02	01.4	06	01.5	25	01.9	14	01.4	01	04.0	06				
GOD.	-	07.7	14.3	08.5	09.8	14.7	05.2	32.8	07VII -15.6	24.II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	92		
$\varphi = 45^{\circ}46' N \lambda = 18^{\circ}10' E$ Gr. $\Delta G = + 1h 13 min.$																														
DONJI MIROLJAC																														
BR. ST. 68																														
I	-00.8	02.8	00.2	00.6	03.2	-02.1	09.5	29 -06.6	06	04	02.2	06	02.2	13	02.8	36	02.6	01	02.0	02	01.5	10	02.2	21	02.7	.				
II	-01.3	03.7	-00.4	00.4	04.4	-03.6	15.5	28 -20.5	21	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
III	-04.4	12.1	06.4	07.3	13.2	01.7	21.6	30 -03.6	23	10	03.4	04	02.8	05	02.2	26	02.7	05	02.4	17	02.2	17	02.7	.						
IV	-07.2	14.8	08.8	09.9	15.6	04.4	25.0	30 -01.5	07	01	02.0	18	02.9	08	02.4	19	02.4	03	02.3	14	02.1	08	02.4	19	02.7	.				
V	-12.3	18.3	11.9	13.6	19.5	08.5	24.6	31 -01.5	12	08	02.5	02	02.5	02	02.0	29	02.2	04	01.8	08	02.2	11	02.9	29	02.3	.				
VI	-16.6	23.9	15.9	16.1	24.7	11.4	30.6	10 -08.0	30	02	01.5	07	03.0	03	02.0	21	02.3	02	02.0	23	02.3	32	02.5	.						
VII	-17.1	25.3	17.4																											

Mesec	Oblačnost Nm (0-10)				Vlažnost vazduha %	Padavine R mm	Broj dana na sat:																														
	Inselacije broj sati						U m s				Tn				Tx				F(0-12)				Nm (0-10)		R mm	•	*	*	A	o	▲	▲	R	T	≡		
	7	14	21	Sred. (Dnev.)			7	14	21	Max.	Min.	Σ	Max.	Dat.	<	<	≥	≥	≤	≤	≤	≤	2.0	8.0	0.1	1.0	0.0	•	*	*	A	o	▲	▲	R	T	≡
BR. ST. 66 SLAVONSKA POZEGA																													$H = 152 \text{ m} H_s = - \text{ m} h = 2.0 \text{ m} h = 1.0 \text{ m}$								
I	6.4	7.0	5.7	6.4	-	04.3	91	82	91	88	59	036	008.8	04	.	05	23	03	11	12	08	.	07	05	01	08	03		
II	9.0	7.9	6.5	7.5	-	04.5	87	87	91	88	35	070	030.8	20	04	03	18	02	14	17	10	01	08	09	03	03	13		
III	6.1	6.6	4.6	5.8	-	07.0	90	80	86	85	57	055	014.6	25	.	07	03	07	13	09	03	12	03	01	01	.			
IV	7.6	7.6	6.5	7.2	-	07.5	88	67	83	79	46	038	008.6	06	09	17	11	11	17	04	01	.				
V	6.3	7.0	5.0	6.1	-	10.1	89	68	85	81	45	072	015.6	14	.	.	01	06	16	13	03	16	05	.	.			
VI	4.3	5.9	3.5	4.6	-	12.3	84	59	83	76	40	080	032.1	13	.	.	14	02	.	.	.	06	07	10	08	02	10	04	.	.			
VII	3.1	5.2	2.2	3.5	-	13.1	84	54	83	74	41	059	013.6	22	.	.	20	03	.	01	.	08	01	09	09	03	09	03	01	.			
VIII	4.0	4.8	2.6	3.8	-	12.7	87	53	84	75	37	044	033.5	31	.	.	17	06	.	.	09	03	07	05	01	07	01	.	.				
IX	4.9	5.2	3.7	4.6	-	10.8	88	60	88	78	46	063	024.0	20	.	.	06	01	.	.	.	08	05	08	06	03	08	03	01	.			
X	8.1	5.7	4.5	6.1	-	08.5	89	69	86	82	55	018	009.4	05	.	.	04	01	.	.	.	02	09	05	04	05	05	01	10	.			
XI	9.6	9.2	9.4	9.4	-	04.8	92	85	91	89	64	016	011.2	28	02	01	17	01	.	.	.	02	25	05	02	01	03	03	01	.	.	13	02	.			
XII	7.4	7.7	6.8	7.3	-	05.1	91	87	89	89	67	068	011.2	19	02	05	22	.	.	.	01	19	14	12	03	12	04	02	.	.	.	02	07	06			
GOD.	6.3	6.7	5.1	6.0	-	08.4	88	71	86	82	35	619	033.5	548	VII	06	14	92	58	12	.	01	.	44	112	133	97	20	114	24	03	.	.	.	24	45	25
BR. ST. 67 SLAVONSKI BROD																													$H = 88 \text{ m} H_s = 89.0 \text{ m} h = 2.1 \text{ m} h = 1.2 \text{ m}$								
I	7.6	8.5	7.2	7.8	043.9	04.2	92	79	92	87	45	043	014.4	26	01	05	26	.	.	.	03	01	01	17	12	09	01	09	05	01	.	01	.	16	02	.	
II	9.6	9.5	7.5	8.5	035.4	04.3	95	78	92	88	43	084	019.5	20	04	05	26	.	.	.	02	18	13	03	13	13	04	.	01	.	14	19	.				
III	6.5	6.8	6.0	6.5	191.4	3.3	90	51	73	71	24	059	014.2	07	.	.	08	.	.	.	09	01	03	11	16	11	02	16	03	03	.	01	04	06	.		
IV	7.5	7.8	6.0	7.1	124.7	06.5	91	51	81	74	27	046	017.5	16	.	.	08	.	.	.	05	02	01	08	14	09	01	14	.	.	.	01	04	07	.		
V	7.7	8.5	6.2	7.5	159.8	09.4	92	56	87	79	35	146	032.5	03	.	.	01	.	.	.	04	.	13	19	13	06	19	01	18	12	.		
VI	6.0	6.6	5.9	6.2	219.3	11.4	90	51	84	75	29	050	016.3	28	.	.	13	.	.	.	03	.	09	14	09	02	14	.	.	.	07	09	.				
VII	3.7	5.1	3.0	3.9	296.3	11.9	94	46	83	74	31	063	032.6	08	.	.	20	03	.	.	02	04	02	08	04	02	08	.	.	.	04	16	07	.			
VIII	4.5	4.9	3.9	4.4	250.8	10.9	92	41	74	69	26	024	018.7	31	.	.	17	06	.	.	04	05	09	07	03	01	07	.	.	.	09	07	.				
IX	6.2	5.9	5.1	5.7	185.4	09.4	95	47	89	77	27	061	015.1	20	.	.	06	01	.	.	03	11	09	07	03	09	.	.	.	01	11	.					
X	8.2	6.2	5.2	6.5	096.1	07.8	95	43	92	83	31	021	015.7	05	.	.	05	01	.	.	02	01	11	08	03	01	08	.	.	.	01	14	.				
XI	9.7	9.7	9.3	9.6	002.6	04.9	95	87	93	92	60	010	004.7	30	.	.	16	.	.	.	27	04	04	04	04	03	01	.	.	.	16	03	.				
XII	7.6	7.8	6.9	7.4	041.4	04.9	94	78	90	87	40	065	010.7	10	02	05	22	.	.	.	01	.	01	15	15	11	01	14	03	.	.	.	01	21	10	.	
GOD.	7.1	7.2	6.0	6.8	1596.2	07.6	92	40	85	79	24	672	032.6	08.VII	07	15	104	57	10	.	36	04	23	149	144	98	23	135	27	09	.	02	.	02	33	149	30
BR. ST. 68 DONJI MIMOLJAC																													$H = 97 \text{ m} H_s = - \text{ m} h = 2.0 \text{ m} h = 1.5 \text{ m}$								
I	7.6	6.9	7.3	7.2	-	04.2	89	78	91	86	56	024	009.3	25	0	04	27	.	.	.	02	15	13	04	.	10	07	04	.	.	.	01	04	01	.		
II	7.1	6.7	7.4	7.1	-	04.3	85	76	82	84	51	053	014.2	20	06	04	18	.	.	.	04	14	19	09	02	09	14	03	.	.	.	03	13	.			
III	5.2	5.1	5.2	5.2	-	05.9	84	60	86	77	33	054	013.2	07	.	.	09	.	.	.	07	09	12	09	02	12	04	04	.	.	.	01	01	.			
IV	6.6	6.2	7.1	6.6	-	07.0	85	60	82	76	34	037	013.6	16	.	.	01	01	.	.	02	09	14	07	01	14	.	.	.	05	01	.					
V	6.7	6.6	6.3	6.4	-	09.6	85	63	88	79	23	082	022.5	03	.	.	02	01	.	.	01	.	08	19	12	02	19	.	.	.	05	03	.				
VI	4.8	5.3	4.5	4.9	-	11.3	81	51	87	72	28	059	017.0	13	.	.	15	03	.	.	07	08	14	11	01	14	.	.	.	05	01	.					
VII	3.1	3.0	3.0	3.6	-	12.1	81	50	84	72	31	060	015.0	07	.	.	21	06	.	.	01	01	10	04	07	03	09	.	.	.	02	01	.				
VIII	3.7	3.2	3.9	3.6	-	11.3	81	45	81	69	19	048	033.2	31	.	.	20	08	.	.	11	04	06</td														

Mjesec	Vrijednost pratiljek Fm (m)	Temperatura vazduha $^{\circ}\text{C}$								Cestina pravaca i srednja jačina vетра m/s, Fm (0-12)																			
		1m				Srednji (10m)				N	NE	E	SE	S	SW	W	NW	C											
		7	14	21	Srednji (10m)	N	NE	E	SE	N	NE	E	SE	S	SW	W	NW	C											
$\varphi = 45^{\circ}32' \text{N } \lambda = 18^{\circ}44' \text{E Gr. } \Delta G = + 1h 15 \text{ min.}$																													
I	754.8	-01.1	03.1	-06.2	00.4	03.7	-02.2	10.3	29	-0.1	10	02.2	09	02.1	24	02.5	16	02.8	08	01.9	05	01.4	08	01.8	13	02.2	.		
II	750.5	-02.5	03.2	-00.2	00.1	04.0	-03.9	16.0	27	-24.8	21	19	02.2	10	01.8	05	01.6	20	01.8	06	02.0	05	01.4	09	02.1	12	02.0	.	
III	752.3	03.4	11.9	07.0	07.3	13.4	02.4	22.0	30	-02.0	13	20	02.4	02	02.0	09	02.3	15	02.1	11	01.6	14	01.9	11	02.8	.			
IV	749.3	06.8	14.9	09.7	10.3	15.9	03.1	25.2	12	-01.4	07	14	02.2	17	01.9	13	01.7	15	01.7	04	02.5	05	01.6	13	02.1	09	01.8	.	
V	751.8	12.1	16.7	13.4	14.4	19.7	09.3	25.0	01	-00.6	12	18	01.9	04	01.5	10	01.6	15	02.3	09	01.4	06	01.3	11	01.6	20	02.0	.	
VI	752.5	16.1	23.2	17.6	18.7	24.7	12.7	31.1	10	08.7	27	15	01.5	06	01.8	07	01.9	16	01.7	09	01.1	15	01.7	12	02.2	.			
VII	754.1	14.7	24.7	18.5	19.6	25.9	13.1	31.6	18	08.0	23	11	01.8	11	01.5	10	01.2	18	01.7	06	01.7	04	01.2	13	01.5	16	01.6	.	
VIII	754.6	15.5	24.9	18.4	19.2	26.0	13.0	33.0	08	08.6	20	13	01.7	17	01.4	07	01.0	12	02.1	03	02.0	08	01.1	10	01.8	15	01.9	08	
IX	754.0	12.0	20.6	14.2	15.3	21.6	10.1	30.6	11	02.8	21	14	02.0	06	01.3	04	01.2	07	01.3	10	01.3	09	01.2	16	01.8	20	01.6	04	
X	758.3	07.2	16.8	10.0	11.0	17.5	05.8	26.1	04	-02.3	29	19	01.7	13	01.4	09	01.5	05	01.4	08	01.1	13	01.4	11	01.6	04			
XI	763.5	01.3	03.4	01.9	02.1	04.1	00.9	14.9	01	-02.4	36	07	01.4	18	01.2	12	01.2	22	01.3	05	02.1	07	01.0	09	01.8	06	01.5	04	
XII	751.9	00.1	04.3	01.4	01.8	05.2	-01.3	14.4	29	-16.8	37	06	02.0	08	01.6	13	02.1	23	01.7	12	01.7	13	01.8	14	01.5	01	02.0	03	
GOD.	754.0	07.3	14.1	09.3	10.0	15.1	05.4	33.0	08.VII	-24.8	24.II	166	01.9	121	01.6	123	01.8	190	01.8	07	01.7	90	01.3	145	01.7	146	01.9	27	
$\varphi = 45^{\circ}13' \text{N } \lambda = 19^{\circ}22' \text{E Gr. } \Delta G = + 1h 18 \text{ min.}$																						OSIJEK		BR. ST. 71					
I	-	-00.4	03.0	00.0	00.7	03.7	-01.9	12.4	13	-10.8	38	08	01.5	05	02.4	08	03.1	17	02.5	05	03.4	10	01.3	13	01.3	18	01.3	09	
II	-	00.0	03.8	00.8	01.3	04.0	-01.5	17.8	26	-21.9	21	13	01.0	10	01.1	01	01.0	01	01.6	11	01.7	09	01.4	23	01.1	11	01.2	.	
III	-	04.8	12.0	07.4	07.9	13.1	03.1	22.1	30	-03.8	33	07	01.4	02	01.0	05	01.0	12	02.1	17	01.8	13	01.8	08	01.9	19	01.9	06	
IV	-	07.4	15.0	09.6	10.5	15.5	05.5	23.9	30	-01.1	37	08	01.2	12	01.4	08	01.1	13	01.8	14	01.8	08	01.5	13	01.7	07	01.4	07	
V	-	12.5	18.5	12.8	14.2	19.3	09.4	26.7	01	00.6	32	07	01.4	03	01.7	08	01.5	14	01.6	10	01.2	06	02.0	14	02.0	18	01.7	13	
VI	-	17.1	23.6	17.4	18.9	24.1	13.5	30.0	20	05.7	28	01.2	12	01.3	08	01.6	12	01.5	24	01.4	05	01.2	06	01.2	18	01.7	11	01.7	.
VII	-	18.0	25.7	17.6	19.7	26.0	13.6	30.4	27	08.3	25	02	01.0	04	01.0	14	01.6	14	01.1	18	01.2	13	01.2	15	01.7	21	01.7	06	
VIII	-	17.0	23.8	17.3	19.3	26.3	12.9	32.7	28	07.6	28	06	01.3	13	01.0	01	01.0	15	01.3	03	01.3	13	01.8	06	01.7	13	01.8	23	
IX	-	13.2	21.0	14.3	15.7	21.5	10.9	29.0	11	04.5	34	02	01.5	06	01.0	01	01.0	02	01.0	11	01.4	17	01.5	10	01.9	25	01.6	16	
X	-	08.0	18.0	08.3	10.6	18.2	04.5	24.5	03	-05.5	28	05	01.0	02	01.5	02	01.0	06	01.3	12	01.8	15	01.1	05	01.0	14	01.5	32	
XI	-	00.8	03.3	01.0	01.5	03.5	-00.2	13.7	01	-03.1	21.20	12	01.0	09	01.1	01	01.0	03	01.0	01	01.0	06	01.0	11	01.0	17	01.1	28	
XII	-	06.0	04.8	02.6	02.8	05.3	-00.5	17.1	29	-11.5	37	01	01.0	04	01.0	03	01.3	05	02.2	12	01.7	14	02.2	13	01.5	07	01.0	23	
GOD.	-	08.3	14.5	09.1	10.3	15.1	05.8	32.7	08.VII	-21.9	24.II	90	01.2	82	01.2	50	01.6	118	01.8	112	01.6	130	01.5	192	01.5	200			
$\varphi = 45^{\circ}32' \text{N } \lambda = 13^{\circ}51' \text{E Gr. } \Delta G = + 55 \text{ min.}$																						PULA		BR. ST. 73					
I	-	05.3	06.7	05.7	06.3	10.0	03.1	13.4	29.15	-03.1	66	01	02.0	33	02.7	04	01.8	17	02.4	01	03.0	01	03.0	01	03.0	01	03.0	30	
II	-	04.3	08.3	05.6	04.0	09.4	03.0	13.6	27.11	-05.2	16	03	01.0	27	02.7	09	02.1	20	03.5	03	03.0	01	02.0	18	02.0	23	01.8		
III	-	06.8	11.6	08.0	06.6	12.0	05.1	15.3	31.0	-01.0	20	02	01.5	14	02.4	10	02.4	18	02.8	02	03.0	01	02.0	21	02.3	21	02.0	.	
IV	-	09.3	13.7	10.5	11.2	14.8	07.0	19.5	23	02.1	29	07	05.4	24	03.2	24	02.7	01	01.0	08	02.0	08	02.0	08	02.0	18	02.0	.	
V	-	14.7	17.8	14.3	15.3	19.1	11.7	26.0	29	05.0	32	01	01.0	16	03.1	08	02.2	24	02.5	03	04.0	07	03.4	01	03.0	01	03.0	25	
VI	-	18.0	22.0	18.3	19.3	23.7	14.5	28.0	29	05.5	39	01	01.0	29	05.0	05	03.0	09	02.4	22	02.5	06	03.5	01	03.0	30			
VII	-	21.7	25.6	21.0	22.2	27.1	17.2	32.0	29	11.0	39	01	01.0	13	02.3	01	01.5	21	02.4	01	03.0	04	03.0	01	04.0	12	02.2	32	
VIII	-	20.0	25.2	20.8	21.4	26.5	16.7	30.8	31	11.9	31	02	01.0	12	03.2	12	01.8	12	02.6	01	03.0	02	03.0	02	03.0	02	03.0	34	
IX	-	15.4	21.8	16.7	17.7	22.8	13.2	27.3	36	08.0	30	03	01.0	12	02.4	19	02.4	11	02.2	01	05.0	01	03.0	01	03.0	01	03.0	33	
X	-	11.6	17.7	12.7	13.7	18.9	10.3	23.0	28	06.0	38	02	01.0	23	03.1	06	02.3	09	02.4	01	03.0	01	05.0	01	03.0	01	05.0	38	
XI	-	05.2	12.5	06.5	07.7	13.5	03.7																						

Meseč	Oblačnost mm (0-10)				Vlažnost vazduha %	Padavine mm	Broj dana u meseču																													
							U m s				T m s				P (0-12)				Ra (0-10)		R mm		• * ♀ □ ▲ △ △ ▲ △ T =													
	7	14	21	Sred. (Dnev.)			7	14	21	Max.	Σ	Max.	Dat.	7	14	21	Max.	7	14	21	Max.	6	8	2.0	8.0	0.1	1.0	0.0	• ♀ □ ▲ △ △ ▲ △ T =							
OSTIJEK																																				
Br. ST. 71																																				
I	7.4	7.5	6.5	7.2	064.6	04.0	90	71	87	83	49	020	008.8	04	•	04	24	•	•	03	•	01	15	12	03	•	09	04	•	•	01	•	•	05	01	
II	8.4	8.5	7.8	8.2	048.7	04.2	93	74	90	86	46	057	011.1	20	03	07	17	•	•	03	•	•	17	17	11	03	07	11	•	•	•	•	06	14		
III	6.0	6.5	4.6	5.7	147.8	05.5	90	52	76	73	29	057	009.6	24	•	•	08	•	•	•	04	07	13	11	03	02	•	•	•	•	01	01				
IV	6.5	6.6	5.6	6.3	146.6	06.7	89	50	79	73	27	037	009.6	28	•	•	01	01	•	•	03	11	18	09	•	18	•	•	•	01	06	01				
V	7.4	8.1	4.5	6.7	154.1	09.3	85	53	82	75	36	063	021.4	03	•	•	01	01	•	•	01	10	21	11	02	21	•	•	•	•	02	01				
VI	5.1	6.2	4.5	5.3	230.6	10.8	82	44	78	69	28	093	021.6	04	•	•	15	02	•	•	03	05	13	10	04	13	•	•	•	•	03	01				
VII	3.5	4.6	3.3	3.8	264.8	11.7	83	47	77	69	29	041	012.7	07	•	•	22	02	•	•	09	03	08	08	01	09	•	•	•	•	03	01				
VIII	3.2	3.2	3.2	3.5	253.8	10.9	84	44	72	67	27	051	022.7	31	•	•	17	06	01	•	12	03	04	05	03	04	•	•	•	•	02	•				
IX	6.2	5.5	4.1	5.3	179.3	09.4	90	49	82	74	33	048	019.8	07	•	•	07	01	•	•	04	08	10	06	02	10	•	•	•	•	01	01				
X	6.3	5.0	3.6	5.0	139.2	07.6	93	52	84	76	35	009	004.1	05	•	•	03	01	•	•	09	07	07	03	•	07	•	•	•	03	•					
XI	6.0	5.6	5.6	5.7	009.0	04.8	94	85	91	90	53	010	006.8	28	•	•	14	•	•	•	28	05	02	•	03	02	•	•	•	•	01	08	04			
XII	6.0	6.2	5.8	7.3	046.6	04.8	91	82	90	88	48	043	009.6	10	02	03	22	•	•	•	01	14	13	09	•	11	04	•	•	•	•	01	08	04		
GOD.	6.5	6.7	5.2	6.2	1684.9	07.5	89	58	82	76	27	529	022.7	34.VII	07	14	90	64	11	01	07	•	46	128	144	88	15	129	24	02	•	01	28	36	19	
ILOK																											H _a = 89 m H _b = 91.8 m h _r = 2.0 m h _t = 1.5 m									
Br. ST. 72																											H _a = 133 m H _b = - m h _r = 2.0 m h _t = 1.0 m									
I	6.8	7.0	7.1	7.0	-	03.7	74	71	76	74	42	023	009.1	31	01	07	20	•	•	03	01	05	15	09	07	•	03	04	•	•	•	09	07			
II	7.7	7.6	8.1	7.8	-	04.2	79	72	78	76	21	090	026.7	20	03	06	16	•	•	02	17	14	11	04	09	09	02	•	•	•	•	10	11			
III	5.0	6.3	5.0	5.4	-	05.4	79	57	69	68	29	057	009.4	21	•	•	05	•	•	04	09	14	10	04	01	01	01	•	•	03	•					
IV	6.8	7.1	6.2	6.7	-	06.7	78	57	75	70	39	032	006.2	20	•	•	01	•	•	03	12	14	10	•	14	•	•	•	02	•						
V	6.0	7.1	5.6	6.2	-	09.0	79	60	77	72	34	111	034.6	03	•	•	04	•	•	02	08	16	12	03	16	01	01	•	01	03	02					
VI	4.8	5.0	3.9	4.5	-	11.1	76	57	71	68	29	112	035.7	28	•	•	13	01	•	08	06	03	03	13	01	04	•	•	04	•						
VII	2.3	2.5	1.9	2.2	-	11.4	74	47	74	65	29	036	012.9	08	•	•	21	•	•	20	01	06	05	01	06	•	•	•	•	02	•					
VIII	3.7	3.7	4.8	4.4	-	10.6	72	44	71	62	32	010	003.9	27	•	•	19	06	02	•	09	05	05	03	03	05	•	•	•	•	03	•				
IX	5.5	6.0	4.9	5.4	-	09.5	78	54	77	70	28	097	019.8	28	•	•	07	•	•	05	09	07	07	06	07	•	•	•	•	03	•					
X	5.3	4.2	2.7	4.1	-	07.2	81	52	78	70	34	087	004.2	05	•	•	03	•	•	09	04	05	03	03	03	•	•	•	•	14	•					
XI	9.9	9.6	9.4	9.6	-	04.7	94	88	92	91	39	005	002.1	29	•	•	19	•	•	02	28	05	02	02	02	02	•	•	•	•	23	01				
XII	8.0	8.0	7.7	7.3	-	-	-	-	-	-	-	052	006.7	10	02	03	16	•	•	01	02	16	12	10	11	01	01	01	•	•	11	03				
GOD.	5.8	6.0	5.1	5.5	5.5	5.5	2343.8	08.8	77	61	79	73	17	937	050.5	23.XI	•	•	12	05	09	12	23	05	76	123	124	97	27	122	01	01	•	01	38	14
CRES																										H _a = 30 m H _b = - m h _r = 2.0 m h _t = 1.0 m										
Br. ST. 73																											H _a = 53 m H _b = 51.7 m h _r = 2.0 m h _t = 1.0 m									
I	7.3	7.0	5.1	6.5	-	06.2	83	79	80	81	45	124	035.4	18	•	•	03	•	•	08	14	14	12	05	14	01	01	•	01	01	01					
II	6.8	6.3	5.5	6.2	-	05.7	75	71	76	74	32	093	043.1	20	•	•	04	•	•	07	12	09	08	02	09	01	01	•	01	01	01					
III	6.0	6.8	5.3	6.0	-	07.5	87	75	82	83	25	074	025.5	24	•	•	05	•	•	07	12	15	09	03	15	01	01	•	02	•						
IV	6.8	6.0	6.9	7.2	-	07.8	77	64	76	73	36	045	031.3	12	•	•	05	•	•	02	14	11	07	02	11	•	•	•	•	•	•					
V	7.0	7.0	6.2	6.7	-	10.3	81	72	78	77																										

Mesec	Vazdušni pritisak Pa	Temperatura vazduha °C										Cestina pravaca i srednja jačina vjetra m/s, fm (0-12)																
		Tm			Sred. (Dnev.)	M	N	S	E	M	D	N	NE	E	SE	S	SW	W	NW	C								
		7	14	21								8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.				
$\varphi = 44^{\circ}45' N \lambda = 14^{\circ}46' E$ Gr. $\Delta G = + 59$ min.																												
I	758.5	07.2	10.0	07.1	07.9	11.2	05.1	15.0	15 -02.0	06	23	02.1	12	01.8	C5	01.4	33	04.9	03	02.0	.	04	01.0	10	01.9	03		
II	754.6	06.4	10.0	06.9	07.6	11.0	04.8	14.8	26 -00.0	16	12	01.8	13	01.7	09	03.4	28	04.0	05	02.6	05	01.4	03	01.3	06	01.3	03	
III	758.5	08.2	12.9	09.3	09.9	13.0	06.7	17.8	03 03.3	20	19	02.3	15	03.3	05	01.0	34	03.3	07	02.9	06	01.5	01	02.0	06	02.8	09	
IV	754.6	11.5	15.1	11.7	12.5	16.2	09.2	20.3	23 05.2	17	19	02.2	14	02.7	13	03.1	20	03.4	08	02.0	01	01.0	06	02.0	04	01.8	15	
V	757.9	14.6	18.5	14.4	15.5	19.0	12.3	25.4	31 06.8	12	14	03.1	10	02.2	08	01.6	22	03.1	07	02.4	08	01.9	05	02.2	04	01.5	15	
VI	758.3	19.1	23.1	19.2	20.1	24.3	16.0	27.8	11 13.2	27	10	01.7	17	02.1	08	01.0	25	02.7	06	02.3	07	02.1	08	01.8	06	01.6	14	
VII	759.6	20.8	26.3	21.4	22.5	27.4	18.2	32.5	28 14.2	09	15	01.7	14	01.9	02	01.0	18	02.4	06	02.5	04	02.5	12	02.1	09	02.3	13	
VIII	760.1	20.2	26.1	20.9	22.0	27.0	17.9	31.3	07 14.6	31	17	01.6	17	01.2	05	02.4	12	03.2	07	01.7	05	02.0	10	02.3	10	01.9	10	
IX	760.0	16.2	22.8	17.5	18.5	23.4	14.5	27.3	09 05.7	28	13	02.6	15	01.8	C3	02.0	18	03.2	08	01.5	07	01.3	04	01.2	08	01.9	14	
X	762.3	13.4	19.9	14.3	15.5	20.9	12.2	25.9	03 06.3	28	21	01.7	25	02.1	06	01.8	11	04.3	08	01.4	04	01.8	07	01.9	13	01.4	04	
XI	766.3	08.4	15.5	09.0	10.5	16.7	07.2	21.1	15 04.7	30	06	01.0	26	01.6	16	02.8	11	03.5	05	01.2	03	01.7	12	01.5	06	01.8	05	
XII	756.5	08.3	11.0	08.8	09.2	11.8	06.6	15.5	14 -01.6	08	07	01.4	10	01.3	11	02.5	42	03.6	06	02.0	02	01.0	04	01.2	08	01.6	03	
GOD.	759.0	12.9	17.6	13.4	14.3	18.6	10.9	32.5	28.VII -02.0	06.1	157	02.0	181	01.9	85	02.4	274	03.5	73	02.0	52	01.7	76	01.8	89	01.8	108	
$\varphi = 44^{\circ}59' N \lambda = 14^{\circ}54' E$ Gr. $\Delta G = + 1h 00$ min.																												
SENJ																												
BR. ST. 76																												
I	758.2	05.8	07.9	06.4	06.6	09.7	03.8	15.9	12 -03.6	06	05	02.6	26	05.6	39	04.6	09	03.1	08	02.9	02	03.5	01	01.0	03	01.7	.	
II	754.6	04.8	07.2	05.7	05.8	08.6	03.4	14.8	26 -02.7	21	05	02.4	22	06.3	31	05.1	08	01.6	04	02.8	06	02.3	.	08	02.8	.		
III	758.0	07.8	12.3	09.5	09.8	13.5	06.5	18.0	30 02.7	20	05	03.0	18	04.7	26	03.8	16	02.2	11	02.8	06	01.7	02	01.0	03	02.0	06	
IV	754.2	10.3	13.9	11.3	11.7	15.1	08.7	20.9	23 03.3	08	03	02.3	24	05.2	27	04.9	13	02.1	10	02.1	03	01.7	01	02.0	04	01.7	03	
V	757.4	14.1	17.3	14.7	15.2	19.2	12.0	24.6	31 04.4	12	04	03.0	13	04.8	26	03.4	17	02.0	06	02.0	05	01.6	03	01.0	14	01.6	05	
VI	757.9	18.9	23.0	19.7	20.3	24.5	16.4	28.5	02 11.8	13	02	03.0	13	04.8	27	03.6	16	02.0	11	02.2	05	01.5	09	01.3	05			
VII	759.1	21.0	26.4	22.0	22.9	27.3	18.5	31.9	29 14.0	22.2	21	02.7	19	04.8	32	03.8	13	02.5	07	01.7	05	01.6	05	01.8	08	01.8	01	
VIII	759.6	20.1	25.6	21.4	22.1	27.0	18.1	33.7	07 11.8	31	03	02.0	19	05.2	42	03.7	14	02.4	05	01.6	02	02.0	06	01.8	01	01.0	01	
IX	759.6	16.6	22.0	17.8	18.5	23.0	14.8	27.4	16 06.2	28	08	02.2	12	05.3	33	03.5	18	02.3	07	02.0	05	01.0	.	.	06	02.0	03	
X	762.1	13.7	18.2	14.6	15.3	19.2	12.4	25.6	03 05.8	28	04	02.8	33	05.9	43	05.0	07	02.9	01	04.0	02	01.0	.	03	01.3	.		
XI	766.0	08.2	12.9	09.2	09.9	13.7	07.0	20.0	30 01.3	29	03	04.0	26	06.5	45	05.2	10	03.0	03	01.1	.	.	.	03	.	03	01.7	03
XII	756.2	06.9	08.7	06.9	07.4	10.1	04.3	16.4	16 -05.6	08	.	08	12	08.3	30	04.7	22	02.4	09	03.4	05	03.2	04	02.5	08	01.5	03	
GOD.	758.6	12.4	16.3	13.3	13.8	17.6	10.5	33.7	07.VII -05.6	08.XII	45	02.7	237	05.6	401	04.3	163	02.3	82	02.4	46	01.9	24	01.7	67	01.7	30	
$\varphi = 44^{\circ}49' N \lambda = 14^{\circ}59' E$ Gr. $\Delta G = + 1h 00$ min.																												
ZAVIĆAN																												
BR. ST. 78																												
I	624.4	-04.3	-03.5	-04.7	-04.3	-01.6	-07.0	03.5	09 -17.0	06	36	04.4	19	04.4	05	05.6	04	04.0	27	03.7	01	03.0	01
II	621.1	-05.5	-04.0	-04.9	-04.8	-01.5	-07.5	06.8	25 -15.1	21	36	05.0	04	05.2	09	05.3	08	04.6	23	04.2	01	02.0	03
III	625.3	-02.2	00.2	-01.6	-01.3	01.8	-04.1	09.0	03 -09.8	20	33	04.1	06	03.3	05	04.1	03	04.0	34	03.8	05	02.2	04
IV	623.0	-01.1	01.0	-00.4	-00.3	02.3	-02.2	10.0	30 -07.6	17.0	01	02.0	.	.	.	45	04.6	09	02.2	13	03.1	03	02.4	07	02.0	03	02.0	03
V	627.2	03.0	05.1	03.6	03.8	07.2	01.5	11.8	05 -09.8	12	32	03.8	05	03.6	14	03.9	15	03.0	21	03.4	01	02.0	05
VI	630.0	07.9	11.0	08.5	09.0	12.5	06.2	16.6	10 01.0	27	01	03.0	.	.	.	26	02.7	06	02.3	02	06.0	04	04.2	36	02.7	10	02.3	05
VII	631.6	09.8	13.6	09.9	10.8	14.9	07.5	20.0	13 02.8	08	03	02.8	08	.	.	44	03.1	01	03.0	05	04.0	08	03.5	21	03.0	04	02.5	10
VIII	632.0	09.1	13.2	09.7	10.4	15.0	07.4	21.0	07 -06.4	31	08	03.0	14	03.7	05	01.6	16	02.8	02	01.5	05	01.4	14	01.9	11	01.0	11	
IX	630.7	10.2	17.7	08.1	11.9	05.2	17.7	11 -02.6	21	.	.	01	01.0	32	03.6	02	02.0	03	04.3	10	02.9	27	02.6	10	01.9	05		
X	631.4	03.4	06.8	03.8	04.5	08.7																						

Mjesec	Vrstdana pritisk Pm mm	Temperatura vazduha °C								Cestina pravaca i srednja jačina vетра mD, Pm (0-12)																						
		Tm			Hm		Rm		Nm		Dm		Ms		Ds		N		NE		E		SE		S		SW		W		NW	
		7	14	21	Sred. (Dise)	Hm	Rm	Nm	Dm	Ms	Ds	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.			
$\varphi = 44^{\circ}48' N \lambda = 15^{\circ}19' E$ Gr. $\Delta G = + 1h 01 min.$																																
I	-	-01.3	02.5	00.2	00.2	03.6	-03.7	11.1	13	-09.9	10	13	01.5	05	01.0	.	.	05	02.4	14	03.6	01	03.0	.	.	38	01.2	17				
II	-	-30.6	02.7	00.4	00.7	02.6	-02.4	14.2	25	-12.2	10	08	01.4	03	01.7	.	.	06	01.7	17	02.3	02	01.0	03	01.0	33	01.1	12				
III	-	-20.9	10.0	04.8	05.6	11.5	00.5	19.1	31.29	-04.8	23.13	10	01.8	03	01.7	01	01.0	07	01.6	19	01.8	12	01.7	02	01.0	25	01.3	14				
IV	-	05.6	10.9	06.7	07.4	12.3	02.8	19.8	30	-03.4	19	20	01.5	08	01.2	01	01.0	06	01.5	11	02.3	03	03.0	01	01.0	23	01.4	17				
V	-	09.7	15.8	09.7	11.2	17.4	06.0	23.4	21.20	-02.3	12	10	01.7	06	02.0	.	.	06	01.7	15	01.7	05	01.2	09	01.1	22	01.1	20				
VI	-	13.2	20.7	12.5	14.7	22.2	08.7	26.6	10	04.5	30	12	01.8	03	01.3	01	01.0	07	01.6	11	02.5	03	02.3	05	01.0	27	01.3	21				
VII	-	14.3	23.6	13.6	16.3	24.7	08.8	29.6	13	03.8	23	17	01.5	07	01.7	05	01.2	07	01.6	12	01.9	09	01.2	05	01.0	12	01.3	19				
VIII	-	12.6	23.0	13.1	15.4	23.9	08.7	31.4	07	03.6	21	17	01.7	05	01.6	03	01.0	02	02.0	08	01.8	09	01.3	16	01.2	30						
IX	-	09.3	14.2	10.4	12.3	20.6	05.6	27.6	11	-00.6	21	14	01.4	07	01.1	05	01.2	04	01.2	10	02.3	03	01.3	05	01.0	16	01.1	26				
X	-	06.9	13.8	06.9	08.6	14.5	04.3	21.2	03	-02.5	25	06	01.3	11	01.7	05	01.8	.	.	06	01.5	03	01.7	03	01.0	32	01.2	27				
XI	-	-01.9	05.4	-01.3	00.2	04.1	-04.3	12.3	02	-16.1	30	11	01.8	08	01.2	01	01.0	07	01.0	03	01.0	12	01.3	05	01.0	25	01.3	18				
XII	-	-00.1	02.9	00.7	01.1	04.0	-02.7	12.8	31.29	-16.9	06	09	02.2	03	01.0	01	01.0	19	01.6	07	03.3	10	01.9	.	.	26	01.2	18				
GOD.	-	05.9	12.5	06.4	07.8	13.7	02.7	31.4	07VII	-16.9	06.XII	147	01.6	69	01.4	23	01.3	77	01.5	127	02.3	71	01.6	47	01.1	295	01.2	239				
$\varphi = 44^{\circ}33' N \lambda = 15^{\circ}22' E$ Gr. $\Delta G = + 1h 02 min.$																																
$\varphi = 44^{\circ}33' N \lambda = 15^{\circ}22' E$ Gr. $\Delta G = + 1h 02 min.$																																
I	711.0	-02.2	01.9	-00.8	-00.5	03.2	-04.2	11.4	12	-13.4	09	20	01.8	07	03.0	01	01.0	16	03.0	04	04.2	05	02.4	.	.	08	01.9	32				
II	707.1	-01.0	03.0	00.8	00.9	04.7	-02.9	12.5	25	-14.6	10	27	02.7	.	.	02	02.0	16	02.5	04	02.8	06	02.2	06	01.3	04	02.0	19				
III	706.6	01.9	09.4	04.2	04.7	10.4	-00.5	17.4	03	-08.0	20	18	02.6	06	03.3	.	.	13	02.2	05	02.2	11	03.1	07	02.6	08	02.0	25				
IV	707.6	04.3	09.9	06.5	06.8	11.1	02.6	19.3	30	-03.0	19	22	02.1	08	03.0	02	03.0	07	02.0	05	03.3	13	02.5	04	02.5	03	02.0	24				
V	710.8	08.7	14.5	10.3	11.0	16.2	05.9	21.6	20	-02.0	12	14	02.4	06	02.5	03	02.7	14	02.6	04	01.8	15	01.9	07	02.3	05	02.0	25				
VI	712.1	12.3	20.0	14.2	15.2	21.2	08.6	26.4	11	03.2	29	12	01.8	02	02.0	01	02.0	06	01.5	03	02.3	10	02.1	08	01.9	14	01.4	29				
VII	713.0	13.0	22.6	15.6	16.7	23.7	09.0	28.7	13	03.6	24	16	01.8	05	02.4	03	02.0	05	01.4	05	02.3	10	02.1	08	01.6	05	01.6	36				
VIII	714.0	11.7	22.1	14.7	15.8	23.2	08.6	29.6	07	04.5	20	17	01.8	04	02.2	01	01.0	02	03.0	01	05.7	11	02.5	10	01.7	05	02.0	42				
IX	713.5	07.3	18.8	11.0	12.0	19.8	05.2	26.8	11	-00.6	29	14	01.9	05	02.4	02	02.0	29	01.9	03	02.0	07	02.4	06	01.8	06	02.0	38				
X	716.0	05.2	13.2	06.9	08.1	14.0	03.6	21.7	03	-02.8	25	20	02.0	05	03.2	05	02.0	32	03.5	04	01.5	.	.	24	01.2	15	01.7	38				
XI	719.3	-03.3	04.3	-00.9	00.3	07.6	-05.0	14.5	16	-12.4	30	18	02.3	02	01.5	03	02.7	10	03.0	01	01.0	.	.	12	01.5	51						
XII	709.4	-00.8	02.1	00.2	00.4	03.5	-03.3	11.4	13	-16.8	01	11	02.1	.	.	01	02.0	15	01.9	07	02.4	12	02.0	10	02.5	04	02.0	33				
GOD.	712.1	04.7	12.0	06.9	07.6	13.2	02.3	29.6	07VII	-16.6	04.XII	209	02.1	50	02.7	23	02.0	108	02.3	50	02.5	101	02.3	71	02.0	91	01.8	392				
$\varphi = 44^{\circ}18' N \lambda = 15^{\circ}51' E$ Gr. $\Delta G = + 1h 05 min.$																																
$\varphi = 44^{\circ}18' N \lambda = 15^{\circ}51' E$ Gr. $\Delta G = + 1h 05 min.$																																
I	-	-00.9	02.5	00.5	00.6	04.0	-02.7	10.5	14	-11.8	09	18	02.2	01	04.0	09	01.1	11	02.6	07	03.6	03	01.3	22	01.2	05	01.0	17				
II	-	00.0	03.6	01.8	01.8	02.6	-01.6	11.8	25	-13.0	10	28	02.4	02	03.0	04	01.5	14	02.1	10	02.7	02	02.0	08	01.5	06	01.2	10				
III	-	01.8	09.1	05.0	05.2	10.4	00.4	18.6	03	-05.3	23	26	02.2	08	02.2	03	01.3	14	01.5	07	01.9	06	02.3	04	01.5	09	01.6	16				
IV	-	05.3	10.0	07.3	07.5	11.4	03.8	18.5	30	-03.4	19	20	02.3	05	01.6	06	01.0	09	02.8	10	03.1	12	02.1	14	01.4	04	01.0	10				
V	-	09.2	14.4	11.1	11.5	16.4	07.1	21.6	20	-06.5	12	17	01.8	05	02.4	05	01.0	14	01.9	13	02.6	07	01.3	13	01.3	05	01.0	14				
VI	-	12.2	20.2	14.9	15.5	21.8	09.8	25.5	03	04.7	29	09	01.2	03	02.3	02	01.0	05	02.0	08</td												

Mesec	Oblačnost Nm (0-10)				Insolacije broj satija	Vlažnost vazduha				Padavine R mm				Broj dana na sat																								
						Srednja vazdušna temperatura Srednji Dien Min				Tn H ≤ < =				Tx Tn Tx Tx Tn F(0-12) Nm(0-10) R mm				T H ≤ < =																				
	7	14	21	Srednji (Odeš.)		7	14	21	Srednji (Dien) Min	Σ	M	N	Dat.	30.00	0.0	25.0	30.0	20.0	6	8	2.0	8.0	0.1	1.00	0.0	•	*	Δ	▲	▲	T	III	■					
BR. ST. 81 LICKO LESCE																																						
I	7.9	8.1	7.3	7.8	-	04.2	86	82	89	85	58	150	040.5	29	.	06	26	.	.	04	01	04	19	19	16	05	12	10	02	.	02	.	01	07	17			
II	9.0	8.5	7.4	8.3	-	04.4	86	80	89	85	60	112	029.8	20	02	05	23	.	.	01	.	02	19	19	08	04	09	12	.	05	.	01	08	14				
III	5.9	5.8	5.1	5.6	-	05.1	84	59	80	74	34	144	027.9	01	.	.	14	.	.	01	.	06	04	18	15	06	14	09	02	.	01	03	03					
IV	7.4	8.5	6.6	7.6	-	06.0	83	65	81	76	43	104	021.2	14	.	.	04	.	.	01	.	01	14	17	11	05	16	05	02	01	01	02	04	02				
V	7.6	7.0	5.5	6.7	-	08.0	84	63	87	78	39	133	040.6	14	.	.	02	02	18	12	03	17	01	01	.	.	.	07	06					
VI	5.1	5.4	4.5	5.0	-	09.7	83	57	88	76	30	059	017.6	14	.	.	09	.	.	01	.	07	08	15	11	01	15	.	.	.	07	07						
VII	4.5	4.2	1.9	3.5	-	10.6	85	53	85	74	33	066	031.5	06	.	.	17	.	.	01	.	10	01	06	06	01	06	.	.	.	02	04	14					
VIII	7.8	6.5	3.2	5.2	-	09.9	88	51	87	75	32	069	031.2	31	.	.	12	02	.	01	01	04	10	07	02	10	07	16						
IX	8.7	4.2	3.0	5.3	-	09.0	91	59	91	81	45	103	045.3	13	.	.	01	02	.	.	01	.	03	07	11	08	03	11	.	.	.	01	04	17				
X	8.7	5.9	4.8	6.3	-	07.1	88	65	89	81	40	059	032.7	02	.	.	06	01	11	08	02	08	01	01	.	.	.	02	08					
XI	8.8	4.6	6.2	6.5	-	04.1	87	72	87	82	41	037	017.5	27	01	02	23	.	.	03	13	04	04	02	01	04	.	.	.	15	04							
XII	8.5	7.7	6.7	8.3	-	04.6	84	81	86	84	54	114	027.2	20	05	08	19	.	.	02	02	.	19	19	12	04	13	09	.	.	.	04	12	22				
GOD.	7.5	6.2	5.4	6.6	-	06.9	85	65	86	79	30	1150	045.3	45	XIX	08	21	120	46	02	.	12	04	43	133	164	214	38	132	51	08	01	07	01	03	40	117	62
BR. ST. 82 GOSPIĆ																																						
I	7.8	8.4	6.6	7.6	038.2	04.1	92	82	90	88	45	198	036.5	30	04	06	26	.	.	03	.	05	19	22	17	07	13	12	.	.	.	02	08	23				
II	9.0	7.9	6.9	8.0	053.2	04.6	92	82	90	84	50	097	037.6	20	04	06	20	14	11	09	03	08	06	01	02	.	.	02	03	10				
III	5.9	6.8	5.0	5.9	152.9	04.9	94	56	82	77	29	148	022.9	07	.	.	18	.	.	04	09	19	17	06	15	09	01	.	.	.	02	03	03					
IV	8.2	8.6	7.7	8.2	098.9	05.9	91	65	84	80	40	161	038.7	14	.	.	06	20	19	13	04	18	04	01	01	.	.	03	03	03				
V	7.6	8.1	6.2	7.2	162.5	07.8	89	63	84	79	35	136	041.4	14	.	.	02	01	19	14	06	19	01	01	.	.	.	05	03					
VI	5.3	6.7	4.9	5.6	229.9	09.6	85	55	82	75	31	128	033.9	14	.	.	06	.	.	03	07	16	14	03	16	01	.	.	.	04	05							
VII	3.6	4.2	2.4	3.4	322.6	10.3	92	48	82	74	34	060	035.6	06	.	.	11	.	.	01	12	04	10	03	02	10	.	.	.	01	04	04						
VIII	4.2	5.1	2.9	4.1	257.1	09.8	93	50	83	75	26	104	049.6	31	.	.	12	.	.	01	01	09	09	08	01	07	.	.	.	04	09							
IX	6.1	5.6	3.3	5.0	208.3	08.3	95	52	91	80	36	129	027.5	13	.	.	01	02	.	.	01	.	05	11	09	05	11	.	.	.	05	18						
X	7.4	5.7	4.4	5.8	130.2	06.7	93	61	91	82	33	068	043.8	02	.	.	07	.	.	06	11	08	04	01	08	.	.	.	02	05								
XI	6.6	5.4	4.8	5.6	105.1	04.0	94	63	91	83	26	044	023.6	28	01	04	28	.	.	06	12	04	03	02	01	04	.	.	.	01	11	03						
XII	6.0	8.1	8.2	8.1	038.8	04.5	90	84	88	88	58	181	042.8	20	07	08	18	.	.	01	01	17	17	16	06	13	07	01	.	.	04	13	24					
GOD.	7.1	6.4	6.1	6.5	-	06.8	88	63	78	76	25	2116	085.7	02.X	09	13	103	41	02	.	09	01	54	169	156	133	68	135	33	08	.	.	24	34	66			
BR. ST. 84 KNIN																																						
I	7.7	7.3	6.6	7.2	074.8	04.8	82	69	76	72	22	160	023.2	30	.	.	13	.	.	03	.	04	17	18	16	06	18	02	02	.	.	01	.	23				
II	6.4	6.7	5.6	6.2	085.2	04.9	77	61	73	70	38	098	041.0	20	01	03	20	.	.	03	.	04	10	11	10	06	11	01	.	.	01	03						
III	6.0	6.8	4.8	5.9	178.8	05.4	80	53	68	67	24	126	033.3	18	.	.	03	.	.	02	.	04	10	11	12	05	13	.	.	.	01	02						
IV	8.2	8.0	6.6	7.4	8.1	133.9	06.6	73	57	68	67	29	098	019.9	27	.	.	01	.	.	02	.	19	16	11	03	14	.	.	.	03	02	03					
V	7.7	7.8	6.9	7.5	157.5	08.8	80	58	77	71	34	194	051.7	07	.	.	02	.	.	02	.	01	14	16	13	05	14	.	.	.	01	07						
VI	5.0	6.3	4.2	5.2	235.1	11.3	84	49	73	69	26	113	028.3	22	.	.	20	01	.	.	.	08	08	16	12	04	14	.	.	.	07							
VII	2.3	4.8	3.0	3.4	362.0	11.3	74	40	65	59	26	042	020.1	08	.	.	24	13	.	.	11	05	03	02	05	.	.	.	02	04								
VIII	2.9	4.7	2.7	3.4	301.7	10.8	74	79	39	65	24	048	015.7	31	.	.	24	11	.	01	.	13	04	09	08	01	09	.	.	01	03							
IX	4.6	5.1	3.5	4.6	220.9	09.5	81	48	74	68	33	082	020.9	13																								

1978

Mjesec	Vrijeme godine UT	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta nD, fm (0-12)																									
		UT				N						NE						E			SE			S			SW			W			NW			C	
		7	14	21	Sred. (fm)	NW	NE	SW	SE	W	E	NW	NE	SW	SE	S	SW	W	NW	C	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	
$\varphi = 43^{\circ}03' N \lambda = 16^{\circ}05' E$ Gr. $\Delta G = + 1h 04 min.$																									KOMIZA		BR. ST. 86										
I	-	08.9	11.7	08.9	09.6	12.2	06.7	15.4	14	01.2	09	15	03.6	05	04.2	17	03.3	36	03.7	05	03.6	05	03.6	05	02.6	04	02.8	01									
II	-	08.3	11.9	09.0	09.6	12.2	06.1	16.8	18	06.2	16	27	02.9	07	02.9	02	03.5	23	03.7	05	05.2	08	03.5	03	01.7	06	04.0	03									
III	-	10.0	14.4	10.1	11.1	14.7	07.5	18.2	21	03.4	23.13	20	03.7	01	04.0	02	03.0	29	03.0	01	01.0	05	02.4	10	02.0	19	02.8	06									
IV	-	13.2	15.9	12.9	13.7	16.3	10.2	19.6	22	06.2	18	11	02.8	02	04.5	08	04.2	34	03.2	08	04.1	08	01.8	04	01.5	09	02.4	06									
V	-	15.9	19.3	15.9	16.7	19.7	13.0	24.4	31	09.0	13	0	01	03.3	04	03.2	41	02.8	08	02.9	04	01.2	16	01.8	05	02.6	14										
VI	-	20.9	24.8	19.6	21.2	25.4	16.4	28.4	09	13.0	27	18	02.4	02	01.5	02	03.0	14	02.4	04	01.5	03	01.0	09	01.3	18	02.2	18									
VII	-	23.1	27.1	21.2	23.2	27.5	17.0	32.6	12	13.2	10	31	02.2	02	03.0	02	03.0	14	02.4	03	01.3	01	01.0	04	01.5	23	02.5	13									
VIII	-	23.5	27.6	21.3	23.5	28.1	17.6	32.2	06	14.6	31	28	02.4	01	04.0	01	02.0	12	02.1	01	04.0	01	05.0	21	01.7	20	02.3	08									
IX	-	19.9	23.0	18.4	20.0	23.8	15.2	27.5	17	12.2	21	27	02.8	04	03.2	01	05.0	16	03.0	0	0	09	01.6	17	02.6	16											
X	-	16.2	20.2	15.8	17.0	20.6	12.7	24.4	13	07.2	28	31	02.8	06	03.5	07	04.3	13	04.4	04	02.2	03	03.0	11	01.4	18	01.9	.									
XI	-	10.6	14.6	10.5	12.1	11.9	07.5	19.7	02	04.4	30	29	02.3	11	02.3	01	02.0	04	02.2	06	04.8	01	02.0	26	02.0	08											
XII	-	10.1	13.7	10.4	11.2	14.1	07.8	17.6	17	-0.2	07	07	03.4	01	04.0	05	03.8	30	03.1	10	03.3	05	01.8	14	01.6	17	02.1	04									
GOD.	-	15.0	18.8	14.5	15.7	19.3	11.5	32.6	42.VII	-00.2	07.VII	244	02.7	43	03.1	52	03.6	268	03.1	55	03.4	44	02.4	110	01.7	182	02.4	97									
$\varphi = 43^{\circ}31' N \lambda = 16^{\circ}26' E$ Gr. $\Delta G = + 1h 06 min.$																									SPLIT-MARJAN		BR. ST. 87										
I	749.1	07.0	08.8	07.7	07.8	10.0	05.5	14.1	15.14	-01.5	06	05	03.0	35	03.2	19	03.0	20	04.2	07	05.6	01	01.0	04	02.2	02	03.0	.									
II	749.1	06.8	09.6	07.9	08.1	10.7	05.5	15.0	27	06.2	16	01	03.0	33	03.9	10	02.7	23	04.7	07	03.1	04	02.0	03	02.3	03	01.3	.									
III	748.9	08.8	12.7	10.3	10.5	13.7	07.5	17.2	29	04.0	20	13	02.8	25	03.2	13	01.9	19	03.4	05	03.4	10	01.7	05	02.2	03	02.0	.									
IV	745.2	11.6	15.0	12.6	12.9	15.9	10.2	20.2	23	06.3	17.16	02	01.0	21	02.8	12	02.2	31	03.7	08	03.1	13	02.2	02	02.0	01	01.0	.									
V	748.6	14.8	18.3	15.6	16.1	19.6	12.8	24.2	31	06.3	12	04	01.2	24	03.0	12	03.6	22	03.8	06	02.7	16	02.2	05	01.8	04	02.0	.									
VI	749.2	20.4	24.6	21.0	21.7	26.4	18.3	29.6	11	13.2	27	08	02.1	20	01.8	09	02.7	14	03.2	03	01.3	19	02.1	06	01.8	11	01.8	.									
VII	750.2	22.3	27.8	23.4	26.2	28.5	20.3	32.6	13	16.7	09	05	02.8	23	02.8	11	02.0	13	03.6	05	02.4	21	02.3	07	02.0	08	01.9	.									
VIII	750.6	21.6	27.1	23.0	23.7	28.2	19.8	32.8	07	11.8	31	05	01.4	29	02.7	09	01.8	10	02.3	02	02.5	24	02.3	07	02.4	07	02.1	.									
IX	750.4	17.2	21.5	18.7	19.0	22.6	15.5	26.1	16	10.4	28	11	03.3	26	02.8	10	02.0	09	04.0	08	01.5	16	01.9	07	01.7	02	02.0	01	.								
X	752.6	14.7	18.7	15.8	16.3	19.4	13.6	24.4	03	06.4	27	09	03.8	37	03.1	09	03.4	16	04.0	06	02.0	14	01.6	03	01.7	.											
XI	756.4	09.3	14.1	11.2	11.4	14.6	08.6	17.0	02	03.3	29	08	01.8	40	03.0	05	01.8	11	01.8	16	01.4	.	01	03.0	.												
XII	747.6	09.0	11.3	09.7	09.9	11.9	07.6	15.8	19	-0.6	07	07	01.9	29	02.9	15	03.2	22	03.4	04	03.2	03	01.3	07	02.1	06	01.5	.									
GOD.	749.5	13.6	17.5	14.7	15.1	18.5	12.1	32.8	07.VII	-01.5	06.1	77	02.5	342	03.0	134	02.6	208	03.7	72	02.7	157	02.0	56	02.0	48	01.9	01	.								
$\varphi = 43^{\circ}10' N \lambda = 16^{\circ}27' E$ Gr. $\Delta G = + 1h 06 min.$																									HVAR		BR. ST. 88										
I	758.1	08.4	10.8	08.5	09.1	11.8	06.1	16.0	16	00.2	06	11	02.2	13	03.3	40	03.3	16	05.4	01	01.0	02	02.5	.	07	03.1	03										
II	754.0	08.2	11.1	09.1	09.4	12.4	06.3	16.0	18	-0.3	16	11	01.8	18	02.4	12	03.8	15	04.6	05	04.2	01	03.0	02	02.5	12	02.7	01	.								
III	758.0	09.5	13.8	10.5	11.1	15.0	07.3	18.0	29	03.6	13	22	02.6	09	02.6	19	03.4	11	03.5	02	02.5	25	03.3	08	01.3	.											
IV	754.2	12.7	15.7	12.9	13.5	16.8	10.5	20.4	23	05.8	17	08	02.0	05	02.6	28	03.1	22	03.8	08	01.5	02	03.0	06	03.2	09	.										
V	757.5	15.9	18.5	15.8	16.5	20.1	13.0	24.5	30	08.0	13	06	02.2	07	02.7	21	03.5	28	03.4	04	02.2	01	02.0	05	02.8	13	02.5	08	.								
VI	758.0	21.0	24.3	20.5	21.6	25.6	17.9	29.0	11	13.0	28.27	09	02.0	07	02.7	14	02.7	16	04.5	01	01.0	11	02.8	22	02.5	16	.										
VII	759.0	22.7	26.4	22.3	23.4	27.6	19.3	31.7	30	15.4	09	11	01.5	06	02.3	10	03.5	12	03.0	12	01.7	.	16	02.6	15	02.4	17	.									
VIII	759.4	22.4	26.7	22.1																																	

Mesec	Oblađnost Nm (0-10)					Vlažnost vazduha %	Padavine R mm	Broj dana na sat																												
								Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	●	*	▲	▲	▲	▲	▲	▲	T	■	■									
	7	14	21	Gred. (Dose)	Insekticija broj sati	7	14	21	Strešni (Dose)	Min	Dat.	W	<	<	≥	≥	W	≥	≤	≥	≤	≥	≤	≥	≤	≥	≤									
BR. ST. 86																																				
KOMIZA																																				
I	6.5	6.0	6.0	6.1	-	07.3	80	76	79	79	43	351	058.1	18	10	01	08	12	14	14	11	14	.	.	05	.					
II	4.5	4.4	4.8	4.5	-	07.0	73	72	76	75	53	048	010.4	13	03	01	06	06	07	07	02	07	.	.	01	.					
III	3.5	3.7	4.5	3.7	-	07.2	72	66	71	70	46	117	045.4	07	02	12	04	09	09	02	09	.	.	01	.						
IV	5.3	5.4	4.5	5.1	-	08.5	72	66	73	71	49	058	019.6	08	03	02	08	07	11	09	01	11	.	.	02	.					
V	4.6	3.5	4.3	4.2	-	10.1	72	63	71	69	40	140	049.1	07	03	01	06	03	11	10	05	11	.	.	03	.					
VI	3.3	2.3	3.1	2.9	-	12.7	66	62	67	65	50	072	032.2	16	.	.	20	.	.	03	17	03	04	04	02	04	.	.	03	.						
VII	0.9	0.2	0.6	0.6	-	12.4	55	53	59	56	41	014	011.2	22	.	.	24	05	03	.	28	02	02	01	02	02	.	.	03	.						
VIII	1.8	1.3	1.5	1.5	-	12.9	59	54	58	57	41	020	020.4	31	.	.	30	08	03	.	23	01	01	01	01	01	.	.	01	.						
IX	2.8	2.4	1.9	2.4	-	12.0	69	63	66	66	47	051	024.4	07	.	.	07	.	.	02	19	02	04	06	02	06	.	.	01	.						
X	3.3	3.2	2.8	3.1	-	10.4	69	65	70	68	41	054	022.3	06	04	01	20	07	04	04	03	04	.	.	02	.					
XI	2.4	2.4	1.7	2.2	-	08.4	78	73	75	75	58	026	015.2	30	02	21	02	03	02	02	03	.	.	02	.						
XII	6.4	5.3	5.6	5.8	-	08.6	83	82	85	83	61	109	032.2	23	.	.	01	.	.	02	04	09	12	12	03	12	.	.	03	.						
GOD.	3.8	3.3	3.4	3.5	-	09.8	70	66	70	69	40	1060	058.1	48.1	.	.	01	81	13	09	31	06	174	56	84	80	35	84	.	.	27	.				
SPLIT-MARJAN																											$H_a = 122 \text{ m } H_b = 128.0 \text{ m } h_c = 6.5 \text{ m } = 1.0 \text{ m}$									
I	7.2	7.8	6.2	7.1	-	073.4	055.5	66	66	66	19	185	029.3	18	.	.	02	.	.	11	09	06	17	21	16	08	21	01	.	01	01	06				
II	7.7	7.7	6.6	6.8	-	084.3	055.3	64	52	62	76	083	038.5	27	15	02	04	13	10	10	14	10	01	01	01	02					
III	5.4	6.7	4.1	5.4	-	181.3	055.9	63	57	61	60	24	104	027.4	06	13	03	05	06	14	10	04	14	.	.	04	02					
IV	7.4	8.0	6.3	7.2	-	151.5	073.3	69	58	67	65	33	074	019.4	08	10	02	.	13	17	11	03	16	.	.	04	.					
V	7.5	6.8	5.9	6.7	-	189.5	092.5	69	62	69	67	28	182	054.5	07	08	03	02	11	17	14	08	17	.	.	09	.					
VI	3.8	5.3	4.0	4.4	-	273.3	114.8	66	52	62	60	29	106	079.2	16	.	.	24	07	02	06	10	07	02	10	.	.	02	.							
VII	1.9	2.7	1.8	2.2	-	358.6	113.3	92	42	54	50	25	003	001.6	15	.	.	28	11	18	03	01	19	04	02	04	.	.	01	.						
VIII	2.0	3.6	1.9	2.5	-	313.2	114.4	54	44	56	52	28	027	011.2	29	.	.	28	08	11	03	01	16	01	05	03	01	05	.	.	04	.				
IX	4.7	4.3	3.7	3.9	-	236.6	10.0	63	55	61	60	29	088	022.6	07	.	.	05	.	07	04	13	04	10	09	04	10	.	.	01	01	03	01			
X	3.7	3.8	2.6	3.4	-	210.1	07.9	57	49	59	55	23	028	015.2	04	08	04	16	06	07	04	01	07	.	.	01	.					
XI	2.6	3.0	2.0	2.5	-	196.8	05.6	53	52	59	55	32	047	017.7	28	04	01	15	03	04	04	03	01	.	.	03	.					
XII	6.8	7.1	5.2	6.3	-	100.3	06.5	69	65	70	68	24	107	022.0	20	.	.	01	.	13	02	03	12	17	13	05	17	01	.	.	06	.				
GOD.	5.1	5.5	4.0	4.9	-	2368.9	08.1	62	54	62	60	19	1034	079.2	16.1	.	.	03	85	19	36	97	32	105	90	140	103	42	139	04	01	01	02	02	46	03
HVAR																											$H_a = 20 \text{ m } H_b = 25.4 \text{ m } h_c = 2.0 \text{ m } = 1.2 \text{ m}$									
I	7.2	7.3	5.7	6.8	-	085.7	06.3	72	66	72	70	23	191	034.1	21	.	.	01	.	08	01	07	15	19	17	08	19	.	.	02	02	18				
II	7.9	6.9	5.7	6.8	-	094.3	06.2	70	63	67	67	35	103	051.3	13	.	.	01	.	03	01	14	12	08	03	12	02	02	.	.	02	.				
III	5.6	6.3	4.4	5.4	-	198.3	06.4	66	58	65	63	23	093	034.3	07	03	01	07	09	14	10	03	14	.	.	04	.					
IV	7.5	7.3	5.6	6.8	-	168.7	08.2	74	63	73	70	32	056	016.3	08	05	01	01	01	12	13	10	02	13	.	.	01	04				
V	7.2	5.7	5.4	6.1	-	228.7	10.0	71	67	74	71	30	162	039.8	08	04	01	04	09	14	09	07	14	.	.	06	.					
VI	3.7	4.0	3.5	3.7	-	310.9	13.1	71	59	70	67	38	073	039.8	28	.	.	20	.	05	01	13	04	09	06	02	09	.	.	02	.					
VII	1.7	1.4	1.8	1.6	-	380.0	13.2	61	54	65	60	28	006	004.6	16	.	.	27	04	11	01	20	03	01	03	01	03	01	.	.	01	.				
VIII	2.5	2.7	1.5	2.2	-	323.1	13.8	66	55	68	63	36	029	026.8	15	.	.	29	05	14	01	17	02	02	01	02	02	.	.	01	03	02				
IX	4.8	4.0	2.2	3.7	-	237.3	11.5	73	58	70	66	27	080	021.4	07	.	.	09	.	01	02	01	10	04	08	08	04	08	.	.	01	04				
X	3.9	3.7	3.0	3.5	-	215.5	09.4	67	55	69	64	25	032	015.8	04	.	.	01	.	04	01	17	05	08	06	02	08	.	.	01	.					

Meseč Broj	Vremenski redoslijed (1-12)	Temperatura vazduha °C										Čestina pravaca i srednja jačina vjetra m/s, fm (0-12)																		
		Im		Srednji Godišnji					Mjesečni					N			NE		E		SE		S		SW		W		NW	
		7	14	21	Srednji Godišnji	Mj	H	M	N	D	S	A	8.	1.	8.	1.	8.	1.	8.	1.	8.	1.	8.	1.	8.	1.	8.	1.		
$\varphi = 43^{\circ}01' N \lambda = 17^{\circ}34' E$ Gr. $\Delta G = + 1h 10 min.$														OPUZEN		BR. ST. 91														
I	-	05.3	09.2	06.7	06.9	10.4	03.0	17.3	14	-03.8	09	07	03.4	09	07.3	24	02.2	43	02.1	09	02.6	01	01.0		
II	-	06.7	10.9	08.6	08.7	11.8	04.6	17.7	26	-01.9	16	06	02.5	09	02.9	26	02.1	32	02.3	08	02.8	02	03.0		
III	-	08.9	14.6	11.3	11.5	15.5	06.3	21.7	04	02.5	13	09	03.3	10	02.9	19	02.1	23	02.4	06	02.8	15	02.1	09	02.1	02	02.5	.		
IV	-	11.8	15.8	13.2	13.5	17.2	08.6	23.4	30	04.3	19	02	02.5	06	03.2	18	01.9	37	02.7	11	02.9	03	02.7	12	02.2	01	02.0	.		
V	-	15.3	20.3	16.8	17.3	21.3	11.8	25.6	31	06.7	13	01	02.0	10	02.3	13	02.2	40	02.3	08	03.2	14	02.1	07	02.3	.	.	.		
VI	-	20.1	25.4	21.7	22.2	26.2	15.9	30.2	11	11.6	30	06	02.5	09	02.9	27	02.6	40	02.0	08	03.0	11	01.9	30	02.1	.	.	.		
VII	-	21.6	28.2	23.2	24.0	29.0	17.0	33.5	14.12	13.3	10	07	02.7	02	02.5	10	02.9	22	02.7	02	04.0	04	02.0	42	02.3	04	03.0	.		
VIII	-	20.5	28.6	23.7	24.1	29.2	16.2	33.6	02	13.2	14	04	02.8	01	03.0	20	02.4	28	04.0	02	04.0	11	02.2	26	02.0	01	02.0	.		
GOD.	-	12.7	18.6	15.0	15.3	19.6	09.6	33.6	02.0	-03.8	09.1	59	03.2	75	02.8	237	02.3	415	02.3	72	02.7	94	02.2	131	02.2	12	02.7	.		
$\varphi = 42^{\circ}24' N \lambda = 16^{\circ}16' E$ Gr. $\Delta G = + 1h 05 min.$														PALAGRUŽ		BR. ST. 92														
I	750.9	09.1	11.1	09.2	09.7	11.6	07.3	14.3	14	02.1	06	12	04.9	09	03.3	03	05.7	09	06.0	27	04.9	15	02.2	04	02.0	11	02.5	03		
II	746.6	09.1	10.6	09.6	09.7	11.7	07.4	14.0	27	03.0	09	10	03.7	09	03.1	03	02.0	07	06.9	23	04.9	07	02.9	01	05.0	24	04.2	.		
III	751.0	10.1	12.7	10.9	11.2	12.8	08.3	17.6	21	04.0	22	19	04.7	08	04.1	03	02.0	07	04.9	20	03.8	13	02.6	05	01.8	15	04.4	03		
IV	747.3	11.9	14.3	12.0	12.6	15.3	10.4	17.8	29	08.6	16	06	03.0	03	03.0	05	04.2	16	03.9	29	03.9	11	02.3	05	02.4	15	03.2	.		
V	750.7	15.0	18.4	15.3	16.0	19.1	13.0	23.1	27	09.1	13	06	03.5	05	01.6	08	02.5	16	03.9	15	03.7	14	02.2	07	01.4	22	02.8	.		
VI	751.5	20.4	24.0	19.9	21.0	24.8	18.0	-	-	08.2	09	04.8	07	01.4	13	03.6	11	02.7	09	02.2	07	03.1	25	03.4	06	02.0	.			
VII	752.5	22.2	26.1	21.6	22.9	26.7	19.5	29.8	29.19	19.2	08.7	14	02.6	04	01.2	14	02.4	11	02.7	04	02.0	05	02.6	36	02.8	02	02.0	.		
VIII	753.1	22.6	26.4	22.2	23.4	27.3	20.5	30.5	03	14.0	31	13	02.4	06	01.2	02	01.0	06	03.3	15	01.9	04	03.5	08	02.8	36	02.5	06		
GOD.	751.6	14.9	17.5	15.0	15.6	18.3	13.0	-	-	-	138	03.4	67	02.6	48	02.6	122	04.1	222	03.7	100	02.4	65	02.6	306	03.1	27	.		
$\varphi = 42^{\circ}58' N \lambda = 16^{\circ}43' E$ Gr. $\Delta G = + 1h 07 min.$														VELA LUKA		BR. ST. 93														
I	-	06.5	10.1	07.4	07.9	11.2	04.9	15.0	15.14	-03.2	09	13	02.8	07	01.9	16	01.7	49	02.8	02	02.0	01	01.0	03	03.3	02	02.5	.		
II	-	06.9	11.0	08.1	08.5	12.2	04.8	16.3	27.26	-02.5	16	08	02.4	07	02.1	22	01.5	29	03.2	03	04.0	15	02.2	.		
III	-	08.9	13.4	09.9	10.5	14.4	06.7	18.5	29	01.9	13	20	02.8	01	02.0	19	01.2	27	02.7	02	02.6	05	02.7	13	02.9	.				
IV	-	12.1	15.3	12.0	12.9	16.4	09.5	20.6	29	05.0	21	05	02.8	03	01.3	45	02.6	05	03.4	01	01.0	05	02.6	11	02.7	.				
V	-	15.6	19.1	15.3	16.3	20.3	12.2	24.0	30	06.0	13	03	02.0	02	02.0	18	01.2	45	02.6	05	01.8	01	02.0	04	03.0	15	02.9	.		
VI	-	20.6	24.2	19.9	21.2	25.4	16.5	29.5	11	12.6	30	06	02.0	01	02.0	20	01.0	28	02.3	02	02.0	01	01.0	12	02.8	18	03.2	02		
VII	-	21.9	26.6	21.7	23.0	27.9	17.2	33.0	29	13.3	23	06	02.0	00	01.5	26	01.1	20	02.4	02	01.5	03	30	26	14	01.5	03			
VIII	-	21.0	25.9	21.3	22.4	27.7	17.1	32.5	02	13.4	31	04	01.8	00	01.5	26	01.0	16	02.0	03	01.7	00	01.7	28	02.8	14	02.1	02		
IX	-	17.0	22.2	17.6	18.6	23.5	14.3	27.0	16	07.0	22	13	03.5	00	02.0	22	01.1	26	02.3	01	01.0	01	01.0	11	02.7	15	02.3	01		
X	-	12.2	19.1	13.6	14.6	20.3	10.6	25.5	12	01.2	29	08	02.5	00	03.2	33	01.2	30	02.2	04	01.5	00	01.5	14	02.6	01	03.0	03		
XI	-	05.6	15.4	08.3	09.4	16.3	04.6	19.6	15	02.1	17	09	01.6	02	03.0	38	01.1	22	02.0	02	01.0	.	.	11	02.4	06	01.8	.		
XII	-	09.2	12.9	09.7	10.4	13.7	06.3	17.7	17	00.0	01	05	02.0	06	01.8	22	01.1	40	02.8	02	01.5	00	03	02.7	15	02.9	03			
GOD.	-	13.1	17.9	13.7	14.6	19.1	10.4	33.0	29.0	-03.2	09.1	100	02.5	29	02.1	269	01.2	377	02.6	33	02.1	10	01.9	127	02.7	139	02.5	11		
$\varphi = 42^{\circ}46' N \lambda = 16^{\circ}34' E$ Gr. $\Delta G = + 1h 08 min.$														LASTOVO		BR. ST. 94														
I	743.5	07.8	09.0	08.2	08.3	10.2	06.4	13.4	14	00.4	06	14	04.1	10	04.7	11	04.5	34	05.2	10	05.1	03	03.3	03	03.7	05	02.6	03		
II	739.9	07.9	09.1	08.4	08.5	10.4	06.6	14.8	27	01.9	16	06	03.0	13	04.5	06	03.8	24	05.2	10	06.2	01	02.0	06						

Mesec	Oblačnost Nm (0-10)				Vlažnost vazduha %	Padavine R mm	Broj dana na sat														• * * * * R T =									
							L m s			Tn Tx Tn Tx Tn Tx			F(0-12)	Nm (0-10)	R mm	• * * * * R T =						•	*	*	Δ	○	▲	■		
	7	14	21	Sred. (Dnes)			%	7	14	21	Sred. (Dnes)	Min	Σ	Max	Dat.	%	<	<	N	N	N	N	N	•	*	*	Δ	○	▲	■
BR. ST. 91																														
CPUZEN																														
I 6.5 7.1 7.4 7.0 -	35.9	81	71	76	76	34	323	054.8	16	.	.	08	.	.	.	03	01	04	18	20	17	10	20	.	.	.	01	03	01	
II 7.7 7.5 6.8 7.3 -	36.4	79	69	72	73	44	106	035.8	13	.	.	03	.	.	.	02	12	13	10	03	13	01	.	.	.	01	01	.		
III 4.9 5.4 5.8 5.4 -	37.0	74	60	69	68	31	100	021.8	22	07	08	12	09	05	12	.	.	.	01	02	.			
IV 7.4 8.3 8.2 8.0 -	38.8	82	66	77	75	40	188	068.4	26	01	01	18	15	13	04	15	.	.	.	01	02	.		
V 6.9 6.6 6.9 6.8 -	10.9	79	65	73	73	47	131	038.4	02	.	.	02	.	.	.	01	01	11	12	11	04	12	.	.	.	01	01	.		
VI 3.8 3.5 3.1 4.5 -	12.9	78	50	66	65	32	139	051.4	16	.	.	22	02	.	.	01	09	07	07	03	07	.	.	.	04	04	.			
VII 1.4 2.0 2.4 1.9 -	11.9	66	39	56	54	21	002	001.9	07	.	.	31	11	02	01	21	16	02	01	02	02	.	.	.	02	02	.			
VIII 2.8 2.6 2.9 2.8 -	11.8	71	38	53	54	24	026	005.3	31	.	.	30	10	01	01	17	02	03	01	03	03	.	.	.	03	03	.			
IX 4.5 5.0 4.6 4.7 -	11.2	77	58	69	68	32	222	062.2	07	.	.	15	.	.	.	01	01	09	09	11	10	06	11	.	.	.	05	01	.	
X 4.0 4.1 3.9 4.0 -	09.1	75	52	62	63	26	059	018.8	21	.	.	05	.	.	.	16	09	11	09	01	11	.	.	.	03	01	.			
XI 3.2 3.1 3.4 3.2 -	05.6	77	45	57	60	25	082	029.6	29	.	.	01	.	.	.	18	07	03	03	03	03	.	.	.	01	04	.			
XII 7.2 6.7 6.9 7.0 -	06.6	83	58	73	72	32	083	022.5	23	.	.	04	.	.	.	03	13	16	12	02	16	.	.	.	04	03	.			
GOD. 5.0 5.2 5.4 5.2 -	09.0	76	55	67	66	21	1441	068.4	26.IV	.	.	16	105	23	03	09	02	108	114	129	103	41	125	01	.	.	.	03	30	08
BR. ST. 92																														
PALAGRUZ																														
I 6.0 6.3 5.8 6.0 -	108.3	06.8	75	68	76	73	38	117	047.9	22	16	05	03	04	13	11	03	13	.	.	.	02	02	.	
II 7.1 7.3 4.8 6.4 -	083.1	-	-	-	-	-	-	037	014.6	03	17	04	02	09	07	06	01	07	.	.	.	01	02	.	
III 5.1 5.8 4.2 5.0 -	185.7	-	-	-	-	-	-	089	024.8	07	11	04	03	10	10	05	10	.	.	.	01	02	.		
IV 7.3 6.8 5.7 6.6 -	169.1	08.6	80	70	82	77	36	037	012.2	04	11	04	02	08	12	08	01	12	.	.	.	02	02	.	
V 6.2 5.4 4.8 5.4 -	258.6	-	-	-	-	-	-	037	013.3	07	08	01	01	04	10	06	01	10	.	.	.	01	01	.	
VI 3.4 3.3 3.7 3.5 -	296.0	-	-	-	-	-	-	025	011.0	16	06	12	02	10	04	01	01	07	.	.	.	03	02	.	
VII 1.4 0.9 1.5 1.3 -	378.5	14.6	72	56	78	69	34	067	004.3	08	.	.	26	.	15	01	24	02	01	02	.	.	.	07	07	.				
VIII 2.9 2.4 2.7 2.7 -	339.1	15.1	72	58	76	69	40	000	000.0	05	.	.	29	01	23	03	14	03	01	.			
IX 4.2 2.9 2.1 3.1 -	246.3	-	-	-	-	-	-	017	007.2	26	.	.	04	.	01	07	01	09	01	06	03	06	.	.	.	03	01	.		
X 6.7 4.1 3.1 4.0 -	197.0	-	-	-	-	-	-	009	005.6	04	.	.	04	.	01	09	04	04	03	06	.	.	.	01	01	.				
XI 5.2 4.4 3.6 4.0 -	124.9	-	-	-	-	-	-	022	014.5	30	.	.	02	.	05	01	03	03	03	01	03	.	.	.	01	02	.			
XII 6.4 6.0 5.0 5.0 -	080.7	08.1	78	74	78	77	41	058	024.4	05	.	.	15	01	01	03	10	09	02	10	.	.	.	03	03	.				
GOD. 5.0 4.6 3.9 4.5 -	455.0	047.9	22.I	-	-	-	-	-	-	-	-	101	17	88	41	89	64	15	89	.	.	.	05	28	05	
VELA LUKA																														
BR. ST. 93																														
VELA LUKA																														
I 7.4 7.6 6.8 7.3 -	06.3	81	69	77	76	26	297	062.6	21	.	.	03	.	.	.	03	01	06	18	20	17	11	20	.	.	.	05	.		
II 8.6 7.3 6.6 7.5 -	36.4	80	63	77	73	31	076	016.7	27	.	.	03	.	.	.	01	03	17	13	10	03	13	.	.	.	02	.			
III 6.1 6.7 5.2 6.0 -	06.6	75	58	73	69	33	116	035.6	07	02	01	17	14	13	01	14	.	.	.	01	02	.		
IV 8.0 7.6 7.4 7.7 -	08.3	77	64	80	74	32	076	019.5	09	02	01	17	14	13	01	14	.	.	.	01	02	.		
V 7.1 6.1 6.3 6.5 -	10.1	77	62	78	72	32	132	027.2	23	02	03	12	15	13	06	15	.	.	.	04	04	.		
VI 4.1 4.4 3.8 4.1 -	13.1	75	58	73	69	31	090	052.6	16	.	.	20	02	.	.	01	11	05	07	04	02	07	.	.	.	02	02	.		
VII 1.7 1.3 2.0 2.1 -	13.1	66	50	67	61	29	091	006.7	16	.	.	27	08	03	.	.	20	01	01	01	01	01	.	.	.	01	01	.		
VIII 2.8 3.4 2.8 3.0 -	13.9	75	57	72	68	36	004	033.6	15	.	.	30	05	03	.	.	17	05	03	01	03	04	.	.	.	04	04	.		
IX 5.1 4.4 3.7 4.4 -	11.4	77	58	74	69	29	087	030.4	07	.	.	09	.	.	.	01	11	07	07	03	07	07	.	.	.	04	01	.		
X 5.3 3.7 3.9 4.3 -	09.4	83	59	78	73	31	057	026.0	04	.	.	02	.	.	.	01	15	10	08	05	02	08	.	.	.	02	04	.		
XI 3.3 3.2 2.9 3.1 -	06.6	88	54	81	75	31	038	018.0	29	03	17													

Mjesec	Vremenski prirodni red	Temperatura vazduha °C										Čestina pravaca i srednja jačina vетра m/s, Fm (0-12)																									
		Sv.			H&M			M&S			D&T			M&S			D&T			N		NE		E		SE		S		SW		W		NW		C	
		7	14	21	Sred. (Dnev.)	H&M	M&S	M&S	D&T	M&S	D&T	M&S	D&T	M&S	D&T	M&S	D&T	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.							
$\varphi = 42^{\circ}58' N \lambda = 17^{\circ}10' E$ Gr. $\Delta G = + 1h\ 09\ min.$																									DREBIC		BR. ST. 96										
I	-	07.7	10.7	07.7	08.5	11.4	05.1	15.2	14 -02.5	09	17	01.6	22	03.5	13	02.1	22	03.5	03	01.7	01	03.0	07	02.0	07	01.3	01										
II	-	08.0	11.1	08.5	09.0	11.8	05.8	15.6	24 -03.3	16	12	01.8	27	02.7	13	02.6	17	02.9	02	03.0	02	04.0	04	02.2	03	01.7	04										
III	-	10.3	13.9	10.1	11.1	14.7	07.1	16.7	30.03	03.4	26	12	01.8	28	02.8	03	02.3	24	02.5	-	07	02.9	09	02.6	06	02.2	04										
IV	-	12.5	15.8	12.5	13.3	16.9	10.1	20.5	30.23	05.5	21	07	01.9	15	02.9	07	02.4	29	02.8	04	02.2	03	03.7	12	02.3	04	01.8	09									
V	-	14.1	19.4	14.8	16.3	20.3	12.7	25.2	30	06.2	13	11	01.5	19	02.4	08	03.2	36	02.6	03	01.3	03	03.0	09	03.1	01	03.0	03									
VI	-	21.3	24.8	19.5	21.3	25.8	16.9	24.6	03	13.4	01	16	01.7	08	02.4	02	02.0	28	02.4	04	02.0	09	03.0	14	02.6	07	01.6	02									
VII	-	23.0	27.4	21.2	23.2	28.3	18.7	33.2	29	14.8	10.09	09	01.4	28	02.6	03	02.7	19	02.5	-	11	03.2	12	03.2	08	01.4	03	-	-								
VIII	-	22.0	27.0	20.6	22.5	28.3	17.9	31.5	07.05	12.5	31	20	01.8	15	02.5	02	02.0	20	02.2	03	02.3	07	03.6	10	03.3	08	01.9	08									
IX	-	17.8	22.9	17.6	19.0	23.9	14.7	27.5	16	08.7	22	16	01.4	20	02.8	02	03.0	17	02.5	02	02.0	08	02.9	11	02.9	09	01.7	05									
X	-	15.1	20.2	14.7	16.2	21.3	12.3	27.6	14	06.5	23	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-									
XI	-	08.5	15.6	08.8	10.4	16.9	06.0	19.6	03	03.3	20	19	01.2	24	02.7	01	02.0	09	02.9	02	02.5	10	02.5	08	02.6	14	01.2	03									
XII	-	10.0	13.0	10.2	10.9	13.8	07.2	18.0	14	01.0	07.01	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-									
GOD.	-	14.4	18.5	13.8	15.1	19.4	11.2	33.2	29	07.5	09.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-									
$\varphi = 42^{\circ}50' N \lambda = 17^{\circ}42' E$ Gr. $\Delta G = + 1h\ 11\ min.$																									STON		BR. ST. 97										
I	-	05.7	10.4	06.5	07.3	11.5	03.1	16.8	15 -04.2	09	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-										
II	-	06.9	10.7	07.4	08.2	12.1	04.4	15.0	26.11	-02.6	02	27	01.7	. .	02	02.0	31	03.3	01	02.0	02	01.5	. .	05	01.8	16	-	-									
III	-	08.6	13.7	09.5	10.3	14.8	05.1	18.5	03	00.5	29.14	27	02.6	02	02.5	01	05.0	22	03.1	06	01.5	06	02.0	04	01.5	03	02.0	22									
IV	-	12.0	15.4	12.9	13.3	16.5	08.4	21.0	30	01.0	19	13	01.2	05	01.2	08	02.5	33	03.4	01	02.0	02	01.5	03	01.7	23	-	-									
V	-	15.4	18.9	14.3	15.7	19.9	10.5	24.5	31	03.0	13	14	01.8	01	02.0	06	02.7	34	03.4	03	02.3	04	02.2	04	01.8	02	02.5	25									
VI	-	20.4	24.5	19.3	20.8	25.6	15.0	29.0	19	11.0	07.05	12	01.6	08	01.4	03	02.7	23	02.6	-	05	02.0	03	01.7	09	02.3	27	-	-								
VII	-	22.1	27.1	20.5	22.5	28.0	16.2	32.7	13	10.5	10	28	01.8	06	01.3	01	03.0	12	03.5	03	03.0	09	02.0	07	02.1	06	02.3	21									
VIII	-	21.0	27.0	20.7	22.3	28.2	15.2	32.0	07.05	11.3	31	28	01.5	01	02.0	14	03.1	20	02.3	06	02.2	05	01.6	05	02.0	30	-	-									
IX	-	16.2	22.2	15.8	17.5	23.1	12.2	27.2	25	08.2	23	31	02.2	01	02.0	16	02.6	01	01.0	02	02.0	06	01.7	02	02.5	33									
X	-	12.8	19.7	13.7	15.0	20.7	10.1	26.7	03	04.3	26.25	34	02.6	01	01.0	02	02.5	16	02.7	01	01.0	04	01.8	05	01.2	01	03.0	29									
XI	-	05.8	15.4	07.1	08.9	16.5	03.4	19.7	17	00.0	10	21	02.1	10	01.7	. .	09	02.7	02	01.3	01	01.0	06	01.2	02	01.0	03	09									
XII	-	08.6	12.7	08.0	09.4	13.7	04.6	18.7	19	-01.7	01	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-									
GOD.	-	13.0	18.1	13.0	14.3	19.2	09.0	32.7	45	01.2	04.2	09.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-								
$\varphi = 42^{\circ}39' N \lambda = 18^{\circ}06' E$ Gr. $\Delta G = + 1h\ 12\ min.$																									DUBROVNIK		BR. ST. 98										
I	-	07.9	10.6	08.6	09.0	11.7	06.3	17.0	15	00.9	07	16	01.8	02	03.0	07	01.9	26	03.0	09	03.6	02	02.0	02	02.0	07	02.3	03									
II	-	08.7	10.9	09.3	09.5	12.0	07.1	14.6	25	01.9	16	10	01.8	21	03.0	07	01.9	27	03.0	09	03.6	02	02.0	02	02.0	07	02.3	05									
III	-	-	-	-	-	-	-	-	-	-	-	16	02.4	09	03.6	13	01.6	17	02.8	11	03.4	04	02.0	06	02.3	12	02.7	05									
IV	-	-	-	-	-	-	-	-	-	-	-	06	02.0	05	03.0	12	01.9	37	03.3	11	03.0	02	01.5	04	01.8	10	02.6	03									
V	-	16.1	18.5	16.3	16.8	-	-	-	-	-	-	08	01.9	03	03.0	15	01.5	27	02.7	16	03.2	03	01.7	05	02.2	11	02.8	05									
VI	-	21.6	24.2	21.6	22.2	-	-	-	-	-	-	08	02.0	01	01.0	13	01.4	20	02.6	12	02.6	05	02.0	07	03.1	18	02.3	06									
VII	-	23.4	26.6	23.6	24.3	-	-	-	-	-	-	12	02.5	06	03.6	07	02.1	14	02.6	09	02.6	06	02.3	10	02.3	24	02.2	03									
VIII	-	23.0	26.2	23.0	23.8	-	-	-	-	-	-	15	02.0	04	02.2	08	11	02.5	07	01.9	03	01.7	07	02.5	19	01.7	17										
IX	-	10.2	21.1	12.7	14.2	22.4	08.4	32.0	11	02.0	21	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-									
X	-	07.7	15.0	08.9	10.1	15.8	06.3	22.0	10.06	-05.0	28	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-									
XI	-	01.4	04.2	02.1	02.4	04.3	00.5	15.8</td																													

Mesec	Oblačnost Nm (0-10)	Srednji broj sati (Dana)	Vlažnost vazduha %	Padavine R mm	Broj dana na sat																																										
					Tn			Tx			Tx			Tx			F(0-12)	Nm(0-10)	R mm	•	*	•	Δ	•	▲	■	T	≡																			
					M	A	<	M	A	<	M	A	<	M	A	<	6	8	2.0	8.0	0.1	1.0	0.0	•	Δ	•	▲	■																			
CREBIC																																															
BR. ST. 96																																															
I	6.9	7.3	6.0	6.7	-	06.4	77	68	76	73	24	201	032.2	21	.	.	03	.	.	04	01	06	16	19	18	08	19	.	.	.	05	01															
II	7.1	6.8	6.0	6.6	-	06.5	75	67	74	72	28	140	050.5	13	.	.	01	.	.	.	04	11	17	14	04	17	.	.	.	03	.																
III	4.5	5.5	4.1	4.7	-	07.1	71	63	73	69	30	151	030.3	22	08	04	11	10	06	11	.	.	.	01	.																
IV	7.6	6.7	7.3	7.2	-	08.6	77	66	78	73	32	132	028.6	09	01	14	16	14	05	14	.	.	.	03	.																
V	6.6	6.0	6.0	6.2	-	10.2	73	65	78	72	31	145	045.1	23	.	.	.	01	.	.	02	09	15	13	05	15	.	.	.	01	.																
VI	4.0	3.8	4.4	4.0	-	13.4	71	60	75	68	37	096	044.6	16	.	.	24	.	02	.	09	03	08	07	02	08	.	.	.	02	.																
VII	1.6	1.5	1.7	1.6	-	12.7	60	51	63	58	28	001	000.8	07	.	.	31	06	11	.	21	.	01	.	.	01	.	.	.	01	.																
VIII	3.0	2.5	2.4	2.6	-	13.2	66	55	66	63	33	052	040.3	31	.	.	29	07	05	.	18	04	06	03	01	04	.	.	.	03	.																
IX	4.5	4.1	3.7	4.1	-	11.4	73	60	69	67	31	192	042.6	21	.	.	11	.	.	01	01	14	09	09	09	05	09	.	.	.	04	.															
X	-	-	-	-	-	09.9	67	64	72	68	29	087	026.9	04	.	.	04	.	.	.	-	11	06	03	11	.	.	.	02	.																	
XI	3.2	3.0	1.8	2.7	-	06.6	74	55	76	68	30	038	027.4	29	19	04	05	02	01	05	01	.	01	.	03	.															
XII	7.0	7.1	6.1	6.7	-	07.9	79	70	80	76	26	138	038.7	23	04	12	17	15	04	17	.	.	.	03	.																
GOD.	-	-	-	-	-	09.5	71	62	73	68	24	1373	050.5	45.II	.	.	04	100	13	18	05	02	-	-	135	111	44	135	01	.	01	.	30	01													
STON																																															
BR. ST. 97																																															
I	5.6	6.9	5.5	6.0	-	06.3	86	70	79	78	28	241	036.8	22	.	.	07	.	.	07	01	07	11	19	17	08	18	.	.	.	01	.															
II	6.7	6.5	6.1	6.4	-	06.8	85	74	81	80	49	100	017.9	13	.	.	04	.	.	03	04	12	16	14	03	14	02	.	.	.	01	.															
III	5.0	5.0	3.8	4.6	-	07.2	82	65	77	75	32	174	042.0	22	.	.	.	02	.	.	02	10	07	13	12	08	13	.	.	.	03	01															
IV	6.6	6.4	6.8	6.7	-	06.1	85	72	81	80	32	163	031.3	09	.	.	.	04	.	.	02	15	18	15	05	18	.	.	.	02	.																
V	5.2	5.0	5.1	5.1	-	10.4	80	66	82	76	40	145	038.0	02	.	.	.	03	.	.	06	07	13	13	03	13	.	.	.	01	.																
VI	3.1	3.7	2.9	3.2	-	13.5	76	61	78	72	38	122	026.2	28	.	.	19	01	.	12	01	09	02	05	09	.	.	.	01	.																	
VII	1.3	1.4	1.5	1.6	-	13.9	70	55	74	66	36	002	001.7	07	.	.	27	09	04	01	23	.	01	01	01	01	.	.	.	01	.																
VIII	2.4	1.8	1.7	1.9	-	14.6	79	58	73	71	38	003	024.6	29	.	.	31	06	01	01	20	02	02	01	02	02	.	.	.	01	.																
IX	3.6	3.2	2.8	3.2	-	12.2	82	69	84	78	45	221	046.2	06	.	.	10	.	.	01	15	05	10	08	07	10	.	.	.	04	.																
X	3.1	3.2	3.0	3.1	-	10.2	84	68	79	77	37	087	021.4	04	.	.	02	.	.	02	18	09	10	07	04	10	.	.	.	01	02																
XI	2.2	2.5	1.7	2.1	-	07.0	88	63	87	79	44	084	032.7	27	.	.	.	04	.	.	21	04	03	03	03	03	04	.	.	.	01	02															
XII	6.2	6.3	5.4	6.0	-	07.9	87	77	88	83	41	103	019.6	16	.	.	03	.	.	01	03	10	14	13	04	15	.	.	.	01	.																
GOD.	4.3	4.3	3.9	4.1	-	09.9	82	66	80	76	28	1447	066.2	06.IX	.	.	14	09	15	06	25	01	143	79	130	113	47	128	02	.	.	01	16	04													
DUBROVNIK																																															
BR. ST. 98																																															
I	6.1	6.5	5.7	6.1	-	05.8	64	61	69	65	18	182	026.8	05	.	.	.	03	.	.	12	03	06	10	19	16	08	19	01	.	01	.	01	01													
II	6.8	7.1	5.9	6.6	-	06.4	68	69	69	67	27	132	032.6	10	.	.	04	.	.	09	01	02	12	18	14	06	18	02	.	01	.	03	01														
III	4.9	5.0	5.6	5.1	-	07.2	82	65	77	75	32	174	042.0	22	.	.	.	02	.	.	08	01	05	07	14	11	07	14	.	01	.	06	.														
IV	6.5	6.9	7.0	6.8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-																
V	5.9	5.6	5.3	5.6	-	10.3	71	67	75	71	31	166	045.7	23	06	02	02	05	16	13	06	16	.	.	.	06	.														
VI	4.0	4.0	4.4	4.1	-	14.0	67	67	72	69	43	143	041.7	15	.	.	.	04	.	.	07	01	07	05	03	07	.	.	.	08	.																
VII	1.2	1.6	1.9	1.6	-	13.5	56	58	61	59	31	003	001.7	07	.	.	.	08	.	.	22	02	04	03	03	04	.	.	.	05	.																
VIII	2.3	2.4	2.0	2.2	-	14.5	58	64	67	63	30	000	000.0	05	.	.	.	02	.	.	18	01	02	03	01	02	.	.	.	02	.																
IX	4.1	4.1	4.1	4.1	-	11.3	62	60	66	63	29	180	049.9	07	.	.	.	03	.	.	05	02	11	05	11	10	04	11	.	.	.	06	01														
X	3.6	3.7	3.3	3.6	-	09.5	60	58																																							

Mjesec	Vrijeme prije 00:00 Hr.	Temperatura vazduha °C										Cestina pravaca i srednja jačina vjetra m/s, Fm (0-12)																																	
		24					15					Max.		Min.		Raz.		Hrs.		Raz.		N			NE			E			SE			S			SW			W			NW		
		7	14	21	Sred. (Dnev.)	Max.	Min.	Max.	Min.	Raz.	Hrs.	Max.	Min.	Raz.	Hrs.	Max.	Min.	Raz.	Hrs.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.								
$\varphi = 45^{\circ}00' N \lambda = 17^{\circ}55' E$ Gr. $\Delta G = + 1h\ 12\ min.$																												DERVENTA		BR. ST. 101															
I	-	-01.6	02.8	-00.4	00.1	03.2	-03.1	15.4	29	-10.0	09	02	03.5	06	01.7	08	01.5	04	02.5	02	01.0	03	02.0	68													
II	-	-01.9	03.3	-00.5	00.1	03.9	-03.5	12.6	26	-13.5	22	.	.	18	01.3	01	01.0	01	01.0	65													
III	-	03.7	12.5	06.7	07.4	13.7	01.6	22.4	30	-03.5	24.13	.	.	10	02.4	12	01.3	01	02.0	05	01.2	09	01.6	56																	
IV	-	06.6	15.1	08.9	09.9	15.8	04.6	25.8	12	00.0	07	.	.	17	02.3	10	01.6	01	03.0	05	01.4	09	01.9	48																	
V	-	11.9	18.4	12.7	13.9	19.6	04.9	25.8	01	00.0	13	.	.	02	03.0	15	01.3	01	03.0	07	01.3	04	01.8	64																	
VI	-	15.9	23.2	16.8	18.2	24.3	12.1	30.4	10	09.5	30.27	.	.	03	01.3	13	02.1	08	01.6	09	01.7	57																		
VII	-	16.6	25.7	16.9	19.1	24.7	12.2	38.0	01	07.5	24	.	.	09	01.7	15	01.7	04	02.0	02	02.0	63																			
VIII	-	15.1	25.6	16.9	18.6	26.3	12.2	39.6	07	06.5	20.14	.	.	07	01.9	19	01.7	03	01.7	01	05.0	01	04.0	03	01.7	58																			
IX	-	11.4	21.3	13.6	15.0	22.2	09.3	31.6	11	01.5	21	.	.	08	02.5	08	01.4	06	01.7	06	01.8	62																		
X	-	07.7	14.9	09.1	10.2	15.3	06.2	25.0	04	-02.5	28	.	.	01	03.0	09	01.4	01	02.0	.	.	.	04	01.5	02	01.0	76																		
XI	-	01.0	03.7	02.0	02.3	03.9	00.6	14.2	01	-04.0	16	.	.	03	01.7	20	01.4	03	01.0	.	.	64																			
XII	-	-00.6	04.6	00.8	01.4	05.6	-02.3	16.2	30	-11.5	06	.	.	06	02.2	10	01.4	01	01.0	10	01.4	.	.	66																	
GOD.	-	07.2	14.3	08.6	09.7	15.0	04.9	38.0	04.VII	-13.5	22.II	02	03.5	90	02.0	139	01.5	09	02.2	01	05.0	04	02.8	55	01.5	48	01.8	747																	
$\varphi = 44^{\circ}49' N \lambda = 15^{\circ}53' E$ Gr. $\Delta G = + 1h\ 04\ min.$																											BIHAC		BR. ST. 102																
I	739.8	-00.3	03.1	00.9	01.1	04.4	-02.2	14.0	12	-07.8	11.10	04	01.8	05	01.6	10	02.4	11	04.0	06	03.5	13	01.2	26	01.5	15	01.6	03																	
II	735.9	00.1	03.4	01.5	01.6	04.7	-01.8	17.0	25	-10.2	22.21	03	01.7	.	.	11	02.3	11	03.0	04	03.0	07	01.7	26	01.5	19	01.5	03																	
III	738.5	04.1	12.0	07.2	07.6	13.3	02.0	21.8	30	-04.8	23	09	02.1	12	02.0	10	02.1	15	03.1	12	02.0	09	02.6	11	01.8	12	01.8	03																	
IV	735.5	06.5	12.0	08.5	08.9	13.6	04.5	23.8	30	-02.0	17	06	01.8	06	02.2	11	02.0	13	02.4	09	02.0	08	01.5	18	01.8	10	02.0	09																	
V	738.3	11.0	16.9	12.5	13.2	18.7	08.2	24.8	05	-01.0	12	36	01.3	10	01.7	12	01.9	12	02.8	13	02.0	11	01.5	14	01.5	13	01.5	02																	
VI	739.2	14.6	22.1	16.6	17.5	23.4	11.2	29.8	08	06.0	29	05	02.0	13	01.4	12	01.4	10	01.9	07	02.1	15	01.8	12	01.3	15	01.5	01																	
VII	740.6	14.0	24.5	17.7	18.7	25.8	11.8	32.0	18	06.2	24	07	01.4	14	01.9	14	01.2	11	02.0	03	01.3	17	01.7	13	01.5	08	01.5	06																	
VIII	741.3	13.6	24.0	17.2	18.0	25.3	11.4	34.0	07	07.4	20	05	02.0	13	01.2	15	01.2	03	02.3	10	02.1	06	02.0	19	01.7	13	01.6	09																	
IX	740.8	10.4	20.6	13.5	14.5	21.0	08.3	31.2	11	00.8	21	35	01.4	17	01.5	13	01.2	08	02.6	11	01.8	15	01.2	11	01.3	07	01.4	03																	
X	744.5	07.4	13.6	08.8	09.7	14.6	03.9	21.8	04	-01.0	28	07	01.7	15	01.3	15	01.3	02	02.5	03	01.0	16	01.1	22	01.3	10	01.4	08																	
XI	748.8	00.2	04.0	01.2	01.6	04.9	-00.9	16.4	25	-07.4	30	08	01.0	05	01.2	09	01.6	01	02.0	08	01.2	16	01.1	26	01.3	15	01.4	02																	
XII	737.5	01.1	04.3	02.6	02.6	05.9	-01.4	16.2	29	-14.4	01	03	01.7	02	01.0	08	02.0	15	02.9	11	02.4	26	01.3	21	01.3	04	01.8	03																	
GOD.	740.1	07.0	13.4	09.0	09.6	14.7	04.7	34.0	07.VII	-14.4	04.VIII	68	01.6	112	01.6	140	01.7	112	02.7	97	02.1	159	01.5	141	01.6	47																			
$\varphi = 44^{\circ}51' N \lambda = 16^{\circ}10' E$ Gr. $\Delta G = + 1h\ 05\ min.$																											BOSANSKA KRUPA		BR. ST. 103																
I	-	-00.6	03.0	00.5	00.8	04.1	-02.2	16.0	12	-09.0	06	11	01.6	.	02	02.0	01	02.0	06	02.2	02	01.5	71															
II	-	-00.4	04.0	00.9	01.3	05.0	-02.7	16.4	26	-11.6	19	15	01.3	01	02.0	01	02.0	06	02.3	04	01.6	60																
III	-	03.2	12.6	05.7	04.8	14.2	01.0	23.2	30	-05.0	13	13	02.0	.	01	02.0	04	02.2	13	02.2	02	01.6	62																
IV	-	06.8	12.9	08.1	09.0	14.0	03.7	24.2	30	-01.5	19	07	01.9	01	02.0	.	.	02	02.0	19	02.6	01	02.0	.	.	.	00	01.6	60																
V	-	10.5	17.9	11.1	12.7	18.8	07.4	24.2	05	00.5	15.12	10	01.4	13	02.4	70																	
VI	-	15.6	23.0	15.8	17.6	23.0	10.5	30.4	06	06.0	30	15	01.4	01	02.0	.	.	02	02.0	11	02.4	61																		
VII	-	15.7	25.1	16.0	18.2	26.1	11.0	33.0	18	06.2	24	14	01.9	.	01	02.0	05	02.4	.	.	01	01.0	.	.	.	72																			
VIII	-	14.5	25.2	16.5	18.2	26.0	10.7	35.2	07	04.5	20	11	01.7	09	02.3	73																					
IX	-	11.2	20.9	13.3	14.7	22.0	08.4	32.1	11	03.2	22	12	01.5	04	02.8	74																					
X	-	08.5	14.5	08.4	10.0	15.2	05.7	21.8	04	-04.0	28	08	01.5	02	0																										

Mesec	Obladnost Nm (0-10)				Vlažnost vazduha %	Padavine R mm	Broj dana na sat																														
							Tn				Tx				Tn				Tx				Tn				P(0-12) Nm(0-10)				R mm						
	7	14	21	Sred. (Dnev.)			7	14	21	Max	7	14	21	Max	7	14	21	Max	7	14	21	Max	7	14	21	Max	7	14	21	Max	7	14	21	Max			
DERVENTA																										$H_s = 105 \text{ m} H_b = - \text{ m} h = 2.0 \text{ m} h = 1.0 \text{ m}$											
BR. ST.101																																					
I 8.1	7.9	8.0	8.0	-	04.3	92	83	93	89	45	054	021.8	26	01	05	24	02	21	11	09	01	08	03	06	05				
II 8.8	8.3	6.9	7.7	-	04.3	93	82	91	89	54	097	031.1	20	04	04	20	01	05	13	14	13	04	08	11	.	01	.	.	05	16			
III 6.2	5.8	6.1	6.0	-	06.3	93	63	89	82	28	067	018.3	07	.	.	07	.	.	.	01	05	12	14	11	01	14	03	03	01	02			
IV 8.1	6.9	5.8	6.9	-	07.2	92	58	89	80	29	060	017.1	16	.	.	02	01	12	11	10	02	11	03	01					
V 6.9	7.5	7.0	7.2	-	10.3	93	68	92	84	41	159	033.9	03	.	.	02	01	15	22	14	07	22	02	01					
VI 4.8	5.4	5.2	5.1	-	12.5	88	61	89	80	31	058	017.2	28	.	.	16	03	.	.	.	11	10	15	09	02	15	01	01					
VII 2.1	3.7	2.1	2.6	-	13.2	88	55	92	79	21	067	028.4	08	.	.	24	04	.	.	01	15	01	09	06	03	09	02	.					
VIII 4.5	4.0	3.8	4.1	-	12.3	88	52	99	76	38	052	025.9	31	.	.	18	06	.	.	.	11	07	07	06	02	07	04	.					
IX 5.0	4.8	4.9	4.9	-	10.3	92	56	92	80	21	097	029.2	20	.	.	06	01	.	.	.	10	08	10	09	04	10	01	04					
X 8.1	5.8	7.0	7.0	-	08.5	95	73	95	88	53	025	011.9	05	.	.	04	01	.	.	01	04	16	09	07	01	09	01	15					
XI 19.0	9.3	9.3	9.6	-	05.0	93	85	92	90	21	018	007.0	28	.	.	11	01	.	.	.	27	05	04	03	03	03	12	03					
XII 7.4	5.9	6.9	6.7	-	04.8	93	81	92	89	54	068	014.1	19	02	06	21	.	.	.	04	15	10	10	03	08	02	.	.	01	.	10	08					
GOD.	6.6	6.3	6.1	6.3	-	08.2	91	68	91	83	21	822	033.9	03.V	07	15	87	69	14	.	03	.	63	157	139	108	30	124	22	03	01	01	.	11	01	32	
BIHAC																											$H_s = 246 \text{ m} H_b = 230.4 \text{ m} h = 2.0 \text{ m} h = 1.0 \text{ m}$										
BR. ST.102																											$H_s = 246 \text{ m} H_b = 230.4 \text{ m} h = 2.0 \text{ m} h = 1.0 \text{ m}$										
I 8.5	7.8	6.7	7.7	-	043.0	34.1	87	75	84	32	39	130	022.6	30	.	06	25	.	.	.	11	07	03	18	18	14	06	10	11	01	.	.	.	06	13		
II 9.0	8.4	7.2	8.2	-	037.2	04.2	83	72	83	80	45	105	032.8	20	02	04	22	.	.	.	11	01	01	19	16	02	08	16	.	.	02	.	01	02	18		
III 6.5	6.6	5.1	6.1	-	151.1	05.0	83	50	67	26	154	028.7	07	.	.	07	.	.	.	16	03	04	19	17	15	04	15	08	03	.	.	02	01	04			
IV 8.3	9.0	7.6	8.3	-	103.5	06.1	83	61	75	73	33	132	032.8	14	.	.	02	.	.	.	10	01	.	18	23	15	03	23	02	01	.	.	01	04	01		
V 8.0	8.4	6.7	7.7	-	137.8	08.4	80	78	74	31	156	035.3	14	.	.	01	.	.	.	10	31	.	16	20	15	05	20	.	.	.	01	08	03				
VI 5.5	6.3	4.8	5.6	-	223.2	10.1	82	55	73	20	148	028.4	14	.	.	14	.	.	.	08	01	04	16	18	10	02	16	.	.	04	02	.					
VII 4.0	5.5	2.3	4.0	-	299.7	11.2	87	50	75	31	069	027.6	22	.	.	20	02	.	.	06	02	10	02	88	06	03	08	.	.	03	07	02					
VIII 4.3	5.7	3.9	4.4	-	233.7	10.9	50	76	72	27	068	030.1	31	.	.	18	06	.	.	04	02	10	05	08	07	01	08	.	.	03	03	.					
IX 4.8	5.9	3.3	4.7	-	198.5	29.2	92	53	82	25	177	042.4	28	.	.	08	01	.	.	07	.	08	04	10	09	06	10	.	.	.	06	09					
X 8.7	7.2	6.1	7.3	-	080.4	07.6	94	66	89	33	093	051.4	02	.	.	03	.	.	.	03	16	12	08	02	12	.	.	.	02	09							
XI 9.5	7.0	8.0	8.5	-	044.9	04.5	91	78	80	31	045	016.2	29	.	.	02	19	.	.	01	01	21	04	05	02	03	04	.	.	.	12	06					
XII 8.1	8.2	8.0	8.0	-	046.5	04.4	82	71	80	77	36	096	030.0	20	04	08	19	.	.	10	03	.	15	17	10	03	13	07	01	.	01	10	20				
GOD.	7.1	7.2	5.8	6.7	-	1599.5	07.1	86	61	79	75	26	1301	051.4	02.X	06	22	98	60	09	.	97	21	44	149	174	130	41	146	48	08	.	04	05	38	62	46
BOSANSKA KRUPA																											$H_s = 176 \text{ m} H_b = - \text{ m} h = 2.0 \text{ m} h = 1.0 \text{ m}$										
BR. ST.103																											$H_s = 176 \text{ m} H_b = - \text{ m} h = 2.0 \text{ m} h = 1.0 \text{ m}$										
I 8.8	7.9	8.7	8.5	-	04.4	92	85	88	89	52	137	032.5	31	.	05	23	.	.	.	01	20	19	16	05	12	10	.	.	.	09	19						
II 10.0	8.7	8.4	9.0	-	04.5	89	79	88	85	51	083	028.0	20	04	04	20	.	.	.	23	17	15	01	11	12	03	01	.	.	.	06	25					
III 7.5	6.5	5.9	6.6	-	05.6	90	56	80	75	20	109	024.5	25	.	.	11	.	.	.	04	13	15	14	03	15	05	01	.	.	.	08	03					
IV 6.5	6.4	6.4	7.1	-	06.5	86	60	83	76	14	102	025.0	15	.	.	02	.	.	.	10	17	16	03	17	02	01	.	.	.	01	01						

Mjesec	Vaspodjala pričvršćujuća činjenica Fm	Temperatura vazduha °C										Čestina pravaca i srednja jačina vетра nD, Fm (0-12)																									
		TM			RH			RH			Dat.			Min.			Dat.			N		NE		E		SE		S		SW		W		NW		C	
		7	14	21	Spred. (tm)	RH1	RH2	RH3	RH4	RH5	Dat.1	Dat.2	Dat.3	Dat.4	Dat.5	Dat.6	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.							
$\varphi = 44^{\circ}46' N \lambda = 16^{\circ}42' E$ Gr. $\Delta G = + 1h 07 min.$																									SANSKI MOST		BR. ST. 106										
I	-	-00.4	03.1	00.4	00.9	04.6	-02.5	15.0	12	-09.8	09	08	01.8	01	01.0	.	02	13	03.5	05	01.0	07	01.1	14	01.3	45											
II	-	-01.1	03.6	01.0	01.1	05.0	-02.5	18.6	26	-10.0	21	08	01.9	.	01	02.0	01	01.0	03	02.7	02	01.0	06	01.2	27	01.2	36										
III	-	03.0	12.4	04.4	07.1	14.2	01.1	23.2	30.2	-04.8	13	09	02.8	03	01.7	.	11	01.7	09	03.1	08	02.0	04	01.8	17	01.7	32										
IV	-	06.2	13.6	08.4	09.1	14.6	04.3	25.1	30	-00.3	19	09	01.9	02	02.0	02	01.0	03	02.3	14	02.6	06	02.2	02	01.0	11	01.2	41									
V	-	10.5	17.4	12.0	13.0	19.0	00.0	27.5	01	-00.4	12	10	02.1	01	02.0	01	01.0	06	02.7	09	02.4	06	01.8	05	01.2	10	01.8	45									
VI	-	14.4	22.0	16.2	17.4	24.1	11.2	30.4	10.0	08	07.2	30	06	02.0	08	02.2	02	02.0	.	02	04.5	07	01.7	05	01.2	16	01.6	44									
VII	-	14.6	25.3	16.9	18.4	26.4	11.3	33.1	18	05.6	24	07	02.6	12	02.2	02	01.5	.	02	03.0	06	01.8	05	01.2	09	01.7	50										
VIII	-	13.9	24.8	16.4	17.9	25.8	11.1	35.0	07	06.7	22.20	07	02.4	08	01.8	01	02.0	.	02	03.5	09	02.0	03	01.0	16	01.7	47										
IX	-	09.6	21.1	12.7	14.0	22.1	07.6	32.2	11	00.3	21	07	01.7	01	02.0	01	02.0	05	01.4	03	01.0	07	01.4	11	01.6	54											
X	-	07.3	14.5	08.9	09.9	15.5	05.9	24.2	04	-0.4	28	06	02.2	05	02.8	.	0.	03	03.0	01	01.0	05	01.0	24	01.5	49											
XI	-	00.9	04.6	01.9	02.2	05.1	-00.1	15.0	01	-05.2	30	06	01.8	07	01.7	02	01.0	.	02	01.5	04	01.2	07	01.3	24	01.2	38										
XII	-	-00.6	04.0	00.5	01.1	05.2	-03.1	16.5	30.2	-14.4	06	01	02.0	04	01.8	03	01.3	04	02.2	05	03.6	13	01.6	07	01.7	08	01.6	48									
GOD.	-	04.5	13.9	08.5	09.3	15.1	04.4	35.0	07	07.0	06.20	06	XV	84	02.1	52	02.0	15	01.5	26	02.1	69	02.9	70	01.7	63	01.3	187	01.5	529							
$\varphi = 44^{\circ}39' N \lambda = 16^{\circ}45' E$ Gr. $\Delta G = + 1h 07 min.$																									PRIJEDOR		BR. ST. 107										
I	-	-00.8	02.5	00.2	00.6	03.5	-02.3	15.7	29	-09.5	11	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-										
II	-	-01.0	03.5	00.7	01.1	04.6	-02.2	17.8	26	-11.9	22	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-											
III	-	02.7	12.5	07.4	07.8	14.1	02.3	23.0	29	-04.2	20	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-											
IV	-	06.8	14.0	09.3	10.0	15.3	05.0	24.9	30	00.5	18	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-											
V	-	11.4	18.2	13.0	13.9	19.6	09.0	27.0	01	00.3	12	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-											
VI	-	15.4	23.4	17.6	18.5	24.5	12.3	30.6	07	08.1	29	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-											
VII	-	15.2	23.8	18.4	19.5	26.8	12.6	34.5	18	07.7	24	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-											
VIII	-	15.1	25.5	18.5	19.4	26.4	12.8	36.0	07	09.0	22.20	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-											
IX	-	11.2	21.1	14.1	15.1	22.1	08.6	31.4	11	01.3	21	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-											
X	-	07.8	16.1	09.6	10.3	15.1	04.6	24.0	04	-0.2	28	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-											
XI	-	01.2	03.5	02.0	02.2	03.9	00.5	15.0	01	-0.4	24	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-											
XII	-	-00.7	02.8	00.3	00.7	03.6	-02.5	17.0	30	-12.8	06	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-											
GOD.	-	07.1	13.9	09.3	09.9	15.0	05.3	36.0	07	07.0	06.XV	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-										
$\varphi = 44^{\circ}16' N \lambda = 16^{\circ}32' E$ Gr. $\Delta G = + 1h 07 min.$																									MLINISTE		BR. ST. 108										
I	-	-02.9	-00.9	-03.2	-02.5	00.4	-06.0	06.5	14	-13.4	06	-	-	03	.	08	02.2	16	02.6	09	03.1	01	03.0	25	01.7	.	02	34									
II	-	-02.9	-00.6	-02.4	-02.1	00.7	-05.7	07.5	26	-25.3	21	-	-	03	02.0	05	02.4	17	03.3	16	03.1	.	15	01.5	09	02.0	19										
III	-	00.2	04.6	00.8	01.6	05.8	-02.5	14.5	03	-09.0	23	10	01.7	04	03.8	01	03.0	09	03.6	18	01.7	.	24	02.4	06	04.7	21										
IV	-	02.9	05.9	03.0	03.7	07.0	03.7	16.4	30	-04.8	17	10	01.5	.	03	03.7	07	02.6	12	01.5	13	02.5	18	01.4	02	02.5	25										
V	-	07.0	11.0	07.4	08.4	12.2	04.6	19.1	05	-05.2	12	06	01.3	03	02.0	01	01.3	13	03.0	12	01.3	06	02.3	16	01.4	02	02.0	34									
VI	-	13.0	16.8	11.7	13.3	18.0	08.4	24.0	10	03.2	27	06	01.2	05	01.6	03	02.0	20	02.4	10	01.8	05	02.2	08	01.9	.	03										
VII	-	12.6	19.2	13.0	14.4	19.7	08.9	25.6	12	05.0	24	07	01.3	02	03.0	.	01	11	02.4	14	01.3	06	02.0	11	01.4	02	01.5	40									
VIII	-	13.8	18.7	12.7	14.5	19.5	08.8	27.0	20	02.0	31	10	01.2	04	01.8	.	06	03.7	11	01.5	04	02.5	08	01.6	03	02.0	42										
IX	-	09.7	14.4	09.4	10.7	15.4	05.8	24.3	11	-00.8	21	09	01.0	.	03	02.0	19	02.7	07	01.9	02	02.5	09	02.1	08	02.0	33										
X	-	05.0	08.8	05.3	06.1	09.7	02.9	20.4	03	-05.6	29.28	08	01.1	.	03	01.7	13	02.2	03	01.3	.	08	02.4	05	01.6	53											
XI	-	-00.1	04.8	00.0	01.2	05.9	-01.8	14.5	10	-0.0	29	11	01.5	.	05	01.0	10	01.7	03	01.3	.	14	01.9	02	02.0	45											
XII	-	-00.7	01.5	-00.6	-00.1	02.7	-03.1	07.3	11	-17.0	08	02	01.0	.	03	02.3	37	02.6	09	01.3	04	03.2	17	01.9	.	21											
GOD.																																					

Meseč	Oblačnost Nm (0-10)				Insolacija broj sati	Vlažnost vazduha				Padavine R mm		Broj dana na sat																										
	7	14	21	Sred. (Dnev.)		U m s	Tn	Tx	Tn	Tx	Tx	Tn	P(0-12)	Nm(0-10)	R mm	•	*	*	Δ	○	▲	■	R	T	≡	■												
	mm	mm	mm	mm		Σ	Max	Dat.	≤	<	≤	≥	IV	IV	IV	IV	IV	<	>	IV	IV	IV	IV	IV	IV	IV												
SANSKI MOST																																						
BR. ST. 106																																						
I	9.0	8.7	6.2	8.0	-	045.3	04.3	91	80	89	86	48	078	017.2	26	.	02	23	.	.	05	01	01	17	18	10	03	12	10	06	.	.	.	01	10	11		
II	9.2	8.6	6.9	8.4	-	037.1	04.4	93	75	91	86	49	068	015.1	20	01	05	22	.	.	05	01	03	18	17	15	01	08	12	06	.	.	.	01	03	19		
III	7.3	7.4	5.4	6.7	-	148.8	05.4	90	53	80	74	24	084	021.0	07	.	.	11	.	.	05	01	03	11	17	13	03	17	04	03	.	.	.	01	01	.		
IV	7.9	8.4	7.4	7.9	-	107.0	06.8	90	59	88	79	36	075	016.0	16	.	.	01	01	.	02	.	15	22	11	03	22	02	.	.	.	04	04	01				
V	8.0	8.5	6.5	7.7	-	138.8	09.3	93	63	90	82	33	121	024.0	14	.	.	01	01	.	04	.	14	22	14	05	22	08	05	.			
VI	6.2	6.9	5.0	6.0	-	224.2	11.3	90	55	86	77	34	078	022.0	22	.	.	14	02	.	06	10	16	11	04	16	03	03	.				
VII	4.6	5.1	2.4	4.0	-	298.1	12.3	93	51	89	78	35	042	013.4	22	.	.	23	02	.	02	02	09	03	08	06	02	08	.	.	.	04	05	.				
VIII	4.7	4.9	3.1	4.2	-	238.9	11.4	92	49	87	76	26	063	022.4	31	.	.	17	07	.	01	01	09	04	11	02	11	.	.	.	02	04	.					
IX	7.5	5.7	3.5	5.6	-	179.1	09.8	97	55	93	82	30	104	028.7	13	.	.	08	01	.	02	.	04	09	10	09	04	10	.	.	.	02	11	.				
X	9.3	7.0	6.3	7.6	-	087.7	08.1	97	68	93	86	41	056	016.7	02	.	.	07	.	.	01	.	01	16	11	09	02	11	.	.	.	01	14	.				
XI	9.7	8.5	9.7	9.3	-	026.5	04.5	94	91	92	89	51	030	011.5	28	.	.	15	.	.	03	04	04	01	02	03	01	.	.	.	07	03	.					
XII	9.3	8.0	7.3	8.2	-	040.9	04.5	91	78	92	87	43	073	019.2	20	03	04	21	.	.	03	02	.	18	17	09	02	13	04	01	.	.	.	03	17	22		
GOD.	7.8	7.3	5.8	7.0	-	1570.4	07.7	92	63	89	81	24	892	028.7	43	X	04	13	101	64	12	.	25	07	31	158	173	120	32	152	37	09	.	.	.	01	30	24
PRIJEDOR																																						
BR. ST. 107																																						
I	9.0	8.5	8.7	8.7	-	04.4	04	83	91	90	89	39	089	016.7	31	.	04	21	.	.	01	24	12	12	04	09	09	06	.	.	.	07	08	.				
II	9.6	7.8	8.1	8.5	-	04.4	01	76	68	85	84	46	049	024.6	20	02	06	21	.	.	02	.	16	16	11	02	14	12	08	.	.	.	01	03	.			
III	6.5	6.0	5.8	6.1	-	05.4	04	49	75	75	72	21	065	018.0	07	.	.	06	.	.	03	09	14	11	01	14	04	04	.	.	.	01	03	.				
IV	7.6	6.9	7.8	7.4	-	04.7	08	53	82	74	74	26	080	023.8	16	.	.	01	.	.	01	13	19	10	03	19	.	.	.	03	03	.						
V	7.2	7.5	6.8	7.2	-	09.4	90	60	87	79	79	29	158	025.2	14	.	.	03	.	.	01	19	15	17	09	17	19	.	.	.	06	01	.					
VI	5.3	5.2	5.3	5.3	-	11.3	86	53	93	73	73	28	060	019.3	22	.	.	18	05	.	04	07	12	10	01	12	.	.	.	02	05	.						
VII	4.7	4.1	3.6	4.1	-	04.0	04	92	81	86	85	35	040	019.8	08	.	.	22	04	.	01	05	03	07	06	03	07	.	.	.	01	03	13					
VIII	5.1	4.0	4.0	4.7	-	04.0	04	82	91	88	85	55	026	013.0	27	.	.	20	07	.	01	05	04	06	05	02	06	.	.	.	04	.	.					
IX	6.8	5.2	5.0	5.7	-	10.0	92	54	90	78	73	23	098	023.8	13	.	.	05	01	.	01	08	10	10	04	10	.	.	.	01	11	.						
X	9.2	6.0	6.6	7.3	-	08.0	93	67	91	84	85	35	047	014.6	02	.	.	02	.	.	01	14	11	08	02	11	.	.	.	01	11	.						
XI	10.0	9.4	9.8	9.7	-	04.8	92	81	92	88	85	55	026	013.0	28	01	01	12	.	.	01	28	04	01	01	02	03	01	.	.	01	08	03					
XII	9.9	8.6	8.5	9.0	-	04.5	94	83	92	90	84	44	088	019.3	10	01	07	22	.	.	01	09	11	11	04	10	04	02	.	01	01	01	19	.				
GOD.	7.6	6.6	6.7	7.0	-	900	026.8	27	WII	03	10	84	68	17	21	166	141	113	34	133	32	18	.	01	01	01	23	07	-			
MLINISTE																																						
BR. ST. 108																																						
I	7.9	7.7	6.6	7.4	-	03.3	83	81	83	82	84	64	195	034.1	30	09	10	28	.	.	01	.	02	18	21	19	06	10	19	07	.	.	.	01	13	31		
II	8.2	8.4	7.3	8.0	-	33.3	78	75	80	78	75	55	237	042.7	20	10	13	22	.	.	05	.	04	19	22	21	07	10	19	06	.	.	.	01	13	28		
III	6.0	6.0	5.4	5.9	-	04.1	80	69	85	78	79	39	203	038.6	18	04	21	.	.	02	.	02	12	22	21	07	09	18	04	.	.	.	01	09	31			
IV	8.4	9.1	8.1	8.5	-	04.8	83	71	85	80	81	51	214	025.1	16	02	10	.	.	.	01	.	01	27	25	07	22	13	07	.	.	.	01	10	16			
V	7.5	7.5	6.6	7.3	-	06.4	79	68	81	76	75	51	230	045.7	23	.	.	03	.	.	01	.	03	16	20	18	09	18	03	01	.	.	.	01	09	02		
VI	6.2	6.0	4.7	5.6	-	08.8	75	67	79	76	75	53	226	060.1	22	.	.	01	.	.	04	11	14	11	06	16	14	.	.	.	04</							

Mjesec	Vrhodni pritisak Pa	Vrhodni temperatura vazduha Pa	Temperatura vazduha °C								Čestina pravaca i srednja jačina vетра nD, Pa (0-12)																						
			Tm				Hs				N			NE			E			SE			S			SW			W			NW	
			7	14	21	Sred. (Dnev.)	Hs	Hs	Hs	Hs	Hs	Hs	Hs	Hs	Hs	Hs	Hs	Hs	Hs	Hs	Hs	Hs	Hs	Hs	Hs	Hs	Hs	Hs	Hs	Hs	Hs		
$\varphi = 44^{\circ}21' N \lambda = 17^{\circ}16' E$ Gr. $\Delta G = + 1h 09 min.$																													JAJCE				
$\varphi = 44^{\circ}21' N \lambda = 17^{\circ}16' E$ Gr. $\Delta G = + 1h 09 min.$																													BR. ST. 111				
I	-	-01.4	02.8	-00.1	00.3	04.0	-03.3	12.6	13	-13.0	09	02	02.5	04	04.8	06	04.9	*	*	01	02.0	03	03.3	01	02.0	01	05.0	75					
II	-	-00.3	04.4	01.7	01.9	05.6	-02.6	16.0	11	-13.2	21	*	02	03.0	07	04.0	*	*	01	03.0	05	02.6	04	03.2	03	03.3	62						
III	-	02.7	11.0	06.3	06.6	12.6	00.7	22.2	30	-05.0	13	03	01.7	05	02.8	05	03.2	*	*	02	03.0	09	03.0	03	02.3	06	03.2	60					
IV	-	06.6	12.4	08.8	09.2	13.6	04.1	22.4	30	00.0	08	06	02.5	03	03.0	06	03.2	32	02.0	01	03.0	04	03.5	06	03.0	03	04.3	59					
V	-	10.7	16.2	11.6	12.5	18.2	07.6	24.5	01	-00.5	12	01	05.0	09	03.8	03	02.3	01	02.0	01	02.2	03	04.7	*	*	01	02.0	74					
VI	-	13.9	22.0	15.9	16.9	23.3	11.1	30.0	10	07.0	30	01	05.0	03	04.3	04	02.5	*	*	02	02.0	05	02.8	07	01.9	01	04.0	67					
VII	-	14.2	24.5	17.3	18.3	25.7	11.6	31.7	12	07.2	25.24	*	*	03	03.3	05	02.0	01	02.0	02	02.5	06	02.3	02	04.0	73							
VIII	-	13.6	24.6	17.2	18.2	25.4	11.5	33.2	07	07.4	31.3	02	01.5	03	03.3	02	02.5	*	*	03	05.0	*	*	02	02.5	01	02.0	80					
IX	-	09.5	19.2	12.6	13.5	20.2	07.9	29.2	11	01.8	21	05	02.8	02	02.0	03	01.7	02	02.5	*	*	01	03.0	03	02.3	01	05.0	73					
X	-	07.5	14.1	09.5	10.2	15.0	05.9	27.2	03	-03.6	29	02	02.0	06	02.5	04	02.2	02	03.0	01	03.3	02	02.5	10	03.1	01	05.0	67					
XI	-	-00.1	04.2	01.4	02.2	06.8	-01.5	14.2	01	-06.4	18.16	02	01.5	02	01.5	03	02.3	01	03.0	*	*	02	02.5	04	03.2	*	01	76					
XII	-	00.4	03.8	00.7	01.4	04.4	-02.8	13.8	31.30	-14.8	07.06	*	*	05	01.8	06	01.0	04	03.8	02	03.0	10	04.1	05	01.8	03	02.0	58					
GOD.	-	06.4	13.4	08.6	09.3	14.6	04.2	33.2	07.VII	-14.8	07.06	XII	24	02.5	45	03.1	54	02.7	13	02.9	15	03.1	46	03.3	51	02.6	23	03.4	824				
$\varphi = 44^{\circ}00' N \lambda = 17^{\circ}17' E$ Gr. $\Delta G = + 1h 09 min.$																													KUPRES				
$\varphi = 44^{\circ}00' N \lambda = 17^{\circ}17' E$ Gr. $\Delta G = + 1h 09 min.$																													BR. ST. 112				
I	-	-05.0	-00.3	-03.0	-02.8	00.9	-06.6	07.0	15	-16.2	27	35	03.2	*	*	*	*	*	*	*	31	04.2	*	*	*	*	*	*	*	*	27		
II	-	-04.7	-00.3	-02.6	-02.4	01.3	-06.8	07.0	26	-19.6	16	30	02.9	*	*	*	*	*	*	*	36	03.6	*	*	*	*	*	*	*	*	20		
III	-	-02.6	04.9	-00.1	00.5	06.1	-03.7	15.2	03	-12.0	23	36	03.7	*	*	*	*	*	*	*	31	03.7	*	*	*	*	*	*	*	*	26		
IV	-	02.1	05.9	03.2	03.6	07.5	00.4	14.4	30	-03.4	18	34	02.3	*	*	*	*	*	*	*	50	03.7	*	*	*	*	*	*	*	*	06		
V	-	05.5	10.8	06.6	07.4	12.3	03.2	18.8	05	-05.0	12	19	02.7	*	*	*	*	*	*	*	51	03.5	*	*	*	*	*	*	*	*	23		
VI	-	10.5	17.1	11.5	12.6	18.7	07.5	23.2	10	03.2	28	16	02.2	*	*	*	*	*	*	*	46	02.5	*	*	*	*	*	*	*	*	30		
VII	-	10.1	19.4	13.6	14.2	20.7	06.4	24.2	29	02.6	09	31	02.9	*	*	*	*	*	*	*	39	03.6	*	*	*	*	*	*	*	*	23		
VIII	-	10.0	20.2	13.9	14.5	21.4	06.8	26.4	07.03	01.6	31	24	04.6	*	*	*	*	*	*	*	36	03.2	*	*	02	03.0	*	*	*	31			
IX	-	05.9	14.5	09.5	09.8	16.1	03.5	24.2	26	00.2	29.21	41	03.1	*	*	*	*	*	*	*	30	02.6	*	*	*	*	*	*	*	*	19		
X	-	03.3	10.6	06.4	06.8	12.2	01.3	20.8	03	-06.8	28	42	02.5	01	02.0	*	*	*	*	*	*	29	03.8	*	*	*	*	*	*	*	*	21	
XI	-	-04.2	07.0	-01.5	00.0	08.3	-05.2	16.2	11	-12.4	30	42	02.5	01	04.0	*	*	*	*	*	*	05	02.8	*	*	*	*	*	*	*	*	42	
XII	-	-03.3	01.3	-01.9	-01.5	02.2	-05.4	06.4	11	-20.4	07	18	02.4	*	*	*	*	*	*	*	422	03.4	*	*	*	*	*	*	*	*	33		
GOD.	-	02.3	09.3	04.6	05.2	10.6	00.1	26.4	07.VIII	-20.4	07.XII	369	02.6	02	03.0	*	*	*	*	*	*	02	03.0	*	*	*	*	*	*	*	*	301	
$\varphi = 44^{\circ}38' N \lambda = 17^{\circ}23' E$ Gr. $\Delta G = + 1h 10 min.$																													KOTOR VARDOS				
$\varphi = 44^{\circ}38' N \lambda = 17^{\circ}23' E$ Gr. $\Delta G = + 1h 10 min.$																													BR. ST. 113				
I	-	-01.7	03.4	00.1	00.5	04.9	-03.8	17.2	29	-16.0	09	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*
II	-	-02.0	04.1	00.6	00.8	05.9	-04.0	17.5	26	-17.0	21	*	*	*	*	*	*	*	*	*	*	17	03.7	*	*	*	*	*	*	*	*	66	
III	-	02.5	12.1	04.6	06.9	13.8	00.4	23.0	30	-05.0	13	10	02.7	*	*	*	*	*	*	*	12	03.2	03	06.0	*	*	*	*	*	68			
IV	-	06.2	13.5	08.6	09.2	14.7	00.5	24.0	30	00.7	24	08	02.1	04	02.2	01	02.0	*	*	*	*	05	04.4	*	*	*	*	*	*	*	*	87	
V	-	10.4	17.3	11.7	12.8	19.1	07.4	29.0	01	-01.0	15	*	*	*	*	*	*	*	*	*	08	03.6	*	*	*	*	*	*	*	*	85		
VI	-	14.4	22.5	16.4	17.4	23.9	11.0	31.0	10	07.5	27	*	*	*	*	*	*	*	*	*	09	03.4	*	*	*	*	*	*	*	*	81		
VII	-	15.0	25.1	16.5	16.3	26.0	11.1	32.3	18	05.5	23	*	*	*	*	*	*	*	*	*	02	03.3	*	*	01								

Mjesec	Oblačnost Nm (0-10)			Inzolacijska broj sati	Vlažnost vazduha			Padavine R mm			Broj dana na sat																								
					Um			R mm			Tn	Tn	Tn	Tn	Tn	P(0-12)	Nm(0-10)	R mm	•	*	*	*	Δ	○	▲	▲	R	≡	■						
	7	14	21	Sred. (Dnev.)		7	14	21	Sred. (Dnev.)	Min.	Σ	Max	Dat.	≥	<	≥	≤	≥	≤	<	>	≥	≤	•	Δ	○	▲	▲	T	≡	■				
JAJCE																																			
BR. ST. 111																																			
I	8.5	7.1	5.7	7.1	-	052.0	34.2	90	77	90	86	48	050	015.0	30	03	07	26	•	•	02	•	01	16	15	12	01	10	08	•	•	06	09		
II	9.2	8.0	5.5	7.6	-	033.8	04.0	86	60	80	75	20	067	018.4	13	02	01	20	•	•	01	•	13	17	11	02	06	13	•	•	04	11			
III	7.5	6.8	5.9	6.7	-	135.4	04.5	84	47	68	66	17	057	018.3	18	•	•	11	•	•	03	•	02	13	16	12	01	15	10	04	•	•	06		
IV	6.9	8.0	6.7	7.2	-	099.0	05.8	87	51	73	70	14	071	016.6	06	•	•	•	•	•	03	19	09	01	18	06	•	•	•	•	•	•			
V	7.8	8.4	6.9	7.7	-	128.8	08.8	71	62	88	80	25	151	030.0	03	•	•	02	01	•	02	•	01	16	21	15	06	21	02	•	•	01	03		
VI	6.3	6.2	5.1	5.9	-	205.8	10.9	94	55	82	77	30	155	049.3	22	•	•	•	13	01	•	01	•	02	09	14	11	05	14	•	•	02	03		
VII	5.3	4.5	3.5	4.4	-	273.5	11.2	92	44	83	73	31	061	018.4	07	•	•	•	20	02	•	•	06	01	08	37	03	08	•	•	07	13			
VIII	6.9	5.9	4.3	5.5	-	229.5	11.1	94	66	80	73	33	031	014.8	31	•	•	•	16	04	•	01	•	03	05	09	03	02	09	•	•	13			
IX	7.7	5.6	5.5	6.3	-	156.1	08.4	91	47	84	74	23	182	036.0	08	•	•	05	•	•	01	•	04	11	11	11	07	11	•	•	•	13			
X	9.0	8.8	6.7	7.2	-	104.8	07.5	91	61	88	80	26	032	005.8	02	•	•	04	01	•	•	01	•	01	14	10	09	10	01	•	•	06			
XI	9.5	6.0	6.4	7.3	-	065.3	04.5	88	69	85	81	32	029	021.0	28	•	•	21	•	•	•	01	•	15	04	04	01	02	03	01	•	11	03		
XII	8.1	7.3	7.4	7.6	-	036.2	04.4	83	74	84	80	54	121	025.2	23	03	09	19	•	•	05	01	•	16	11	10	06	09	03	01	•	04	13	20	
GOD.	7.7	6.6	5.8	6.7	-	1520.2	07.1	89	57	82	76	14	1007	049.3	22.VI	08	17	103	56	09	•	20	01	19	142	155	114	35	133	48	07	•	07	05	43
KUPRES																																			
BR. ST. 112																																			
I	7.3	7.4	7.8	7.4	-	03.3	76	64	82	80	21	115	028.2	30	08	12	28	•	•	09	02	01	15	21	19	03	09	16	01	•	•	31			
II	8.0	8.4	8.1	8.1	-	13.5	78	85	82	82	17	114	026.4	13	09	13	21	•	•	02	02	01	17	17	15	04	08	13	03	•	•	28			
III	6.5	7.9	7.7	7.4	-	034.3	83	83	90	85	33	090	013.6	16	01	01	26	•	•	11	03	•	15	18	16	03	08	12	01	•	•	16			
IV	8.9	9.0	8.9	8.9	-	055.3	92	88	91	90	65	133	025.6	14	•	•	11	•	•	06	02	•	22	22	21	02	18	07	01	•	•	08			
V	7.9	8.5	7.9	8.1	-	06.7	90	76	89	85	49	227	051.2	23	•	•	08	•	•	04	02	•	18	21	19	07	21	02	01	•	•	01			
VI	6.8	6.3	6.3	6.4	-	08.8	89	63	84	79	45	165	051.2	28	•	•	•	•	•	01	•	04	17	12	05	17	•	•	01	•	•	01			
VII	3.8	4.9	4.4	4.4	-	09.4	86	64	80	77	48	029	013.4	06	•	•	•	•	•	07	•	01	05	05	01	05	•	•	05	•	•	03			
VIII	5.0	5.4	5.0	5.1	-	09.7	87	82	83	78	47	039	022.9	31	•	•	06	•	•	03	02	02	04	08	04	01	08	•	•	•					
IX	6.4	7.2	6.7	6.8	-	08.0	93	78	87	86	47	216	044.0	13	•	•	•	•	•	04	02	•	10	12	11	08	12	01	01	•	•	03			
X	7.1	6.9	7.3	7.1	-	06.8	92	82	90	88	57	056	017.4	04	•	•	10	•	•	04	02	•	14	10	09	02	08	02	•	•	03	03			
XI	4.2	3.7	3.7	3.9	-	04.0	83	69	80	81	28	047	028.4	28	01	03	26	•	•	07	01	03	05	03	02	02	02	•	•	03					
XII	7.3	6.8	7.0	7.1	-	03.9	79	85	87	84	-	170	032.6	23	08	07	22	•	•	03	04	14	19	15	07	14	04	02	•	•	27				
GOD.	6.6	6.6	6.6	6.7	-	06.2	85	76	86	82	-	1401	051.2	28.VI	27	36	152	06	•	53	17	21	138	169	149	45	130	41	10	•	01	03	117		
KOTOR VAROS																																			
BR. ST. 113																																			
I	110.0	9.3	10.0	9.8	-	04.3	91	80	87	86	40	101	032.5	26	04	05	26	•	•	•	•	31	14	13	02	08	06	02	•	•	•	05			
II	110.0	9.7	9.5	9.8	-	04.4	88	81	85	82	35	097	015.0	12	04	02	22	•	•	•	02	01	18	17	12	03	09	13	01	01	01	19			
III	9.6	7.6	9.3	8.8	-	059.8	86	63	81	77	26	102	020.0	22	•	•	13	•	•	02	01	•	26	16	15	03	03	14	•	•	01	01			
IV	9.3	8.5	8.5	9.3	-	06.7	83	63	81	76	33	059	011.0	23	•	•	01	•	•	01	•	25	18	12	01	18	•	•	•	•	•	•			
V	9.3	8.2	6.5	7.6	-	09.1	85	71	88	80	21	149	028.4	29	•	•	01	02	•	•	•	26	20	16	06	20	•	•	01	01	01	05			
VI	11.4	8.6	6.																																

1978

Mjesec	Vrijeme	Temperatura vazduha °C										Cestina pravaca i srednja jačina vетра m/s (0-12)																													
		Temperatura					Vjetar					N						NE						E			SE			S			SW			W			NW		
		7	14	21	Avg (D)	Max	Min	Max	Min	Max	Min	S.	J.	E.	J.	S.	J.	E.	J.	S.	J.	E.	S.	J.	E.	J.	S.	J.	E.	S.	J.	E.	J.	S.	J.	E.	J.	S.	J.	E.	
$\varphi = 44^{\circ}32' N \lambda = 17^{\circ}42' E$ Gr. $\Delta G = + 1h 11 min.$																																									
I	-	-01.8	02.3	-00.5	-00.2	03.1	-02.7	15.0	29	-09.6	09	10	01.1	15	01.1	12	01.0	04	01.0	15	01.0	31	01.2	01	01.0	01	03.0	04	.	.	.	02	01.5	01							
II	-	-02.5	02.9	-00.4	-00.1	03.7	-03.5	13.0	26	-18.6	21	04	01.5	14	01.1	15	01.1	06	01.3	20	01.0	22	01.2	.	.	02	01.5	01	.	.	02	01.5	01								
III	-	03.4	11.8	06.5	07.0	13.1	02.1	22.5	30	-03.2	13	04	01.0	13	01.0	08	01.1	03	01.0	20	01.1	32	01.3	02	01.5	01	01.0	10		
IV	-	06.1	13.8	08.8	09.4	15.2	04.9	25.0	30	01.4	07	02	01.0	03	01.7	19	01.5	03	01.3	11	01.3	37	01.7	04	03.0	11					
V	-	11.2	17.7	12.3	13.4	19.0	08.8	27.5	01	06.6	12	04	01.0	06	01.2	17	01.1	01	01.0	10	01.1	37	01.3	01	02.0	17						
VI	-	16.0	23.0	16.5	18.6	23.8	12.2	30.0	10.7	10.0	27	20	01	02.0	14	01.1	13	01.0	03	01.3	17	01.3	20	01.2	02	02.0	01	02.0	19		
VII	-	15.7	25.3	17.3	18.9	26.1	12.3	32.0	18	07.6	09	05	01.2	08	01.2	08	01.0	01	02.0	12	01.0	17	01.5	02	01.5	40						
VIII	-	15.3	25.2	17.1	18.7	26.0	12.4	33.5	07	06.2	13	04	01.0	04	01.5	10	01.0	.	.	22	01.1	18	01.4	35								
IX	-	11.4	21.1	13.7	15.0	21.8	09.3	32.0	11	-	-	08	01.0	05	01.0	15	01.2	06	01.8	13	01.0	23	01.2	02	02.0	18							
X	-	07.5	14.2	09.0	10.0	14.9	06.2	24.5	04	-01.6	28	03	01.0	11	01.0	13	01.0	03	01.0	27	01.0	16	01.2	02	01.0	01	01.0	17			
XI	-	01.3	03.8	01.9	02.2	04.1	00.7	14.5	01	-04.6	16	02	01.1	10	01.3	14	01.0	03	01.0	18	01.0	23	01.0	02	01.0	03	01.3	05			
XII	-	-00.3	04.8	01.4	01.8	09.8	-02.5	16.5	29	-12.4	06	04	01.0	12	01.5	25	01.2	06	01.2	21	01.2	23	01.2	.	.	.	01	01.0	01				
GOD.	-	06.9	13.8	08.6	09.5	14.7	05.0	33.5	07VM	-	-	61	01.2	115	01.1	169	01.1	39	01.3	206	01.1	299	01.3	18	01.8	10	01.5	178			
$\varphi = 44^{\circ}36' N \lambda = 17^{\circ}34' E$ Gr. $\Delta G = + 1h 11 min.$																																									
I	-	-01.7	03.0	-00.1	00.3	03.8	-03.3	15.2	29	-14.2	09	27	01.2	01	01.0	01	02.0	01	01.0	63				
II	-	-02.0	03.7	00.4	00.7	04.4	-03.2	16.6	26	-22.0	21	18	01.1	02	01.5	.	.	03	01.0	61						
III	-	02.2	12.0	06.4	06.7	13.4	00.7	22.0	30.0	-06.0	09	08	01.2	02	02.5	.	.	21	01.4	02	01.5	00	01.6	60					
IV	-	05.7	13.3	08.8	09.2	14.0	04.5	23.6	12	01.0	18	14	01.4	06	01.5	.	.	01	02.0	04	01.5	01	02.0	10	01.6	54							
V	-	09.7	18.0	12.6	18.9	07.7	27.8	01	-06.4	15	03	01.0	01	04.0	01	01.0	01	01.0	17	01.1	70							
VI	-	13.9	22.0	15.6	16.8	23.0	10.7	30.4	10	08.6	29	28	09	01.0	69									
VII	-	13.9	24.7	16.1	17.7	25.2	11.2	32.6	18	07.4	23	06	01.3	01	02.0	75											
VIII	-	13.3	24.5	16.9	17.9	25.1	10.6	32.6	07	07.6	20	16	01.1	01	02.0	14	01.9	62								
IX	-	09.9	20.1	13.8	14.4	20.8	08.0	30.4	11	00.0	21	08	01.0	04	01.2	.	.	02	01.5	76								
X	-	06.6	13.3	08.6	09.3	13.7	04.6	23.6	04	-05.0	29	18	01.3	03	01.0	.	.	03	01.0	72								
XI	-	01.1	04.4	01.7	02.2	05.0	00.2	14.0	26	-05.2	26	29	01.2	01	01.0	.	.	01	01.0	68								
XII	-	-00.6	05.0	02.0	02.1	05.0	-02.2	15.6	06	05.1	06	09	01.3	06	03.0	.	.	10	01.5	68									
GOD.	-	06.0	13.7	08.6	09.2	14.4	04.1	32.6	07VM	-22.0	24H	165	01.2	06	01.5	.	.	03	02.7	20	01.9	03	01.7	106	01.4	02	01.5	790			
$\varphi = 44^{\circ}13' N \lambda = 17^{\circ}54' E$ Gr. $\Delta G = + 1h 12 min.$																																									
I	-	-00.7	03.3	00.8	01.0	04.2	-01.7	16.4	29	-11.3	09	03	01.3	01	04.0	.	.	.	02	03.0	01	04.0	.	.	.	01	02.0	.	.	.	01	02.0	84								
II	-	00.1	04.5	01.3	01.9	05.2	-01.7	18.0	26	-10.4	20	01	01.0	06	01.2	01	01.0	09	01.7	08	01.2	.	.	.	04	01.5	07	01.3	48												
III	-	04.3	12.7	07.4	08.0	14.1	02.5	23.2	30	-02.0	23.0	09	13	01.9	06	01.7	.	.	11	01.7	05	01.2	.	.	.	01	01.0	22	01.5	35											
IV	-	07.2	14.2	07.4	10.1	15.6	05.6	25.8	30	02.8	07	01	04.0	04	02.2	.	.	13	02.1	07	01.9	08	01.9	04	02.2	46															
V	-	11.5	18.0	12.7	13.7	19.2	09.2	29.0	01	00.6	13	05	02.0	03	01.7	01	02.0	11	02.7	10	01.4	01	01.0	06	01.3	05	01.8	51													
VI	-	19.5	22.5	17.0	17.9	23.8	12.5	30.0	10	08.6	30	03	01.3	05	01.4	01	01.0	13	01.7	10	01.2	03	01.3	04	02.0	11	01.4	43													
VII	-	15.3	25.3	17.5	18.9	26.4	12.6	32.8	18	07.8	24	11	01.7																												

Mjesec	Oblačnost Nm (0-10)			Inzolačija Broj sati	Vlažnost vazduha			Padavine R mm		Broj dana na sat																					
					%	U	m			T	N	Tx	Tn	Tx	Tn	P(0-12)	Nm(0-10)	R mm	•	*	*	Δ	▲	■	□						
	7	14	21	Sred. (Dnev.)		mm	7	14	21	Σ Sred. (Dnev.)	Min	Σ	Max	Dat.	≤	<	<	≥	≥	IV	IV	<	>	IV	IV	IV	IV				
BR. ST. 116																															
PRNJAVOR																															
I	8.9	8.5	7.5	8.3	-	04.1	91	83	90	88	49	086	037.0	26	.	03	20	.	.	.	01	20	14	11	02	08	03				
II	8.0	7.9	6.5	7.5	-	13.9	79	81	83	81	33	105	021.0	20	04	03	22	.	.	.	03	16	15	14	03	18	11	01			
III	7.6	6.6	5.3	6.4	-	25.5	80	63	74	73	38	067	014.5	22	.	04	.	.	.	06	12	12	12	04	12	02	02				
IV	9.0	7.4	5.2	7.2	-	06.1	78	58	73	69	33	061	015.5	27	.	01	.	.	.	10	18	18	20	18	.	.	01				
V	7.6	7.4	6.5	7.2	-	18.4	78	60	75	71	30	150	031.0	29	.	.	02	.	.	.	01	12	20	19	05	20	.	.			
VI	5.5	5.2	5.4	5.4	-	10.1	76	51	69	66	24	119	030.0	14	.	.	16	03	.	.	02	07	14	14	03	14	.	.			
VII	3.9	3.7	3.6	3.7	-	11.0	83	48	73	67	31	084	033.0	08	.	.	21	03	.	.	27	02	07	07	03	37	.	.			
VIII	5.3	4.3	4.1	4.5	-	10.9	82	49	72	68	29	046	027.0	31	.	.	20	06	01	.	09	08	07	07	01	27	.	.			
IX	6.4	5.2	4.6	5.4	-	19.4	83	52	74	70	34	124	029.0	13	.	.	05	01	.	.	05	08	09	09	06	39	.	.			
X	9.4	8.6	6.0	7.4	-	07.6	89	73	81	80	53	038	021.5	05	.	04	.	.	.	15	08	08	01	08	.	07	.				
XI	9.0	9.6	9.7	9.8	-	34.6	87	84	84	85	51	032	039.0	28	.	14	.	.	.	28	34	33	.	34	32	01	.				
XII	8.0	7.3	6.7	7.3	-	04.3	79	74	82	78	39	078	014.5	14	01	06	20	.	.	.	04	14	11	11	04	09	02	.			
GOD.	7.5	6.6	5.9	6.7	-	17.1	81	64	77	74	20	987	037.0	26.1	05	12	84	65	13	01	.	38	152	136	133	32	124	20	04		
BR. ST. 117																															
TESLIC																															
I	8.2	7.2	7.7	7.7	-	04.6	94	90	94	93	66	971	016.6	26	04	06	23	.	.	.	04	21	16	13	03	11	06	.			
II	8.0	8.0	7.9	8.0	-	14.6	91	88	92	90	56	073	015.6	13	04	07	23	.	.	.	02	16	14	13	03	13	13	.			
III	6.1	6.4	7.3	6.6	-	16.5	94	75	89	65	38	074	015.8	22	.	11	.	.	.	04	12	18	19	03	18	04	02	.			
IV	8.0	7.2	6.1	7.1	-	17.7	94	78	91	87	37	042	039.6	06	.	.	11	.	.	.	01	14	16	11	16	.	.	.			
V	7.1	7.3	6.9	7.1	-	10.6	93	78	93	85	53	192	052.2	03	.	.	01	02	.	.	01	12	21	18	07	21	.	.			
VI	5.0	6.1	4.9	5.3	-	12.2	92	70	92	85	40	146	052.6	22	.	.	14	02	.	.	05	08	10	07	04	10	.	.			
VII	3.5	5.5	2.2	3.7	-	12.9	93	64	82	83	30	084	028.4	16	.	.	17	01	.	.	07	02	07	06	05	37	.	.			
VIII	4.6	5.1	3.1	4.3	-	12.3	91	63	89	80	24	040	025.8	31	.	.	16	04	.	.	09	05	05	04	01	35	.	.			
IX	5.4	5.6	4.7	5.7	-	10.7	93	73	92	85	41	187	036.8	28	.	.	04	01	.	.	07	08	11	08	07	11	.	.			
X	7.4	7.0	6.5	7.0	-	07.8	92	73	82	86	53	033	024.6	22	.	05	.	.	.	03	17	09	08	01	09	.	.				
XI	9.0	8.0	8.0	8.3	-	05.1	94	88	93	92	66	032	013.6	28	.	17	.	.	.	02	23	07	03	02	05	03	.	.			
XII	5.8	6.0	5.0	5.6	-	14.9	87	87	85	87	-	075	020.4	19	03	06	22	.	.	01	06	10	10	09	03	09	02	01			
GOD.	6.5	6.6	5.8	6.3	-	08.3	92	76	91	85	-	1049	052.6	22.VI	11	19	102	53	08	.	01	51	148	144	109	39	125	28	03		
BR. ST. 118																															
ZENICA																															
I	7.7	6.7	6.8	7.1	-	054.9	94.1	87	72	85	81	064	023.4	30	06	05	24	.	.	.	02	16	18	10	02	11	09	02			
II	9.1	8.4	7.5	8.3	-	037.8	04.3	88	71	83	81	073	015.6	13	02	03	22	.	.	.	01	21	19	11	02	16	15	.			
III	5.8	7.1	5.5	6.1	-	125.1	75.1	86	52	72	27	062	020.9	18	.	0.	10	.	.	.	01	36	11	18	01	18	05	01			
IV	7.8	8.4	7.2	7.8	-	096.2	08.4	84	57	76	23	078	012.4	06	.	.	10	.	.	.	32	.	16	21	02	21	01	01			
V	8.0	8.2	6.3	7.5	-	110.1	08.6	87	58	85	77	181	026.8	14	.	.	01	02	.	.	.	15	23	16	08	23	.	.			
VI	6.2	6.7	4.6	5.8	-	19.9	10.5	84	54	80	73	139	027.7	28	.	.	16	03	.	.	.	03	38	16	14	16	16	16	.		
VII	4.4	4.6	3.7	4.3	-	259.9	11.1	86	44	82	70	054	015.9	06	.	.	24	03	.	.	.	07	02	06	05	03	36	.	.		
VIII	4.7	4.8	3.3	4.3	-	238.6	10.8	87	45	79	28	032	012.7	31	.	.	18	07	.	.	.	31	12	33	08	05	01	38	.		
IX	7.6	6.1	4.5	6.1	-	145.1	09.4	95	57	91	81	21	194	038.2	01	.	.	35	03	11	13	10	07	13	.	.	
X	8.1	6.1	5.9	6.7	-	096.0	07.7	93	63	87	81	29	031	037.4	02	.	04	01	.	.	.	02	13	09	08	03	35	.	.		
XI	9.8	7.1	7.5	8.1	-	118.8	24.5	88	75	87	83	55	012	008.2	28	.	20	01	16	04	03	32	03	03	.		
XII	8.4	7.2	6.7	7.4	-	050.6	04.5	88	74	85	82	39	091	026.5	14	02	06	20	.	.	01	02	18	13	09	03	12	04	.		
GOD.	7.3	6.8	5.8	6.6	-	1428.0	07.2	87	60	82	76	21	1011	038.2	0.0.IX	10	14	101	64	13	07	.	39	150	168	117	35	145	37	03	01
DOBOJ																															
I	8.3	7.6	6.9	7.6	-	139.8	04.6	94	86	91	90	50	029	007.6	31	01	04	21	.	.	.	01	19	13	10	01	09	04	.	.	
II	8.5	8.4	6.5	7.8	-	135.3	04.9	95	83	92	90	54	087	021.2	13	02	04	18	.	.	.	01	15	16	11	03	07	12	.	.	
III	6.9	6.6	5.6	6.4	-	110.3	03.6	93	62	83	79	31	084	011.0	22	.	07	.	.	.	01	34	11	15	13	02	15	31	01	.	
IV	7.0	7.4	5.6	6.7	-	083.3	07.3	91	63	83	79	28	037	009.6	09	.	.	01	01	.	.	.	01	11	17	11	01	17	.	.	
V	7.5	8.0	5.4	7.0	-	108.3	10.0	93	67	89	83	37	123	031.0	03	.	.	01	12	19	15	03	19	.	.	.	
VI	5.2	6.1	4.0	5.1	-	151.8	12.1	91	61	84	79	41	098	024.8	28	.	.	16	02	.	.	.	13	07	15	11	04	15	.	.	
VII	3.6	4.1	1.7	3.1	-	217.6	12.9	94	55	87	80	36	069	018.8	08	.	0.	22	03	.	.	.	12	07	07	03	07	07	.	.	
VIII	4.1	4.2	3.5	3.9	-	192.1	12.4	92	54	83	77	37	020	011.0	05	.	.	20	07	01	.	.	11	06	07	04	01	07	.		

Sesija	Vreme dneva mesta	Temperatura vazduha °C								Čestina pravaca i srednja jačina vjetra mD, fm (0-12)																										
		fm				fm				fm						fm																				
		7	14	21	Sred. (fm)	7	14	21	Sred. (fm)	fm	fm	fm	fm	fm	fm	M	NE	E	SE	S	SW	W	NW	C												
$\varphi = 44^{\circ}11' N \lambda = 18^{\circ}22' E$ Gr. $\Delta G = + 1h 14 min.$																																				
I	-	-05.5	-01.1	-04.0	-03.7	00.5	-07.4	07.2	12	-20.0	09	13	01.2	07	01.7	02	02.0	01	01.0	01	04.0	07	03.6	07	01.6	14	01.9	41								
II	-	-04.9	00.5	-03.0	-02.6	01.8	-06.3	12.5	25	-23.0	21	10	01.6	-	-	-	-	-	-	-	-	07	01.6	11	02.0	02	01.1	01.0	02.0							
III	-	-00.2	05.3	00.9	01.7	06.3	-	17.8	31	-	15	01.3	-	-	-	01	01.0	-	-	-	-	02	03.0	09	01.8	66	01.8	01.8	01.8	01.8	01.8					
IV	-	03.6	08.1	04.1	05.0	09.5	-	18.6	30	-	11	01.5	02	02.5	02	03.5	-	-	-	-	-	04	01.0	04	02.5	07	01.7	01.7	01.7	01.7	01.7					
V	-	08.1	13.3	06.9	08.8	15.2	04.9	23.2	05	-02.6	12	11	01.9	02	02.0	-	-	-	-	-	-	-	05	01.0	03	02.0	02	01.0	01.0	01.0	01.0	01.0				
VI	-	11.9	18.4	11.3	13.2	20.1	08.7	29.6	12	03.0	28	13	01.1	-	-	-	-	-	-	-	-	03	01.3	06	01.8	68	01.8	01.8	01.8	01.8	01.8					
VII	-	13.9	20.3	13.7	15.4	21.6	09.6	29.6	19	06.4	24.0	10	01.3	-	-	-	-	-	-	-	-	04	01.0	03	01.3	76	01.3	01.3	01.3	01.3	01.3					
VIII	-	12.9	19.6	13.4	14.9	21.3	10.6	27.0	07.0	03.0	31	13	01.1	-	01	01.0	-	-	-	-	-	02	01.0	05	01.4	72	01.4	01.4	01.4	01.4	01.4					
IX	-	07.5	14.8	09.4	10.3	17.0	05.6	26.8	26	01.8	13	14	01.3	-	-	-	-	-	-	-	-	09	01.2	05	01.6	62	01.6	01.6	01.6	01.6	01.6					
X	-	03.8	10.9	05.7	06.5	12.1	02.3	19.4	08	-06.2	29	12	01.2	-	-	-	-	-	-	-	-	05	01.0	03	02.0	73	01.0	01.0	01.0	01.0	01.0					
XI	-	-02.4	06.4	-01.7	00.1	07.8	-04.5	12.4	11	-10.0	15.4	16	01.3	-	-	-	-	-	-	-	-	05	01.2	05	01.4	66	01.4	01.4	01.4	01.4	01.4					
XII	-	-02.0	02.8	-00.8	-00.2	04.4	-04.0	10.2	29	-16.2	06	18	02.1	-	-	-	-	-	-	-	-	01	03.0	07	01.9	14	02.6	02.6	02.6	02.6	02.6					
GOD.	-	03.9	10.0	04.7	05.8	11.5	-	29.6	12.VI	-	154	01.4	11	01.9	05	02.4	02	01.0	01	04.0	08	03.5	60	01.4	82	02.0	772	02.0	02.0	02.0	02.0	02.0				
$\varphi = 44^{\circ}19' N \lambda = 18^{\circ}26' E$ Gr. $\Delta G = + 1h 14 min.$																																				
I	-	-01.0	03.1	00.0	00.4	04.8	-02.7	16.4	29	-12.0	09	03	01.0	03	01.7	19	01.8	10	03.1	02	02.5	-	-	-	21	01.2	35	01.0	01.0	01.0						
II	-	-00.3	04.5	01.0	01.5	01.5	05.9	-02.1	18.5	25	-19.6	21	-	-	15	01.5	14	01.4	01	03.0	-	-	-	30	01.0	01.0	01.0	01.0	01.0							
III	-	03.4	11.2	05.0	06.2	12.7	01.4	22.0	04	-03.4	23.13	03	01.0	01	02.0	32	01.3	03	03.2	-	-	-	01	01.0	19	01.1	66	01.1	01.1	01.1	01.1	01.1				
IV	-	07.0	12.9	08.1	09.0	14.5	04.9	23.5	30	01.0	07	-	02	01.5	14	01.1	04	04.5	06	03.8	-	-	-	20	01.1	01.1	01.1	01.1	01.1							
V	-	11.4	16.7	10.7	12.4	18.3	08.3	29.0	01	-01.2	13	01	01.0	02	01.5	21	01.2	03	02.0	04	03.8	-	-	-	03	01.0	18	01.2	41	01.2	01.2	01.2	01.2	01.2		
VI	-	15.0	20.7	14.3	16.1	22.9	11.2	30.5	12.10	07.6	27	01	02.0	-	24	1.3	03	04.0	-	-	01	02.0	06	01.0	12	01.2	01.2	01.2	01.2	01.2						
VII	-	16.0	24.3	15.3	17.8	25.5	11.6	31.5	18	06.2	24.23	02	01.0	01	01.0	21	01.2	04	01.2	-	-	-	06	01.0	23	01.5	36	01.5	01.5	01.5	01.5	01.5				
VIII	-	15.4	24.0	15.3	17.5	25.3	11.6	34.0	07	07.0	20	-	-	04	02.0	17	01.2	02	02.0	01	01.0	-	-	09	01.0	16	01.1	44	01.1	01.1	01.1	01.1	01.1			
IX	-	11.0	18.4	12.0	13.3	19.6	08.5	27.2	11	01.0	21	10	01.3	05	01.6	05	01.8	01	04.0	07	01.6	-	-	-	10	06.6	02	02.0	02.0	02.0	02.0	02.0				
X	-	07.2	13.7	08.2	09.3	14.5	08.1	24.2	03	-02.0	29	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-					
XI	-	00.7	04.0	01.1	01.6	04.6	-	11.5	01	-	15	01.4	06	01.8	06	02.0	32	01.5	-	-	03	01.3	01	01.0	59	01.0	01.0	01.0	01.0	01.0	01.0					
XII	-	00.9	05.1	01.7	02.3	06.1	-	16.0	29	-	05	01.4	01	02.0	18	02.3	05	02.0	05	01.6	08	02.9	03	01.7	-	-	-	-	-	-	-	-	-			
GOD.	-	07.2	13.2	07.7	09.0	14.5	-	34.5	07.VII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
$\varphi = 44^{\circ}33' N \lambda = 18^{\circ}42' E$ Gr. $\Delta G = + 1h 15 min.$																																				
I	-	733.2	-01.6	03.3	00.0	00.4	04.8	-02.7	16.4	29	-13.5	09	01	05.0	12	01.6	02	02.5	03	03.3	01	01.0	-	-	11	01.3	06	01.7	57	01.7	01.7	01.7	01.7	01.7		
II	731.2	-00.9	04.7	01.3	01.6	06.2	-02.2	18.7	26	-12.7	22	02	01.5	09	01.2	04	01.2	03	02.0	01	02.0	03	02.0	08	01.1	01	01.3	47	01.3	01.3	01.3	01.3	01.3			
III	730.7	02.8	11.7	06.2	06.7	13.5	01.7	23.4	04	-03.8	09	03	02.7	17	01.4	04	01.5	02	01.5	03	01.7	03	01.3	01	01.7	15	02.0	02	02.0	02	02.0	02	02.0			
IV	730.7	06.8	13.1	08.7	09.3	15.1	05.1	25.0	30	02.0	07.0	03	01.7	13	01.8	03	01.3	09	02.7	02	02.0	01	02.0	11	02.2	08	02.2	40	02.2	02	02.2	02	02.2	02	02.2	
V	733.6	10.9	16.4	12.6	19.0	08.2	29.4	01	-08.9	13	04	01.5	07	01.3	02	02.0	03	01.0	02	02.5	02	02.0	08	01.4	09	01.8	56	01.8	01.8	01.8	01.8	01.8	01.8			
VI	734.6	14.9	21.3	15.7	16.9	23.4	11.4	30.0	10	08.2	27	05	01.0	11	01.5	02	01.5	03	01.0	02	01.5	-	-	03	01.7	11	01.6	11	01.2	44	01.2	01.2	01.2	01.2	01.2	01.2
VII	736.1	15.2	24.3	16.2	18.0	25.8	11.8	32.4	18	06.7	23	01	01.0	07	01.0	01	01.0	06	01.0	02	01.5	-	-	07	01.9	04	02.0	65	02.0	02.0	02.0	02.0	02.0	02.0		
VIII	736.7	14.4	24.1	17.0	17.7	25.9	11.7	34.1	07	07.8	20	03	01.0	03	01.0	02	01.0	10	01.3	03	01.0	01	07.0	04	01.0	08	01.1	09	01.0	05	01.0	05	01.0	05	01.0	05
IX	736.0	10.2	19.1	11.9	13.3	20.6	08.6	29.6	11	03.2	21	03	01.0	12	01.2	02	01.5	02	01.5	03	01.3	03	10	01.3	09	01.8	47	01.8	01.8	01.8	01.8	01.8	01.8			
X	739.7	04.6	13.8	08.7	09.5	15.1	05.5	25.3	03	-04.6	29	-	09	01.3	03	01.7	05	01.4	01	04.0	01	02.0	11	01.3	01	01.3	31	01.3	01	01.3	01	01.3	01	01.3		
XI	736.0	00.5	04.0	01.5	01.9	05.1	-00.1	15.4	26	-08.4	16	01	02.0	03	01.0	01	01.0	07	01.1	01	01.0	-	-	10	01.6	01	01.0	66	01.0	01	01.0	01	01.0	01	01.0	
XII	733.0	00.2	01.1	02.8	02.5	05.9	-01.9	16.7	29	-10.6	06	03	02.8	-	14	01.9	03	02.3	21	02.6	-	-	25	01.9	-	-	41	01.9	-	-	41	01.9	-	-		
GOD.	733.4	06.7	13.4	08.3	09.2	15.1	04.8	34.1	07.VII	-	59	02.2	08	02.2	176	01.8	13	02.1	41	02.9	11	02.4	378	01.8	41	03.0	368	03.0	03.0	03.0	03.0	03.0	03.0			
$\varphi = 44^{\circ}33' N \lambda = 18^{\circ}50' E$ Gr. $\Delta G = + 1h 15 min.$																																				
I	-	-00.9	03.3	00.2	00.7	-	-	-	-	15	02.5	-	-																							

Mjesec	Oblačnost Nm (0-10)			Vlažnost vazduha %	Padavine R mm	Broj dana na sat												•	*	*	Δ	▲	▲	R					
						U m t			Tn	Tx	Tn	Tx	Tn	F(0-12)	Nm (0-10)	R mm	•	*	*	Δ	▲	▲	R						
	7	14	21	Sred. (Dnev.)	Inovacije broj sati	mm	7	14	21	Min	Σ	M	Dat.	=	<	<	IV												
PONIKVE																													
BR. ST. 121																													
I	6.5	5.8	5.8	6.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-							
II	7.3	6.6	5.8	6.4	-	-	-	-	-	164	030.2	14	06	13	23	-	-	-	-	-	-	-	-						
III	6.6	5.6	5.6	6.0	-	34.9	94	86	91	90	44	122	017.9	18	-	02	-	-	-	-	-	-	-						
IV	7.2	7.7	6.7	7.0	-	66.3	92	91	91	91	61	125	029.4	09	-	-	-	-	-	-	-	-	-						
V	7.1	6.6	7.3	7.0	-	88.3	92	89	91	91	74	217	049.2	30	-	02	01	-	-	03	15	21	21	08	19	02			
VI	4.1	4.1	4.8	4.3	-	10.5	88	81	92	87	54	211	046.2	28	-	04	-	-	-	07	07	16	15	07	16	-			
VII	2.5	2.1	3.1	2.6	-	10.6	90	59	89	79	40	360	019.4	16	-	05	-	-	-	18	04	36	06	03	06	-			
VIII	3.4	3.8	3.8	3.7	-	11.1	92	70	91	86	51	067	024.8	31	-	07	-	-	-	12	04	08	08	02	08	-			
IX	5.0	4.2	4.8	4.7	-	-	-	-	-	-	180	044.0	01	-	-	02	-	-	-	11	07	11	11	07	11	01			
X	6.6	4.9	5.8	5.6	-	66.7	94	80	93	89	61	046	014.2	28	-	07	-	-	-	08	13	12	12	01	11	02			
XI	5.1	4.2	4.7	4.7	-	34.7	89	-	91	88	70	130	032.4	30	02	03	24	-	-	14	11	04	04	01	01	03			
XII	7.7	6.0	6.6	6.8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	03	14	14	14	05	08	07				
GOD.	5.7	5.0	5.5	5.4	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-					
MACA																													
BR. ST. 122																													
I	5.9	6.4	6.4	6.2	-	34.3	88	80	88	86	48	069	016.0	30	04	04	23	-	-	08	16	15	11	03	07	11	03		
II	6.8	7.8	6.9	7.2	-	34.6	88	81	90	86	50	106	023.0	14	01	04	18	-	-	08	16	17	16	03	07	14	01		
III	6.6	6.6	5.4	5.8	-	55.3	84	59	84	75	29	103	018.8	22	-	07	-	-	-	01	08	14	17	15	04	17	04		
IV	6.9	7.7	6.6	7.1	-	66.6	83	63	84	77	28	062	016.0	06	-	-	01	-	-	03	13	17	15	01	17	-			
V	6.9	8.2	6.2	7.1	-	39.1	85	68	92	82	30	223	045.5	03	-	02	01	-	-	14	20	18	09	20	-	-			
VI	4.7	6.4	4.7	5.3	-	11.2	85	65	92	81	38	208	047.2	18	-	08	14	02	-	01	08	10	17	14	06	17	-		
VII	2.6	3.8	2.6	3.0	-	11.9	84	54	91	76	32	079	019.0	22	-	08	19	03	-	11	01	07	06	04	07	-			
VIII	2.8	4.4	3.3	3.5	-	11.2	82	53	88	74	23	042	016.8	31	-	08	16	04	-	-	14	03	09	06	01	09	-		
IX	5.5	5.6	4.7	5.2	-	09.7	90	66	90	82	46	217	042.7	01	-	-	03	-	-	06	07	11	10	08	11	-			
X	7.7	6.3	6.0	6.7	-	88.1	94	76	94	88	46	028	005.7	21	-	04	-	-	-	04	15	10	09	10	-	-			
XI	6.4	5.8	6.7	6.3	-	34.7	90	84	90	86	69	027	017.0	30	-	-	-	-	-	08	14	03	03	01	03	-			
XII	8.3	6.9	6.4	7.2	-	34.8	88	74	90	84	35	110	023.0	10	-	05	-	-	-	01	01	14	10	09	05	08	02		
GOD.	5.9	6.3	5.5	5.9	-	07.6	86	68	89	81	25	1274	047.2	28.VI	-	13	-	53	09	-	06	71	137	153	132	45	140	36	
TUZLA																													
BR. ST. 123																													
I	6.9	6.6	6.4	6.6	073.5	04.2	90	79	89	86	41	047	019.5	26	04	05	23	-	-	01	04	12	19	11	01	11	09		
II	8.2	8.5	6.9	7.8	060.4	034.5	90	76	88	85	46	069	018.2	13	03	04	19	-	-	04	16	12	04	06	14	-	01		
III	6.5	6.7	5.8	6.3	134.5	54.5	90	55	81	75	31	077	012.7	18	-	-	-	-	-	01	04	10	20	14	02	19	06		
IV	7.5	8.0	6.7	7.6	111.4	06.9	88	64	83	78	32	061	012.7	09	-	-	01	-	-	05	12	18	12	02	18	-	04		
V	8.0	8.6	6.6	7.8	118.4	09.5	91	72	91	85	24	178	055.8	03	-	01	01	-	-	01	17	22	19	06	22	-	01		
VI	5.9	7.3	5.9	6.4	189.7	11.1	80	64	87	80	35	162	033.0	28	-	-	15	01	-	-	07	17	12	06	17	-	02		
VII	2.7	4.2	3.0	3.3	280.9	12.3	90	56	90	79	39	076	024.2	08	-	-	20	03	-	01	10	01	05	05	04	-	04		
VIII	3.9	4.8	3.2	4.0	237.4	11.4	89	53	84	75	30	032	013.0	31	-	-	18	05	01	02	09	03	10	06	01	10	-		
IX	5.9	6.0	4.9	5.6	151.6	09.6	96	59	94	83	36	151	030.7	01	-	-	04	-	-	07	09	13	10	05	13	-	03		
X	6.9	7.0	6.0	6.6	100.2	28.1	96	73	93	88	44	008	002.4	22	-	04	01	-	-	04	16	12	04	12	-	-	12		
XI	9.6	7.4	7.7	8.2	322.0	04.8	96	82	92	80	40	013	036.6	30	-	-	08	01	-	01	21	07	03	04	04	03	-	10	
XII	7.0	7.2	7.8	7.3	93.6	06.4	97.0	75	88	84	46	079	018.1	15	01	05	21	-	-	01	17	12	09	04	10	02	01		
GOD.	6.6	7.0	5.9	6.5	1546.6	07.8	91	67	88	82	24	973	055.8	03.V	-	-	-	-	-	-	13	-	42	133	114	110	31	100	23
BRČKO																													
I	6.7	7.2	7.3	7.1	-	044	015.3	-	-	-	-	-	-	-	-	-	03	-	01	14	10	09	01	08	03	01	-		
II	8.0	7.7	8.1	8.3	-	34.3	83	81	87	83	42	137	032.8	20	05	06	20	-	-	01	17	13	10	05	04	12	-		
III	5.3	5.6	5.7	5.5	-	05.8	82	56	77	72	27	065	010.5	18	-	-	03	-	-	05	04	06	15	15	01	15	04		
IV	7.0	6.8	5.9	6.6	-	66.7	79	57	74	70	24	056	011.2	09	-	-	01	01	-	-	02	10	13	13	01	13	-		
V	7.1	6.5	7.3	7.0	-	05.5	79	65	81	75	40	123	034.1	03	-	01	-	-	-	10	13	13	05	13	-	-	01		
VI	6.2	4.8	5.4	5.5	-	12.4	83	59	85	76	32	137	032.0	28	-	-	17	03	-	01	08	12	12	06	17	-	03		
VII	2.9	3.8	3.0	3.3	-	12.7	79	51	85	72	34	077	029.7	08	-	-	22	03	-	02	11	33	08	08	04	08	-	02	
VIII	3.0	4.4	4.1	4.4	-	12.3	80	67	82	71	33	025	010.0	31	-	-	16	04	-	01	09	04	04	01	04	-	-		
IX	5.2	4.8	5.6	5.2	-	10.4	83	60	84	76	35	111	026.6	13	-	-	05	01	-	-	09	08	09	05	09	19	-	01	
X	7.7	6.1	4.7	6.2	-	07.9	88	65	87	80	44	013	006.0	22	-	04	01	-	-	02	11	03	03	03	33	-	10		
XI	9.6	8.0	8.5	8.9	-	34.8	82	88	85	80	60	017	097.4	30	-	-	10	0	-	-	27	04	04	32	03	-	-	13	
XII	7.0	7.2	7.2	7.1	-	04.7																							

Mesec	Vremenska redoslijed red. n.	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta nD, fm (0-12)																	
		Temperatura			Vetar			Vremenski				Pravac						Jačina											
		7	14	21	Sred. (pozic.)	NW	NE	SW	SE	Dan.	Mes.	Dan.	N	NE	E	SE	S	SW	W	NW	C								
$\varphi = 44^{\circ}47' N \lambda = 19^{\circ}16' E$ Gr. $\Delta G = + 1h 17 min.$																													
I	-00.9	03.6	00.2	00.8	04.5	-02.2	13.0	13	-11.3	09	04	01.8	.	09	01.7	02	03.0	13	01.5	17	32.4	04	01.2	25	01.5	19			
II	-01.3	03.8	00.2	00.8	05.1	-03.3	17.7	28	-17.7	21	02	01.0	01	01.3	09	01.0	03	02.3	08	01.1	06	01.2	04	01.2	31	01.5	20		
III	-04.1	12.2	07.0	07.6	13.6	02.6	21.1	30	-02.2	23.13	02	02.5	02	01.5	07	01.3	02	01.0	11	01.2	15	01.3	04	01.2	31	01.6	19		
IV	-07.7	14.8	09.6	10.4	16.3	05.6	24.5	30	00.3	07	02	01.0	02	01.0	06	01.0	.	09	01.6	12	01.5	12	01.5	25	01.6	22			
V	-12.3	18.6	13.3	14.4	20.1	09.6	28.6	01	00.2	13	.	01	01.0	05	01.2	06	01.5	06	01.2	04	01.5	17	01.4	34	01.7	20			
VI	-16.2	22.9	16.8	18.1	24.5	13.2	31.3	10	05.4	27	02	01.0	01	01.3	03	02.0	15	01.3	06	01.2	07	01.4	32	01.6	19				
VII	-16.6	26.2	17.7	19.6	26.9	13.5	32.6	18	06.4	24	01	01.0	.	09	01.1	05	01.0	09	01.1	12	01.4	07	01.3	30	01.3	20			
VIII	-15.2	25.9	17.2	18.9	27.1	13.4	34.6	07	00.2	20	05	01.0	03	01.3	09	01.3	05	01.2	04	01.2	10	01.5	05	01.4	35	01.3	17		
IX	-12.0	20.6	13.1	14.7	21.7	10.2	29.5	11	04.4	21	03	01.7	01	01.0	02	01.0	01	01.4	05	01.4	10	01.6	42	01.6	21				
X	-07.1	15.4	08.8	10.0	16.4	05.3	26.0	04	-03.4	29	02	01.5	01	02.0	02	01.0	03	01.0	06	01.2	15	01.3	36	01.2	23				
XI	-01.6	03.8	02.1	02.4	04.5	01.0	13.5	01	-02.6	16	04	01.0	08	01.0	12	01.1	04	01.0	01	01.0	07	01.1	06	01.7	17	01.3	31		
XII	-00.9	05.3	01.8	02.4	06.3	-01.4	17.7	29	-08.8	06	01	01.0	01	01.0	08	01.4	03	01.7	14	01.2	15	01.4	02	01.5	17	01.2	32		
GOD.	-	07.6	14.4	09.0	10.0	15.6	05.6	34.6	07.VII -17.7	24.II	28	01.3	21	01.1	84	01.2	38	01.4	98	01.3	115	01.5	93	01.4	355	01.5	263		
$\varphi = 43^{\circ}50' N \lambda = 17^{\circ}01' E$ Gr. $\Delta G = + 1h 08 min.$																													
I	696.7	-01.1	03.3	00.1	00.6	04.5	-03.2	11.2	14	-13.1	09	11	02.6	02	03.5	67	02.0	20	02.6	04	01.5	03	01.7	01	01.0	04	02.2	41	
II	693.0	-00.4	04.0	01.1	01.5	05.5	-02.4	11.2	11	-10.0	02	14	02.9	02	02.0	16	02.3	11	02.5	01	01.0	06	01.7	05	01.4	03	02.0	26	
III	696.6	01.1	08.4	04.1	06.4	10.0	-03.3	17.4	03	-05.5	13	17	03.2	02	01.0	08	02.5	12	02.0	02	01.5	06	01.8	06	01.8	06	01.8	34	
IV	693.7	05.7	10.4	06.9	07.5	11.4	03.8	17.4	30	-01.4	19	13	02.9	09	02.4	16	02.9	07	02.1	01	02.0	04	02.2	06	02.0	05	01.8	29	
V	697.2	09.8	14.4	10.0	11.0	15.9	06.5	20.8	20	-01.8	13	05	02.8	14	02.1	14	02.6	05	01.8	02	02.5	06	01.5	04	02.0	06	02.2	37	
VI	698.7	13.8	20.4	14.1	15.6	21.8	09.5	26.4	11	03.7	30	05	02.4	01	01.0	08	02.0	37	02.4	06	02.0	19	02.0	08	01.9	.	.	45	
VII	700.0	14.1	23.5	17.6	24.3	09.0	28.9	18.13	13.7	07	09	13	02.2	02	02.0	07	02.7	02	03.5	09	01.8	07	02.0	05	02.0	01	03.0	47	
VIII	700.4	12.5	23.4	15.5	16.7	24.6	08.6	30.3	07	04.4	13	04	02.0	05	01.8	04	02.0	02	02.0	05	02.4	09	01.9	11	01.8	03	01.7	50	
IX	699.8	09.1	18.3	11.2	12.4	19.8	06.4	26.4	11	02.3	18	15	02.6	03	01.7	04	01.8	03	02.0	03	01.3	02	02.0	10	01.7	10	01.7	40	
X	701.7	05.2	15.1	07.8	09.0	16.3	03.7	23.6	11	-02.2	25.23	11	02.5	03	02.3	13	02.4	08	02.2	04	02.5	05	01.4	11	01.5	03	01.7	42	
XI	704.3	-04.0	11.1	00.3	01.9	12.2	-05.0	14.8	15	-05.3	16	05	02.0	02	03.5	04	01.8	04	01.8	01	01.0	.	.	06	01.5	03	02.3	45	
XII	695.8	-01.1	04.9	01.0	01.5	05.9	-03.1	12.5	19	-17.8	07	03	02.7	.	.	10	02.2	14	02.1	02	02.5	03	01.0	05	02.2	01	02.0	55	
GOD.	-	698.1	05.4	13.1	07.4	08.3	14.4	02.0	30.3	07.VM -17.8	07.XII 116	02.7	45	02.2	104	02.4	95	02.3	43	01.9	61	01.8	78	01.8	45	01.9	511		
$\varphi = 43^{\circ}34' N \lambda = 17^{\circ}27' E$ Gr. $\Delta G = + 1h 10 min.$																													
I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	41		
II	-	-00.3	02.7	00.6	00.9	-	27	04.7	02	05.5	06	02.5	01	02.0	19	03.3	01	01.0	01	01.0	.	.	.	27	
III	-	01.8	07.4	03.3	03.9	08.1	00.1	16.4	03	-04.0	26	10	03.1	.	05	02.8	01	03.0	14	01.7	01	01.0	12	02.2	04	02.8	46		
IV	-	05.6	14.7	06.1	06.6	09.6	15.0	21.2	30	-01.0	21	20	03.1	05	04.2	07	01.7	01	04.0	01	01.0	03	01.7	.	.	.	39		
V	-	09.1	12.6	09.0	10.0	13.8	06.0	19.0	31.21	-01.0	13.12	15	03.5	03	04.0	07	01.4	03	03.0	11	02.5	51		
VI	-	14.4	19.0	13.4	15.0	20.2	09.9	24.8	11	06.4	28	08	03.5	01	01.0	08	01.9	04	02.8	01	03.0	01	02.0	09	01.7	03	01.3	55	
VII	-	15.9	21.8	15.5	17.2	22.7	11.1	28.4	13	07.0	10	14	02.9	03	03.7	08	01.4	04	03.2	02	03.0	03	01.3	08	01.0	02	01.0	49	
VIII	-	15.0	22.3	15.4	17.0	23.4	10.8	29.0	03	03.6	31	14	02.4	09	02.8	08	02.5	.	01	04.0	02	01.0	09	01.0	01	01.0	49		
IX	-	10.3	16.7	11.4	12.5	18.0	07.2	24.8	26	02.8	30	15	03.3	08	03.8	03	01.3	01	02.0	05	02.2	.	.	.	12	01.3	07	01.9	39
X	-	07.8	13.6	08.8	09.7	14.9	05.4	22.4	21	-01.0	28	19	02.9	14	03.4	13	02.4	01	03.0	01	01.6	01	02.3	02	01.0	03	02.0	32	
XI	-	00.8	10.9	03.9	04.9	11.8	-01.2	18.0	15	-06.2	21	25	03.																

Mesec	Oblakost Nm (0-10)			Vlažnost vzduха e _m %	Padavine R mm			Broj dana na sat																																		
	Isolacijski broj sati	U m s			Tn ≤ -0.00.0	Tx < 0.025.0	Tn ≥ 0.020.0	Tx ≥ 0.020.0	Tx ≥ 0.020.0	F(0-12) Nm(0-10)	R mm	• 9	* 8	* 7	Δ 6	Δ 5	Δ 4	Δ 3	Δ 2	Δ 1	R _t T =																					
		7	14	21	Sred. (Dien.)	7	14	21	T ₂ H ₂	H ₁	Min	Σ	X	Dat.																												
BIJELJINA																																										
BR. ST. 126																																										
I	7.6	6.5	5.6	6.6	073.0	34.4	92	81	88	87	57	035	013.4	26	01	05	23	•	•	•	01	08	13	07	01	09	04	•	•	•	•	05	07									
II	7.9	6.7	7.2	7.3	056.7	34.4	86	83	87	85	43	102	022.7	13	05	04	19	•	•	•	11	17	12	03	39	11	•	•	•	•	09	16										
III	6.3	5.4	5.9	5.9	129.7	06.3	87	65	85	79	36	038	009.8	18	•	•	05	•	•	•	31	09	17	13	•	17	•	•	•	01	•	•										
IV	6.3	6.2	6.4	6.4	121.6	07.0	82	55	84	74	31	050	014.2	09	•	•	•	•	•	•	06	17	12	02	17	•	•	•	•	05	•	•										
V	6.9	6.5	7.1	6.8	165.0	39.7	83	61	90	78	31	096	015.8	29	•	•	•	01	•	•	09	21	15	05	21	•	•	•	•	07	•	•										
VI	5.1	5.5	5.7	5.4	227.0	12.0	79	62	85	76	44	116	027.5	28	•	•	16	03	•	•	01	04	13	10	05	13	•	•	•	02	•	•										
VII	4.3	3.8	4.3	4.1	311.2	13.4	83	58	76	71	41	043	015.6	08	•	•	23	03	•	•	31	01	01	08	05	02	08	•	•	04	•	•										
VIII	5.0	3.7	4.0	4.4	270.0	12.9	89	58	86	78	33	025	009.7	31	•	•	19	08	•	•	32	04	02	08	06	•	07	•	•	03	•	•										
IX	6.2	5.4	4.6	5.4	149.0	10.3	87	61	92	80	40	110	026.8	01	•	•	•	35	•	•	01	04	10	08	06	10	•	•	•	02	02	•										
X	6.7	5.2	4.7	5.5	121.7	17.8	90	63	92	82	28	017	007.0	05	•	•	04	01	•	•	02	07	09	05	•	09	•	•	01	•	•											
XI	9.8	9.4	9.6	9.6	008.4	05.0	92	85	92	90	72	118	008.5	30	•	•	10	08	•	•	27	10	03	•	36	03	•	•	10	02	02											
XII	8.1	6.8	6.6	7.2	058.0	04.8	86	75	89	84	46	062	014.5	19	•	06	21	•	•	•	12	12	09	02	11	02	•	•	02	10	07	•										
GOD.	6.7	5.9	6.0	6.2	1693.2	08.2	86	67	88	80	28	712	027.5	28.VI	06	15	82	65	14	•	33	01	11	100	155	105	26	137	20	•	•	25	38	32								
LIVNO																																										
BR. ST. 127																																										
I	7.1	7.6	6.5	7.1	073.3	33.9	83	68	79	77	35	131	030.3	30	03	02	22	•	•	13	04	03	15	19	18	05	14	08	•	01	01	•	03	12								
II	8.2	7.7	7.1	7.7	069.4	04.0	79	66	77	74	41	098	030.0	13	01	01	21	•	•	19	01	01	17	15	12	04	11	07	02	•	•	01	01	05	10							
III	6.2	7.5	6.0	6.6	156.1	04.4	80	70	69	73	36	102	018.7	18	•	•	19	•	•	18	06	04	13	17	11	04	14	06	02	01	•	01	01	05	02							
IV	8.2	8.7	8.3	8.4	105.2	35.5	79	58	74	71	39	165	043.8	16	•	03	•	•	15	03	•	19	20	13	03	19	02	01	•	•	02	•	02									
V	7.6	8.1	6.8	7.5	141.4	07.2	77	59	78	71	36	241	059.2	23	•	•	02	•	•	08	02	•	14	21	17	08	21	•	•	•	•	02	•	•								
VI	5.3	7.0	4.0	5.6	236.3	09.3	78	53	75	69	38	102	033.2	16	•	•	04	•	•	07	02	09	17	09	04	17	•	•	03	•	•	05	•	•								
VII	2.4	5.2	2.6	3.4	329.4	09.3	74	43	67	61	31	021	008.6	31	•	•	14	•	•	08	11	07	04	07	07	07	07	07	07	07	07	07	07									
VIII	3.0	5.5	2.9	3.8	283.2	06.8	81	41	67	63	23	042	024.8	31	•	•	15	03	•	04	04	10	03	10	06	01	10	01	01	03	03	03	03									
IX	5.4	6.2	3.8	5.1	216.3	07.6	81	50	77	69	33	150	032.9	28	•	•	03	•	•	09	02	05	07	12	11	07	12	12	12	12	12	12										
X	5.6	4.7	3.5	4.6	206.6	36.1	81	51	75	69	34	056	030.1	04	•	05	05	05	•	11	03	11	10	12	05	02	11	01	•	01	02	02										
XI	3.7	3.4	2.1	3.1	216.2	03.6	85	47	73	68	29	077	046.9	28	•	07	27	•	•	06	01	14	05	04	03	02	02	02	02	02	02	01	03									
XII	6.9	7.4	6.8	7.0	075.7	04.4	84	48	83	78	43	196	046.1	23	07	05	17	•	•	10	02	03	16	18	15	06	16	02	•	02	01	01	13									
GOD.	5.8	6.6	5.1	5.8	2109.1	06.2	80	55	74	69	25	1387	059.2	23.V	11	08	116	36	03	•	122	24	64	128	172	124	48	154	24	05	02	01	•	24	09	45						
RAKITNO																																										
BR. ST. 128																																										
I	6.1	7.2	5.2	6.2	-	-	-	-	-	-	-	430	096.4	13	-	-	-	-	02	•	06	12	16	16	09	13	08	•	•	•	•	04	•	•								
II	7.1	7.4	5.4	6.6	-	04.4	82	85	84	84	47	307	074.2	11	-	-	-	-	09	•	04	14	14	14	07	10	06	•	•	•	•	02	•	•								
III	5.3	6.7	4.8	5.6	-	05.4	88	81	87	85	56	172	045.4	01	-	-	19	•	•	06	09	14	14	04	10	05	05	02	•	•	02	•	01	01								
IV	7.0	8.2	7.0	7.4	-	06.2	86	78	86	83	53	318	076.4	14	-	-	02	•	01	13	15	15	09	15	02	02	•	•	•	01	•	•	01									
V	6.7	7.6	6.1	6.9	-	07.7	85	73	85	81	54	317	056.4	23	-	-	02	•	02	13	16	16	08	16	16	08	08	08	08	08	08	08	08	08	08							
VI	4.6	6.2	4.8	5.2	-	09.8	78	65	78	74	45	273	132.2	14	-	-	04	•	•	06	04	09	09	05	05	09	09	09	09	09	09	09	09	09	09	09						
VII	1.8	4.1	2.5	2.8	-	10.2	70	57	75	74	67	4015	012.4	31	-	-	09	•	01	01	15	01	02	02	01	02	02	02	02	02	02	02	02	02								
VIII	2.2	4.5	1.4	2.7	-	10.2	72	58	70	67	41	323	015.4	31	-	-	12	•	01	18	03	03	02	01	03	03	03	03	03	03	03	03	03	03	03	03	03	03	03			
IX	5.0	5.5	4.2	4.9	-	08.6	81	68	80	76	46	240	096.0	01	-	-	01	•	01	07	06	15	15	10	15	05	05	05	05	05	05	05	05	05	05	05	05					
X	4.6	4.6	3.0	4.1	-	08.4	80	63	77	73	42	078	023.2	03	-	-	01	04	•	04	02	17	99	10	09	10	09	09	09	09	09	09	09	09	09	09	09	09	09	09	09	09
XI	2.3	2.3	1.9	2.2	-	05.8	84	66	76	74	44	079	J38.6	28	-	-	19	•	•	04	01	21	04	03	03	03	03	03	03	03	03	03	03	03	03	03	03	03	03	03	03	
XII	7.0	7.0	6.7	6.9	-	06.1	84	76	88	83	50	240	036.2	20	-	-	13	•																								

Meseč	Oblačnost Nm (0-10)	Vlažnost vazduha %	Padavine R mm	Broj dana na sat																																		
				Ime			Umr			Padavine R mm			Tn	Tx	Tn	Tx	Tn	Tx	Tn	Tx	Tn	Tx	Tn	Tx	•	*	*	Δ	Δ	▲	▲	R	T	≡	■			
				7	14	21	Sred. (Dnev.)	Broj dneva	Broj minut	Min	Σ	M	Dat.	<	<	≥	≥	≥	≥	<	>	≤	≤	≤	≤	•	*	*	Δ	Δ	▲	▲	R	T	≡	■		
ČAPLJINA-KLEPCI																									$H = 5 m H_b = - m h = 2.0 m h = 1.0 m$													
I	7.1	7.1	5.6	6.6	-	05.8	85	72	84	41	32	190	046.5	30	.	.	12	.	.	01	.	05	14	18	15	09	18	.	01	.	04	02	.					
II	7.7	8.2	6.0	7.3	-	06.4	85	74	84	51	59	108	032.5	13	.	.	05	.	.	01	.	02	15	14	12	04	14	02	01	.	01	01	03	.				
III	5.3	6.5	4.6	5.5	-	07.6	83	68	86	79	47	048	013.0	18	.	.	01	.	.	01	.	06	08	13	11	04	13	.	01	01	03	.						
IV	7.8	8.5	7.5	7.9	-	09.1	82	73	88	81	41	166	061.0	26	.	.	01	.	.	01	.	17	20	15	04	20	03	.					
V	6.6	7.0	5.8	6.5	-	11.1	83	69	90	81	50	129	026.0	02	.	.	12	.	.	01	.	01	10	16	11	05	16	03	.				
VI	4.6	4.9	5.2	4.9	-	14.3	85	61	93	79	46	109	040.5	28	.	.	26	04	.	01	.	06	04	10	06	03	10	02	.				
VII	1.4	2.5	3.1	2.4	-	14.8	77	52	86	72	38	002	002.4	07	.	.	31	16	.	01	.	20	.	01	01	.	01	01	.				
VIII	3.2	4.5	1.8	3.1	-	14.0	81	46	92	73	23	036	023.0	29	.	.	30	17	01	.	.	13	03	04	03	02	04	02	.				
GOD.	5.3	5.8	4.6	5.2	-	09.8	84	64	88	75	23	1283	078.0	07 IX	.	-	43	-	-	01	02	01	102	109	139	111	48	139	02	01	.	03	01	36	03	.		
JABLJANICA																									$H = 192 m H_b = - m h = 2.0 m h = 1.0 m$													
I	7.3	7.0	5.8	6.7	-	-	-	-	-	-	-	285	092.0	30	01	01	23	.	.	01	.	06	16	16	14	09	14	06	02	.	.	.	11	07	.			
II	6.8	8.2	7.4	8.2	-	05.4	89	77	88	85	42	309	085.0	13	.	.	16	.	.	01	.	02	19	19	14	10	15	03	02	.	.	.	03	05	.			
III	6.4	6.9	5.9	6.4	-	06.1	89	61	79	76	29	174	047.5	18	.	.	10	.	.	01	.	01	10	18	13	05	18	03	08	.			
IV	7.5	9.0	7.0	7.5	-	07.4	87	66	83	79	30	272	056.5	16	.	.	01	.	.	02	.	17	22	18	06	22	01	01	.	.	.	03	08	.				
V	7.4	7.9	6.6	7.3	-	09.6	87	64	93	81	35	304	075.3	14	.	.	03	.	.	01	.	16	20	14	08	20	03	05	.				
VI	6.1	6.8	5.3	6.3	-	12.7	89	59	88	79	41	212	078.0	14	.	.	20	02	.	02	.	02	06	11	08	04	11	.	.	.	04	01	.					
VII	3.0	5.3	1.9	3.4	-	12.6	81	52	85	73	35	046	023.6	16	.	.	24	06	.	07	01	06	04	02	06	.	.	.	02	.	01	03	03	.				
VIII	3.4	4.6	2.5	3.5	-	13.2	88	59	86	82	32	050	018.9	31	.	.	21	07	.	14	03	05	04	02	05	.	.	.	01	03	03	.						
IX	6.8	5.8	5.7	5.4	-	10.9	93	71	92	85	42	209	037.4	28	.	.	05	.	.	05	06	12	10	07	12	.	.	.	02	14	.							
X	7.6	5.4	5.9	6.3	-	-	-	-	-	-	-	154	065.0	02	.	.	01	01	.	05	15	09	08	05	09	.	.	.	02	13	.							
XI	3.7	3.0	2.8	3.2	-	05.2	94	63	93	83	40	057	020.0	27	.	.	19	.	.	19	06	04	04	03	03	02	.	.	.	01	14	02	.					
XII	8.5	6.8	7.3	7.5	-	05.4	92	76	92	87	44	226	043.1	17	01	02	11	.	.	03	19	15	15	08	13	04	01	.	.	.	01	18	14	.				
GOD.	6.4	6.4	5.2	6.0	-	-	-	-	-	-	-	2298	092.0	30	01	02	03	81	74	15	*	05	.	64	134	153	130	69	148	16	06	.	.	01	22	101	27	.
DOMANOVIĆI																									$H = 146 m H_b = - m h = 2.0 m h = 1.0 m$													
I	5.1	5.5	4.6	5.1	-	05.8	87	72	87	82	31	142	039.0	30	.	.	12	.	.	01	.	08	05	15	15	05	15				
II	5.9	5.4	4.5	5.3	-	05.8	85	64	81	77	38	108	028.5	13	.	.	05	.	.	01	.	05	07	12	12	03	12	01	.				
III	3.9	4.0	4.3	4.1	-	06.7	81	58	80	73	39	093	014.0	25	.	.	01	.	.	01	.	09	03	12	12	05	12	01	.				
IV	6.4	6.3	6.3	6.3	-	08.1	83	62	83	76	30	176	042.5	24	.	.	01	.	.	01	.	07	16	15	04	14					
V	5.4	6.1	5.2	5.5	-	09.7	80	63	83	75	36	127	025.5	02	.	.	01	.	.	01	.	03	04	13	12	04	13				
VI	3.4	4.4	3.4	3.7	-	11.9	76	51	77	68	31	111	043.2	28	.	.	23	01	.	07	02	07	07	03	07	01	.						
VII	1.0	2.0	1.4	1.5	-	11.9	63	42	69	58	30	002	002.4	07	.	.	28	10	.	21	01	01	01	01	01						
VIII	1.8	2.3	0.9	1.7	-	11.6	71	37	71	60	26	009	006.2	31	.	.	29	08	01	21	01	03	03	03	03						
IX	3.6	3.5	3.2	3.4	-	10.4	80	53	79	71	35	224	077.6	07	01	.	11	01	.	01	13	03	10	10	06	10					
X	3.0	2.6	2.9	2.8	-	08.8	80	56	79	72	32	072	027.8	04	.	.	01	04	.	02	.	18	04	08	08	01	08	01	.				
XII	5.4	5.4	5.5	5.4	-	05.4	82	45	79	69	12	084	047.5	28	.	.	10	.	.	01	01	01	19	03	03	03	01	02	.				
XII	6.7	6.9	7.1	7.1	-	06.7	89	69	88	82	44	123	022.3	20	.	.	06	.	.	01	02	02	14	19	16	10	19	01	02	.			
GOD.	3.9	4.1	3.7	3.9	-	08.6	79	56	79	71	12	1271	077.6	07 IX	.	.	34	96	19	01	09	01	127	42	114	112	39	114	05	01	.		
NOSTAR																									$H = 99 m H_b = 107.5 m h = 2.0 m h = 1.0 m$													
I	6.																																					

Mesec	Oblastnost Nm (0-10)	Ispolazicijski broj sati (Dnes)	Vlažnost vanduha %	Padavine mm	Broj dana u mjesecu																																	
					Tn				Tx				P(0-12)				Nm(0-10)																					
					Tn	Tx	Tn	Tx	Tn	Tx	Tn	Tx	M	N	M	N	M	N																				
					≤	<	≤	<	≤	<	≤	<	M	N	M	N	M	N																				
					≥ 40.00.0	0.025.0	≥ 30.00.0	0.020.0	≥ 6	8	≥ 2.0	8.0	≥ 0.1	1.00.0	≥ 6	8	≥ 2.0	8.0																				
					*	*	*	*	*	*	*	*	*	*	*	*	*	*																				
					•	△	•	▲	•	▲	•	▲	•	▲	•	▲	•	▲																				
					R	T	R	T	R	T	R	T	R	T	R	T	R	T																				
					=	=	=	=	=	=	=	=	=	=	=	=	=	=																				
BERKOVICI																																						
BR. ST. 136																																						
I	5.1	6.3	5.1	5.5	-	34.4	80	76	79	78	37	190	048.4	30	•	01	15	•	•	•	09	10	14	14	06	14	02	•	•	04								
II	6.3	6.0	6.1	6.1	-	35.0	83	74	81	79	46	195	031.4	12	-	13	•	•	•	•	•	05	09	15	14	08	14	01	•	•	02							
III	4.3	4.8	4.4	4.5	-	35.8	79	65	74	73	41	157	031.2	01	-	03	•	•	•	•	10	06	14	14	06	14	01	01	•	•								
IV	6.2	6.5	6.5	6.4	-	37.1	79	73	76	76	45	250	051.4	26	-	01	•	•	•	•	02	10	20	20	10	20	10	•	•	•								
V	5.2	6.5	5.3	5.6	-	39.1	80	74	76	77	39	219	035.4	23	-	01	•	•	•	•	03	07	15	15	07	15	•	•	•	•								
VI	3.7	4.1	3.3	3.6	-	36.9	74	62	72	69	40	128	037.4	16	-	10	•	•	•	•	01	02	08	03	10	•	•	•	•	•								
VII	1.1	2.3	1.2	1.5	-	36.8	59	45	60	55	25	012	009.8	07	-	22	06	•	•	24	•	03	02	03	03	03	03	03	•	•								
VIII	1.0	3.2	1.0	2.3	-	36.9	54	42	51	49	20	014	011.6	31	-	28	09	•	01	17	01	03	02	01	03	03	03	03	03									
IX	3.5	4.1	3.4	3.6	-	36.9	67	63	67	66	38	226	059.4	07	-	07	•	•	02	01	13	04	10	10	07	10	•	•	01	•								
X	2.0	2.9	2.8	2.8	-	37.6	70	61	65	65	41	170	044.2	02	-	02	•	•	01	01	18	04	09	09	06	09	•	•	•	•								
XI	2.3	2.3	1.7	2.1	-	36.6	70	51	62	61	30	100	056.4	28	-	14	•	•	22	03	04	03	03	04	04	04	04	04	04									
XII	6.7	6.0	5.5	6.0	-	35.3	85	74	82	80	49	230	076.4	20	-	02	13	•	•	02	02	06	12	17	17	08	16	02	•	•								
GOD.	4.1	4.6	3.9	4.2	-	37.3	73	63	70	69	20	1891	076.4	20.XH	-	03	00	60	15	•	04	04	140	48	134	129	67	132	07	01	•	01						
BJELAŠNICA																																						
BR. ST. 137																																						
I	6.6	8.1	7.0	7.2	069.5	32.8	89	91	89	90	29	143	049.8	30	10	31	31	•	•	20	25	04	16	21	16	03	•	21	•	20	31							
II	8.3	8.6	8.3	8.4	047.1	02.8	93	93	93	93	77	147	024.0	13	14	25	28	•	•	27	24	01	20	20	18	02	02	20	•	01	24	20						
III	6.0	7.4	7.1	6.8	133.9	03.3	93	93	94	93	71	180	029.2	18	03	24	28	•	•	28	24	04	17	22	21	07	02	22	•	01	20	31						
IV	8.3	9.3	8.9	8.9	049.5	04.0	94	97	96	96	71	164	028.5	14	-	12	27	•	•	27	24	•	22	23	22	04	05	25	04	01	•	03	20	30				
V	8.2	9.1	7.7	8.3	085.9	04.7	89	88	93	91	44	210	047.4	02	01	03	14	•	•	29	18	•	18	23	18	09	18	16	05	02	•	01	05	26	31			
VI	7.6	7.6	5.2	6.8	163.1	04.5	89	82	89	87	56	166	049.6	16	-	03	•	•	•	25	19	•	12	16	11	04	16	02	01	•	02	09	13					
VII	3.9	5.5	4.5	4.6	283.1	06.9	82	77	89	83	50	047	017.9	14	-	01	•	•	•	26	13	06	06	09	07	01	09	•	•	03	19	17						
VIII	3.7	6.9	3.1	4.6	217.4	06.9	84	79	87	83	40	105	036.8	11	-	01	•	•	•	16	05	09	05	09	06	03	09	•	•	01	03	17						
IX	7.5	7.1	5.6	6.8	112.6	05.5	88	86	89	88	21	160	043.0	01	-	01	10	•	•	26	18	03	14	15	13	05	09	08	•	01	24	15						
X	5.6	5.4	5.8	5.6	044.3	79	83	84	82	10	065	010.8	21	02	07	15	•	•	25	16	10	13	13	12	02	12	04	•	•	01	24	16						
XI	3.2	4.0	3.0	3.4	193.1	02.8	67	67	67	67	29	029	010.2	29	02	07	21	•	•	18	08	14	06	04	01	04	04	•	•	01	15	04						
XII	7.3	7.5	6.8	7.2	083.3	03.5	95	91	93	93	18	099	017.0	17	07	20	31	•	•	30	26	03	14	14	13	05	03	15	02	•	01	30	31					
GOD.	6.4	7.2	6.1	6.6	-	34.5	87	85	88	87	10	1917	049.8	30.I	41	130	210	•	•	305	220	56	163	193	161	46	85	137	12	09	02	04	•	28	283	220		
BUTIMIR - AERODROM																																						
BR. ST. 138																																						
I	7.8	7.2	6.4	7.1	048.3	04.0	91	79	87	86	52	076	040.2	30	07	07	24	•	•	03	01	03	16	14	08	01	07	39	02	•	01	18	14					
II	9.2	8.3	7.7	8.4	035.6	04.1	88	74	81	81	28	107	031.3	14	04	03	21	•	•	03	01	03	18	15	12	03	04	13	01	•	01	11	13					
III	6.7	6.5	5.5	6.2	134.9	05.0	86	55	76	72	30	115	041.0	18	-	12	•	•	•	01	05	11	14	11	13	08	04	06	•	01	01	01	01	01	01			
IV	9.1	8.7	7.8	8.4	056.7	16.0	83	60	72	72	24	081	014.0	14	-	01	01	•	•	06	02	•	17	18	13	02	18	•	•	01	07	07						
V	7.9	7.7	7.6	7.7	-	08.6	85	65	81	78	28	187	038.7	14	-	01	01	•	•	08	02	•	16	23	17	07	23	01	•	01	02	02						
VI	6.8	6.6	4.5	5.8	217.0	09.5	81	52	72	68	25	148	067.1	16	-	09	01	•	•	05	02	•	08	19	10	04	16	04	01	01	01	01	01					
VII	2.6	5.0	2.9	3.5	319.1	39.7	83	42	65	65	23	080	052.3	16	-	17	01	•	•	04	03	•	29	01	08	07	02	08	•	•	01	05	01					
VIII	3.6	5.5	3.9	4.4	252.3	07.6	84	47	72	68	28	038	013.3	31	-	17	03	•	•	02	01	•	08	39	05	01	09	•	•	04	•	•	04					
IX	5.8	6.6	4.7	5.7	145.5	08.6	92	60	82	78	36	159	045.6	01	-	03	•	•	•	03	01	03	16	14	05	01	01	01	01	01	01	01	01	01				
X	6.3	5.8	5.1	5.7	127.6	06.9	93	60	84	78	29	031	097.4	06	-	04	01	•	•	03	01	03	38	12	11	07	10	02	01	01	01	01	01	01				
XI	8.7	9.1	7.3	7.7	342.6	04.2	92	74	90	84	46	044	022.7	28	-	04	21	•	•	02	01	04	04	04	02	02	03	03	03	03	03	03	03	03	03	03	03	03
XII	7.7	6.3	6.3	6.6	018.5	04.5	87	71	83	83	23	109	026.6	20	03	05	17	•	•	12	01	01	01	12	14	10	04	13	05	01	•	01	03	11	13			
GOD.	6.4	6.8	5.7	6.3	1692.4	06.6	85	59	78	74	23	1169	052.3	06.6	09	26	90	05	•	70	12	42	143	174	123	34	145	49	08	•	05	01	32	34	52			
KALINOVIK																																						
BR. ST.																																						

Mjesec	Vremenska perIODA	Temperatura vazduha °C										Cestina pravaca i srednja jačina vjetra m/s, fm (0-12)																							
		S					W					N			NE			E			SE			S			SW			W			NW		
		7	14	21	28	FM	7	14	21	28	FM	7	14	21	28	FM	7	14	21	28	FM	7	14	21	28	FM	7	14	21	28	FM	8.	15.	22.	29.
$\varphi = 43^{\circ}10' N \lambda = 16^{\circ}33' E$ Gr. $\Delta G = + 1h 14 min.$																													GACKO		BR. ST. 141				
I	-	-02.7	01.9	-01.1	-00.8	02.6	-04.5	09.5	14	-13.4	28.10	.	.	34	02.8	.	.	28	02.8	05	02.0	26	.	.	
II	-	-02.2	02.7	-00.1	00.1	04.0	-04.2	13.0	24	-15.0	16	.	.	33	03.2	.	.	27	02.7	.	.	01	02.0	02	02.5	21	.	.		
III	-	01.1	07.9	03.2	03.9	09.0	-00.6	18.2	04	-04.4	23	01	02.0	20	03.2	.	.	20	02.7	.	.	12	03.0	17	02.9	23	.	.		
IV	-	05.1	08.8	03.5	06.2	10.2	02.7	16.6	30	-02.0	18	.	.	34	02.7	.	.	36	03.1	.	.	11	02.8	04	02.2	05	.	.		
V	-	09.0	13.4	08.9	10.9	14.9	03.2	21.4	20	-03.0	12	01	02.0	26	02.5	.	.	35	03.1	.	.	13	03.2	01	02.0	05	02.6	12	.	.	.				
VI	-	14.1	19.7	13.4	15.2	21.0	09.1	25.3	18	06.0	28.01	02	02.0	21	02.4	.	.	23	02.6	01	02.0	15	02.7	16	02.2	12	.	.		
VII	-	14.7	22.4	15.3	16.9	23.4	09.2	25.6	18	04.5	01	.	.	37	02.4	.	.	18	02.6	.	.	03	02.7	06	02.3	29	.	.		
VIII	-	13.7	22.7	14.9	16.5	24.4	08.7	30.0	02	03.5	31	.	.	28	02.4	01	02.0	09	02.3	.	.	09	02.2	18	02.4	28	.	.		
IX	-	09.1	14.3	10.3	11.5	17.5	09.9	25.0	26.11	01.4	30	01	03.0	32	03.2	.	.	12	02.8	01	02.0	05	02.8	01	02.0	12	02.4	26	.	.					
X	-	05.9	10.7	07.8	06.7	14.8	03.7	22.6	18.0	02.6	25	.	.	45	02.9	.	.	14	02.5	.	.	06	03.0	06	02.7	22	.	.		
XI	-	-01.7	10.2	01.9	03.1	11.4	-02.1	16.0	10	-07.6	14	.	.	42	03.1	.	.	13	02.7	.	.	02	02.0	01	02.0	.	.	.	32	.	.	.			
XII	-	-00.1	04.0	01.2	01.8	03.1	-02.8	11.3	19	-13.0	07	.	.	17	03.6	.	.	26	03.0	.	.	05	04.8	11	02.5	24	.	.		
GOD.	-	05.5	12.0	06.8	07.7	19.2	02.5	30.0	02LM-15.0	4.11	05	02.2	369	02.9	01	02.0	261	02.8	02	02.0	82	02.9	03	02.0	102	02.5	270	.	.						
$\varphi = 43^{\circ}14' N \lambda = 18^{\circ}36' E$ Gr. $\Delta G = + 1h 14 min.$																															ČEMERNO		BR. ST. 142		
I	648.9	-03.9	-01.2	-02.7	-02.6	00.0	-03.5	07.1	14	-13.2	09	13	02.8	04	01.8	17	03.3	02	04.5	10	02.8	17	03.1	15	02.1	01	03.0			
II	648.9	-02.7	-00.9	-02.0	-01.9	00.7	-03.0	09.6	23	-13.1	16	12	02.2	05	02.8	11	02.3	03	03.0	14	03.4	24	03.3	05	02.0	03	02.7	05	.	.	.				
III	648.8	-00.5	03.6	00.8	01.2	04.8	-01.7	13.0	04	-07.6	23	11	02.5	04	04.0	19	03.6	01	01.0	08	03.2	32	03.3	09	02.9	03	01.7	07	.	.					
IV	647.0	02.3	05.1	03.0	03.4	06.6	00.7	14.0	30	-04.8	18	11	01.9	04	02.0	09	02.4	06	04.0	12	03.5	31	03.0	11	01.8					
V	650.6	04.3	09.6	06.7	07.1	11.3	04.1	17.7	01	-05.0	12	10	02.4	05	02.2	02	02.5	04	02.5	11	04.7	34	03.4	17	02.2	02	02.0	08	.	.					
VI	652.5	11.7	16.0	11.4	12.6	17.1	09.0	21.5	11	03.5	28	10	01.8	07	02.0	07	02.7	02	01.5	02	02.5	35	03.0	09	02.8	01	02.0	17	.	.					
VII	653.0	13.4	16.4	13.0	14.7	19.4	09.4	24.6	12	04.9	24	06	01.0	07	01.1	11	02.2	04	02.5	05	02.6	16	02.9	22	01.8	05	01.6	17	.	.					
VIII	654.2	12.4	18.7	13.0	14.3	19.9	09.1	26.0	07	02.0	31	08	01.2	10	01.6	14	01.8	07	01.7	03	02.3	12	02.5	10	02.0	07	01.4	22	.	.					
IX	652.5	08.0	12.6	08.3	09.3	13.7	08.4	22.1	11	-06.2	13.01	03	02.0	06	02.2	23	03.8	07	03.0	04	02.2	17	03.0	17	02.6	03	02.7	10	.	.					
X	654.3	04.3	08.6	05.4	05.9	09.7	02.7	20.3	03	-05.6	28	17	01.9	28	01.9	19	03.6	04	03.0	06	02.5	11	03.7	07	03.4	01	04.0	02	.	.					
XI	656.3	-00.7	04.1	00.5	01.1	03.0	-01.9	12.6	16	-06.7	30	09	01.7	26	01.7	24	02.0	03	03.7	03	02.7	01	03.0	07	02.9	06	02.3	11	.	.					
XII	658.6	-00.7	01.3	00.2	00.3	02.9	-02.3	09.0	19	-15.0	07	11	02.9	10	02.1	08	02.2	04	03.8	04	05.5	20	04.4	22	03.9	09	02.8	05	.	.					
GOD.	651.7	04.1	08.0	04.8	05.4	09.3	02.0	26.0	07/02LM-13.2	09.1	121	02.1	116	01.9	163	02.8	47	02.9	80	03.4	252	03.2	151	02.5	41	02.2	124	.	.						
$\varphi = 43^{\circ}57' N \lambda = 18^{\circ}40' E$ Gr. $\Delta G = + 1h 15 min.$																															SDOKOLAC		BR. ST. 143		
I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
II	-	-05.4	06.7	-02.4	-02.4	02.5	-07.4	11.2	25	-04.6	21	28	02.4	01	01.0	01	02.0	08	01.6	06	03.2	02	03.5	11	02.2	27	.	.		
III	-	-01.6	07.7	01.6	02.4	08.0	-03.4	17.8	04	-15.7	23	17	03.9	.	.	03	02.0	11	02.1	08	03.6	07	03.3	01	02.0	17	03.6	29	.	.					
IV	-	04.1	06.9	03.2	03.9	10.7	01.6	16.8	12	-03.1	24	07	03.1	03	02.0	15	02.5	09	04.7	05	05.6	19	02.9	31	.	.				
V	-	07.9	13.3	08.6	09.7	15.0	04.6	23.0	01	-04.2	13	17	02.5	06	02.0	01	02.0	04	01.8	04	03.5	10	02.8	36	.	.				
VI	-	11.8	16.6	12.0	14.0	20.5	07.6	27.0	12	03.8	30	09	03.2	03	02.7	.	.	03	01.0	02	02.0	12	02.5	22	02.5	39	.	.		
VII	-	11.6	21.3	13.0	15.2	22.9	06.6	26.4	12	06.1	24	12	02.8	10	02.6	01	01.0	02	01.0	04	03.7</td										

Mjesec	Godina	Vrijeme	Temperatura vаздуха °C						Coeficijenti pravaca i srednja jačina vетра m/s, fm (0-12)																							
			7	14	21	24	27	30	31	1.	2.	3.	4.	N	NE	E	SE	S	SW	W	NW	C										
$\phi = 45^{\circ}22' N \lambda = 19^{\circ}34' E$ Or. AG = + 1h 17 min.																																
I	-	-06.7	03.4	00.2	00.6	04.6	-02.1	11.6	13 -10.4	10	09	01.2	05	01.4	21	02.4	22	02.6	01	01.0	07	01.6	08	01.2	12	02.1	08					
II	-	-01.6	03.4	00.5	00.7	04.5	-02.1	17.2	16 -0.2	22	04	01.2	06	01.4	15	01.3	09	01.5	06	01.0	03	01.3	10	01.2	13	01.6	09	01.3	06			
III	-	04.2	11.9	07.2	07.6	13.6	02.7	21.7	30 -0.2	15	07	02.7	06	01.2	15	01.3	11	02.0	10	01.7	12	01.3	07	01.6	19	02.3	04	01.6	06			
IV	-	07.3	14.8	16.1	16.6	16.1	05.4	23.9	30 -0.2	07	12	01.6	08	01.8	13	01.4	17	01.9	06	01.5	08	01.6	11	01.6	09	01.6	06	01.6	06			
V	-	12.6	18.7	13.3	14.5	20.1	09.2	24.6	01 -0.2	12	09	01.7	05	01.6	08	01.2	16	01.7	06	01.5	06	02.0	07	02.1	16	02.0	12	02.0	08			
VI	-	16.9	23.1	17.2	18.6	24.5	12.7	30.6	10 0.9	27	03	01.7	04	01.2	09	01.3	05	01.5	08	01.2	01	01.0	09	01.2	07	02.7	18	02.4	29	01.6	08	
VII	-	17.1	23.7	17.6	19.3	26.4	12.9	31.4	18 0.8	23	02	01.0	05	01.2	06	01.2	07	01.3	06	01.3	06	01.5	05	01.8	18	01.9	16	01.6	18	01.5	08	
VIII	-	16.1	23.6	17.8	19.1	26.7	12.4	35.7	08 0.8	21	04	01.5	03	01.0	03	01.3	11	01.6	05	01.0	04	02.2	19	01.6	23	01.5	20	01.6	08			
IX	-	12.3	20.3	13.7	15.0	21.6	04.9	29.5	11 01.6	21	07	01.4	04	01.0	03	01.0	05	01.4	05	01.2	05	01.0	13	01.7	25	01.8	23	01.6	08			
X	-	06.9	17.0	09.3	10.8	17.5	03.3	27.0	04 -0.3	28	10	01.9	03	01.3	11	01.7	12	01.6	08	01.2	06	01.0	07	01.9	18	01.6	18	01.6	18	01.5	08	
XI	-	01.4	03.4	02.0	02.2	04.6	00.7	13.7	03 -0.2	26	07	01.0	09	01.0	13	01.2	17	01.3	08	01.0	05	01.0	04	01.7	15	01.7	17	01.7	15	01.6	08	
XII	-	01.1	04.6	02.0	02.4	05.7	-00.9	16.1	29 -11.9	07	05	01.2	07	01.7	16	02.2	11	02.0	14	01.4	12	01.2	08	02.2	08	01.4	12	01.2	08	01.4	12	
GOD.	-	07.8	14.3	09.2	10.2	15.4	05.4	33.7	08.WN -22.0	22.1	79	01.6	67	01.3	133	01.6	144	01.6	85	01.3	76	01.4	101	01.7	194	01.8	214	01.8	214	01.8	214	01.8
$\phi = 45^{\circ}41' N \lambda = 19^{\circ}36' E$ Or. AG = + 1h 10 min.																						BACKA PETROVAC		BR. ST. 151								
I	-	-01.4	02.4	-00.3	00.1	02.9	-02.6	07.3	13 -11.0	10	.	.	10	01.4	.	.	42	02.9	01	01.0	14	01.0	.	.	21	01.4	05	01.4	05	01.4	05	
II	-	-01.7	02.6	00.2	00.4	02.4	-02.8	16.8	28 -0.1	22	.	.	21	01.1	.	.	30	01.8	01	01.3	09	01.3	01	.	16	01.3	05	01.3	05	01.3	05	
III	-	04.1	11.2	07.2	07.5	12.7	02.3	20.8	30 -0.2	13	.	.	11	01.5	.	.	31	01.6	01	02.0	18	01.6	01	02.0	26	01.8	05	01.8	05	01.8	05	
IV	-	07.3	14.6	09.9	10.4	19.7	05.2	23.5	30 -0.2	07	01	01.0	22	01.5	.	.	23	01.7	.	.	21	01.4	01	01.0	18	01.4	04	01.4	04	01.4	04	
V	-	12.2	18.2	14.1	14.7	19.7	09.9	24.6	31 -0.6	12	.	.	16	01.5	.	.	24	01.6	.	.	14	01.4	.	.	26	01.9	11	01.9	11	01.9	11	
VI	-	16.4	23.3	18.4	19.1	23.5	13.6	30.6	10 0.9	27	.	.	12	01.4	.	.	14	01.1	.	.	20	01.0	.	.	32	01.1	12	01.0	12	01.0	12	
VII	-	17.8	24.7	19.7	20.8	26.1	13.2	31.6	18 0.8	23	.	.	12	01.2	.	.	13	01.2	.	.	17	01.2	.	.	30	01.6	21	01.6	21	01.6	21	
VIII	-	15.7	24.6	18.8	19.5	26.2	13.1	30.4	09 0.7	27	.	.	14	01.3	.	.	24	01.5	.	.	05	01.2	.	.	33	01.3	17	01.3	17	01.3	17	
IX	-	12.3	19.8	14.8	15.3	20.9	05.5	29.8	11 02.5	21	.	.	05	01.0	.	.	04	02.0	.	.	21	01.1	.	.	37	01.8	23	01.8	23	01.8	23	
X	-	07.2	14.7	10.4	11.3	17.4	05.7	25.5	04 -0.6	29	.	.	16	01.3	.	.	18	01.2	.	.	12	01.2	.	.	24	01.9	23	01.9	23	01.9	23	
XI	-	01.0	02.9	02.0	02.6	03.6	00.3	12.5	01 -0.2	16	.	.	14	01.0	.	.	20	01.0	01	01.0	15	01.0	.	.	15	01.4	08	01.4	08	01.4	08	
XII	-	00.4	03.8	02.0	02.1	03.6	-00.6	12.5	29 -11.6	07	.	.	14	01.6	.	.	30	01.9	01	01.0	31	01.1	.	.	09	01.4	08	01.4	08	01.4	08	
GOD.	-	07.6	13.8	09.8	10.2	14.6	05.6	33.4	08.WN -19.1	22.1	91	01.0	169	01.3	.	.	273	01.7	04	01.2	197	01.2	02	01.5	287	01.7	162	01.7	162	01.7	162	01.7
$\phi = 45^{\circ}34' N \lambda = 19^{\circ}39' E$ Or. AG = + 1h 18 min.																						BACKA TOPOLA		BR. ST. 152								
I	-	-01.3	02.9	-00.3	00.1	03.6	-02.7	08.6	13 -12.4	10	10	02.6	01	02.0	19	02.6	19	03.9	12	02.2	01	01.0	13	01.4	09	02.0	02	01.4	09			
II	-	-02.2	02.6	-00.4	-00.1	03.8	-04.3	18.0	28 -24.6	21	16	02.2	05	02.0	25	01.6	05	02.6	06	02.0	01	01.0	16	01.5	05	02.4	05	02.4	05			
III	-	03.4	11.2	04.8	04.8	12.6	01.6	21.6	30 -0.2	20.23	22	02.5	02	01.5	17	01.7	01	01.6	20.3	02.3	01	02.0	26	01.8	05	02.4	05	02.4	05			
IV	-	07.0	14.5	09.4	10.0	19.7	04.7	24.1	30 -0.2	07	16	01.6	11	02.7	23	01.9	07	02.3	08	01.8	04	02.0	16	01.8	05	01.8	05	01.8	05			
V	-	12.6	18.0	12.9	14.1	19.3	07.6	25.2	01 00.8	18	12	02.8	12	02.0	14	01.9	13	02.2	09	01.2	05	01.6	16	01.9	06	03.0	04	03.0	04			
VI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
VII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
IX	-	12.3	19.7	13.6	14.8	21.3	16.1	29.6	11 02.6	21	16	02.6	04	01.8	03	02.0	07	01.6	04	01.2	09	01.8	34	01.8	12	02.3	01	02.3	01			
X	752.0	16.7	16.7	10.0	10.9	17.3	03.6	26.6	04 -0.6	28	09	02.3	03	01.7	16	01.9	14	02.4	02	02.0	07	01.2	09	01.9	14	01.9	09	01.9	09	01.9	09	
XI	752.1	01.1	03.3	02.1	02.1	04.0	00.6	00.7	12.2	03.02 -0.2	24	28	01.8	07	01.7	20	01.8	14	01.8	04	01.5	04	01.2	10	01.3	19	01.7	04	01.7	04		
XII	752.2	00.6	04.3	01.7	02.1	05.8	-01.0	17.0	29 -16.7	08	01	02.0	08	02.3	09	02.0	26	03.0	13	02.8	04	01.8	16	02.4	17	01.9	02	01.9	02			
GOD.	-	07.7	14.0	09.3	10.1	19.1	05.3	34.1	08.WN -22.0	22.11	99	02.2	65	02.0	158	02.3	216	02.6	41	01.9	87	01.8	223	01.9	172	02.0	32	02.0	32	02.0	32	
$\phi = 45^{\circ}38' N \lambda = 19^{\circ}41' E$ Or. AG = + 1h 18 min.																						NOVI SAD-RINSKI BANCEVI		BR. ST. 154								
I	-	-06.9	03.2	00.6	01.9	-02.6	13.8	13 -10.4	06	03	02.3	03	02.0	22	03.5	27	04.6	02	01.0	05	02.0	14	02.2	05	02.2	05	02.2	05				
II	-	-01.9	02.6	00.3	00.4	00.0	-03.2	17.4	28 -25.0	22	02	02.0	06	01.5	22	02.7	14	03.6		
III	752.0	06.3	11.5	08.8	07.5	13.1	02.7	20.5	30 -0.6	13	11	02.8	02	02.0	13	02.4	18	02.6	03	01.7	14	01.8	16	02.0	16	02.0	16					
IV	749.0	07.6	14.6	09.4	09.6	16.2	05.9	02.5	30 -0.1	07	04	02.5	13	02.2	22	02.2	26	02.7	01	01.0	14	02.1	14	02.4	14	02.4	14					
V	752.3	12.4	17.7																													

Meseč	Oblakost Nm (0-10)			Sred. Insolec Hrvoj (Dnes)	Vlažnost vazduha			Padavine Nm mm	Broj dana u sati																												
	7	14	21		7	14	21		<	<	<	>	>	<	>	<	>	<	>	30.00.0	0.025.0	0.020.0	6	8	2.0	8.0	0.1	1.0	0.0								
BR. ST. 151																																					
BACKI PETROVAC																																					
I	6.0	6.4	6.5	6.3	079.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	02	09	09	05	01	07	03	01	-	01	01	-	00	07				
II	7.2	7.6	7.9	7.6	063.3	04.6	89	82	90	87	41	082	017.1	20	04	04	20	-	-	-	01	13	16	11	04	07	10	-	-	11	10	-	-	-			
III	5.2	5.7	4.9	5.3	144.1	-	-	-	-	-	-	045	008.8	21	-	-	07	-	-	-	04	09	13	08	-	13	01	-	-	-	-	06	-				
IV	6.4	6.6	5.4	6.1	146.9	-	-	-	-	-	-	038	010.2	04	-	-	01	-	-	-	03	09	14	07	01	14	01	-	-	-	-	01	07	03			
V	5.7	6.8	5.6	6.0	159.1	-	-	-	-	-	-	111	031.1	08	-	-	01	03	-	-	01	04	22	16	04	22	01	01	-	-	-	-	01	10	03		
VI	4.8	6.1	4.3	5.1	128.9	-	-	-	-	-	-	115	035.7	28	-	-	18	01	-	-	05	04	19	09	02	13	-	-	-	-	01	07	-				
VII	3.1	4.1	3.0	3.4	298.1	13.5	89	63	90	81	-	094	012.4	30	-	-	22	02	-	-	12	01	10	06	01	10	-	-	-	-	03	-	-				
VIII	3.3	4.5	3.3	3.7	264.9	-	-	-	-	-	-	012	007.3	31	-	-	20	07	01	-	08	02	06	03	-	04	-	-	-	-	02	01	-				
IX	5.0	5.4	3.9	4.9	162.7	-	-	-	-	-	-	078	016.1	28	-	-	05	07	-	-	04	07	10	07	03	10	-	-	-	-	01	03	-				
X	4.6	4.0	2.9	4.0	147.9	-	-	-	-	-	-	003	001.9	05	-	-	05	01	-	-	09	04	04	01	-	04	-	-	-	-	00	-	-				
XI	9.8	9.3	9.6	9.6	011.1	05.0	94	90	94	93	67	009	003.3	30	-	02	14	-	-	-	24	08	03	-	04	03	-	-	-	-	16	-	-				
XII	6.9	7.1	6.8	7.0	045.9	05.0	89	83	89	87	59	051	013.2	10	02	05	17	-	-	01	-	02	12	14	11	01	12	04	01	-	-	11	03	-			
GOD.	5.7	6.2	5.3	5.8	1743.4	-	-	-	-	-	-	609	035.7	28VI	08	17	89	71	10	01	-	-	51	102	137	87	17	122	23	03	-	01	01	03	30	70	20
BACKA TOPOLA																												H = 100 m H = - m h = 2.0 m h = 1.0 m									
BR. ST. 152	VRBAS																																				
I	7.1	6.1	5.8	6.3	-	03.9	84	73	84	82	55	020	009.0	04	02	04	25	-	-	01	07	07	05	04	03	-	-	-	-	07	03	-					
II	7.9	7.0	6.8	7.2	-	04.3	88	82	87	84	40	065	014.6	20	05	04	10	-	-	01	-	02	16	17	12	02	05	14	01	-	-	09	15	-			
III	5.9	6.0	5.1	5.7	-	05.8	83	81	79	74	36	039	008.2	21	-	-	08	-	-	01	-	07	08	10	09	01	02	-	-	-	-	03	-	-			
IV	6.5	6.9	6.7	6.1	-	07.0	85	89	79	74	42	035	004.4	18	-	-	01	-	-	-	05	09	12	11	-	12	-	-	-	-	03	01	-				
V	4.5	6.6	6.3	6.8	-	09.4	84	81	78	75	41	087	017.5	03	-	-	01	02	-	-	-	08	14	12	03	14	-	-	-	-	03	-	-				
VI	4.8	6.4	5.3	5.5	-	11.2	79	82	75	73	33	107	032.6	28	-	-	17	01	-	-	02	07	12	10	03	12	-	-	-	-	04	-	-				
VII	3.6	4.6	3.1	4.1	-	12.4	81	92	75	70	38	064	015.0	20	-	-	20	02	-	01	01	02	11	08	04	11	-	04	-	-	-	02	-	-			
VIII	4.6	5.2	4.2	4.3	-	11.0	79	47	70	63	32	024	028.0	31	-	-	18	06	01	-	07	04	04	04	01	04	-	-	-	-	02	-	-				
IX	5.1	5.9	3.3	4.8	-	09.9	86	58	82	75	44	061	018.0	07	-	-	05	-	-	-	06	07	11	08	02	11	-	-	-	-	03	-	-				
X	5.5	4.6	3.6	4.6	-	07.8	89	57	81	75	42	004	002.0	04	-	-	02	01	-	-	07	08	03	01	-	03	-	-	-	03	-	-					
XII	0.0	9.0	9.8	9.9	-	04.8	93	88	91	90	67	020	001.6	29	-	03	15	-	-	-	29	03	01	-	03	-	-	-	-	13	-	-					
GOD.	6.3	6.6	5.5	6.1	-	07.7	85	64	80	76	32	576	032.6	28VI	09	19	85	63	09	01	-	-	41	124	121	90	16	101	20	03	-	-	14	35	23		
NOVI SAD-RIMSKI ŠANČEVI																												H = 87 m H = -7.2 m h = 2.0 m h = 1.2 m									
BR. ST. 154	NOVI SAD-PETROVARADIN																																				
I	6.5	6.8	5.4	6.2	095.5	04.0	88	74	88	83	54	031	010.6	04	02	04	24	-	-	08	02	04	12	11	05	01	07	04	-	-	04	08	-				
II	8.5	8.2	8.4	8.3	061.4	04.4	92	80	87	51	51	086	016.4	13	04	05	16	-	-	01	-	01	16	16	12	04	07	13	03	-	-	05	17	-			
III	5.8	6.6	5.1	5.8	155.2	05.7	86	59	79	74	29	040	008.8	21	-	-	07	-	-	04	-	05	09	10	08	-	10	01	01	-	-	03	-	-			
IV	6.5	7.1	6.2	6.6	152.5	07.0	86	56	82	75	32	034	006.8	29	-	-	01	-	-	07	01	03	14	15	04	-	-	-	01	06	01	-	-				
V	6.4	8.3	6.7	7.1	178.2	09.7	85	66	82	78	46	127	046.0	06	-	-	01	01	-	-	06	-	15	21	12	05	21	-	-	-	-	01	00	03			
VI	5.2	6.8	5.4	6.4	225.8	11.5	80	55	81	72	35	128	034.3	28	-	-	16	-	-	04	-	05	04	16	10	04	16	-	-	01	00	-	-	-			
VII	3.2	5.2	3.1	3.8	312.3	11.6	79	47	76	68	36	026	015.3	06	-	-	21	02	-	04	-																

Meseč	Vremenska prizilika Fm	Temperatura vazduha °C										Cestina pravaca i srednja jačina vetrova m/s, Fm (0-12)																								
		TN					H					E			W			SE			S			SW			N			NW			C			
		7	14	21	28	5/2	H1	H2	H3	H4	H5	E1	E2	E3	E4	E5	W1	W2	W3	W4	W5	SE1	SE2	SE3	SE4	SE5	S1	S2	S3	S4	S5	N1	N2	N3	N4	N5
$\varphi = 45^{\circ}08' N \lambda = 20^{\circ}00' E$ Gr. AG = + 1h 20 min.																									GLADNJE		BR. ST. 156									
I	-	-01.2	03.0	-00.1	00.4	04.4	-03.0	13.4	13	-13.7	10	11	01.7	04	02.2	04	02.2	25	02.9	18	01.6	05	02.0	13	01.4	13	02.5	.								
II	-	-01.1	02.8	00.2	00.5	04.7	-02.7	17.1	20	-12.8	21	11	01.7	11	01.9	09	02.0	10	02.4	08	01.4	09	02.0	13	01.6	13	02.2	.								
III	-	-00.0	11.3	00.6	07.1	13.6	02.3	20.3	30	-01.4	23	15	01.7	02	02.0	03	01.7	18	01.7	14	01.5	11	01.9	15	01.5	15	02.7	.								
IV	-	07.0	14.3	09.1	09.9	15.6	05.3	15.0	30	-02.3	07	11	02.3	09	02.4	16	02.2	14	02.7	07	01.4	11	02.1	11	01.5	11	02.1	.								
V	-	12.6	17.4	12.7	13.9	19.8	00.2	24.6	01	-02.3	13	11	02.1	10	02.2	11	01.7	11	02.2	09	01.7	05	02.4	10	02.0	26	02.8	.								
VI	-	16.4	22.0	16.6	17.9	24.1	11.6	30.1	10	00.4	20	10	02.4	06	02.0	09	01.3	04	02.0	08	01.5	08	02.0	09	01.3	36	03.2	.								
VII	-	16.5	24.9	18.0	19.8	26.1	12.6	32.1	18	02.7	23	17	01.5	16	01.6	09	02.0	14	01.6	07	01.4	08	01.1	12	02.9	.										
VIII	-	17.5	24.8	17.7	19.4	26.3	12.2	34.5	08	07.0	31	24	01.8	10	01.7	22	01.5	04	01.5	11	01.5	14	01.6	08	02.7	.										
IX	-	12.3	19.6	13.6	14.8	21.3	09.8	26.5	11	02.0	21	16	01.4	06	02.0	05	02.0	01	02.0	04	01.5	09	02.2	16	01.4	31	02.8	.								
X	-	08.5	15.8	10.3	11.2	17.1	05.8	26.2	04	-02.6	28	14	01.6	07	16	01.9	11	01.6	05	02.2	16	01.7	16	02.2	.											
XI	-	00.9	03.1	01.1	01.8	04.0	-01.4	12.9	03.0	-02.7	26	18	01.3	07	01.9	17	01.2	08	01.4	06	01.7	02	01.5	15	01.5	17	01.6	.								
XII	-	00.4	04.4	01.8	02.1	04.1	-01.9	14.0	29	-16.8	05	10	01.1	07	02.0	10	01.3	10	02.1	13	01.3	15	02.1	18	01.2	10	01.9	.								
GOD.	-	08.0	13.6	09.0	09.9	15.4	04.8	34.5	08VM-12.8	24.II-168	01.7	97	01.9	140	01.7	125	02.1	119	01.5	79	02.1	159	01.5	208	02.6	.										
$\varphi = 45^{\circ}38' N \lambda = 20^{\circ}02' E$ Gr. AG = + 1h 20 min.																									SEČEVJ		BR. ST. 157									
I	-	-01.1	04.6	-00.3	00.3	02.7	-02.4	11.8	13	-11.5	10	07	01.7	07	02.7	14	02.7	31	03.5	04	01.5	11	01.9	13	01.9	02	.									
II	-	-01.6	02.6	00.0	00.3	04.1	-03.5	17.4	20	-03.6	21	13	01.9	05	01.6	11	01.8	24	02.7	01	02.0	11	01.5	05	02.4	10	02.5	03								
III	-	02.9	11.2	07.1	07.4	12.8	03.6	26.2	30	-03.6	13	10	02.9	05	01.4	07	02.1	23	02.6	09	02.1	17	02.0	04	02.0	15	02.2	01								
IV	-	07.1	14.4	09.0	10.3	15.6	05.5	23.8	12	-02.2	07	12	01.5	14	01.7	10	02.0	20	02.8	16	02.4	06	01.8	14	02.4	03	02.6	01								
V	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-								
VI	-	16.7	22.6	17.2	18.5	24.1	11.7	29.2	10	00.5	27	16	01.6	05	01.6	06	01.7	10	02.0	12	01.9	07	02.3	14	01.9	18	02.1	02								
VII	-	17.0	23.0	18.8	19.9	26.4	13.4	31.3	18	00.6	23	14	01.5	09	01.3	16	01.4	18	02.0	02	01.9	10	02.0	22	02.2	05										
VIII	-	15.6	24.9	17.8	19.5	26.5	12.7	34.8	08	06.4	19	14	01.6	12	02.1	16	01.8	13	02.5	06	02.0	16	01.8	19	02.2	05										
IX	-	12.1	19.9	14.1	15.8	21.3	10.3	29.2	11	01.8	21	10	01.8	02	01.0	05	02.0	10	01.8	09	01.7	10	01.8	11	01.7	31	02.3	02								
X	-	08.6	16.8	10.8	10.8	17.6	05.4	27.6	04	-04.5	29	15	00.3	09	01.2	16	01.8	15	02.6	04	02.2	11	02.0	06	01.8	13	02.4	04								
XI	-	01.1	03.2	01.8	02.0	04.1	00.6	12.7	02	-03.6	16	16	01.3	17	01.4	06	01.5	13	02.0	04	01.0	07	01.7	07	01.3	12	01.6	02								
XII	-	00.3	04.4	01.5	02.0	05.4	-00.8	15.8	29	-12.8	07	10	01.6	05	01.8	11	02.1	28	02.8	12	02.1	06	02.2	16	02.5	02	02.0	01								
GOD.	-	08.0	14.2	09.0	10.4	14.8	05.7	33.2	08VM-19.9	24.II-48	02.0	64	01.8	06	01.8	157	02.1	104	01.8	138	01.6	135	01.9	250	01.9	113	.									
$\varphi = 45^{\circ}56' N \lambda = 20^{\circ}05' E$ Gr. AG = + 1h 20 min.																									SENTA		BR. ST. 158									
I	-	-01.2	03.0	-00.1	00.4	03.3	-02.6	03.1	13	-16.4	10	04	02.2	05	01.8	16	02.2	20	03.4	10	02.1	18	01.9	07	01.9	08	02.5	05								
II	-	-00.8	02.8	00.7	01.0	03.9	-02.3	17.0	20	-19.5	21	06	02.8	02	02.0	09	02.0	22	02.2	08	02.4	11	01.6	09	02.0	14	02.1	03								
III	-	00.1	11.4	07.6	07.7	12.5	03.6	26.4	30	-03.6	23	06	02.0	03	01.7	13	01.8	17	01.9	12	01.6	11	02.3	18	01.8	01	01.0	01								
IV	-	07.6	15.0	10.3	10.9	15.6	05.6	23.3	30	-02.3	07	05	01.8	08	02.0	07	01.9	18	02.2	09	01.6	09	01.7	22	02.0	04										
V	-	12.9	18.5	13.9	14.8	19.3	05.3	26.5	01	-00.4	12	04	02.0	08	02.1	07	01.3	11	02.1	11	02.0	09	01.6	09	02.7	26	01.6	08								
VI	-	17.2	23.6	17.5	19.6	24.3	13.3	29.6	08	00.4	27	14	02.0	03	01.7	05	01.0	04	01.2	06	02.0	09	01.6	14	01.7	31	01.8	14								
VII	-	17.7	25.2	18.5	19.9	26.0	13.5	31.7	18	00.1	23	03	01.0	04	01.5	05	01.7	07	01.3	06	02.2	05	01.8	16	02.0	20	01.7	22								
VIII	-	16.3	25.0	18.6	19.4	26.0	13.5	31.8	08	07.5	27	02	01.5	03	01.7	02	01.5	10	01.5	10	02.2	04	01.8	15	01.6	26	01.7	23								
IX	-	13.0	20.1	14.4	14.7	21.1	09.6	26.1	21	01	05	02.0	01	04.0	01	01.0	11	01.7	15	01.6	10	01.2	18	01.6	27	02.1	20									
X	-	0																																		

Mjesec	Vremenski priznak Fm	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta m/s, Fm (0-12)																														
		Tm				Min		Max		Dut.		Min		Dut.		N			NE			E			SE			S			SW			W			NW					
		7	14	21	Sred. (Dm)										8.	9.	10.	8.	9.	10.	8.	9.	10.	8.	9.	10.	8.	9.	10.	8.	9.	10.	8.	9.	10.							
$\varphi = 45^{\circ}27' N \lambda = 20^{\circ}51' E$ Gr. AG = + 1h 22 min.															JASA TOMIC												BR. ST. 161															
I	-	-00.9	03.4	06.2	00.7	03.8	-01.8	12.0	13	-00.4	10	09	02.3	11	01.1	01	02.0	39	04.2	09	01.2	06	01.7	02	02.0	04	02.5	12														
II	-	-00.5	03.7	06.9	01.2	04.5	-02.3	16.6	20	-22.5	21	08	01.1	09	01.5	.	.	31	02.8	04	01.0	06	01.0	02	01.0	12	02.2	12														
III	-	04.6	11.9	06.9	07.6	12.8	03.1	20.6	20	-03.6	13	11	02.4	02	03.5	01	01.0	36	02.2	06	01.3	10	01.7	03	03.3	17	03.5	07														
IV	-	08.5	15.6	10.1	11.1	16.4	06.3	24.0	12	-03.4	07	10	02.4	07	01.9	05	02.0	37	03.1	05	01.2	09	01.7	04	01.5	05	02.0	08														
V	-	12.9	19.0	13.5	14.7	20.2	09.8	25.6	01	00.8	13	07	02.3	10	02.0	04	01.8	27	03.4	01	02.0	12	02.2	02	02.5	13	03.0	17														
VI	-	17.5	23.0	17.3	19.0	24.9	13.1	25.5	10	08.9	20	08	02.1	05	02.0	03	01.3	18	01.7	04	01.0	13	01.7	18	03.0	19												
VII	-	16.1	26.4	18.5	20.4	27.1	13.9	32.4	19	08.8	23	11	01.8	07	01.4	05	01.2	20	02.2	03	01.0	05	01.4	05	02.2	15	02.5	22														
VIII	-	16.7	26.4	18.1	19.8	27.2	13.1	32.4	08	08.6	13	13	02.0	09	01.8	02	01.0	20	02.8	01	03.0	06	01.5	05	01.6	13	02.3	24														
IX	-	12.5	21.0	14.2	15.5	21.7	16.2	29.6	26	08.2	21	05	03.2	05	01.4	01	-01.0	16	01.8	04	01.5	11	01.6	.	.	.	37	02.7	11													
X	-	07.6	17.3	10.2	11.4	17.9	04.1	26.4	06	-03.6	29	02	01.5	17	01.4	04	01.0	22	02.6	05	01.8	10	01.4	05	02.0	10	02.8	18														
XI	-	01.3	03.9	02.3	02.5	04.6	00.8	15.6	02	-02.4	21	12	01.8	15	01.1	07	01.0	22	01.6	02	01.0	05	01.5	03	02.0	13	01.6	14														
XII	-	01.0	04.9	02.1	02.5	05.6	-00.6	15.0	29	-06.6	07	06	01.3	15	02.2	04	01.2	36	02.9	03	02.0	12	02.8	04	01.7	02	01.5	12														
GOD.	-	08.3	14.8	09.5	10.5	15.6	04.6	23.4	08/VII	-22.5	24	11	00.1	112	01.6	37	01.3	324	02.7	49	01.3	102	01.8	37	01.9	159	02.6	176														
$\varphi = 45^{\circ}09' N \lambda = 21^{\circ}19' E$ Gr. AG = + 1h 25 min.															VR SAC												BR. ST. 162															
I	755.6	00.4	03.7	01.1	01.6	04.5	-01.8	13.6	13	-00.8	10	08	02.4	08	01.6	.	.	38	05.7	22	03.0	03	01.7	05	02.0	03	02.7	06														
II	751.0	00.8	04.2	01.6	05.6	01.2	-01.5	16.6	20	-16.8	21	11	02.3	12	02.0	02	02.5	20	05.8	18	02.3	04	02.0	07	02.4	02	03.0	08														
III	752.8	05.3	11.6	07.5	08.0	12.6	03.7	20.6	05	-03.9	13	13	02.7	03	01.3	06	01.3	19	04.9	22	03.1	04	02.5	09	02.8	10	02.4	07														
IV	750.0	09.6	14.4	10.5	11.2	15.6	06.8	22.4	12	-03.6	07	06	02.7	07	02.0	05	02.6	29	04.8	20	03.2	03	02.0	08	02.5	05	02.8	07														
V	752.3	13.0	18.0	13.8	14.6	19.7	09.6	24.8	01	-01.2	13	08	02.4	10	02.3	02	02.0	21	05.4	14	02.6	06	02.0	16	02.7	05	02.6	11														
VI	752.6	16.7	22.3	17.7	18.6	23.6	13.1	28.3	25	06.2	27	13	02.2	13	02.0	02	02.0	09	04.0	21	02.6	07	02.4	11	02.8	09	02.7	11														
VII	754.5	17.7	24.9	17.9	19.6	26.1	12.7	30.9	19	03.4	23	18	02.1	12	01.7	05	01.6	10	03.7	05	03.6	04	02.5	09	02.0	12	02.2	18														
VIII	755.0	16.8	25.0	19.9	19.4	26.1	12.1	32.4	08	05.7	20	19	02.1	09	02.0	.	.	17	04.4	11	03.0	09	02.1	04	02.0	11	02.9	13														
IX	754.1	12.8	19.6	13.9	15.0	20.8	09.4	28.6	26	02.5	22	11	02.2	05	02.0	.	.	04	03.8	23	02.8	08	01.8	13	02.2	17	02.9	09														
X	756.7	16.2	20.5	11.2	17.1	20.7	05.7	26.5	03	-07.3	29	11	02.0	09	01.7	01	02.0	17	04.9	16	02.8	03	01.7	12	01.9	05	02.2	19														
XI	760.0	01.0	04.2	02.1	02.4	05.0	00.0	13.0	27	-0.8	25	26	01.8	07	02.0	03	01.7	05	04.0	22	02.5	02	02.0	06	01.8	09	02.2	24														
XII	752.8	02.3	05.1	03.4	03.6	04.7	-00.2	16.0	29	-10.7	07	07	02	04	01.8	04	02.0	20	05.5	32	03.5	07	02.3	08	02.5	01	02.0	10	02.0	10												
GOD.	751.4	08.0	14.4	09.3	10.2	15.8	05.9	34.6	08/VIII	-14.6	24	11	51	02.2	19	01.5	36	01.8	08	02.2	19	02.6	67	02.1	39	02.2	65	02.5	791													
$\varphi = 44^{\circ}33' N \lambda = 19^{\circ}14' E$ Gr. AG = + 1h 17 min.															LOZNICA												BR. ST. 163															
I	-	-01.7	04.5	-00.2	00.6	05.4	-03.1	16.1	29	-13.4	09	02	01.0	01	01.0	08	02.1	16	03.4	.	.	08	01.2	21	01.1	06	01.0	04	03.2	74		</td										

1978

Mjesec	Vremenski pristup Pm M	Temperatura vazduha $^{\circ}\text{C}$										Cestina pravaca i srednja jačina veta mD, Pm (O-12)																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																			
TM					RH					RH					Dat.		Min		Dat.		N		NE		E		SE		S		SW		W		NW		C																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																										
7	14	21	Sred. (Ges.)	M	RH	RH	M	RH	M	RH	M	RH	M	Dat.	Min	Dat.	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100	101	102	103	104	105	106	107	108	109	110	111	112	113	114	115	116	117	118	119	120	121	122	123	124	125	126	127	128	129	130	131	132	133	134	135	136	137	138	139	140	141	142	143	144	145	146	147	148	149	150	151	152	153	154	155	156	157	158	159	160	161	162	163	164	165	166	167	168	169	170	171	172	173	174	175	176	177	178	179	180	181	182	183	184	185	186	187	188	189	190	191	192	193	194	195	196	197	198	199	200	201	202	203	204	205	206	207	208	209	210	211	212	213	214	215	216	217	218	219	220	221	222	223	224	225	226	227	228	229	230	231	232	233	234	235	236	237	238	239	240	241	242	243	244	245	246	247	248	249	250	251	252	253	254	255	256	257	258	259	260	261	262	263	264	265	266	267	268	269	270	271	272	273	274	275	276	277	278	279	280	281	282	283	284	285	286	287	288	289	290	291	292	293	294	295	296	297	298	299	300	301	302	303	304	305	306	307	308	309	310	311	312	313	314	315	316	317	318	319	320	321	322	323	324	325	326	327	328	329	330	331	332	333	334	335	336	337	338	339	340	341	342	343	344	345	346	347	348	349	350	351	352	353	354	355	356	357	358	359	360	361	362	363	364	365	366	367	368	369	370	371	372	373	374	375	376	377	378	379	380	381	382	383	384	385	386	387	388	389	390	391	392	393	394	395	396	397	398	399	400	401	402	403	404	405	406	407	408	409	410	411	412	413	414	415	416	417	418	419	420	421	422	423	424	425	426	427	428	429	430	431	432	433	434	435	436	437	438	439	440	441	442	443	444	445	446	447	448	449	450	451	452	453	454	455	456	457	458	459	460	461	462	463	464	465	466	467	468	469	470	471	472	473	474	475	476	477	478	479	480	481	482	483	484	485	486	487	488	489	490	491	492	493	494	495	496	497	498	499	500	501	502	503	504	505	506	507	508	509	510	511	512	513	514	515	516	517	518	519	520	521	522	523	524	525	526	527	528	529	530	531	532	533	534	535	536	537	538	539	540	541	542	543	544	545	546	547	548	549	550	551	552	553	554	555	556	557	558	559	560	561	562	563	564	565	566	567	568	569	570	571	572	573	574	575	576	577	578	579	580	581	582	583	584	585	586	587	588	589	590	591	592	593	594	595	596	597	598	599	600	601	602	603	604	605	606	607	608	609	610	611	612	613	614	615	616	617	618	619	620	621	622	623	624	625	626	627	628	629	630	631	632	633	634	635	636	637	638	639	640	641	642	643	644	645	646	647	648	649	650	651	652	653	654	655	656	657	658	659	660	661	662	663	664	665	666	667	668	669	670	671	672	673	674	675	676	677	678	679	680	681	682	683	684	685	686	687	688	689	690	691	692	693	694	695	696	697	698	699	700	701	702	703	704	705	706	707	708	709	710	711	712	713	714	715	716	717	718	719	720	721	722	723	724	725	726	727	728	729	730	731	732	733	734	735	736	737	738	739	740	741	742	743	744	745	746	747	748	749	750	751	752	753	754	755	756	757	758	759	760	761	762	763	764	765	766	767	768	769	770	771	772	773	774	775	776	777	778	779	780	781	782	783	784	785	786	787	788	789	790	791	792	793	794	795	796	797	798	799	800	801	802	803	804	805	806	807	808	809	810	811	812	813	814	815	816	817	818	819	820	821	822	823	824	825	826	827	828	829	830	831	832	833	834	835	836	837	838	839	840	841	842	843	844	845	846	847	848	849	850	851	852	853	854	855	856	857	858	859	860	861	862	863	864	865	866	867	868	869	870	871	872	873	874	875	876	877	878	879	880	881	882	883	884	885	886	887	888	889	890	891	892	893	894	895	896	897	898	899	900	901	902	903	904	905	906	907	908	909	910	911	912	913	914	915	916	917	918	919	920	921	922	923	924	925	926	927	928	929	930	931	932	933	934	935	936	937	938	939	940	941	942	943	944	945	946	947	948	949	950	951	952	953	954	955	956	957	958	959	960	961	962	963	964	965	966	967	968	969	970	971	972	973	974	975	976	977	978	979	980	981	982	983	984	985	986	987	988	989	990	991	992	993	994	995	996	997	998	999	1000	1001	1002	1003	1004	1005	1006	1007	1008	1009	1010	1011	1012	1013	1014	1015	1016	1017	1018	1019	1020	1021	1022	1023	1024	1025	1026	1027	1028	1029	1030	1031	1032	1033	1034	1035	1036	1037	1038	1039	1040	1041	1042	1043	1044	1045	1046	1047	1048	1049	1050	1051	1052	1053	1054	1055	1056	1057	1058	1059	1060	1061	1062	1063	1064	1065	1066	1067	1068	1069	1070	1071	1072	1073	1074	1075	1076	1077	1078	1079	1080	1081	1082	1083	1084	1085	1086	1087	1088	1089	1090	1091	1092	1093	1094	1095	1096	1097	1098	1099	1100	1101	1102	1103	1104	1105	1106	1107	1108	1109	1110	1111	1112	1113	1114	1115	1116	1117	1118	1119	1120	1121	1122	1123	1124	1125	1126	1127	1128	1129	1130	1131	1132	1133	1134	1135	1136	1137	1138	1139	1140	1141	1142	1143	1144	1145	1146	1147	1148	1149	1150	1151	1152	1153	1154	1155	1156	1157	1158	1159	1160	1161	1162	1163	1164	1165	1166	1167	1168	1169	1170	1171	1172	1173	1174	1175	1176	1177	1178	1179	1180	1181	1182	1183	1184	1185	1186	1187	1188	1189	1190	1191	1192	1193	1194	1195	1196	1197	1198	1199	1200	1201	1202	1203	1204	1205	1206	1207	1208	1209	1210	1211	1212	1213	1214	1215	1216	1217	1218	1219	1220	1221	1222	1223	1224	1225	1226	1227	1228	1229	1

Mesec	Oblačnost Nm (0-10)				Vlažnost varžduha %	Padavine mm	Broj dana na mesečno												F(0-12)		Nm(0-10)		R mm																		
	Inspecija broj esti (Dnes)						Tn			Tx			Tx			Tn			F(0-12)		Nm(0-10)		R mm																		
	7	14	21	Sred. (Dnes)			mm	7	14	21	Sred. (Dnes)	Mm	M	N	Dat.	=	<	<	=	=	=	N	<	>	N	N	N	•	*	*	Δ	○	▲	■	T	≡	■				
BR. ST. 166 SABAC																										$H = 80 \text{ m H}_0 - \text{m h} = 2.0 \text{ m h} = 1.0 \text{ m}$															
I	5.0	3.5	5.5	5.5	-	-	-	-	-	-	032	013.3	24	.	05	20	04	07	08	06	01	05	03	.	.	01	01	01	01	01	01	01	01	01	01		
II	7.0	7.0	8.2	7.5	-	-	-	-	-	-	125	025.8	20	03	04	20	03	15	13	13	06	09	08	01	.	01	01	01	01	01	01	01	01	01	01		
III	5.8	5.1	4.3	5.0	-	-	-	-	-	-	037	008.2	18	.	.	05	09	08	14	09	.	14	02	02	02		
IV	6.8	6.4	6.1	6.4	-	-	-	-	-	-	051	013.4	06	.	.	01	02	12	15	11	01	15	01	01			
V	6.3	5.9	5.3	5.8	-	-	-	-	-	-	077	016.7	14	.	.	.	03	03	05	13	13	03	13	01	06	01		
VI	4.2	5.6	4.0	4.6	-	-	-	-	-	-	128	035.6	28	.	.	.	18	02	.	.	.	06	06	11	10	05	11	03	01			
VII	2.4	2.8	2.2	2.5	-	-	-	-	-	-	033	010.7	06	.	.	.	22	03	.	.	.	18	02	07	07	01	07	05	01			
VIII	3.7	2.6	3.7	3.3	-	-	-	-	-	-	026	007.4	31	.	.	.	23	08	01	.	.	12	03	09	07	09	04	02	01				
IX	4.3	5.8	3.3	4.5	-	-	-	-	-	-	107	027.4	01	.	.	.	06	01	.	.	.	10	06	08	08	06	08	01	07			
X	6.0	3.9	3.6	4.5	-	-	-	-	-	-	020	005.2	05	.	.	03	01	.	.	.	09	06	08	08	08	08	01	07				
XI	9.7	8.8	9.3	9.3	-	-	-	-	-	-	016	008.6	30	.	.	09	01	27	03	02	01	02	06	02				
XII	8.6	5.6	6.9	7.0	-	-	-	-	-	-	050	012.0	19	.	05	21	01	11	10	09	02	10	01	.	.	01	.	.	01	.	01	01	01	01	01		
GOD.	5.9	5.4	5.2	5.5	-	-	-	-	-	-	702	035.6	28.VI	03	14	79	73	14	01	-	-	78	112	119	103	25	110	14	01	.	02	01	18	33	24						
BR. ST. 167 VLADIMIRCI																										$H = 120 \text{ m H}_0 - \text{m h} = 2.0 \text{ m h} = 1.0 \text{ m}$															
I	6.7	6.3	6.2	6.4	-	04.2	87	76	85	83	52	030	-	01	05	21	04	12	-	-	-	-	-	.	.	.	09	-									
II	8.0	7.2	8.1	7.8	-	04.6	88	78	90	85	43	096	024.3	14	04	04	20	01	16	13	10	04	06	11	01	.	01	.	01	01	01	01	01	01	01	01	
III	6.0	6.2	5.4	5.9	-	-	-	-	-	-	052	023.0	18	.	.	02	06	13	13	09	01	13	03	01				
IV	6.6	7.3	6.2	6.7	-	-	-	-	-	-	043	009.0	09	.	.	01	02	11	10	04	.	10				
V	7.0	6.4	6.5	6.6	-	-	-	-	-	-	126	036.0	09	.	.	01	01	.	.	.	02	02	13	12	11	07	12	04	01				
VI	4.7	5.6	4.9	5.1	-	-	-	-	-	-	167	045.6	28	.	.	17	01	01	.	.	01	07	08	12	11	05	12	03	02					
VII	2.3	3.1	3.2	2.9	-	-	-	-	-	-	038	008.9	03	.	.	23	03	01	01	01	11	01	07	07	07	07	07	07	.	.	.	01	01	01	01	01	01	01	01	01	01
VIII	4.6	4.2	3.4	4.0	-	-	-	-	-	-	022	-	.	.	19	07	01	.	.	10	03	-	-	-	-	-	-	02	02				
IX	5.8	6.2	4.5	5.5	-	-	-	-	-	-	104	025.5	01	.	.	05	05	.	.	.	08	09	08	08	05	08	01	03					
X	6.9	4.9	4.4	5.4	-	-	-	-	-	-	022	009.7	27	.	.	03	02	.	.	.	05	08	05	05	05	05	15	02					
XI	9.5	9.1	9.7	9.4	-	-	-	-	-	-	016	010.6	30	.	.	13	01	27	02	02	01	02	17	02					
XII	8.4	7.5	8.1	8.0	-	-	-	-	-	-	-	-	.	05	17	01	19	-	-	-	-	-	13	06						
GOD.	6.4	6.2	5.9	6.1	-	-	-	-	-	-	-	-	05	16	78	67	11	01	-	-	-	-	-	-	-	-	-	-	-	-	-	-	74								
BR. ST. 168 VALJEVO																										$H = 174 \text{ m H}_0 = 176.9 \text{ m h} = 2.0 \text{ m h} = 1.2 \text{ m}$															
I	6.1	6.8	5.6	6.2	085.4	04.0	88	70	86	81	38	026	007.1	26	02	04	25	.	.	.	07	05	11	09	07	06	04	01	01	01	01	01	01	01	01	01	01	01			
II	7.7	8.1	7.5	7.8	077.6	04.4	92	69	87	83	38	086	028.7	14	02	04	20	.	.	.	J1	J1	16	17	13	03	08	13	03	01	01	01	01	01	01	01	01	01	01	01	
III	5.5	6.4	5.5	6.1	145.8	05.5	88	50	78	72	20	067	013.5	18	.	.	04	.	.	.	03	01	07	12	18	13	01	18	01	01	01	01	01	01	01	01	01	01			
IV	7.6	8.3	5.9	7.3	101.7	06.8	87	54	82	74	24	040	006.0	05	.	.	01	01	.	.	01	01	01	01	13	17	16	01	01	01	01	01	01	01	01	01	01				
V	8.2	8.0	7.1	7.8	136.4	09.4	86	60	87	78	27	117	034.4	09	.	.	01	02	01	.	03	.	17	18	15	05	18	01	07	01				
VI	5.6	6.8	5.3	5.9	214.5	11.8	83	60	87	77	31	175	047.9	28	.	.	18	01	.	.	04	.	02	08	17	14	07	17	01	07	01			
VII	2.9	4.3	3.4	3.5	324.5	12.3	83	45	90	73	31	043	012.8	03	.	.	20	05	.	.	03	.	11	02	08	06	01	08	01	05	01			
VIII	4.0	4.7	3.3	4.1	254.4	11.2	84	44	83	73	21	047	018.7	05	.	.	18	07	01	.	03	01	09	02	08																

Meseč Nume ri	Vreme dani čas u m inuti	Temperatura vremena °C										Čestina pravaca i srednja jačina vatre mD, fm (0-12)																		
		Im					Im					W NW E SE S SW W NW C																		
		7	14	21	28	35	Im	Im	Im	Im	Im	Im	Im	Im	Im	Im	Im	Im	Im	Im	Im	Im	Im							
$\varphi = 44^{\circ}08' N \lambda = 20^{\circ}31' E$ Gr. AG = + 1h 22 min.																														
I	-	-01.6	00.7	-00.4	-00.3	02.4	-03.4	09.7	13	-11.8	09	-	-	-	-	-	-	-	-	-	-	-	-							
II	-	-00.2	01.8	00.9	00.9	03.8	-02.2	14.2	25	-11.6	21	-	-	-	-	-	-	-	-	-	-	-	-							
III	+	03.2	07.4	04.9	05.1	09.3	01.6	19.2	04	-04.9	23.13	-	-	-	-	-	-	-	-	-	-	-	-							
IV	-	04.4	10.1	07.2	07.7	12.0	04.7	20.8	12	-01.3	18	-	-	-	-	-	-	-	-	-	-	-	-							
V	-	10.0	14.0	10.5	11.3	16.1	07.9	25.6	01	-01.1	13.12	05	01.6	08	01.5	10	01.5	12	02.0	03	01.3	22	02.0	05	01.4	02	01.5	26		
VI	-	14.2	18.8	14.5	15.6	20.7	11.7	26.3	04	06.6	29	07	01.9	13	01.7	12	01.6	01	02.0	14	01.9	11	02.5	08	02.5	16	02.4	14	02.5	24
VII	-	15.3	21.2	16.2	17.2	22.5	13.6	26.8	19	07.4	22	13	01.4	18	01.6	15	01.4	01	02.0	09	02.1	04	03.2	09	02.1	19	02.1	15	02.1	28
VIII	-	15.1	20.8	16.2	17.1	22.2	13.2	26.2	01	06.8	31	15	01.4	22	01.5	14	01.4	05	02.8	11	03.0	03	02.3	03	01.7	10	01.5	10	01.5	19
IX	-	10.3	14.8	12.0	12.3	16.5	08.5	24.0	26	01.7	21	15	01.4	10	02.1	04	01.0	02	01.5	05	02.0	09	02.8	11	01.9	24	01.9	10	01.9	10
X	-	07.7	10.8	08.5	08.9	12.3	04.1	21.9	03	-04.5	28	21	01.4	12	01.4	15	01.5	06	02.3	04	02.0	05	01.4	09	01.8	08	01.8	13	01.8	13
XI	-	-00.3	01.9	00.7	00.7	03.4	-01.4	10.8	25	-06.5	13	14	01.4	21	01.4	03	01.3	02	01.5	05	02.0	07	01.7	06	02.3	03	01.7	06	02.3	03
XII	-	01.8	03.4	02.4	02.5	05.0	-00.7	13.0	29	-11.9	07.04	16	01.6	07	01.9	05	02.0	02	03.0	07	03.3	24	03.2	20	02.6	09	01.9	03		
GOD.	-	06.9	10.5	07.8	08.2	12.2	04.9	20.2	06VN	-11.0	07.06	XH	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
$\varphi = 44^{\circ}18' N \lambda = 20^{\circ}33' E$ Gr. AG = + 1h 22 min.																														
I	-	-01.1	03.6	00.1	00.7	04.5	-02.4	14.0	13	-09.2	10	02	01.5	01	03.0	05	01.4	26	01.7	07	01.3	01	02.0	09	01.7	12	03.0	30		
II	-	-00.2	04.5	01.0	01.6	05.3	-01.6	19.1	28	-11.3	22	-	01.0	12	01.1	23	01.0	03	01.0	01	01.0	17	02.3	12	01.6	14	02.3	20		
III	+	04.1	11.3	06.1	06.9	12.5	-02.4	16.8	30	-03.8	09	01	04.0	03	01.3	02	01.5	17	01.2	03	02.0	05	01.6	17	02.1	27	02.2	18		
IV	-	08.5	13.6	09.3	10.2	15.1	05.9	23.9	12	-00.2	07	03	02.3	01	02.0	11	01.5	19	01.6	03	01.4	08	02.1	16	02.8	14	03.0	13		
V	-	12.6	17.7	12.8	14.0	19.1	09.3	28.0	01	-01.1	13	02	02.5	02	01.5	06	01.5	21	01.3	04	02.3	13	02.1	23	02.5	17	02.6	03		
VI	-	16.7	21.6	16.5	17.8	23.5	12.9	30.2	10	09.0	28	02	02.5	06	01.8	03	01.0	11	01.5	02	01.5	08	01.5	26	02.4	12	02.4	20		
VII	-	15.2	24.7	17.3	18.6	25.8	12.9	35.0	07	09.5	30	01	01.0	02	03.0	04	01.0	10	01.5	07	01.9	12	02.1	12	01.8	16	02.2	29		
IX	-	12.7	16.7	13.3	14.3	20.0	09.7	27.5	26	04.8	30	01	01.0	01	01.0	01	02.0	13	01.1	04	01.5	10	01.8	31	02.2	19	02.3	10		
X	-	07.6	14.5	08.9	10.0	15.7	04.8	25.9	04	-02.5	29	-	03	01.3	04	01.0	17	01.1	07	01.0	04	01.5	12	01.5	33	02.5	13			
XI	-	06.8	03.1	01.4	01.7	04.3	-00.4	12.8	26	-04.2	25	03	01.0	07	01.0	13	01.0	12	01.2	01	01.0	16	01.4	27	01.7	10	01.2	01		
XII	-	01.7	04.9	03.1	03.2	06.5	-00.9	17.6	29	-09.3	07	03	01.0	03	02.0	17	01.5	20	02.1	09	01.3	12	02.3	25	02.2	22	04	02.0	04	
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
$\varphi = 44^{\circ}51' N \lambda = 20^{\circ}40' E$ Gr. AG = + 1h 22 min.																														
I	-	-00.7	03.3	00.3	00.8	04.5	-02.2	15.5	14	-08.0	10	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
II	-	-00.3	03.6	00.6	01.0	04.7	-02.4	19.7	28	-17.8	21	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
III	+	04.2	11.3	07.1	07.5	12.8	02.8	20.0	30	-01.5	09	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
IV	-	08.3	14.6	10.8	10.7	15.8	05.9	24.2	12	-02.0	07	06	02.5	01	01.0	11	03.1	27	03.2	01	03.0	01	02.0	21	02.9	05	02.4	17		
V	-	12.4	18.2	13.5	14.4	20.3	09.7	27.2	01	-00.5	13	03	02.3	06	01.8	07	02.4	15	03.1	01	02.0	06	02.0	20	02.8	06	02.7	29		
VI	-	14.5	22.4	17.1	18.3	24.1	13.1	29.5	10	08.5	27	07	02.7	02	02.0	09	02.3	05	01.6	07	01.9	23	03.1	07	02.6	28				
VII	-	16.6	25.2	18.5	19.7	26.3	13.9	31.5	14	10.0	25	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
VIII	-	14.0	25.1	17.9	19.2	26.3	12.8	34.0	08	08.0	30	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
IX	-	12.1	20.0	13.9	15.0	21.5	09.9	28.6	26	04.5	30.04	06	02.7	-	-	03	02.0	06	01.3	03	02.0	06	02.3	31	03.0	05	03.4	30		
X	-	07.9	14.1	09.9	11.0	17.0	06.0	27.1	04	-03.8	28	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
XI	-	01.3	03.7	02.2	02.4	04.4	00.4	12.7	03	-02.6	16	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
XII	-	06.4	04.4	02.0	02.8	06.1	-01.7	18.3	29	-10.2	07	05	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
GOD.	-	07.8	14.2	09.5	10.3	15.4	05.9	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
$\varphi = 44^{\circ}31' N \lambda = 20^{\circ}46' E$ Gr. AG = + 1h 24 min.																														
I	-	-00.6	04.0	00.9	01.3	04.7	-01.8	13.8	13	-08.2	07	07	02.4	07	02.7	-	-	13	02.9	22	03.0	06	02.3	-	-	06	03.3	32		
II	-	-00.4	05.2	02.1	02.4	06.3	-01.6	19.8	28	-15.0	21	11	01.9	02	02.0	-	-	05	03.0	11	02.4	09	02.2	-	-	11	02.5	35		
III	-	04.0	12.0	07.1	07.6	13.3	02.6	21.2	05.04	-04.2	09	07	02.4	-	-	02	02.0	11	02.3	06	02.2	14	01.9	20	02.6	38				
IV	-	08.0	14.8	10.2	10.8	16.0	06.1	23.6	12	01.0	07	06	02.0	05	02.0	00	00	08	03.0	14	02.4	01	02.0	20	08	02.2	41			
V	-	12.3	17.9	13.7	14.4	19.8	09.9	28.0	01	-00.6	13	08	02.1	02	02.0	-	-	03	02.7	13	02.2	08	02.0	02	02.5	10	02.5	47		
VI	-	16.2	22.6	17.5	18.5	24.2	12.6	29.4	10	09.4	27	10	02.3	05	02.0	-	-	02	02.5	09	02.0	18	02.0	02	02.5	11	02.5	33		
VII	-	16.4	25.5	18.2	19.6	24.6	12.7	30.4	19	08.8	25.24	11	02.1	06	02.0	-	-	03	02.0	04	02.2	16	02.0	02	02.0	16	02.7	51		
VIII	-	15.1	24.9	16.5	18.3	25.8	11.4	35.0	08	07.0	28	05	02.0	05	02.0	01	02.0	11	04.1	09	02.0	12	02.1	01	02.0	18	02.2	31		
IX	-	12.0	19.8	13.2	14.6	21.2	09.4	27.8	26	11.0	02.6																			

Mesec	Oblačnost Nm (0-10)				Vlažnost vzdušna % H ₀	Padavine R mm	Broj dana na mesečno																											
	Insekcija broj sati			Sred. (Gles.)			Tn	Tn	Tn	Tn	Tn	P(0-12)	Nm(0-10)	R mm	•	*	*	Δ	Δ	▲	▲	□	T	≡										
	7	14	21		≤	<	<	≥	≥	≥	≥	<	≥	≥	≥	•	Δ	Δ	Δ	▲	▲	□	T	≡										
RUDNIK																																		
BR. ST. 171																																		
I	5.4	6.4	5.0	5.6	-	-	-	-	-	-	-	032	006.9	26	04	09	25	-	-	-	07	10	15	07	-	05	12	01	-	-	03	20		
II	6.2	7.8	7.4	7.8	-	-	-	-	-	-	-	122	027.4	14	01	10	20	-	-	-	02	17	17	13	06	01	17	-	-	03	26			
III	6.1	6.3	4.8	5.8	-	-	-	-	-	-	-	108	014.3	22	-	-	16	-	-	-	09	12	19	14	03	09	13	02	-	-	01	01	11	
IV	6.9	7.6	6.0	6.8	-	-	-	-	-	-	-	075	014.3	06	-	-	04	-	-	-	02	12	19	14	02	17	04	01	-	-	01	03	02	
V	7.8	7.7	5.9	7.1	-	-	-	-	-	-	-	150	022.6	09	-	-	02	01	-	-	02	13	23	20	05	23	01	-	-	01	-	-		
VI	4.8	6.1	4.3	5.1	-	10.4	84	71	79	78	41	220	057.1	22	-	-	06	-	-	-	05	07	13	11	08	13	-	-	01	02	04			
VII	2.7	4.3	2.9	3.3	-	-	-	-	-	-	-	043	012.0	08	-	-	07	-	-	-	11	03	09	06	01	09	-	-	02	02	02			
VIII	4.4	4.5	2.4	3.8	-	-	-	-	-	-	-	048	016.1	27	-	-	07	01	01	-	11	03	12	09	01	12	-	-	03	02	-			
IX	5.9	6.4	4.4	5.6	-	08.3	79	73	81	78	09	205	053.9	01	-	-	06	-	-	-	06	07	10	10	06	10	-	-	02	07	01			
X	5.0	6.2	3.5	4.9	-	07.0	84	76	81	80	46	033	017.5	20	-	-	04	-	-	-	10	07	11	05	01	10	01	-	-	07	01			
XI	7.0	8.0	6.2	7.0	-	04.2	90	87	86	88	39	025	019.9	30	-	-	09	19	-	-	05	17	07	03	01	02	03	-	-	17	02			
XII	7.4	7.5	5.5	6.8	-	04.6	83	83	80	82	45	072	014.1	15	03	04	14	-	-	-	01	-	06	16	12	04	10	08	-	-	01	13		
GOD.	6.0	6.6	4.9	5.8	-	-	-	-	-	-	-	1133	057.1	22.VI	08	34	104	21	01	01	-	-	70	116	171	127	38	121	59	04	-	-	63	79
BUKOVICKA BANJA																																		
BR. ST. 172																																		
I	5.2	5.8	5.2	5.4	-	03.9	86	68	84	79	34	030	014.4	26	-	06	25	-	-	-	08	10	11	06	01	05	07	-	-	04	04			
II	6.9	7.1	6.9	7.0	-	04.4	88	74	85	82	46	103	028.8	14	01	07	22	-	-	-	05	14	18	11	04	05	14	-	-	03	18			
III	4.9	5.2	3.9	4.7	-	-	-	-	-	-	-	084	015.9	13	-	-	05	-	-	-	11	06	18	13	04	16	04	02	-	-	01			
IV	5.9	6.8	5.8	6.2	-	06.7	79	60	78	72	29	071	016.0	25	-	-	01	-	-	-	10	22	15	01	22	-	-	02	01	-	-			
V	5.9	6.8	5.5	6.1	-	09.2	81	61	83	75	25	123	020.3	09	-	-	01	02	-	-	02	09	22	17	07	22	-	-	04	01	-	-		
VI	3.9	5.5	3.6	4.3	-	13.3	80	68	82	77	41	185	054.6	28	-	-	15	01	-	-	11	06	15	11	06	15	-	-	01	02	-	-		
VII	-	-	-	-	-	-	-	-	-	-	-	050	028.1	03	-	-	-	-	-	-	01	-	-	-	09	04	01	05	-	-	01	01	-	-
VIII	2.7	3.6	3.5	3.2	-	-	-	-	-	-	-	032	007.2	31	-	-	18	07	-	-	14	03	09	07	04	-	-	02	-	-	-			
IX	5.5	5.2	3.3	4.7	-	-	-	-	-	-	-	128	025.8	01	-	-	04	-	-	-	08	04	08	08	05	08	-	-	-	-	-	-		
X	5.2	4.9	3.8	4.6	-	-	-	-	-	-	-	025	008.9	02	-	-	03	01	-	-	01	-	12	07	09	05	04	-	-	14	02	-	-	
XI	9.7	8.7	8.8	9.1	-	-	-	-	-	-	-	015	012.4	30	-	04	20	-	-	-	01	-	23	02	02	01	02	02	-	-	02	-	11	
XII	7.6	7.4	8.1	7.7	-	-	-	-	-	-	-	042	008.4	15	-	04	20	-	-	-	01	-	16	12	09	12	04	03	-	-	01	-	11	
GOD.	-	-	-	-	-	-	-	-	-	-	-	888	054.6	28.VI	-	-	-	-	-	-	-	159	108	30	134	31	07	-	-	01	10	37	30	
PANCEVO																																		
BR. ST. 173																																		
I	6.2	6.0	6.5	6.2	-	04.0	93	79	88	87	-	013	004.5	05	-	05	26	-	-	-	05	02	04	12	06	04	01	05	01	-	05			
II	8.4	7.3	7.3	7.7	-	-	-	-	-	-	-	100	023.0	14	03	03	19	-	-	-	16	18	11	03	07	13	-	-	07	-	-			
III	5.9	5.7	5.2	5.6	-	-	-	-	-	-	-	050	015.0	16	-	-	02	-	-	-	07	10	12	10	01	12	-	-	02	-	-			
IV	7.1	7.7	6.9	7.2	-	07.0	80	57	80	72	35	039	006.6	04	-	-	01	-	-	-	13	15	09	05	-	15	-	-	01	-	-			
V	6.6	7.8	6.1	6.8	-	09.4	84	60	83	75	35	110	024.9	03	-	-	01	04	-	-	01	-	02	13	18	11	03	18	-	-	01	02		
VI	5.0	6.9	4.7	5.5	-	11.9	84	59	83	75	30	127	049.0	28	-	-	17	-	-	-	04	08	13	12	04	13	-	-	03	-	-			
VII	3.8	3.5	3.3	3.3	-	13.8	87	56	83	76	24	052	014.5	06	-	-	22	04	-	-	01	10	03	08	07	08	-	-	02	-	-			
VIII	3.7	4.0	3.2	3.6	-	11.8	85	51	78	72	-	015	007.0	11	-	-	20	04	-	-	01	12	02	09	05	09	-	-	01	01	01			
IX	6.3	5.7	4.3	5.4	-	10.2	89	62	85	79	40	084	023.5	29	-	-	08	-	-	-	07	09	08	07	04	08	-	-	09	-	-			
X	6.3	5.1	3.8	5.1	-	08.2	91	66	86	81	-	018	008.9	22	-	-	03	02	-	-	08	07	04	05	03	06	-	-	12	-	-			
XI	9.6	9.2	9.1	9.3	-	05.1	92	82	95	85	-	011	004.6	29	-	02	14	-	-	01	26	03	03	02	02	02	-	-	11	-</td				

Meseč Broj	Vrijeme u satima	Temperatura vazduha °C										Čestina pravaca i srednja jačina vjetra m/s, fm (0-12)																
		Sjever					Južni					Vrhovni						Doljni										
		7	14	21	Sred. Gorski	NE	SE	NE	SW	W	SW	N	NE	E	SE	S	SW	W	NW	C	8.	9.	10.	11.				
$\varphi = 44^{\circ}12' N \lambda = 21^{\circ}47' E$ Gr., AG = + 1h 27 min.																												
I	-	-04.1	-06.2	-02.2	00.8	-04.9	09.8	14	-12.8	09	-	01	02.0	32	02.9	02	02.5	-	-	06	01.3	-	-	52				
II	-	-02.3	01.9	-00.4	-00.4	02.8	-03.4	14.6	28	-15.6	21	01	02.0	01	03.0	17	02.3	04	01.2	05	01.2	-	04	02.0	-			
III	-	01.5	07.1	04.9	04.6	00.2	00.9	14.0	02	-05.2	09	-	-	15	02.1	01	01.0	02	01.0	02	01.5	22	01.2	-	51			
IV	-	35.4	10.3	08.4	08.1	11.5	04.4	18.2	30	00.6	24.07	-	-	30	01.8	03	02.0	-	-	01	01.0	12	01.4	-	44			
V	-	09.8	15.1	12.5	12.3	14.5	08.6	21.4	01	-01.8	13	-	-	19	01.7	03	02.0	-	-	01	03.0	16	01.2	01	01.0			
VI	-	12.2	19.3	16.1	15.9	20.6	10.8	25.4	10	07.0	04	-	-	04	01.5	01	02.0	01	01.0	01	01.0	24	01.3	-	50			
VII	-	12.2	21.3	17.6	17.2	22.4	11.2	27.8	19	05.8	24	-	-	04	01.2	01	01.0	-	-	09	01.8	06	01.0	73				
VIII	-	11.4	21.5	16.2	16.3	22.5	10.8	30.2	08	05.8	20	-	-	13	01.6	-	-	01	02.0	18	01.3	-	-	71				
IX	-	08.7	16.8	12.2	12.5	17.9	07.9	25.0	26	00.0	22	-	-	03	01.7	-	-	-	-	24	01.5	-	-	61				
X	-	05.7	13.3	08.8	09.2	14.1	04.7	21.4	04	-03.0	23	-	-	19	01.7	-	-	-	-	13	01.3	-	-	61				
XI	-	00.5	03.6	01.4	01.7	04.4	-05.5	10.6	26	-05.8	20	-	-	07	01.6	-	-	-	-	12	01.3	-	-	61				
XII	-	-00.1	02.6	00.9	01.1	03.8	-01.4	15.4	29	-00.0	04	-	-	22	02.5	-	-	-	-	08	01.2	-	-	61				
GOD.	-	09.1	11.0	08.0	08.0	12.1	04.0	30.2	08.VM	-13.0	24.II	01	02.0	02	02.5	187	02.1	15	01.7	08	01.1	06	01.7	168	01.4	07	01.0	701
$\varphi = 44^{\circ}41' N \lambda = 22^{\circ}28' E$ Gr., AG = + 1h 28 min.																												
I	-	-02.3	02.5	-00.8	-00.4	03.7	-03.1	12.4	14	-08.6	10	27	03.8	02	02.5	-	-	-	-	01	03.0	04	03.0	07	03.0	51		
II	-	-01.1	03.0	00.1	00.5	04.0	-01.9	17.2	28	-10.4	22	16	02.4	-	-	-	-	-	-	11	03.4	04	03.2	09	03.0	30		
III	-	04.8	10.5	07.0	07.3	11.8	03.3	18.4	17	-01.0	13	33	03.1	01	03.0	-	-	-	-	14	05.1	10	03.5	30				
IV	-	08.3	13.6	09.6	10.3	15.2	06.4	22.4	14	02.8	01	27	03.0	01	03.0	-	-	-	-	13	04.3	07	05.6	41				
V	-	12.6	18.3	13.5	14.5	20.0	09.8	24.6	06.0	01.6	13	27	02.6	01	07.0	-	-	-	-	11	04.1	17	03.9	37				
VI	-	16.4	23.0	17.1	18.4	24.7	13.6	29.4	25	10.6	03	28	03.0	-	-	-	-	-	-	17	03.8	17	03.7	36				
VII	-	17.6	25.9	19.4	20.6	27.2	14.5	31.3	05	11.2	23	31	02.9	-	-	-	-	-	-	13	03.8	22	03.2	27				
VIII	-	16.6	25.9	19.0	20.1	27.3	13.7	32.8	08	10.8	14	26	03.1	-	-	-	-	-	-	12	03.0	10	03.1	41				
IX	-	13.9	20.7	15.3	16.3	21.8	11.5	27.4	12	04.8	22	16	03.0	01	01.0	-	-	-	-	22	04.3	23	02.7	28				
X	-	08.7	17.0	10.7	11.8	17.9	06.9	25.6	03	-00.6	29	14	02.6	04	04.5	-	-	-	-	13	03.2	09	03.0	31				
XI	-	01.2	06.9	02.3	02.2	07.7	00.2	13.2	16	-0.2	15	27	03.0	-	-	-	-	-	-	11	04.4	10	02.4	40				
XII	-	00.1	03.5	01.4	01.7	04.6	-08.9	15.2	29	-05.6	06.07	14	03.3	-	-	-	-	-	-	21	04.4	05	02.0	51				
GOD.	-	08.1	14.2	09.6	10.4	15.3	06.2	22.8	08.VM	-10.4	22.II	288	03.0	10	03.7	-	-	-	-	01	03.0	162	04.3	141	03.3	491		
$\varphi = 44^{\circ}14' N \lambda = 22^{\circ}39' E$ Gr., AG = + 1h 29 min.																												
I	761.5	-03.2	01.9	-01.6	-01.1	02.9	-04.4	16.3	14	-10.9	11	05	01.4	26	01.3	23	01.8	02	01.0	05	01.0	.	09	02.8	13	03.1	16	
II	756.6	-02.6	01.3	-02.0	-01.3	02.2	-04.1	14.0	28	-19.6	23	04	01.8	19	01.2	12	01.3	01	01.0	.	01	02.0	07	03.3	07	03.0	30	
III	756.7	04.5	10.9	06.8	07.3	11.9	03.3	18.6	17	-02.3	14	03	01.3	11	01.5	08	02.0	02	02.5	01	01.0	05	02.2	27	03.1	17	02.8	16
IV	754.5	08.2	14.1	10.6	10.6	15.6	06.0	22.8	29	00.6	01	14	01.6	05	01.6	17	02.0	07	01.7	03	02.3	03	02.0	19	02.8	09	02.2	11
V	756.3	13.3	19.6	14.2	15.2	20.5	10.7	25.6	31	03.6	13	13	01.8	07	01.6	09	01.4	03	01.7	.	08	01.8	28	02.9	12	02.2	11	
VI	756.1	17.3	24.2	18.0	19.4	25.5	13.4	30.1	11	09.9	21	13	01.7	06	01.5	09	01.4	02	01.0	04	01.0	07	02.3	26	02.8	13	02.5	30
VII	757.6	18.5	26.2	19.1	20.7	27.4	14.5	31.3	09	08.8	24	06	01.8	10	01.0	13	01.4	04	01.5	05	01.2	03	01.7	25	02.6	17	02.5	10
VIII	756.5	14.0	24.3	18.4	19.8	27.7	12.4	33.7	14	07.5	05	02.2	03	01.7	15	01.5	04	01.5	.	09	01.8	22	02.6	17	02.4	24		
IX	757.1	13.0	20.7	14.6	15.8	22.0	10.7	29.4	12	04.3	20	06	01.3	06	01.5	08	01.2	03	02.0	02	01.0	09	01.7	32	03.0	16	02.7	16
X	762.6	07.1	14.7	09.6	10.8	17.6	05.3	24.6	09	-01.6	29	08	01.4	09	01.0	11	01.5	09	01.2	.	04	01.8	16	02.9	15	02.5	22	
XI	766.6	-00.1	07.2	01.8	02.7	05.4	-01.6	14.0	16	-07.4	20.16	12	01.5	10	01.4	12	01.4	04	01.2	05	01.8	04	01.5	18	03.1	09	03.4	16
XII	758.1	06.3	03.5	01.1	01.5	04.9	-01.3	19.0	29	-07.2	07.07	07	01.6	10	01.8	14	02.0	12	01.3	04	01.2	07	01.9	14	03.2	14	02.1	21
GOD.	758.6	07.7	14.4	09.2	10.1	15.6	05.4	23.7	07.VM	-19.6	23.II	96	01.6	121	01.4	151	01.6	53	01.4	29	01.3	60	01.9	243	02.9	159	02.6	181
$\varphi = 43^{\circ}41' N \lambda = 19^{\circ}26' E$ Gr., AG = + 1h 18 min.																												
I	-	-03.4	-01.1	-04.7	-04.0	00.0	-07.7	07.8	29	-19.4	09	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
II	-	-04.3	00.6	-02.9	-02.5	01.4	-04.4	12.6	25	-23.6	21	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
III	-	-02.4	04.5	-00.4	00.3	05.6	-02.2	14.6	04	-12.0	13	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
IV	-	02.2	04.9	03.1	03.6	08.1	00.5	16.6	12	-02.2	17	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
V	-	04.6	11.1	07.4	08.1	12.0	04.1	22.2	01	-02.4	12	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
VI	-	10.8	16.1	12.6	17.4	20.7	07.2	25.2	12	04.6	05.01	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
VII	-	10.6	16.3	13.0	13.7	19.1	07.6	25.6	19	02.0	24	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
VIII	-	09.6	17.3	11.8	12.7	16.3	07.2	27.0	07	02.2	20	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
IX	-	07.9	13.2	09.3	09.9	13.5	06.6	22.3	11	00.7	22	13	01.8	06	01.2	03	02.0	.	06	02.5	35	02.6	03	01.7	04	01.0	01	
X	-	01.5	06.0	02.9	03.3	06.4	0.6	20.8	03	-0.6	28	22	01.7	18	01.7	07	01.7	04	02.0	12	02.5	31	02.1	03	01.5	01	01	
XI	-	-03.2	04.0	-00.6	-00.8	04.0	-03.4	10.7	16	-0.6	18	13	21.5	16	01.2	03	04.0	05	02.									

Meseč Broj	Oblačnost Nm (0-10)				Vlažnost vazduha %	Padavine R mm	Broj dana na sat																												
	Temperatura H m 7 14 21 Srednji (Dien.)						U h t		Tn Tx Tr Tx Tx Tx				F(0-12)		Nm(0-10)		R mm	•	•	*	*	Δ	Δ	UJ	▲	▲	R	T	≡	■					
	Temperatura H m 7 14 21 Srednji (Dien.)	U h t	%	M	7	14	21	U H m MHD	M	%	Σ	X %	N %	M	%	<	N %	M	%	N %	M	%	•	•	*	*	Δ	Δ	UJ	▲	▲	R	T	≡	■
ZAGUBICA																																			
BR. ST. 181																																			
I	7.2	6.5	6.4	6.7	97.0	1	03.3	87	75	84	82	39	010	005.2	30	03	15	29	•	•	•	•	02	14	36	04	01	02	04	•	•	•	•	01	09
II	6.9	7.3	7.0	8.0	97.1	3	03.9	91	73	87	86	30	031	012.2	14	03	11	22	•	•	•	•	17	13	08	01	03	10	•	•	•	•	•	15	
III	6.9	6.6	5.5	6.2	141.0	03.6	94	73	87	85	32	058	015.2	22	•	10	•	•	•	•	03	13	14	12	01	14	•	•	•	•	•	01	02		
IV	7.4	7.8	6.4	7.2	121.6	06.8	93	73	86	84	34	026	006.4	16	•	•	•	•	•	•	13	13	05	•	13	•	•	•	•	•	•	01	02		
V	7.2	7.5	6.3	7.0	138.2	-	-	-	-	-	-	121	028.5	03	•	01	•	•	•	•	10	19	34	04	19	•	•	•	•	•	•	01	02		
VI	5.6	7.1	6.7	6.5	189.1	-	-	-	-	-	-	129	029.4	16	•	•	01	•	•	•	•	03	11	18	16	03	18	•	•	•	•	•	03	04	
VII	4.5	3.8	3.2	3.8	303.2	-	-	-	-	-	-	055	022.2	03	•	•	07	•	•	•	•	08	01	08	06	02	38	•	•	•	•	•	01	04	
VIII	3.9	4.9	2.8	3.9	259.1	-	-	-	-	-	-	035	014.6	11	•	•	08	01	•	•	•	04	02	09	08	01	09	•	•	•	•	•	01	03	
IX	6.3	6.2	4.1	5.5	149.1	-	-	-	-	-	-	108	031.2	01	•	•	07	01	•	•	•	04	08	12	10	03	12	•	•	•	•	•	02	07	
X	5.3	4.9	3.7	4.7	140.8	06.3	100	88	98	95	-	014	009.3	22	•	07	•	•	•	•	08	06	04	03	•	06	•	•	•	•	•	03	08		
XI	5.3	7.8	8.0	8.4	038.6	05.0	98	98	95	61	018	015.6	30	•	05	17	•	•	•	22	03	02	01	03	81	01	•	•	•	•	•	04	01		
XII	8.8	7.9	7.3	8.0	013.6	04.8	94	89	94	93	54	041	011.4	18	•	06	20	•	•	•	01	17	08	06	02	07	01	•	•	•	•	•	03	13	
GOD.	6.8	6.5	5.6	6.3	1635.7	-	-	-	-	-	-	645	031.2	04.IX	06	37	105	17	01	•	•	35	134	129	94	20	114	16	01	•	•	08	44	38	
TEKIJA																																			
BR. ST. 182																																			
I	7.8	6.1	6.2	6.7	-	03.9	90	80	87	86	42	027	036.8	25	•	02	28	•	•	03	03	02	13	13	06	•	03	11	01	•	•	13			
II	8.7	7.6	8.4	8.2	-	04.3	91	81	90	87	53	113	038.4	20	02	•	18	•	•	03	02	01	17	15	10	02	05	11	•	•	•	•	24		
III	7.6	7.4	7.4	7.5	-	06.0	84	69	80	77	39	039	010.6	25	•	02	•	•	•	07	02	01	16	10	08	01	10	•	•	•	•	•			
IV	9.2	8.0	7.7	8.3	-	37.5	86	68	84	79	45	076	013.2	28	•	•	•	•	•	04	01	•	18	18	16	02	18	•	•	•	•	04			
V	7.8	7.0	7.1	7.6	-	09.6	82	64	82	76	43	148	028.2	23	•	•	•	•	•	04	04	•	16	15	13	05	15	•	•	•	•	02			
VI	6.5	6.9	6.2	6.5	-	144.6	028.2	28	•	•	19	•	•	04	04	01	07	14	13	03	16	•	•	•	•	01	11	•	•	•	•	04			
VII	5.1	4.1	5.4	4.9	-	12.3	79	50	74	68	29	010	002.8	07	•	•	26	04	•	09	07	02	02	04	03	•	06	•	•	•	03				
VIII	6.2	5.7	4.5	5.5	-	12.0	82	50	72	68	34	012	004.2	12	•	•	23	04	•	03	02	02	05	03	03	•	09	•	•	•	03				
IX	7.3	6.2	6.0	6.5	-	063	033.2	01	•	•	08	•	•	08	04	03	13	10	12	10	01	12	•	•	•	•	•	01	12	•	•	01			
X	7.5	4.5	4.9	5.6	-	08.4	88	62	83	78	45	024	013.2	22	•	•	01	01	•	04	02	02	09	05	04	01	05	•	•	•	•	•	01		
XI	7.8	3.2	5.8	5.6	-	05.1	92	76	90	86	60	033	015.4	30	•	15	14	•	•	03	03	03	07	05	04	01	05	•	•	•	•	01	07		
XII	9.2	8.0	6.2	8.7	-	04.3	83	79	83	81	53	047	014.4	15	•	03	18	•	•	07	01	•	24	15	11	01	08	07	•	01	•	•	03	07	
GOD.	7.6	6.3	6.3	6.8	-	-	-	-	-	-	-	736	048.2	28.VI	02	05	79	77	10	•	61	35	17	147	135	101	17	108	29	01	•	01	24	04	46
NEGOTIN																																			
BR. ST. 183																																			
I	5.9	6.3	5.0	5.7	-	03.4	86	70	83	80	44	023	005.4	22	02	11	28	•	•	09	01	06	12	13	07	•	03	10	•	•	•	03	14		
II	8.5	7.9	7.6	8.0	-	043.4	03.7	90	78	90	86	47	078	026.6	20	04	05	21	•	•	07	03	02	20	18	11	02	11	11	•	•	09	26		
III	7.5	6.7	5.6	6.6	-	128.9	05.3	52	60	76	73	32	038	013.4	23	•	•	04	•	•	16	01	03	15	16	07	01	14	•	•	03				
IV	7.7	7.0	5.5	6.7	-	125.1	07.2	85	78	84	74	36	074	021.6	05	•	•	•	•	•	10	02	01	13	17	09	01	17	•	•	03				
V	6.5	7.0	5.5	6.6	-	179.8	09.2	76	58	76	70	34	069	017.4	03	•	•	02	•	•	08	02	•	12	15	10	03	15	•	•	04	•	04		
VI	4.1	5.6	5.5	5.1	-	252.2	11.8	78	53	76	69	34	028	028.5	16	•	•	18	01	•	13	02	03	05	10	08	03	10	•	•	06				
VII	3.0	3.3	1.8	2.7	-	349.9	11.7	76	45	71	63	36	015	007.4	16	•	•	26	03	•	17	03	13	02	05	03	03	05	•	•	04				
VIII	3.2	3.0	4.3	4.2	-	200.7	10.4	70	46	66	41	27	041	013.6	31	•	•	02	•	•	16	03	04	06	04	01	06	•	•	03					
IX	5.7	5.9	3.7	5.1	-	169.4	09.9	84	77	73	34	095	028.8	01	•	•	18	•	•	13	06	07	06	11	07	03	11	•	•	06					
X	4.2	6.1	2.8	5.7	-	192.8	07.6	91	56	83	77	39	024	011.6	22	•	•	02	•	•	04	01	13	04	03	01	05	05	•	•	06				
XI	5.5	6.2	2.7	6.1	-	126.8	04.3	88	67	85	80	36	025	018.7	30	•	19	•	24	•	10	02	06	05	03	01	05	05	•	•	05				
XII	7.6	8.0	6.6	7.4	-	347.9	04.3	80	80	85	41	034	010.8	15	•	06	23	•	•	11	02	16	18	10	14	04	01	01	01	05	13				
GOD.	5.8	5.9	4.6	5.4	-	-	-	-	-	-	-	961	044.2	04.IX	-	-	-	-	01	•	-	-	148	122	26	103	58	07	•	01	•	18</			

Mesec	Vremenski period	Temperatura vazduha °C										Čestina pravaca i srednja jačina vetrova m/s, fm (0-12)																			
		7		14		21		Srednji dnešnji		W		E		N		NE		E		SE		S		SW		N		NW		C	
		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
$\varphi = 43^{\circ}52' N \lambda = 19^{\circ}31' E$ Gr. $\Delta G = + 1h 19 min.$																										TITCVC UŽICE		BR. ST. 186			
I	-	-02.8	02.0	-01.2	-00.8	03.1	-04.1	12.5	29	-15.1	09	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
II	-	-01.6	04.0	00.9	01.0	05.2	-02.3	15.7	25	-14.5	21	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
III	-	02.9	10.8	06.0	06.4	12.1	02.0	21.1	30	-05.6	13	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
IV	-	06.7	13.4	09.2	09.6	14.6	05.6	23.6	12	06.9	18	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
V	-	10.6	17.4	12.3	13.2	18.7	06.7	24.0	01	-01.3	13	09	01.8	04	03.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
VI	-	14.8	22.0	16.1	17.3	23.6	12.1	30.1	12.10	08.0	30	06	02.4	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
VII	-	14.8	24.8	17.5	18.7	25.8	12.7	32.6	19	06.3	23	06	02.3	03	03.3	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
VIII	-	13.8	23.6	16.7	17.7	25.1	12.2	32.7	08	06.8	31	07	02.4	01	03.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
IX	-	10.6	18.3	12.4	13.4	19.9	09.6	28.1	11	03.4	22	06	02.3	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
X	-	06.7	13.6	08.8	09.5	14.8	05.9	23.7	03	-02.9	29	09	02.2	02	02.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
XI	-	00.1	04.7	01.6	02.0	05.8	-06.4	18.9	01	-05.4	20.14	03	02.0	04	02.8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
XII	-	00.8	04.7	01.8	02.3	05.7	-06.9	15.5	29	-08.2	06	06	01.8	02	02.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
GOD.	-	06.4	13.3	08.5	09.2	14.6	05.0	32.7	06.VII	-15.1	09.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
$\varphi = 43^{\circ}16' N \lambda = 20^{\circ}01' E$ Gr. $\Delta G = + 1h 20 min.$																										SJENICA		BR. ST. 187			
I	573.0	-07.3	-02.7	-05.9	-05.4	-01.5	-16.1	05.5	29	-24.0	10	10	02.6	-	-	03	02.0	27	02.5	10	02.3	06	01.8	-	-	03	02.0	34			
II	569.1	-09.4	00.2	-02.5	-02.5	02.0	-07.4	11.1	25	-26.6	21	17	01.9	03	02.0	03	01.7	11	01.9	09	02.3	04	01.8	02	02.5	07	01.7	28			
III	572.1	-01.1	06.6	02.0	02.3	08.6	-02.2	17.4	04	-09.5	13	21	02.4	04	02.0	06	01.8	09	02.1	07	01.7	11	03.1	03	02.7	12	02.2	20			
IV	567.7	03.5	08.9	04.8	05.5	10.3	01.3	18.9	12	-03.5	03	13	01.9	04	02.2	06	01.8	11	02.3	16	02.4	03	02.0	07	01.6	14					
V	573.2	07.3	12.9	08.5	09.3	14.4	04.3	22.9	01	-04.4	13	12	01.7	09	02.0	-	-	06	01.5	11	02.1	19	03.5	06	02.8	09	01.9	21			
VI	574.9	11.5	18.5	12.1	13.6	19.9	07.3	26.3	10	02.0	05	12	02.0	04	02.2	03	01.7	04	01.0	04	02.0	20	02.7	04	02.0	11	02.3	28			
VII	576.4	10.2	20.9	13.2	14.4	21.9	04.0	28.8	12	-00.4	24	12	02.0	09	02.0	05	01.8	02	01.0	12	02.7	09	02.1	05	02.0	37					
VIII	574.9	09.4	20.2	12.4	13.6	21.4	04.5	28.1	07	01.9	20	18	01.9	03	02.0	07	01.7	05	01.4	05	03.4	03	01.7	06	02.0	36					
IX	575.6	06.6	14.4	08.2	09.4	15.6	04.0	23.3	16	-01.6	22	17	02.4	05	01.4	03	01.7	03	01.2	04	02.5	07	01.9	20	02.1	26					
X	576.1	03.5	11.1	05.0	06.2	12.1	01.3	21.5	03	-07.0	29	06	02.0	09	01.7	08	01.9	11	01.9	03	01.3	05	02.0	04	01.2	08	01.5	29			
XI	580.0	-05.0	07.1	-02.2	-06.6	08.2	-06.0	16.5	10	-15.6	20.14	08	02.0	02	01.5	06	01.7	03	02.0	06	01.8	01	01.0	10	02.0	32					
XII	571.6	-01.2	03.2	-06.4	06.3	04.2	-04.1	11.0	29	-15.6	02	06	02.1	03	01.0	04	01.2	10	02.0	19	03.8	04	02.5	05	01.2	30					
GOD.	574.1	02.7	10.1	04.6	05.5	11.4	00.1	28.8	12.VII	-26.6	24.II	163	02.1	35	01.9	51	01.7	107	02.0	83	02.0	130	03.0	46	02.1	105	01.9	355			
$\varphi = 43^{\circ}41' N \lambda = 20^{\circ}01' E$ Gr. $\Delta G = + 1h 20 min.$																									UŽIČKA POZEGA		BR. ST. 188				
I	735.2	-04.1	01.3	-01.7	-01.6	02.7	-05.6	14.0	29	-15.3	09	08	01.4	13	01.7	07	01.3	01	01.0	07	01.1	11	01.1	30	01.1	03					
II	730.6	-02.9	03.7	00.0	00.2	05.4	-04.2	17.7	12	-20.8	22	10	01.4	10	01.0	09	01.4	05	01.4	02	01.5	02	02.0	12	01.2	27	01.2	07			
III	732.8	02.1	11.3	06.1	06.4	12.7	01.0	21.2	30	-05.9	13	19	01.4	06	01.5	05	02.0	03	01.3	03	01.7	12	02.2	09	01.3	33	01.8	05			
IV	729.9	06.4	14.4	09.7	10.1	15.5	04.9	24.3	12	00.1	18	03	01.3	11	01.7	09	01.9	08	01.5	10	03.0	04	01.0	25	01.9	12					
V	732.7	10.2	17.9	12.7	13.4	19.3	06.6	21.2	01	-01.3	13	11	01.5	03	01.3	14	01.6	05	01.8	11	02.3	07	02.0	06	01.8	09	01.9	27			
VI	733.5	13.6	22.5	16.3	17.2	23.9	11.1	31.0	12	06.6	30	11	01.4	06	01.5	13	01.2	02	01.0	03	02.0	09	01.6	13	01.7	33					
VII	735.1	13.2	25.0	17.4	18.6	26.1	11.0	32.3	19	-06.7	24	11	01.6	08	02.2	07	01.6	06	01.5	02	03.0	02	01.0	13	01.5	39					
VIII	735.7	12.4	24.3	16.2	17.3	25.3	10.5	33.4	08	02.0	22.20	11	01.9	03	01.0	14	01.8	04	02.2	04	01.5	02	01.0	11	01.7	42					
IX	735.0	09.9	19.0	12.0	13.2	20.3	08.2	27.4	11	-01.4	22	11	01.6	02	01.0	05	01.2	04	01.0	01	01.0	03	02.0	19	01.8	40					
X	736.8	06.3	14.3	07.9	09.1	15.5	04.9	25.3	04	-05.1	29	06	01.8	02	01.5	11	01.3	02													

Meseč	Oblačnost Nm (0-10)				Vlažnost vanduha	Padavine R mm	Broj dana n sas:																																			
	Inzolacijā broj sati			Sred. (Dias)			Tn	Tx	Tn	Tx	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	Δ	Θ	▲	■	R	T	≡	☒																
	7	14	21		mm	7	14	21	Max.	Min.	Σ	Max.	Dat.	=	<	<	≥	≤	<	>	≥	≤	9	8	2,0	8,0	0,1	1,0	0,0	9	8	2,0	8,0	0,1	1,0	0,0	9	8	2,0	8,0	0,1	1,0
TITOVO UZICE																										$H_a = 440 \text{ m } H_b = - \text{ m } h_c = 2.0 \text{ m } h_d = 1.2 \text{ m}$																
BR. ST. 186																																										
I	6.3	6.3	6.3	6.3	-	-	-	-	-	040	011.5	30	05	06	26	-	-	-	-	06	14	12	07	01	05	08	01	01	-	-	01	01	21									
II	7.7	7.8	8.2	7.9	-	-	-	-	-	093	029.9	14	02	02	22	-	-	-	-	02	16	17	13	03	05	16	01	01	-	-	01	01	24									
III	5.7	5.8	6.7	6.1	-	-	-	-	-	041	009.1	19	-	-	05	-	-	-	01	-	08	13	14	09	-	13	04	05	-	-	01	01	01									
IV	7.9	7.9	7.2	7.7	-	-	-	-	-	054	011.4	06	-	-	05	-	-	-	-	14	18	11	01	18	-	-	-	-	-	-	03	03	-	-	-	-	-					
V	7.7	7.8	7.1	7.5	-	08.8	86	61	84	77	25	100	012.1	11	-	-	01	01	-	-	02	-	11	22	16	03	21	02	-	-	-	-	-	-	07	-	-	-	-	-		
VI	5.2	6.6	4.8	5.5	-	10.9	83	57	81	74	37	114	027.0	16	-	-	15	02	-	-	01	-	04	08	13	10	09	13	-	-	-	-	-	-	06	-	-	-	-	-		
VII	2.2	3.7	3.2	3.0	-	11.3	83	49	80	71	29	034	010.2	16	-	-	19	04	-	-	04	-	14	01	07	04	02	07	-	-	-	-	-	-	06	-	-	-	-	-		
VIII	3.1	3.6	3.1	3.3	-	10.8	84	52	79	72	31	041	013.0	05	-	-	17	03	-	-	03	-	17	04	08	07	01	08	-	-	-	-	-	-	03	-	-	-	-	-		
GOD.	6.2	6.2	6.1	6.2	-	-	-	-	-	745	032.5	04.IX	07	12	95	38	89	-	-	-	-	65	130	148	104	22	125	37	08	02	01	-	-	27	33	43	-	-	-	-	-	-
SJENICA																										$H_a = 1015 \text{ m } H_b = 1016.2 \text{ m } h_c = 2.0 \text{ m } h_d = 1.5 \text{ m}$																
BR. ST. 187																																										
I	8.0	6.4	6.2	6.9	073.0	03.0	90	82	90	87	58	053	035.4	30	14	17	31	-	-	09	01	02	15	16	08	01	03	13	-	-	-	-	-	-	10	21						
II	8.4	8.4	7.1	8.0	068.2	03.5	90	78	88	85	50	070	020.8	14	07	12	23	-	-	07	01	01	16	17	10	02	04	16	01	01	-	-	-	07	22							
III	6.5	6.7	5.6	6.3	134.6	04.3	90	64	82	79	30	069	033.7	18	-	-	25	-	-	12	04	12	14	10	02	08	12	03	-	01	-	02	10									
IV	8.6	8.6	7.3	8.2	093.6	03.5	89	68	86	81	35	048	014.1	29	-	-	39	-	-	10	03	-	20	19	14	01	18	05	01	-	01	-	01	01	01							
V	7.9	8.3	6.9	7.7	138.3	07.0	88	66	85	80	31	145	020.8	09	-	-	04	-	-	11	02	-	16	23	17	06	22	02	-	-	-	02	-	07	04							
VI	6.6	6.9	4.8	6.1	243.0	05.0	87	59	82	76	37	095	030.4	16	-	-	03	-	-	11	01	-	08	12	03	09	03	12	-	-	-	01	-	00	00							
VII	4.5	4.2	2.4	3.7	312.7	08.5	90	44	77	71	29	022	011.4	16	-	-	05	-	-	04	01	07	01	06	03	01	06	-	-	-	03	14										
VIII	5.2	5.6	2.4	4.4	248.9	08.7	93	52	84	76	27	083	021.1	12	-	-	07	-	-	10	01	08	06	09	08	04	09	-	-	-	01	07	13									
IX	7.7	7.0	5.7	6.8	132.0	07.5	94	67	91	84	27	174	031.0	13	-	-	02	-	-	05	01	02	12	12	05	12	01	-	-	-	03	16										
X	8.5	5.4	5.0	6.3	117.7	06.3	95	55	70	80	49	028	009.3	22	-	01	10	-	-	02	-	02	13	14	05	-	10	-	-	-	12	22										
XI	6.8	4.1	4.1	5.0	139.1	03.6	92	52	81	80	19	010	006.9	30	05	01	26	-	-	02	09	09	03	03	02	02	-	-	-	06	02											
XII	7.6	8.3	6.8	7.6	053.7	04.3	90	78	87	85	34	065	016.3	20	09	04	20	-	-	08	07	-	15	16	11	02	12	06	01	-	01	-	01	07	14							
GOD.	7.2	6.7	5.4	6.4	1775.2	05.9	90	65	86	80	19	862	051.0	13.IX	35	37	150	15	-	91	21	38	143	159	107	27	118	46	08	01	01	05	01	31	103	88	-	-	-			
UZICKA POZEGA																										$H_a = 311 \text{ m } H_b = 312.1 \text{ m } h_c = 2.0 \text{ m } h_d = 1.5 \text{ m}$																
BR. ST. 188																																										
I	7.9	6.6	6.1	6.9	063.4	03.6	91	74	88	85	52	032	009.6	30	07	09	29	-	-	01	01	03	16	14	08	-	06	09	01	-	-	08	20									
II	9.1	8.1	8.0	8.4	063.1	04.0	93	69	88	84	32	091	032.8	14	03	03	23	-	-	18	17	12	03	09	15	03	01	01	-	-	07	22										
III	7.7	6.3	5.3	6.4	137.7	05.0	88	51	75	72	23	035	016.0	22	-	-	10	-	-	03	01	05	12	19	10	02	18	05	03	-	-	03	-	-								
IV	8.6	7.6	6.0	7.4	106.6	06.3	87	51	71	79	24	051	008.9	06	-	-	05	-	-	13	18	12	-	-	01	-	03	07	-	-	-	-	-	-								
V	8.7	8.1	6.5	7.8	110.6	08.6	90	55	82	76	18	090	010.2	23	-	-	01	02	01	-	02	01	17	23	19	01	23	02	-	-	01	08	12									
VI	6.4	6.6	4.6	5.9	127.0	04.6	89	52	80	74	31	098	030.4	16	-	-	15	02	-	02	07	15	11	03	15	-	-	-	-	-	-	09	10	-	-	-						
VII	8.1	4.1	3.8	3.6	111.1	03.1	83	50	85	73	29	049	02																													

Mesto	Vrednost mernog instrumenta mm	Temperatura vanduha °C										Čestina pravaca i srednja jačina vetrova m/s, fm (0-12)																													
		Ta			Sred. Gdje			Ra.				Ra.				N			NE			E			SE			S			SW			W			NW				
		7	14	21				Ra.	Ra.	Ra.	Ra.	Ra.	Ra.	Ra.	Ra.	Ra.	Ra.	Ra.	Ra.	Ra.	Ra.	Ra.	Ra.	Ra.	Ra.	Ra.	Ra.	Ra.	Ra.	Ra.	Ra.	Ra.	Ra.	Ra.	Ra.						
$\varphi = 43^{\circ}53' N \lambda = 20^{\circ}19' E$ Gr., AG = + 1h 21 min.																																									
I	-	-02.2	02.6	-01.6	-00.4	03.3	-03.6	11.5	29	-12.0	09	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-							
II	-	-00.9	04.7	01.2	01.6	05.7	-01.8	17.8	28	-10.2	21	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-							
III	-	03.6	11.3	06.3	04.8	12.7	02.1	20.5	30	-03.2	09	09	01.4	01	01.0	08	01.4	01	03.0	14	01.1	15	02.5	21	01.2	04	02.2	20	01.4	01	02.2	20									
IV	-	07.4	14.6	09.1	10.1	15.7	03.4	22.7	12	01.8	18	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-								
V	-	11.5	18.3	12.0	13.5	19.3	08.7	31.0	01	-01.5	13	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-							
VI	-	16.0	23.2	16.1	17.8	24.5	12.1	29.8	12	16.0	29.27	02	02.5	03	01.3	23	01.1	01	01.0	01	01.0	02	02.5	20	01.4	01	01.4	20	01.4	01	01.4	20	01.4	01	01.4						
VII	-	16.6	26.7	17.0	19.4	27.0	12.4	34.3	19	04.5	01	02	01.0	02	20.7	01.4	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
VIII	-	15.3	23.6	16.3	18.4	24.4	11.9	34.0	08	08.2	28	05	01.6	06	01.3	21	01.1	01	02.0	01	01.0	01	04.0	10	01.2	03	01.0	10	01.2	03	01.0	10	01.2	03	01.0						
IX	-	11.4	19.7	12.8	14.2	20.8	09.2	28.0	11	03.4	21	06	01.5	-	-	-	23	01.1	01	02.0	08	01.4	02	01.5	09	01.6	-	-	-	-	-	-	-	-	-	-	-				
X	-	07.0	15.2	08.8	10.0	15.9	03.6	25.0	04	-04.2	29	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
XI	-	00.6	04.6	01.5	02.0	05.0	-02.0	11.7	03	-04.7	17.16	01	01.0	-	-	14	01.1	01	02.0	09	01.2	03	02.3	15	01.3	-	-	-	-	-	-	-	-	-	-	-					
XII	-	08.8	04.8	01.4	02.1	03.5	-01.4	17.3	29	-07.5	06.05	08	01.0	01	02.0	11	01.5	02	01.5	06	01.2	07	02.4	12	01.1	01	02.0	12	01.1	01	02.0	12	01.1	01	02.0						
GOD.	-	07.3	14.3	08.5	09.6	15.2	05.0	34.5	(9.VII - 14.2)		24.11	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
$\varphi = 43^{\circ}51' N \lambda = 20^{\circ}31' E$ Gr., AG = + 1h 22 min.																																									
I	-	-03.9	01.5	-02.0	-01.6	01.9	-05.5	09.0	29	-10.5	09	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
II	-	-01.9	04.9	00.6	01.1	05.9	-03.4	16.5	26	-17.0	21	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
III	-	01.3	09.6	03.0	03.2	11.4	00.3	21.5	00	-04.5	29	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
IV	-	04.4	11.9	08.0	08.1	13.4	03.2	21.0	12	01.8	02	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
V	-	08.7	14.3	10.7	11.6	17.7	07.0	25.1	01	-03.5	13	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
VI	-	12.2	22.9	14.0	15.8	23.8	0.9	29.8	11	05.5	01	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
VII	-	11.6	24.8	15.2	16.7	25.6	0.9	33.7	19	05.0	24	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
VIII	-	11.2	23.6	14.8	16.1	25.0	0.7	32.8	03	05.8	14	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
IX	-	09.7	17.0	11.9	12.7	18.7	0.4	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
X	-	02.1	09.5	03.8	04.8	10.8	0.6	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
XI	-	-01.9	06.2	-00.8	00.7	04.9	-03.6	11.6	03	-10.6	21	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-					
XII	-	-00.3	05.3	00.6	01.7	06.2	-02.7	16.0	29	-09.6	02	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-					
GOD.	-	04.4	12.8	06.8	07.7	13.9	02.6	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
$\varphi = 43^{\circ}44' N \lambda = 20^{\circ}41' E$ Gr., AG = + 1h 23 min.																																									
I	742.7	-01.3	03.4	06.8	00.9	04.1	-02.5	13.6	13	-10.6	09	01	02.0	03	01.3	38	04.2	04	01.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
II	739.0	-00.3	03.4	02.6	02.6	04.6	-01.4	20.2	20	-15.0	21	01	01.0	0	0	19	02.9	01	05.0	03	01.7	02	04.5	02	01.5	15	01.8	03	01.3	44	01.5	01.5	01.5	01.5	01.5	01.5	01.5				
III	741.1	04.1	11.9	07.7	07.9	13.2	02.9	20.1	30	-02.3	13.09	02	01.5	02	02.0	19	02.6	04	02.0	02	04.5	02	01.5	15	01.8	03	01.3	44	01.5	01.5	01.5	01.5	01.5	01.5	01.5						
IV	738.0	08.2	14.9	10.4	11.0	16.1	0.6	06.4	23.2	12	02.5	18	03	01.7	02	01.5	28	02.8	01	02.0	03	01.0	08	01.9	02	01.5	02	01.5	02	01.5	02	01.5	02	01.5	02	01.5	02				
V	740.7	12.1	18.6	14.5	19.9	09.7	21.0	01.7	01.0	-01.6	13	03	01.7	02	02.0	19	03.0	03	02.0	03	01.7	05	02.2	07	01.9	01	01.4	01	01.4	01	01.4	01	01.4	01	01.4	01	01.4	01			
VI	741.3	16.0	23.2	17.4	18.5	24.7	12.4	30.2	12	10.0	01.0	02.7	01	01.0	03	02.5	01	01.0	03	02.5	01	01.0	07	02.0	16	02.1	04	02.0	02	01.5	02	01.5	02	01.5	02	01.5	02	01.5	02	01.5	02
VII	742.8	16.3	26.1	19.1	20.2	27.0	12.8	35.3	19	08.7	23	05	01.8	06	02.0	15	02.1	01	04.0	03	02.0	02	02.0	02	01.0	07	02.0	02	01.5	02	01.5	02	01.5	02	01.5	02	01.5	02			
VIII	743.5	14.9	25.0	18.1	19.2	26.7	13.1	35.4	08	07.8	23	10	01.7	02	02.1	03	02.3	03	01.3	03	02.5	01	01.0	05	02.0	14	01.7	04	01.0	06	02.0	02	01.5	02	01.5	02	01.5	02			
IX	-	10.7	19.0	12.7	13.8	20.1	09.0	26.3	11	02.5	22	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
X	-	04.5	14.7	08.8	06.7	15.6	05.3	27.0	29	06	01.5	03	02.3	02	03.0	03	02.3	03	01.3	03	02.5	01	01.0	08	01.8	02	01.0	05	01.5	04	01.5	04	01.5	04	01.5	04	01.5	04	01.5	04	
XI	-	00.5	04.4	01.4	02.0	05.0	-00.4	11.6	01	-04.3	17	18	01.0	08	01.2	03	02.0	03	01.2	03	02.0	03	01.0	08	01.8	02	01.0	06	01.5	04	01.5	04	01.5	04	01.5	04	01.5	04	01.5	04	
XII	-	00.9	04.9	01.5	02.8	05.0	-01.1	18.4	08	-																															

Mjesec	Oblačnost Nm (0-10)			Vlažnost vazduha %	Padavine R mm	Broj dana na sat																											
	Inzolacijski broj sati					U m t			Tn	Tx	Tn	Tx	Tn	F(0-12)	Rm(0-10)	R mm	•	*	•	Δ	▲	▲	R	T	≡								
	7	14	21	Broj (Dnev.)	7	14	21	Min.	Max.	Dat.	≤	<	<	≥	≥	≥	≤	<	>	≥	≤	≥	•	Δ	▲	▲	T	≡					
CACAK																																	
BR. ST. 191	$H_a = 250 \text{ m} H_b = - \text{ m} h = 2.0 \text{ m} h = 1.0 \text{ m}$																																
I 6.0 6.0 5.4 5.6	-	-	-	-	-	-	-	-	028	009.3	30	02	07	28	-	-	-	08	11	09	07	05	04	-	-	-	-						
II 7.9 6.9 7.3 7.6	-	-	-	-	-	-	-	-	078	029.2	14	02	-	20	-	-	-	03	14	14	12	02	09	10	03	-	-						
III 5.7 5.8 5.4 5.6	-	-	-	-	-	-	-	-	061	016.3	22	-	-	05	-	-	-	09	13	16	10	02	15	01	-	-	-						
IV 6.8 6.9 5.7 6.5	-	-	-	-	-	-	-	-	059	010.4	04	-	-	-	-	-	-	11	14	11	01	14	-	-	-	-	04						
V 7.8 7.2 6.6 7.2	-	-	-	-	-	-	-	-	115	024.6	09	-	-	01	02	01	-	-	01	13	22	20	01	22	-	-	-	-	07	03			
VI 5.3 5.5 4.7 5.2	-	-	-	-	-	-	-	-	103	030.3	14	-	-	05	-	-	-	05	04	12	12	03	12	-	-	-	-	04	-				
VII 2.5 2.6 2.4 2.5	-	-	-	-	-	-	-	-	034	018.2	16	-	-	22	05	-	-	18	-	05	04	01	05	-	-	-	-	03	-				
VIII 3.2 3.9 3.4 3.5	-	-	-	-	-	-	-	-	034	008.0	06	-	-	20	07	-	-	14	03	08	07	08	-	-	-	-	04	-					
IX 5.2 5.8 4.3 5.1	-	-	-	-	-	-	-	-	156	068.0	01	-	-	04	05	-	-	-	08	09	09	09	04	08	-	-	-	-	03	-			
X 6.0 5.1 4.5 5.2	-	-	-	-	-	-	-	-	022	013.2	22	-	-	04	01	-	-	-	-	09	04	01	01	01	01	-	-	-	-	07	03		
XI 8.1 7.4 7.3 7.6	-	04.8	91	80	91	87	53	020	011.2	30	-	01	17	-	-	-	-	03	18	06	03	01	36	02	02	-	-	09	03				
XII 8.0 7.3 5.8 7.0	-	04.7	91	78	89	86	35	064	016.2	14	-	05	21	-	-	-	-	01	12	08	08	02	08	02	02	-	-	08	03				
GOD.	6.0	5.9	5.2	5.2	5.7	-	-	-	-	776	068.0	04.IX	04	13	96	68	13	-	-	-	132	107	18	121	20	08	-	-	-	23	27	23	
NOVI PAZAR																																	
BR. ST. 192	$H_a = 343 \text{ m} H_b = - \text{ m} h = 2.0 \text{ m} h = 1.3 \text{ m}$																																
I 6.7 5.1 5.0 5.6	-	-	-	-	-	-	-	-	022	010.6	30	08	10	27	-	-	-	04	05	07	04	01	02	05	-	-	-	-	04	14			
II 6.6 5.1 4.5 5.4	-	-	-	-	-	-	-	-	050	016.2	14	02	04	22	-	-	-	05	09	14	10	01	03	12	01	-	-	-	-	14	-		
III 4.5 3.6 4.6 4.2	-	-	-	-	-	-	-	-	055	022.3	18	-	-	11	-	-	-	04	04	09	07	02	09	02	-	-	-	-	04	-			
IV 6.4 4.8 5.0 5.6	-	-	-	-	-	-	-	-	041	016.1	29	-	-	03	-	-	-	02	07	16	10	01	14	-	-	-	-	01	-				
V 6.2 5.5 6.7 6.1	-	-	-	-	-	-	-	-	100	014.0	19	-	-	02	01	-	-	-	05	10	17	17	05	16	01	-	-	-	02	01			
VI 5.5 5.3 5.6 5.5	-	-	-	-	-	-	-	-	060	012.4	16	-	-	15	-	-	-	04	05	09	09	01	09	-	-	-	-	04	-				
VII 2.8 3.2 3.3 3.1	-	-	-	-	-	-	-	-	032	024.6	16	-	-	19	05	-	-	-	12	02	05	02	01	05	-	-	-	-	01	-			
VIII 3.3 2.8 3.4 3.2	-	-	-	-	-	-	-	-	057	023.4	05	-	-	17	02	-	-	-	15	04	10	09	01	10	-	-	-	-	03	01			
IX 7.0 6.0 5.7 6.2	-	-	-	-	-	-	-	-	210	063.1	13	-	-	-	-	-	-	-	10	10	07	10	-	-	-	-	02	02					
X 6.4 5.2 6.1 5.9	-	-	-	-	-	-	-	-	020	066.6	21	-	-	-	-	-	-	02	-	-	05	04	02	-	-	-	-	02	-				
XI 8.0 2.9 3.5 4.8	-	-	-	-	-	-	-	-	007	007.3	30	01	01	26	-	-	-	01	04	07	01	01	01	01	-	-	-	-	15	01			
XII 7.3 5.2 6.1 6.3	-	-	-	-	-	-	-	-	071	030.2	19	-	03	23	-	-	-	01	01	09	15	08	02	11	04	01	-	-	03	11			
GOD.	5.9	4.6	5.0	5.2	-	-	-	-	-	725	063.1	15.IX	-	-	-	-	-	-	-	118	93	22	93	27	04	-	-	-	17	32	45		
KRALJEVO																																	
BR. ST. 193	$H_a = 219 \text{ m} H_b = -221.0 \text{ m} h = -2.0 \text{ m} h = 1.4 \text{ m}$																																
I 6.1 7.1 5.5 6.2	070	0.3	03.8	84	70	79	77	45	023	006.9	26	02	06	26	-	-	09	02	04	13	10	36	05	06	01	01	01	03	03				
II 8.2 7.8 7.8 8.2	072	0.8	04.4	87	70	80	79	31	078	021.2	14	02	02	19	-	-	01	01	19	14	13	02	07	14	04	01	01	04	16				
III 6.6 6.5 5.6 6.3	150	0.5	05.2	82	53	67	67	25	065	013.0	22	-	-	06	-	-	03	06	13	16	11	01	13	04	02	-	-	01	-				
IV 7.7 8.1 6.0 7.3	139	2	06.6	80	54	71	68	27	044	008.5	06	-	-	-	-	-	04	01	15	16	10	-	14	-	-	01	03	-					
V 8.1 8.1 7.5 7.9	125	3	09.3	85	59	81	75	28	107	018.5	11	-	-	01	02	01	03	01	18	22	15	03	22	-	-	-	-	06	06				
VI 6.2 7.0 4.0 5.8	202	3	11.4	83	58	74	72	36	093	034.2	16	-	-	17	02	-	02	03	08	13	11	03	13	-	-	-	-	06	01				
VII 3.0 3.6 2.3 3.0	290	0	11.8	83	46	72	67	29	025	012.0	14	-	-	22	06	-	01	13	01	06	04	01	08	-	-	-	-	03	01				
VIII 3.9 4.7 3.3 4.0	267	0	10.8	83	45	71	67	22	050	018.9	11	-	-	20	06	-	03	03	08	03	09	07	01	09	-	-	07	01					
IX 6.3 7.1 5.5 6.3	141	5	09.9	93	61	83	79	42	184	041.9	01	-	-	07	-	-	04	11	11	08	04	11	-	-	-	-	03	07					
X 5.9 5.2 3.6 4.9	124	0	07.8	91	63	83	79	41	024	015.2	22	-	-	03	02	-	08	08	10	04	01	08	02	-	-	-	-	13	-				
XI 9.6 7.9 7.2 8.2	030	0	04.7	90	78	86	85	33	022	017.9	30	-	01	15	-	01	01	20	05	02	01	04	02	-	-	-	-	11	08				
XII 9.0 6.5 7.1 8.2	030	0	04.8	86	81	84	84	44	064	016.7	18	-	03	19	-	08	03	19	14	06	03	12	05	01	01	02	-	16	09				
GOD.	6.6	6.6	5.7	6.3	-	-	-	-	-	752	058.5	04.IX	05	12	93	66	09	-	07	-	55	146	156	97	25	132	36	09	-	01	27	30	35
ALEKSANDROVAC																																	
BR. ST. 195	$H_a = 360 \text{ m} H_b = - \text{ m} h = 2.0 \text{ m} h = 1.5 \text{ m}$																																
I 5.9 3.8 6.2 5.3	-	-	-	-	-	-	-	-	024	010.0	02	02	08	28	-	-	03	05	08	07	07	01	01	04	-	-	-	-	12	-			
II 6.2 5.0 6.8 6.0	-	-	-	-	-	-	-	-	045	011.0	14	02	04	23	-	-	-	07	11	13	13	21	02	11	-	-	-	-	11	-			
III 5.0 2.7 4.4 4.0	-	-	-	-	-	-	-	-	040	016.0	22	-	-	04	-	-	-	14	07	11	09	01	09	03	-	-	-	-	02	-			
IV	-	-	-	-	-	-	-	-	034	005.0	05	-	-	-	-	-	-	-	12	10</													

Mjesec	Vremenski prstenski m.	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta m/s, Fm (0-12)																									
		TM			Sred. (Hr.)			Hr.			Hr.			Dati.			Dati.			N		NE		E		SE		S		SW		W		NW		C	
		7	14	21	Sred. (Hr.)	Hr.	Hr.	Hr.	Hr.	Hr.	Dati.	Hr.	Hr.	Dati.	Hr.	Dati.	č.	č.	č.	č.	č.	č.	č.	č.	č.	č.	č.	č.	č.								
$\varphi = 43^{\circ}52' N \lambda = 21^{\circ}06' E$ Gr. AG + 1h 24 min.																										REKOVAC		BR. ST. 196									
I	-	-01.6	03.6	00.1	00.5	04.2	-03.4	13.0	13	-11.4	09	02	03.0	.	.	02	01.5	08	01.9	16	01.6	01	01.0	01	02.0	07	02.9	56									
II	-	-00.3	05.6	01.6	02.1	04.6	-02.3	19.8	24	-15.2	21	03	01.0	.	.	01	03.0	05	02.0	03	01.0	.	.	02	03.0	11	02.2	59									
III	-	02.6	12.1	06.1	07.0	15.0	01.7	20.2	05	-05.0	13	04	01.3	.	.	03	01.3	04	02.8	06	01.6	.	.	01	03.0	28	02.6	49									
IV	-	07.8	15.0	09.5	10.4	16.0	05.0	23.7	12	01.5	24	04	01.5	03	01.7	.	.	08	02.1	10	02.1	03	02.0	03	01.7	08	01.9	51									
V	-	12.5	18.2	12.6	14.0	19.5	08.8	26.0	01	-02.3	13	08	01.8	.	.	02	02.0	.	.	11	01.6	03	02.7	02	02.0	09	02.1	58									
VI	-	16.4	23.1	16.4	18.1	24.4	11.4	29.5	11	08.2	27	01	01.0	.	.	02	01.5	.	.	06	01.3	.	.	05	02.6	16	02.8	60									
VII	-	16.3	23.0	19.2	27.0	11.7	35.4	19	08.2	23	02	01.0	.	.	01	03.0	06	01.7	.	.	05	02.2	16	02.4	63												
VIII	-	15.0	25.3	16.1	18.1	26.3	10.4	35.0	08	06.2	28	05	02.0	.	.	02	01.5	.	.	07	01.6	.	.	05	02.0	06	02.0	68									
IX	-	10.7	19.4	12.6	13.8	20.9	08.3	28.3	24	01.0	22	06	01.5	.	.	01	02.0	.	.	04	03.2	21	02.4	58													
X	-	05.9	15.6	08.3	09.5	16.4	03.9	24.8	03	-03.4	29	05	02.2	.	.	03	01.7	.	.	01	02.0	11	02.7	70													
XI	-	00.3	04.9	01.4	02.0	05.7	-00.8	13.4	26	-07.2	16	02	01.5	.	.	07	01.4	.	.	02	02.0	09	02.1	70													
XII	-	00.6	05.7	01.7	02.4	06.7	-01.4	18.4	24	-11.9	07	.	01	01.0	01	01.0	01	03.0	05	01.2	02	01.5	01	04.0	10	01.7	72										
God.	-	07.3	14.5	08.4	09.4	15.6	06.4	35.4	49.VII	-19.2	24.II	38	01.7	04	01.5	17	01.6	27	02.2	82	01.6	09	02.0	32	02.4	152	02.4	734									
$\varphi = 43^{\circ}59' N \lambda = 21^{\circ}14' E$ Gr. AG + 1h 25 min.																									SVEZOZAREVO		BR. ST. 197										
I	-	-01.4	03.6	00.5	00.8	04.4	-02.3	13.0	13	-10.0	09	10	01.7	.	.	.	28	03.2	01	01.0	06	02.0	01	02.0	.	.	47										
II	-	-00.1	05.0	02.0	02.2	06.0	-02.4	19.5	24	-13.2	21	06	01.2	.	.	.	05	02.0	10	01.3	12	02.1	73										
III	-	03.6	11.9	07.1	07.4	12.7	02.1	20.0	00	-04.6	09	25	01.3	10	01.3	12	02.1	46										
IV	-	06.2	15.0	09.8	10.8	16.3	05.8	22.4	12	00.1	07	06	01.3	26	01.4	09	01.8	49											
V	-	12.3	18.2	13.7	14.5	20.3	08.8	27.4	01	-02.4	13	14	01.3	19	01.5	02	03.0	58										
VI	-	16.1	23.2	16.8	18.2	24.5	-	29.5	12	-	33	01.7	11	01.0	.	.	01	01.0	.	.	.	45										
VII	-	16.7	26.1	18.4	19.9	27.2	12.7	34.5	19	06.0	25.3	23	02.4	16	01.9	02	02.0	49										
VIII	-	14.7	25.0	17.9	18.7	26.0	10.8	34.0	08	07.0	22	22	02.0	13	02.3	01	03.0	57										
IX	-	11.2	19.7	13.3	14.4	20.9	08.5	26.4	20	01.1	22	28	02.6	04	02.0	01	02.0	57										
X	-	07.0	15.6	09.1	10.2	16.3	04.3	24.8	06	-05.2	29	11	02.6	17	02.6	65										
XI	-	01.3	04.7	01.5	02.3	05.4	-00.9	14.0	26	-06.0	26	16	07	02.0	05	01.8	78										
XII	-	01.0	05.3	02.3	02.7	06.1	-01.5	14.0	29	-10.0	07	08	02.0	06	05.3	.	.	08	02.1	71									
God.	-	07.6	14.4	09.3	10.2	15.5	-	34.5	49.VII	-	196	01.9	06	05.3	33	03.0	130	01.8	33	02.1	02	01.5	.	.	695								
$\varphi = 43^{\circ}01' N \lambda = 21^{\circ}16' E$ Gr. AG + 1h 26 min.																									KURSUMLIJA		BR. ST. 198										
I	-	722.1	-02.1	03.7	06.5	00.1	04.4	-03.6	12.6	13	-13.7	09	09	02.0	06	01.5	.	.	07	01.6	11	02.3	16	01.8	.	.	15	01.4	29								
II	723.6	-00.1	05.7	02.2	02.5	07.4	-01.6	18.3	23	-14.8	21	17	01.7	15	01.6	01	02.0	04	02.2	11	03.1	21	01.8	.	.	07	01.4	08									
III	726.0	03.1	11.3	05.9	06.4	12.9	01.6	23.0	04	-03.9	13	12	03.3	16	01.6	02	03.5	01	05.0	17	03.2	27	01.7	.	.	06	01.8	12									
IV	723.6	07.2	14.0	09.9	08.8	15.8	15.4	04.6	24.1	30	00.6	19	12	01.6	06	01.2	02	01.0	08	02.4	15	02.5	16	02.0	.	.	09	01.1	20								
V	724.0	11.1	17.6	12.0	13.0	18.2	09.8	26.0	01	-02.7	13	11	01.4	11	01.1	01	02.0	09	02.1	14	02.9	21	01.3	.	.	05	01.0	21									
VI	724.5	15.4	23.3	15.4	17.4	24.8	10.9	31.1	11	07.3	02	11	01.8	05	01.2	06	01.6	07	01.6	07	02.1	21	01.1	.	.	04	01.2	35									
VII	724.0	15.3	24.0	16.0	16.7	27.0	10.8	33.7	19	05.7	23	09	02.0	13	01.5	01	02.0	06	01.7	05	02.2	31	01.3	.	.	07	01.1	21									
VIII	724.7	13.4	25.1	15.6	17.4	26.5	10.5	33.2	08	06.1	20	12	02.4	05	02.2	06	02.0	.	.	08	01.1	03	02.3	.	.	05	01.2	14									
IX	727.9	10.4	19.2	12.0	13.4	20.5	08.0	28.0	12	00.1	22	11	01.5	07	01.3	02	01.0	34	01.8	05	01.6	34	01.1	.	.	10	01.3	17									
X	731.0	05.6	15.3	07.0	09.2	16.2	04.0	27.7	03	-03.1	23	10	02.5	16	02.1	01	01.0	09	01.7	32	01.2	.	.	08	01.9	21											
XI	734.2	-00.9	05.1	00.7	01.4	05.8	15.0	23.0	05	-06.6	16	01.6	26	01.4	06	02.0	04	02.8	19	01.4	.	.	02	01.0	08	02.0	18										
XII	734.5	01.4	05.3	02.2	03.0	06.0	-00.4	13.4	27	-06.6	26	07	01.7	04	01.																						

Meseč Broj	Oblačnost Nm (0-10)				Uzakost vazduha km	Vlažnost vazduha %	Padavine mm	Broj dana na sat																																							
								Tn				Tx				Tn		Tx		Tx		Tn		P(0-12)		Nm(0-10)		R mm		•		*		Δ		θ		J		A		R		T		≡	
	7	14	21	Grad.	Grad.	Grad.	Grad.	7	14	21	Grad.	Grad.	Grad.	Grad.	7	Max	Dat.	≤	<	<	≥	≥	≥	≥	≥	<	>	≥	≥	≥	≥	≥	≥	≥	≥	≥	≥	≥									
BR. ST. 196 REKOVAC																																															
I 5.4 6.2 5.6 5.7	-	04.0 84 70 86 81 40	016 004.6	26	02	06	27	.	.	.	01	.	09	10	07	05	03	04	02	01													
II 8.1 7.4 7.6 7.7	-	04.4 85 69 85 81 34	062 016.2	14	02	01	19	.	.	.	01	.	01	16	13	11	01	03	10	01	01	12															
III 5.2 5.5 4.9 5.2	-	05.3 83 52 77 71 26	058 012.0	22	.	08	.	.	.	03	.	07	10	12	10	02	10	04	02	01																	
IV 7.4 7.6 6.6 7.2	-	06.6 81 53 77 70 31	031 019.4	06	01	.	13	13	08	01	13	02	01																
V 6.8 7.1 6.7 6.9	-	09.5 83 64 86 78 36	154 034.5	21	.	.	01	02	14	20	17	04	20	01	01																		
VI 4.3 5.7 4.3 6.7	-	11.6 92 62 90 81 46	085 027.6	22	.	.	17	05	04	13	09	03	13	02	01																			
VII 2.3 2.6 3.6 2.8	-	11.5 80 46 80 69 22	015 008.8	16	.	.	22	85	.	.	.	12	04	03	04	01	01																			
VIII 3.2 3.6 4.3 3.7	-	10.8 83 46 82 70 21	042 009.8	11	.	.	20	05	.	.	.	10	10	08	03	10	09	01	01																			
IX 5.1 5.7 5.2 5.4	-	09.9 91 61 89 80 44	155 054.4	01	.	.	08	.	.	.	07	06	12	11	04	12	01	01																				
X 4.9 4.5 4.6 4.7	-	07.5 92 62 90 81 44	013 007.4	22	.	07	02	.	.	.	10	04	06	04	06	04	03	03																				
XI 8.4 7.9 8.3 8.2	-	34.6 89 76 70 85 44	029 017.8	30	01	21	.	.	.	03	22	06	03	01	06	32	01	05	05																				
XII 7.9 7.5 7.9 7.7	-	04.9 93 75 89 85 42	085 016.4	14	01	04	21	.	.	01	.	18	16	09	03	10	09	02	04																				
GOD. 5.8 5.9 5.8 5.8	-	07.5 85 61 84 77 21	745 054.4	04.IX	05	12	104	71	10	.	07	.	-	-	132	100	19	112	29	02	.	.	01	.	14	36																	
BR. ST. 197 SVETOZAREVO																																															
I 6.2 6.4 5.8 6.1	-	03.9 83 74 81 79 50	012 004.2	05	01	02	23	.	.	.	06	.	08	17	06	04	03	03	02	04																			
II 8.4 8.0 8.4 8.2	-	14.6 90 72 84 82 39	065 017.0	14	02	01	21	.	.	.	04	.	18	13	11	01	08	08	01	03	12																			
III 6.1 5.8 6.4 6.1	-	05.3 87 57 77 74 23	060 018.0	19	.	04	.	.	.	02	.	04	13	12	03	13	03	01	05	01																				
IV 7.1 7.4 7.3 7.3	-	07.0 82 50 76 72 31	041 012.0	04	02	.	14	13	09	01	13															
V 7.3 7.8 8.0 7.7	-	09.8 87 66 83 79 36	113 028.2	29	.	.	01	06	.	.	01	01	17	17	17	02	17	03	01																				
VI 5.0 6.4 6.6 5.3	-	12.5 87 63 84 78 45	106 022.4	16	.	.	17	.	.	01	04	05	14	12	05	14	01	01																					
VII 4.4 5.2 3.0 3.6	-	12.1 82 44 77 69 36	017 009.2	16	.	.	24	07	.	01	07	02	03	03	03	03	03	03	01	06																				
VIII 3.5 3.8 3.3 3.6	-	11.6 86 54 77 73 30	046 013.4	09	.	.	19	03	.	02	11	04	10	04	10	04	10	04	01	04																				
IX 5.2 5.1 5.2 5.2	-	09.9 91 61 89 80 35	129 052.0	01	.	.	06	.	.	01	01	09	10	09	07	04	09	01	02																					
X 6.5 4.1 4.3 4.9	-	07.8 89 64 87 80 44	011 004.6	22	.	05	02	.	.	08	09	04	04	04	04	04	04	04	02	01																				
XI 9.5 6.5 8.0 8.6	-	-	-	024 013.5	30	01	18	.	.	22	04	03	01	03	01	03	01	03	01	01	01	01	01	01	01	01	04	03	02																		
XII 8.9 8.0 8.0 8.3	-	05.6 90 80 88 87	054 011.2	14	01	05	19	.	.	02	01	19	13	09	01	10	05	01	04																				
GOD. 6.5 6.2 6.0 6.2	-	-	-	698 052.0	04.IX	-	08	-	72	12	-	14	02	57	152	119	100	19	107	21	02	.	01	01	06	49																	
BR. ST. 198 KURSUMIJA																																															
I 6.6 6.5 4.9 6.0	063.6	037.7	86 61 80 76 36	016 005.7	05	01	05	24	.	.	02	.	05	16	09	05	02	08	01	06																			
II 7.8 7.8 6.6 7.5	062.8	045.6	85 66 81 77 37	065 018.8	14	02	02	19	.	.	01	.	02	17	15	12	02	09	11	04	10	.																		
III 6.3 6.6 4.6 5.8	-	04.8 80 51 71 67 19	057 016.3	22	.	09	.	.	.	04	01	05	09	13	08	02	13	03	02	03	01																			
IV 7.4 7.8 5.4 6.9	085.2	063.3	83 55 76 70 34	066 013.9	04	.	02	.	.	03	01	09	13	12	01	13	03	01																				
V 6.6 7.7 6.2 6.8	106.4	085.5	81 59 83 74 34	098 018.6	28	.	.	01	02	.	01	01	12	18	16	03	18	03	01																				
VI 4.1 3.0 3.8 4.3	181.4	10.8	79 53 86 72 32	058 016.3	28	.	.	15	02	.	01	07	03	11	10	03	11	01	01																				
VII 2.3 3.0 1.8 2.3	281.2	10.6	78 47 76 66 24	014 009.7	16	.	.	23	06	.	01	15	05	02	05	05	02	05	02	01																				
VIII 2.7 3.6 2.7 3.0	250.3	10.0	83 30 67 68 25	057 022.9	05	.	.	19	03	.	01	14	03	09	07	02	09	03	03	01																				
IX 5.5 6.0 4.8 5.5	137.6	09.2	88 59 89 79 32	122 054.6	01	.	.	06	.	.	05	08	12	08	03	12	03	01																					
X 5.3 5.3 4.1 4.9	120.6	07.1	91 59 87 79 39	015 005.8	21	.	06	02	.	.	09	08	04	04	04	04	05	01	01	07	01	04	.	.	02	01																					
XI 7.9 7.0 6.7 7.2	052.1	04.3	91 70 80 84 41	019 01																																											

Mjesec	Vremenski interval dnevi	Temperatura vazduha °C										Čestina pravaca i srednja jačina vjetra m/s (0-12)																										
		TM				Sred. (Dnev.)			Min.			Max.			Dat.		Hrs.		Dat.		N		NE		E		SE		S		SW		W		NW		C	
		7	14	21		Min.	Hrs.	Max.	Dat.	Hrs.	Dat.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.							
$\varphi = 43^{\circ}14' N \lambda = 21^{\circ}36' E$ Gr. AG = + 1h 26 min.																																						
I	-	-01.9	03.4	-00.3	00.2	04.1	-02.5	12.8	13	-12.5	09	09	02.4	13	02.7	*	*	37	03.1	01	07.0	03	02.7	01	02.0	02	02.5	57										
II	-	00.7	06.0	02.8	03.1	07.3	-00.8	18.5	20	-13.5	21	02	03.0	02	02.5	02	02.0	13	03.v	*	06	03.2	01	02.0	05	01.6	53											
III	-	03.4	11.8	06.9	07.2	13.2	02.1	22.0	04	-03.2	14	01	08.0	03	01.7	01	02.0	09	02.7	02	02.5	07	03.0	10	02.5	12	04.0	48										
IV	-	07.4	14.6	10.2	10.6	16.0	05.2	23.1	12	06.7	18	03	02.7	03	03.0	01	02.0	12	02.9	08	03.9	08	03.6	*	*	06	02.8	49										
V	-	11.3	18.2	12.9	13.8	19.8	08.8	28.5	01	-02.2	13	01	04.0	07	02.6	62	02.0	12	02.7	01	02.0	03	03.3	*	*	11	02.7	56										
VI	-	14.9	23.8	17.0	18.2	12.1	30.5	12	08.4	01	06	02.8	02	01.5	*	*	34	02.8	*	10	02.8	02	03.5	12	02.8	54												
VII	-	15.3	26.5	18.4	19.7	27.7	12.2	34.9	19	08.5	25.24	02	01.5	04	02.5	*	*	08	02.5	*	04	02.5	01	03.0	14	03.4	60											
VIII	-	14.2	26.0	17.3	18.7	27.1	11.6	34.0	08	07.0	22	04	02.5	03	02.0	01	01.0	36	02.7	*	07	02.0	*	*	14	02.9	58											
IX	-	10.7	19.3	13.3	14.1	20.6	08.8	28.0	12	01.5	22	*	*	*	*	*	*	*	*	*	*	10	02.5	03	02.7	14	02.9	63										
X	-	05.7	10.8	08.3	09.4	14.6	04.5	26.5	03	-02.5	23	03	03.7	03	02.7	*	*	*	03	02.3	01	01.0	03	02.0	*	*	10	02.8	70									
XI	-	00.3	04.9	01.5	02.0	05.7	-01.1	12.5	01	-06.9	17	*	*	02	02.5	*	*	04	02.2	*	06	02.7	02	02.0	01	02.0	75											
XII	-	01.5	06.2	03.0	03.4	07.2	-00.3	17.5	29	-10.2	07	*	*	06	02.0	01	03.0	06	02.0	*	*	09	03.1	*	*	04	04.2	67										
GOD.	-	07.0	14.7	09.3	10.0	15.8	05.8	34.9	19.VII - 13.5	24.II	31	02.8	48	02.4	08	02.0	84	02.7	13	03.6	76	02.8	20	02.6	105	03.0	710											
$\varphi = 43^{\circ}39' N \lambda = 21^{\circ}41' E$ Gr. AG = + 1h 26 min.																																						
$\varphi = 43^{\circ}39' N \lambda = 21^{\circ}41' E$ Gr. AG = + 1h 26 min.																																						
I	-	-02.9	01.9	-01.2	-00.9	03.2	-05.1	13.5	13	-13.0	09	-	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*						
II	-	-00.8	03.7	00.4	00.9	05.1	-03.0	18.0	28	-10.6	22	-	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*							
III	-	03.7	10.1	03.5	06.2	11.5	01.7	19.0	02	-06.0	09	-	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*							
IV	-	08.3	13.0	08.8	09.7	14.7	05.0	23.0	12	00.5	07	-	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*							
V	-	11.7	17.6	12.2	13.4	19.6	08.4	28.5	01	01.5	13	-	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*							
VI	-	15.2	22.6	15.1	17.0	24.1	10.9	29.0	11.10	08.0	02.01	-	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*								
VII	-	16.1	25.5	16.8	18.8	26.6	10.9	33.0	19	04.3	25	-	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*								
VIII	-	14.5	26.0	15.8	18.0	24.5	10.3	33.2	08	05.0	20	-	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*								
IX	-	10.9	18.9	12.7	13.8	20.0	07.7	27.5	26	-00.5	22	-	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*								
X	-	04.6	15.0	08.7	09.7	15.9	03.9	26.0	04	-03.5	24.23	-	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*								
XI	-	00.1	04.8	01.0	01.7	05.4	-02.1	14.0	26	-07.5	17.16	-	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*								
XII	-	00.8	05.9	02.1	02.2	05.4	-01.7	16.5	29	-06.0	08.07	-	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*								
GOD.	-	07.0	13.6	08.2	09.2	14.8	03.9	33.2	08.VII - 13.0	09.I	-	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*							
$\varphi = 43^{\circ}20' N \lambda = 21^{\circ}54' E$ Gr. AG = + 1h 26 min.																																						
I	745.7	-01.0	03.6	00.7	01.0	04.6	-02.2	13.5	30	-16.2	10	08	01.8	01	04.0	28	03.0	03	01.7	03	02.7	01	02.0	04	01.0	12	02.2	33										
II	740.7	01.2	06.2	02.6	03.2	07.8	-00.2	19.7	28	-07.6	22	01	01.0	01	02.0	21	01.3	04	01.2	05	01.8	02	01.5	02	01.5	13	01.8	35										
III	742.5	04.5	11.8	07.6	07.9	13.3	03.4	23.8	05	-02.1	14	02	02.0	*	*	18	01.9	05	01.4	04	01.8	09	02.2	05	01.0	25	02.7	25										
IV	740.0	08.7	14.9	11.0	11.4	16.2	06.7	23.6	20.12	01.6	16	06	01.7	03	02.0	28	02.0	04	02.2	12	01.8	05	01.3	08	02.2	21												
V	742.4	12.5	18.7	13.9	14.8	20.4	09.9	28.6	01	-01.6	13	04	01.2	01	01.0	14	01.7	09	01.4	01	02.0	07	02.1	01	01.0	21	01.7	35										
VI	742.7	16.3	23.8	17.5	18.8	25.0	12.8	30.8	12	09.2	23	05	01.4	02	01.0	11	01.2	02	01.0	03	01.7	04	02.5	02	01.0	20	02.0	41										
VII	744.2	17.0	26.6	19.5	20.6	27.6	13.1	35.9	19	06.1	24	08	01.2	01	02.0	34	01.1	05	01.2	03	01.3	04	02.0	02	01.0	20	02.3	37										
VIII	744.8	15.7	26.4	18.9	20.0	27.5	13.2	35.0	08	07.6	20	08	01.9	01	02.0	16	01.4	03	01.3	01	01.0	03	01.7	03	01.0	21	02.0	37										
IX	744.0	11.3	19.9	13.6	14.6	21.3	09.6	29.2	12	08.4	22	03	02.0	02	01.0	04	01.8	03	01.0	05	02.5	04	01.5	05	01.4	21	02.2	45										
X	741.1	07.1	14.1	09.8	10.7	17.1	05.4	28.6	03	-01.8	23	05	02.2	07	01.9	16	01.2	03	01.7	04	01.8	01	01.0	03	01.3	15	01.9	39										
XI	752.8	00.8	05.0	02.0	02.4	05.7	-00.4	13.4	03	-04.3	17																											

Meseč Broj	Oblačnost mm (0-10)				Insektacija broj sati (Duges)	Vlažnost vazduha			Padavine R mm			Broj dana u meseču																		
	7	14	21	Sred. (Duges)		7	14	21	Max.	Min.	Tn	Tx	Tn	Tx	Tn	F(0-12)	R mm	0	*	+	*	Δ	Δ	Δ	Δ	R	T	≡	■	
						mm	mm	mm	mm	mm	≤	<	<	≥	≥	≥	≥	≤	<	>	≥	≤	≥	≤	≥	≥	≥			
BR. ST. 201 PROKUPLJE																														
I 6.7 5.7 4.2 5.6	-	03.8 85 72 83 80 48	024 035.6	22 03 05 26	J2	.	06	10	09	08	.	05	06	02	18	06			
II 8.1 7.3 7.0 7.5	-	04.6 85 69 82 79 34	056 013.6	15 01 02 18	01	.	03	16	13	11	01	10	11	07	12	06			
III 6.2 5.5 3.7 5.2	-	05.4 94 55 74 71 28	058 013.9	22	.	07	.	.	03	02	08	09	09	07	03	08	01	02	01			
IV 6.6 7.6 5.3 6.5	-	07.1 89 61 75 75 28	027 009.2	04	02	01	02	10	08	05	.	08	01	01				
V 6.8 7.5 5.3 6.5	-	-	-	-	-	068 008.9	03	.	.	01	04	.	01	.	02	09	18	16	16	.	18	08	04	
VI 4.6 5.6 3.1 4.4	-	-	-	-	-	040 015.0	28	.	.	16	03	.	01	.	07	04	11	08	01	11	.	06	06	04
VII 2.2 4.0 1.6 2.6	-	-	-	-	-	016 010.1	16	.	.	25	09	.	01	01	14	03	03	01	03	.	01	01	01	
VIII 3.3 3.2 3.0 3.2	-	-	-	-	-	033 013.8	05	.	.	21	04	.	02	.	15	04	04	04	04	06	04	04	
IX 4.9 6.1 4.0 5.0	-	09.8 90 63 87 80 24	046 025.4	01	.	.	07	.	.	01	.	38	06	10	07	03	10	02	04			
X 5.6 5.1 3.3 4.6	-	07.6 92 66 88 82 51	013 005.3	22	.	05	02	.	.	.	08	07	05	04	.	05	13	01				
XI 9.0 7.9 6.9 7.9	-	04.6 89 76 87 84 54	018 009.9	29	.	01	20	.	.	03	21	02	02	.	02	01	01	20	01			
XII 9.1 8.7 8.1 8.6	-	05.0 87 78 85 84 46	046 017.8	19	01	03	12	.	.	.	23	12	07	02	10	04	02	07	01				
GOD. 6.1 6.2 4.6 5.6	-	-	-	-	-	465 025.4	04 IX	05	11	89	75	18	.	14	04	76	119	106	82	12	94	23	12	.	.	.	22	77	10	
BR. ST. 202 SOKOBANJA																														
I 7.2 6.0 5.9 6.4	-	-	-	-	-	042 013.8	30	06	10	27	01	11	10	08	01	05	06	15	01
II 7.2 7.0 7.5 7.4	-	-	-	-	-	074 014.5	14	02	04	23	01	14	12	01	07	08	12	02	
III 6.7 5.4 6.6 6.2	-	-	-	-	-	068 015.5	23	.	.	11	02	08	13	11	04	13	02	01	02	01
IV 6.4 6.4 7.3 6.7	-	-	-	-	-	050 008.0	04	11	15	11	.	15		
V 6.1 6.4 6.4 6.3	-	-	-	-	-	109 027.5	03	.	.	02	01	08	19	18	03	19	01	
VI 4.9 5.2 4.6 4.9	-	-	-	-	-	101 024.5	22	.	.	15	06	04	13	11	04	13	01	01	
VII 3.7 2.9 2.3 3.0	-	-	-	-	-	028 016.5	16	.	.	23	08	.	.	.	12	04	04	01	04	04	01	01	
VIII 3.8 3.4 3.7 3.6	-	-	-	-	-	024 005.5	05	.	.	18	03	.	.	.	07	01	08	06	.	08	06	01		
IX 5.0 5.1 4.6 4.9	-	-	-	-	-	087 042.0	01	.	.	01	06	.	.	.	07	05	12	10	02	12	02	01	
X 5.8 4.9 4.0 4.9	-	-	-	-	-	021 007.0	22	.	.	08	01	.	.	.	06	07	05	05	.	05	04	01		
XI 9.2 8.1 8.8 8.7	-	-	-	-	-	023 016.6	30	.	21	01	23	05	03	01	05	01	01	01	
XII 8.2 7.9 8.5 8.2	-	-	-	-	-	061 030.0	20	.	04	17	19	30	06	02	04	05	.	01	04	13	
GOD. 6.2 5.8 5.8 5.9	-	-	-	-	-	708 042.0	04 IX	08	18	108	65	11	.	.	43	108	127	105	19	110	22	01	.	01	.	.	.	12	.	
BR. ST. 203 NIS																														
I 6.0 6.7 5.7 6.2	074.8 03.8 83 67 78 76 43	024 008.9	26	02	05	21	.	.	.	01	.	06	11	12	04	.	38	07	02	01	14				
II 6.4 8.1 7.3 7.9	066.5 04.5 85 66 81 77 36	057 010.0	27	.	01	17	.	.	.	01	.	01	17	15	12	01	10	11	05	.	01	.	.	.	07	.				
III 7.4 6.6 5.8 6.6	143.7 05.4 82 56 70 69 27	097 019.8	19	.	.	03	.	.	.	01	.	04	11	16	12	05	16	01	01	02	01			
IV 6.9 8.3 7.6 7.6	123.8 06.8 95 75 73 68 32	043 010.1	06	15	12	08	01	12	02	01				
V 7.5 8.2 7.0 7.5	141.6 09.1 82 57 77 72 29	081 012.9	03	.	.	01	03	.	.	.	01	.	19	21	15	02	21	07	01				
VI 4.7 5.6 5.5 5.2	230.9 11.3 80 53 77 70 31	074 019.9	28	.	.	14	04	.	.	01	.	04	06	16	10	13	04	14	03	14	01	01				
VII 2.6 3.0 1.8 2.5	343.3 11.1 77 41 68 62 31	016 008.7	16	.	.	24	09	.	.	03	.	14	07	34	03	04	04	02	04	01	01	01				
VIII 3.7 3.5 3.0 3.2	302.0 10.2 77 39 74 67 23	036 010.2	05	.	.	21	04	.	.	02	.	09	01	07	05	01	37	06	01				
IX 5.8 6.4 5.0 5.7	161.1 09.7 90 57 85 78 36	094 047.2	01	.	.	05	08	.	.	01	.	02	08	09	07	03	09	02	.				
X 5.7 4.9 3.6 4.7	159.2 07.5 89 57 82 76 33	009 002.4	20	.	.	05	02	.	.	01	.	05	07	07	05	07	07	05	07	.			
XI 8.8 7.8 7.4 8.0	038.7 04.6 89 73 86 83 46	019 016.5	30	.	01	17	.	.	.	01	.	02	21	04	02	01	34	02	01	01	03	01				
XII 8.8 8.3 6.6 7.4	050.5 05.1 81 71 88 86 48	071 019.4	15	02	04	12	.	.	.	05	01	14	16	12	02	11	06	08	01				
GOD. 6.3 6.6 5.3 6.1	-	-	-	-	-	642 050.4	04 IX	06	12	83	78	17	.	60	04	51	125	130	92	17	114	28	09	.	.	81	38	34		
BR. ST. 204 LESKOVAC																														
I 6.5 6.6 5.3 6.2	-	-	-	-	-	042 024.0	26	02	05	24	04	.	06	13	11	04	.	07	07	02	.	.	.	06	00	
II 6.8 7.8 7.1 7.8	-	-	-	-	-	047																								

Meseč	Vremenski pristup PM	Temperatura vazduha °C							Čestina pravaca i srednja jačina vетра m/s, Fm (0-12)																		
		7	14	21	Sred. (Dnev.)	NW	NE	N	SE	S	SW	W	NW	C	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.			
$\varphi = 43^{\circ}53' N \lambda = 22^{\circ}18' E$ Gr. AG = + 1h 29 min.															ZAJEČAR												
I	-	-03.8	01.6	-02.1	-01.6	02.4	-05.8	14.1	14 -12.0	11 09	02.3	26	02.8	07	02.7	03	01.3	05	02.8	39	02.3	02	01.5	02	02.0	00	
II	-	-02.8	01.8	-01.0	-00.8	02.7	-04.2	19.2	28 -17.5	22 15	02.1	30	02.6	07	02.0	01	01.0	02	03.0	25	02.5	02	02.0	01	01.5	01	
III	-	03.4	10.6	06.4	04.7	11.9	01.7	18.5	15 -04.0	09 12	02.6	20	02.4	03	02.3	03	03.3	05	02.2	34	02.7	10	03.0	05	02.8	01	
IV	-	07.5	13.4	09.1	09.8	15.0	04.3	21.6	29 06.5	23 14	02.4	22	02.6	05	03.0	01	03.0	07	02.6	29	02.6	05	02.6	07	02.6	00	
V	-	12.0	18.6	13.1	14.1	19.9	0.8	24.4	31 -08.5	13 20	02.3	14	02.4	02	03.0	04	02.0	14	02.1	27	02.6	04	03.0	08	02.5	00	
VI	-	15.7	23.6	16.9	18.3	25.2	11.2	30.6	11 08.4	03	07	02.3	10	02.5	03	04	04	02.5	18	02.0	36	02.2	07	02.7	09	03.0	00
VII	-	16.3	26.4	18.1	19.7	27.4	11.1	32.6	05 07.0	23 12	02.5	07	02.4	04	03.0	05	02.2	15	02.2	36	01.9	02	03.0	12	02.9	00	
VIII	-	15.4	26.3	17.7	19.3	27.2	10.1	35.5	08 05.3	14 16	02.4	06	02.2	04	03.0	*	*	18	02.2	48	02.0	*	*	01	02.0	00	
IX	-	11.7	20.9	13.8	15.0	22.0	08.6	29.8	12 06.5	22 12	02.3	03	02.3	02	02.0	03	02.3	23	02.3	36	02.2	09	02.4	02	03.5	00	
X	-	05.6	16.2	09.1	10.0	17.0	03.4	23.6	03 -04.0	29 11	02.3	10	02.4	06	03.0	05	02.2	23	02.2	33	01.8	03	01.7	04	02.8	00	
XI	-	-00.6	07.7	00.8	02.2	08.4	-03.3	17.0	16 -06.0	26.16	08	02.2	11	02.1	*	03	02.3	16	02.8	46	02.4	03	02.0	02	01.0	01	
XII	-	00.5	04.2	01.9	02.1	05.8	-02.0	19.0	29 -07.5	07.04	12	02.6	19	02.7	05	03.0	*	14	02.5	33	02.7	05	02.6	05	01.8	00	
GOD.	-	06.7	14.3	08.6	09.8	15.4	03.6	35.5	08 VM -17.5	22.11 148	02.4	177	02.5	43	02.7	32	02.2	160	02.3	422	02.3	52	02.6	59	02.6	02	
$\varphi = 43^{\circ}04' N \lambda = 22^{\circ}04' E$ Gr. AG = + 1h 29 min.																								BABUŠNICA		BR. ST. 207	
I	-	-02.8	02.8	-01.5	-00.7	03.8	-04.1	14.0	14 -12.0	10	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
II	-	-01.0	04.9	00.7	01.3	06.4	-02.7	17.0	28.23 -13.4	21	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
III	-	02.2	10.2	05.3	05.8	11.5	01.2	22.5	04 -06.0	14	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
IV	-	05.9	13.0	09.0	09.2	14.5	04.3	23.0	30.12 06.0	24	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
V	-	10.9	17.5	12.1	13.1	18.9	0.8	28.5	01 -02.0	13	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
VI	-	14.5	22.3	15.3	16.9	23.7	11.3	29.5	13 07.0	05	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
VII	-	14.7	25.1	16.3	18.1	26.1	10.5	33.0	19 05.5	23	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
VIII	-	12.9	24.7	18.1	17.4	25.9	10.2	-	- 04.0	14	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
IX	-	09.7	18.7	12.0	13.1	19.7	0.8	27.5	12 06.5	22	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
X	-	05.2	15.8	07.6	09.1	16.5	03.7	26.0	04.03 -04.5	23	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
XI	-	-01.1	05.6	00.5	01.4	04.5	-01.8	16.0	02 -00.4	16	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
XII	-	00.7	05.3	02.1	02.5	06.3	-00.9	18.5	29 -15.0	07	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
GOD.	-	06.0	13.8	08.0	08.9	15.0	04.0	-	- 15.0	07 XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
$\varphi = 43^{\circ}05' N \lambda = 22^{\circ}36' E$ Gr. AG = + 1h 29 min.																								PIRČI		BR. ST. 208	
I	-	-02.0	03.5	-00.2	00.3	03.6	-03.1	11.0	14.13 -11.0	11.10	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
II	-	00.1	05.3	02.2	02.5	07.0	-01.3	16.0	28 -08.9	21	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
III	-	03.0	11.1	04.0	04.6	11.6	01.8	23.5	04 -05.6	14	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
IV	-	06.6	14.2	09.7	10.1	14.8	04.9	23.5	12 01.0	03	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
V	-	11.4	18.7	13.3	14.1	19.0	0.9	24.0	01 -01.0	13	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
VI	-	14.5	23.6	16.7	17.9	23.9	11.6	29.5	12.11 08.0	01	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
VII	-	15.2	26.3	18.8	19.6	26.5	12.0	31.5	12 05.0	23	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
VIII	-	14.2	23.6	17.9	18.9	26.5	11.6	34.0	08 05.0	14	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
IX	-	09.9	19.3	13.0	13.8	20.7	0.8	26.0	12 02.6	30.22	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
X	-	05.6	16.0	06.2	10.0	17.0	0.4	26.0	12 04.03 -04.6	30	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
XI	-	00.1	05.2	00.9	01.8	05.0	-01.5	16.0	01 -07.5	17	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
XII	-	01.2	05.6	02.6	03.0	06.4	00.0	17.3	29 -14.0	07	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
GOD.	-	06.6	14.6	09.2	09.9	15.2	04.8	34.0	06 VM -14.0	07 XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
$\varphi = 43^{\circ}05' N \lambda = 22^{\circ}36' E$ Gr. AG = + 1h 30 min.																								TOPLI DO		BR. ST. 209	
I	-	-03.3	01.7	-02.1	-01.4	02.7	-05.8	10.3	13 -15.4	09	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
II	-	-01.0	03.7	00.1	00.7	05.1	-03.2	15.8	25 -14.2	21	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
III	-	01.6	07.9	03.9	04.4	09.3	00.6	20.0	04 -04.5	19	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
IV	-	05.9	10.7	06.8	07.6	11.9	03.6	19.2	12 06.2	01	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
V	-	09.6	14.9	10.3	11.1	16.4	06.7	26.2	01 -02.0	13	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
VI	-	13.7	18.4	13.4	15.0	20.6	0.9	27.0	12 06.2	01	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
VII	-	14.8	22.2	14.7	16.6	23.3	10.5	30.0	19 05.5	24	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
VIII	-	13.2	22.0	14.3	16.0	23.4	09.8	31.3	08 04.0	15	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
IX	-	09.6	14.0	11.2	12.0	17.4	07.4	24.0	12 01.0	22	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
X	-	05.6	13.5	07.2	08.4	14.2	03.8	26.0	03 -03.6	29	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
XI	-	-02.2	04.3	-00.4	00.3	05.3	-03.6	11.0	01 -08.0	19	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
XII	-	-00.1	04.1	00.9	01.5	04.9	-02.0	13.4	29 -14.5	07	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
GOD.	-	05.6	11.7	04.7	07.7	12.9	03.2	31.3	08 VM -15.4	09.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
$\varphi = 43^{\circ}01' N \lambda = 22^{\circ}41' E$ Gr. AG = + 1h 30 min.																								DIMITROGRAD		BR. ST. 210	
I	724.0	-02.8	02.2	-01.7	-01.1	03.3	-04.3	11.7	14 -18.3	09	-	-	01	32.0	15	02.3	04	02.8	.	01	01.0	13	02.2	10	02.9	09	
II	719.1	-00.4	04.9	01.2	01.7	04.5	-01.9	17.5	22 -18.2	21	-	-	10	36.4	32	02.5	.	02.0	.	21	02.3	15	02.9	15	02.6	00	
III	721.0	02.5	16.1	04.9	05.6	11.6	01.3	21.3	04 -03.6	14	-	-	01	3													

Mjesec	Vremenski pristupak Fm	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta m/s, Fm (0-12)																									
		TN					HN					NE					E					SE		S		SW		W		NW		C					
		7	14	21	28	35	HN	HN	HN	HN	HN	HN	HN	HN	HN	HN	E	E	E	E	SE	S	SW	W	NW	C	E.	J.	E.	J.	E.	J.	E.	J.	E.	J.	E.
$\varphi = 42^{\circ}40' N \lambda = 20^{\circ}18' E$ Gr. AG = + 1h 21 min.																					PEC		BR. ST. 211														
I	718.3	-02.1	02.2	-00.6	-00.2	03.8	-03.4	10.1	29	-12.4	09	13	02.8	02	01.5	02	02.0	04	02.0	07	01.4	08	01.4	04	03.2	02	03.0	51									
II	718.5	01.1	05.6	03.0	03.1	06.5	00.1	15.8	12	-06.4	21	07	02.6	03	02.0	03	01.3	03	01.7	07	01.7	03	02.7	05	02.8	02	03.8	53									
III	718.6	04.2	10.7	07.4	07.4	12.8	03.2	19.7	04	-02.3	13	14	03.5	13	01.9	07	02.0	05	02.0	09	02.4	11	03.5	07	03.4	06	04.0	21									
IV	718.5	07.6	12.8	09.3	09.8	14.0	04.1	21.5	30	02.8	19.10	15	02.8	09	02.3	03	01.3	05	03.0	10	03.3	14	02.6	07	02.9	03	01.7	24									
V	718.6	11.9	17.0	13.4	14.0	19.7	08.8	26.6	01	01.1	13	15	02.7	14	02.2	07	01.9	06	02.8	10	03.8	11	03.0	03	04.0	01	03.0	26									
VI	717.1	14.6	22.7	18.3	19.0	24.4	13.1	30.5	12	10.2	03	15	02.5	08	02.0	05	02.4	08	02.6	15	04.1	08	04.0	05	03.8	26											
VII	718.5	17.8	25.3	20.2	20.9	26.7	13.8	32.0	19	08.2	24	12	02.9	14	02.5	11	02.5	05	02.4	13	02.8	03	02.7	02	02.5	22											
VIII	718.1	16.8	24.0	19.4	20.0	25.8	14.0	31.3	04	11.2	30.22	12	02.1	09	01.7	07	02.1	06	02.3	08	03.0	09	02.7	03	02.0	27	02.7	36									
IX	718.2	11.9	18.5	14.1	14.6	19.9	09.2	29.8	19	02.3	22	10	03.4	03	01.7	04	01.5	06	02.8	02	03.0	13	03.9	08	04.2	04	04.8	40									
X	721.3	07.6	14.7	10.4	10.8	15.6	06.3	23.2	04.8	-00.8	23	07	02.1	03	02.0	04	02.5	05	02.0	03	02.3	08	03.1	03	03.0	02	03.0	40									
XI	725.4	-00.3	02.6	01.0	01.0	03.2	-01.1	12.0	02	-04.6	16	04	01.2	03	01.0	04	01.3	02	01.5	02	01.0	03	04.7	04	05.0	02	06.6	66									
XII	716.3	01.4	05.3	02.9	03.2	04.2	00.2	15.3	17	-07.4	07	03	02.7	04	01.5	08	03	01.3	04	02.0	08	02.1	04	01.2	01	01.0	66										
God.	717.8	07.9	13.5	9.9	10.3	14.7	05.9	33.8	49.VII	-12.4	09.I	127	02.7	85	02.0	59	02.0	56	02.3	75	02.6	116	03.1	59	03.3	27	03.3	491									
$\varphi = 42^{\circ}24' N \lambda = 20^{\circ}21' E$ Gr. AG = + 1h 22 min.																					SKIVJANE-OJAKOVICA		BR. ST. 212														
I	-	-02.5	02.8	-00.5	-00.3	03.3	-04.1	12.5	29	-16.8	10	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-									
II	-	02.0	04.2	03.7	03.7	05.9	07.7	00.3	14.4	25	-05.5	22.21	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-									
III	-	04.2	11.9	06.7	07.4	13.3	02.1	19.7	06	-03.6	29	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-									
IV	-	07.8	14.1	09.4	10.2	15.3	05.0	25.4	30	00.0	19.18	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-									
V	-	12.5	19.5	12.9	14.2	19.9	07.7	30.5	01	02.5	15.15	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-									
VI	-	17.4	24.7	17.4	19.2	26.0	11.6	32.0	11	06.0	30	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-									
VII	-	18.1	27.1	19.3	21.0	26.1	11.9	34.0	13	04.5	23	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-									
VIII	-	16.3	27.5	18.2	20.0	26.7	11.8	34.5	03	07.5	21.14	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-									
IX	-	11.2	19.5	12.8	14.0	21.0	08.5	26.5	11	06.5	22	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-									
X	-	06.8	15.3	08.5	09.8	15.9	04.7	24.5	04	-02.0	25	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-									
XI	-	00.5	03.3	00.8	01.4	03.8	-01.0	14.0	02	-07.5	16	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-									
XII	-	01.7	05.5	03.3	03.5	06.6	-	15.5	29	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-									
God.	-	08.0	14.7	09.4	10.4	15.8	-	34.5	03.VII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-									
$\varphi = 42^{\circ}47' N \lambda = 20^{\circ}30' E$ Gr. AG = + 1h 22 min.																						ISTOK		BR. ST. 213													
I	-	-01.1	02.7	00.4	00.6	03.7	-03.4	10.4	29	-13.4	10	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-									
II	-	01.0	05.4	03.2	03.3	03.8	-00.6	17.6	25	-07.8	21	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-									
III	-	06.6	10.2	06.4	06.9	11.6	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-									
IV	-	07.9	13.6	09.1	09.9	14.7	05.3	23.0	30	02.4	19	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-										
V	-	11.6	17.8	12.7	13.7	19.2	-	26.8	20	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-									
VI	-	17.4	24.7	17.4	19.2	26.0	12.3	30.8	12	06.8	30	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-										
VII	-	16.5	26.1	19.0	20.2	27.3	11.1	33.1	13	04.6	23	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-										
VIII	-	15.6	25.7	18.6	19.7	27.1	12.6	31.8	07	09.2	22	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-										
IX	-	10.2	19.2	12.9	13.8	20.4	08.4	27.4	26	02.8	22	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-										
X	-	06.3	15.4	9.1	10.0	16.7	04.7	23.7	04	-02.7	25	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-										
XI	-	-00.2	03.1	00.9	01.0	04.4	-01.1	14.3	02	-08.2	16	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-										
XII	-	01.2	05.7	02.9	03.2	07.2	00.0	16.4	17	-06.2	09	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-										
God.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-									
$\varphi = 42^{\circ}30' N \lambda = 20^{\circ}34' E$ Gr. AG = + 1h 23 min.																						KLINE		BR. ST. 214													
I	-	-03.0	02.5	-00.9	-00.6	03.5	-04.0	11.6	29	-13.9	10	-	-	-	-																						

Mjesec	Geografski položaj km	Temperatura vazduha °C										Čestina pravaca i srednja jačina vjetra m/s, Pa (0-12)																
		Srednji GDP				7	14	21	Srednji GDP	NW	NE	W	E	SE	S	SW	W	NW	C									
$\varphi = 42^{\circ}13' N \lambda = 20^{\circ}44' E$ Gr. AG = + 1h 23 min.																												
I	726.8	-01.9	02.2	08.0	00.0	03.2	-02.4	15.3	29	-12.2	10	16	01.4	33	02.0	16	01.8	11	01.5	05	01.4	01	05.0	.	.			
II	722.0	02.2	06.1	04.3	04.2	07.8	01.2	17.0	12	-06.2	21	07	01.6	12	01.6	07	01.4	06	01.5	11	01.7	12	01.8	10	02.4			
III	726.4	05.2	11.3	07.0	08.0	13.1	03.9	20.6	04	-06.3	13	08	01.5	19	02.5	10	01.7	12	01.8	14	02.6	10	03.0	02	02.5			
IV	722.0	08.1	13.6	10.2	10.5	15.3	06.7	23.9	12	02.2	10	06	02.0	15	01.8	04	01.5	08	01.4	16	01.6	17	01.8	12	02.0	02	01.5	
V	724.7	12.4	18.1	14.1	14.7	20.1	10.1	29.5	01	02.2	13	11	02.1	11	01.5	06	01.3	11	01.5	06	01.3	20	02.2	16	02.7	07	01.6	
VI	725.8	17.5	24.9	19.3	20.2	24.8	14.6	32.7	12	10.6	03	01.1	13	01.8	07	01.4	05	01.4	07	02.0	13	01.8	12	01.8	17	02.2	10	01.5
VII	726.5	18.1	27.4	21.4	22.1	25.4	15.6	33.4	19	09.5	23	13	02.2	17	02.2	05	01.6	10	02.0	14	01.5	14	01.6	11	02.2	04	01.8	
VIII	726.7	17.0	27.4	20.9	21.5	26.9	14.7	34.0	08	11.2	14	13	02.1	09	01.6	05	01.4	09	01.4	21	01.3	15	01.5	10	01.7	06	01.3	
IX	726.5	12.2	19.3	15.2	15.5	21.2	10.6	28.1	12	04.3	22	11	02.0	19	02.3	07	01.6	10	01.6	18	01.6	06	01.2	08	02.0	05	01.0	
X	725.8	07.4	14.5	09.6	10.4	15.3	06.3	23.8	04	-01.8	23	09	01.4	19	02.4	09	01.3	12	01.2	18	01.0	04	01.2	08	01.0	10	01.0	
XI	734.1	00.4	02.9	01.3	01.5	02.5	-00.3	14.0	02	-04.7	16	18	01.1	12	01.1	07	01.1	06	01.2	07	01.1	19	01.2	10	01.0	07	01.1	
XII	724.8	02.3	05.2	03.8	03.8	06.6	01.0	16.5	17	-06.8	09	13	01.4	20	01.8	05	01.0	07	02.0	06	01.3	09	02.4	19	02.1	05	02.0	
GOD.	726.2	08.4	14.4	10.7	11.0	15.9	06.8	36.0	08VM	-12.2	10.1	138	01.7	193	01.9	88	01.5	189	01.6	145	01.5	128	01.9	124	02.2	79	01.4	91
$\varphi = 42^{\circ}51' N \lambda = 20^{\circ}42' E$ Gr. AG = + 1h 24 min.																												
KOSOVSKA MITROVIC																												
I	-	-02.4	02.0	-01.0	-00.6	02.7	-03.9	00.1	13	-13.8	10	12	02.5	01	01.0	02	01.0	14	02.1	08	01.2	04	01.2	05	01.4	08	02.0	37
II	-	00.5	04.7	02.1	02.3	06.1	-01.0	14.7	12	-10.2	21	21	02.0	01	01.0	01	03.0	19	02.1	05	01.6	08	02.2	04	01.8	19	02.3	
III	-	02.7	10.7	05.4	06.1	11.8	01.7	20.8	04	-03.7	14	17	02.7	02	01.5	03	05	01.6	07	01.4	10	02.2	04	02.5	10	02.3	38	
IV	-	04.6	13.1	08.8	09.3	14.2	04.7	21.4	30	06.9	03	07	01.9	04	03	01.0	18	01.5	01	03	13	02.6	07	02.3	17	02.3	26	
V	-	10.6	16.7	12.2	12.9	18.2	08.0	26.3	01	06.5	13	15	01.7	01	01.0	01	01.0	13	01.7	07	02.0	12	01.9	08	02.4	15	01.7	21
VI	-	14.0	22.7	16.0	17.4	23.8	10.6	29.2	12	07.2	02	06	01.7	01	01.0	0.	0.	07	01.0	01	02.0	18	01.8	06	01.3	15	01.6	36
VII	-	15.3	29.5	18.4	19.5	26.6	10.9	32.7	12	03.8	24	08	02.2	04	01.8	03	01.3	08	01.2	02	01.0	14	01.7	04	01.0	11	01.7	36
VIII	-	14.6	29.2	18.0	18.9	26.7	11.2	32.9	07	07.0	22	11	02.2	03	01.0	00	01.0	09	01.2	12	01.5	11	01.9	05	01.2	11	01.6	40
IX	-	10.4	18.7	12.2	13.4	19.6	08.2	26.6	26	01.2	22	12	02.8	01	03.0	01	01.0	02	01.5	0.	0.	07	01.4	04	01.8	26	02.4	37
X	-	06.0	19.3	09.6	09.8	16.0	04.6	29.3	03	-03.2	23	15	02.4	01	02.0	01	01.0	08	01.5	0.	0.	14	01.2	03	01.3	13	01.9	36
XI	-	-01.0	05.1	-00.3	00.8	05.0	-02.7	12.2	03	-07.4	16	09	02.3	01	02.0	01	01.0	13	01.3	07	01.0	02	01.0	10	01.9	47	01.8	
XII	-	01.5	05.3	02.6	03.0	06.4	-00.5	14.7	17	-11.7	07	09	02.7	0.	0.	03	01.0	07	01.1	08	01.2	10	02.3	04	01.2	05	01.8	47
GOD.	-	06.6	13.8	08.6	09.4	14.8	04.3	32.9	07VM	-13.8	10.1	162	02.3	16	01.7	17	01.2	125	01.6	41	01.4	128	01.8	58	01.7	145	02.0	423
$\varphi = 42^{\circ}39' N \lambda = 21^{\circ}09' E$ Gr. AG = + 1h 25 min.																												
PRIESTINA																												
I	708.5	-02.8	01.3	-01.0	-00.7	02.5	-04.6	09.3	13	-15.1	89	09	03.2	03	03.0	04	02.5	09	03.4	0.	0.	01	02.0	01	02.0	06	02.0	66
II	703.8	-00.3	04.1	01.9	01.9	04.2	-01.5	15.3	25	-12.4	21	18	02.6	02	01.5	04	03.2	07	02.9	07	02.6	01	03.0	0.	0.	02	0.0	63
III	706.4	02.9	10.1	05.5	06.0	11.7	01.3	21.0	04	-03.4	13	17	03.1	02	02.0	01	02.0	05	02.6	11	02.6	04	03.3	02	02.0	03	02.3	46
IV	707.4	04.5	12.6	08.4	09.0	14.0	04.3	21.4	30	06.7	19	16	02.5	01	03.0	05	03.0	09	03.3	08	02.6	02	03.0	0.	0.	02	0.0	47
V	710.3	10.6	18.7	12.0	18.0	07.9	24.3	01	05.5	13	15	02.1	01	02.0	04	02.5	07	02.9	05	03.4	07	03.7	0.	0.	01	02.0	35	
VI	711.1	14.9	23.2	16.3	17.7	24.0	10.7	29.7	12	07.1	83	04	02.2	01	02.0	0.	0.	02	0.0	08	02.3	08	02.9	01	02.0	07	02.1	61
VII	712.5	15.4	25.5	18.5	19.3	26.4	11.0	31.5	19	06.1	24	23	02.2	04	02.1	01	02.0	02	02.0	05	02.4	06	02.5	01	02.0	01	02.0	57
VIII	713.0	14.2	25.4	18.8	19.6	26.7	11.2	32.9	08	04.6	16	26	01.8	03	01.7	02	02.0	0.	0.	01	02.0	03	03.7	0.	0.	01	02.0	61
IX	712.0	10.2	18.2	12.3	13.2	19.5	07.8	27.0	12	06.0	23	24	01.8	01	02.0	01	01.0	03	01.3	11	01.3	06	02.5	06	02.0	05	02.2	59
X	715.2	03.6	14.6	09.6	15.0	04.1	24.8	03	-03.4	23	16	02.6	01	02.0	03	02.7	04	02.2	03	02.0	01	02.0	04	02.0	0.	0.	61	
XI	-01.8	01.1	00.1	00.6	04.8	-02.5	13.0	01	-06.2	16	23	01.2</																

Mjesec	Oblačnost Nm (0-10)			Inzolacije Broj sati (Srednje vrijednosti)	Vlažnost vazduha		Padavine R mm	Broj dana na sat												•	*	*	Δ	Δ	▲	▲	R	T	≡						
								Tn	Tx	Tn	Tx	Tn	F(O-12)	Nm(0-10)	R mm	•	*	*	Δ	Δ	Δ	Δ	Δ	Δ	▲	▲	R	T	≡						
	7	14	21	Srednje vrijednosti	7	14	21	Vrh (O-12)	Min	Σ	M	Dat.	≤	<	<	≥	≥	≥	≤	<	>	≥	≥	≥	P	Δ	Δ	Δ	Δ	Δ	Δ				
BUJANOVAC																																			
BR. ST. 221																																			
I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-							
II	8.0	6.6	6.5	7.1	-	04.8	91	77	81	83	55	085	019.8	15	01	01	18	-	-	-	-	11	18	04	07	07	07	01	01						
III	6.8	5.8	3.3	5.3	-	05.5	88	62	76	75	40	076	031.0	20	-	-	07	-	-	-	01	05	10	08	02	10	02	02	01						
IV	7.3	7.2	5.9	6.8	-	07.1	94	62	79	79	34	091	016.4	15	-	-	01	-	-	-	01	01	13	14	12	09	14	-	-						
V	5.5	6.4	4.9	5.6	-	09.4	90	68	79	79	39	070	016.2	08	-	-	02	-	-	-	01	04	10	15	12	02	15	-	04	01					
VI	3.3	5.2	2.1	3.5	-	-	-	-	-	-	-	037	009.8	01	-	-	18	02	-	-	01	09	11	07	-	11	-	01	07	04					
VII	-	-	-	-	-	-	-	-	-	-	-	004	007.5	16	-	-	25	11	-	-	01	-	-	01	01	-	-	01	-	-					
VIII	2.8	2.8	1.0	2.2	-	10.9	84	44	77	69	31	010	008.0	31	-	-	26	04	-	-	19	03	03	02	-	03	-	-	-	-					
IX	5.3	5.5	5.3	5.6	-	09.0	96	58	83	79	18	112	031.8	01	-	-	06	-	-	-	01	06	07	09	09	03	09	-	-	02	08				
X	4.6	4.6	2.8	3.9	-	07.0	94	57	79	77	39	002	001.2	22	-	-	05	02	-	-	-	12	13	02	01	-	02	-	-	-	03	01			
XI	9.4	6.5	4.7	6.9	-	04.2	94	72	80	82	43	012	088.4	30	-	-	24	06	-	-	01	13	02	02	-	02	01	-	-	03	01				
XII	8.2	8.6	6.8	7.8	-	06.7	93	77	81	84	50	090	018.0	18	03	05	15	-	-	-	01	19	08	07	02	04	02	-	-	07	12				
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-						
VRANJE																																			
BR. ST. 222																																			
I	7.5	7.5	6.6	7.2	076.1	04.0	88	71	83	81	49	029	008.8	30	04	06	17	-	-	-	06	02	17	14	07	09	06	02	-	03	12				
II	8.3	7.8	7.1	7.7	075.9	04.6	86	73	82	80	39	064	020.9	15	-	02	18	-	-	-	01	16	15	11	02	08	12	03	-	01	24				
III	7.8	7.5	5.2	6.7	139.5	05.1	85	56	69	70	32	068	021.0	20	-	-	05	-	-	-	08	01	02	13	09	03	13	06	05	-	01	02			
IV	7.8	7.8	7.6	7.7	120.7	04.5	87	52	71	71	30	044	008.7	28	-	-	08	-	-	-	14	19	11	-	19	-	-	-	-	-	01				
V	7.0	7.9	6.9	7.3	173.6	08.3	81	56	72	70	35	085	021.7	03	-	-	01	-	-	-	13	01	-	14	18	12	04	18	-	-	05				
VI	4.3	5.9	4.9	5.0	249.0	10.5	81	48	72	67	28	064	027.7	03	-	-	15	01	-	-	09	03	03	11	09	02	11	-	-	02	19	06			
VII	2.5	3.5	1.9	2.6	346.9	10.0	74	39	57	57	26	016	014.4	16	-	-	25	11	-	-	04	01	13	05	01	01	05	-	-	02	02				
VIII	3.4	4.3	3.6	3.8	298.4	09.3	73	34	57	56	26	019	012.3	31	-	-	24	05	-	-	07	04	02	04	01	01	04	-	-	04	03				
IX	5.8	6.6	4.8	5.6	154.8	08.8	88	54	76	73	34	114	028.0	01	-	-	07	-	-	-	06	05	07	19	04	04	13	-	-	06	11				
X	6.5	5.9	3.8	5.4	147.9	07.1	90	54	76	73	36	008	003.3	20	-	-	04	02	-	-	05	01	05	07	06	02	04	-	-	01	15				
XI	9.5	6.0	6.8	7.4	155.7	07.4	91	74	87	84	54	023	011.5	30	-	01	21	-	-	02	01	17	03	03	02	01	01	-	-	01	01				
XII	8.5	8.2	7.9	8.2	045.0	05.0	91	80	87	86	46	080	021.7	15	01	04	13	-	-	-	03	01	01	19	17	12	04	11	06	-	10	12			
GOD.	6.6	6.6	5.6	6.2	1881.3	07.0	84	58	74	72	26	614	028.0	04IX	05	13	78	74	17	-	79	06	42	129	130	90	23	120	33	11	-	03	34	00	
KUKAVICA																																			
BR. ST. 223																																			
I	7.8	6.6	6.5	6.9	-	03.2	87	85	88	87	52	047	008.6	26	05	13	28	-	-	-	04	15	08	08	01	07	-	-	08	01	08	31			
II	7.9	7.1	7.4	7.5	-	03.6	86	82	85	84	40	083	026.4	15	03	09	21	-	-	-	01	17	12	13	04	10	-	-	01	01	24				
III	7.5	5.9	4.7	6.1	-	04.2	85	74	81	80	44	106	026.4	23	-	02	19	-	-	-	02	03	13	13	12	04	12	02	-	10	21				
IV	7.0	7.0	7.1	7.5	-	05.2	84	73	85	81	40	074	015.8	29	-	04	-	-	-	-	14	18	17	02	14	05	03	-	-	02	09	04			
V	5.7	6.2	5.1	5.7	-	06.6	81	72	79	77	42	135	023.8	08	-	-	02	-	-	-	01	05	09	16	14	05	16	01	01	-	05	06			
VI	4.1	5.1	3.8	4.3	-	08.6	75	65	79	73	43	112	021.0	12	-	-	01	-	-	-	07	04	13	13	04	13	-	-	09	01	09	03			
VII	2.8	2.5	1.6	2.3	-	08.9	72	59	70	67	44	031	025.8	16	-	-	05	-	-	-	18	01	04	03	01	04	-	-	01	03	03				
VIII	3.4	3.4	3.1	3.2	-	08.4	72	57	68	66	38	014	012.0	05	-	-	03	-	-	-	12	02	03	02	01	03	-	-	02	03	03				
IX	6.2	5.9	5.2	5.8	-	07.5	87	75	83	82	41	237	043.8	14	-	-	06	-	-	-	05	08	14	14	04	14	-	-	03	10	16				
X	5.3	4.5	4.4	4.7	-	06.1	87	74	86	82	40	014	004.2	21	-	01	07	-	-	-	10	07	06	05	03	01	-	-	07	02	02				
XI	4.1	3.5	4.0	3.9	-	03.7	73	68	72	72	17	012	007.2	29	-	01	22	-	-	-	14	06	02	02	02	02	-	-	07	01	07				
XII	8.0	7.5	6.9	7.4	-	04.2	87	82	88	86	63	081	014.6	27	02	07	17	-	-	-	02	01	17	11	04	06	05	-	-	08	18				
GOD.	6.1	6.0	5.5	5.8	-	05.8	81	72	80	78	17	946	056.0	04IX	02	10	56	84	27	-	-	58	114	127	166	30	115	22	08	-	-	01	17	35	28
VLASOTINCE																																			
BR. ST. 224																																			
I	6.3	6.4	5.6	6.1	-	-	-	-	-	-	-	046	012.0	05	-	03	16	-	-	-	04	11	07	06	03	05	02	-	-	02	06	06			
II	8.0	7.3	6.7	7.3	-	-	-	-	-	-	-	036	018.0	15	-	01	16	-	-	-	02	15	14	12	01	10	04	-	-	04	06	04			
III	6.6	6.0	5.3	5.9	-	-	-	-	-	-	-	120	032.0	20	-	-	05	-	-	-	05	10	16	13	04	16	01	-	-	01	01	01			
IV	7.0	7.4	7.4	7.3	-	-	-	-	-	-	-	059	014.0	09	-	-	08	-	-	-	11	16	11	02	14	-	-</td								

Mjesec	Vrhunski kritični vrijednosti	Temperatura vazduha °C										Čestina pravaca i srednja jačina vetroa m/s, fm (0-12)														
		Tm				Hm				N		NE		E		SE		S		SW		W		NW		
		7	14	21	Sred. noći	Hm	Hm	N	E	Hm	Hm	Dst.	N	NE	E	SE	S	SW	W	NW	C	8.	9.	8.	9.	8.
$\varphi = 42^{\circ}41' N \lambda = 22^{\circ}11' E$ Gr., AG = + 1h 29 min.																										
I	-	-01.9	03.0	-00.5	00.0	04.1	-03.3	12.4	29	-13.2	09	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
II	-	-00.3	05.2	02.4	06.9	-01.1	17.0	12	-10.0	21	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
III	-	03.2	10.1	05.7	06.2	11.0	02.1	21.8	04	-02.4	14	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
IV	-	07.1	13.2	08.7	09.3	14.9	05.2	20.6	36	01.6	19	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
V	-	11.4	17.7	12.6	13.6	19.3	09.3	27.8	01	-06.6	13	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
VI	-	15.3	23.2	16.2	17.7	24.3	12.2	30.7	12	08.4	02	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
VII	-	16.9	25.7	18.7	20.0	26.0	13.7	34.5	19	08.6	23	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
VIII	-	15.2	25.9	17.9	19.2	26.0	13.0	34.0	08	08.0	14	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
IX	-	10.6	18.2	12.9	13.6	19.6	09.0	26.7	07	-03.3	22	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
X	-	06.7	15.2	09.4	10.2	15.9	05.3	27.0	04	-02.4	23	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
XI	-	-01.1	03.9	00.7	01.1	05.1	-01.8	14.2	01	-06.5	16	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
XII	-	00.7	04.7	02.3	02.5	05.6	-00.7	15.0	29	-11.3	07	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
GOD.	-	07.0	13.8	08.9	09.7	15.1	05.2	34.5	19	-13.2	09.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
$\varphi = 42^{\circ}44' N \lambda = 22^{\circ}21' E$ Gr., AG = + 1h 28 min.																										
I	-	-06.2	-01.6	-03.9	-04.9	-00.4	-09.1	07.5	14	-21.8	09	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
II	-	-03.3	01.5	-02.7	-01.8	03.3	-06.4	13.2	25	-17.0	10	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
III	-	-01.3	04.6	00.2	00.9	06.0	-03.1	15.5	04	-16.3	24	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
IV	-	02.6	06.9	03.6	04.2	09.1	00.4	15.8	30	-04.1	20	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
V	-	07.4	12.0	07.1	08.4	13.9	03.8	21.9	01	-07.1	13	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
VI	-	11.6	16.7	10.5	12.3	16.5	06.6	24.7	12	02.6	01	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
VII	-	12.9	19.5	11.3	13.8	20.6	07.4	24.5	19	02.3	25	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
VIII	-	11.0	19.2	10.6	12.9	20.4	06.6	27.0	08	01.4	14	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
IX	-	04.8	13.8	07.2	08.6	14.1	04.7	22.0	26	-02.6	22	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
X	-	03.2	09.9	04.3	05.4	11.2	01.3	21.4	03	-07.6	23	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
XI	-	-02.6	05.8	-01.4	00.1	07.2	-04.4	13.7	16	-08.2	18	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
XII	-	-01.7	01.3	-00.5	-00.4	02.6	-03.3	08.7	29	-14.3	04	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
GOD.	-	03.4	09.1	03.7	03.6	10.4	00.4	27.0	08	-21.8	09.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
$\varphi = 42^{\circ}30' N \lambda = 22^{\circ}28' E$ Gr., AG = + 1h 29 min.																										
I	-	-04.7	02.2	-01.3	-01.4	03.5	-04.1	10.0	14	-14.5	07	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
II	-	-01.3	05.8	01.1	01.7	07.3	-02.5	15.0	25	-09.0	22	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
III	-	01.0	05.4	02.2	04.0	11.1	-00.4	-	-	-04.6	14	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
IV	-	04.3	10.5	05.6	06.3	11.9	02.5	19.0	30	-12.3	20	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
V	-	10.1	15.9	09.9	11.1	17.6	06.8	25.0	01	00.5	13.12	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
VI	-	13.7	20.6	14.1	15.7	23.4	09.2	26.0	12	05.6	01	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
VII	-	13.8	23.2	14.6	14.7	25.3	09.9	32.0	12.07	05.5	23	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
VIII	-	12.3	23.0	14.2	15.9	24.8	08.9	31.5	08	05.4	14.13	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
IX	-	08.2	16.3	10.3	11.2	18.6	06.3	26.0	12	-01.0	22	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
X	-	04.2	14.1	05.9	07.5	15.5	02.0	26.5	03	-05.0	20.23	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
XI	-	-03.9	07.7	-01.3	00.2	09.5	-03.2	15.0	13	-09.5	21.20	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
XII	-	-01.0	02.7	-00.1	00.3	03.9	-02.5	13.0	19.07	-08.5	07.06	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
GOD.	-	04.7	12.6	06.3	07.5	14.4	02.4	-	-	-14.5	07.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
SR CRNA GORA																										
I	-	-02.6	02.1	-00.4	-00.3	03.2	-04.2	09.5	14	-10.5	10	10	06.3	08	04.5	02	03.0	20	02.6	01	02.0	02	01.5	-	-	44
II	-	-01.4	02.6	-00.3	00.1	03.6	-04.2	10.0	24	-15.0	16	13	03.6	04	03.5	01	02.0	35	02.6	23	02.7	01	01.7	03	05.0	35
III	-	01.0	07.1	01.2	03.6	04.3	-00.9	18.0	04	-05.0	13	21	03.6	05	02.1	01	01.5	11	02.0	30	02.6	01	01.7	01	03.0	21
IV	-	04.9	09.0	05.4	06.2	10.4	02.6	18.0	30	-01.5	10	10	02.6	04	02.5	02	02.5	35	02.3	20	02.5	04	02.0	01	01.5	21
V	-	08.4	12.9	08.7	09.7	13.7	06.6	20.0	21.05	08.0	12	13	02.8	05	02.2	01	03.0	36	03.2	02	03.5	07	02.4	-	-	17
VI	-	13.7	19.1	14.0	15.2	20.2	12.1	25.5	11	06.0	28	09	32.0	06	01.7	01	02.5	28	03.1	02	02.0	03	03.3	02	03.0	32
VII	-	14.0	21.0	16.2	16.9	22.3</td																				

Mesec	Oblačnost Nm (0-10)			Inzolacija broj sati	Vlažnost vazduha			Padavine R mm			Broj dana na sat																											
	7	14	21		7	14	21	Min	Max	Dat.	Tn	Tx	Tn	Tx	Tn	F(0-12)	Nm(0-10)	R mm	•	*	*	*	*	Δ	▲	▲	▲	▲	T	≡	■							
					mm	mm	mm		mm		30,00	0,0	25,0	30,0	20,0	6	8	2,0	8,0	0,1	1,0	0,0	•	Δ	*	Δ	▲	▲	▲	▲	T	≡	■					
BR. ST. 226 SURDULICA																																						
I	6.2	5.5	5.6	5.7	-	-	-	-	-	-	041	008.8	30	07	07	18	.	.	01	.	05	10	10	08	-	04	07	.	02	.	02	17						
II	6.3	6.1	6.9	6.4	-	-	-	-	-	-	042	017.0	15	01	01	18	05	12	12	11	01	04	10	01	12				
III	6.9	6.9	4.7	6.2	-	-	-	-	-	-	135	040.0	20	.	.	05	.	.	.	04	11	12	11	06	10	07	02	03					
IV	5.8	7.5	7.5	6.9	-	-	-	-	-	-	056	017.4	29	01	11	17	12	02	17	02	02	.	.	.	01	.	01					
V	5.8	6.7	5.7	6.1	-	-	-	-	-	-	121	017.3	03	.	.	01	01	.	.	.	02	08	18	14	06	18	01	.	.				
VI	4.1	4.9	5.3	4.8	-	-	-	-	-	-	088	024.0	09	.	.	15	01	.	.	.	06	07	08	04	12	02	03						
VII	2.3	3.1	1.9	2.4	-	-	-	-	-	-	024	022.5	16	.	.	23	08	.	.	.	15	02	02	01	02					
VIII	3.5	3.6	3.7	3.6	-	-	-	-	-	-	013	004.4	05	.	.	22	05	.	.	.	09	02	04	04	04	.	04					
IX	5.8	6.3	5.1	5.7	-	-	-	-	-	-	165	040.2	01	.	.	06	.	.	.	07	08	13	12	05	12	02	03						
X	4.5	4.7	4.0	4.4	-	-	-	-	-	-	010	004.4	22	.	.	03	02	.	.	.	39	07	05	03	05	01					
XI	6.7	6.2	7.4	7.4	-	-	-	-	-	-	029	022.5	30	.	02	20	.	.	.	01	15	04	02	01	33	01	05					
XII	7.4	7.0	6.9	7.1	-	-	-	-	-	-	094	018.5	15	02	05	14	.	.	.	01	12	18	12	04	11	07	04	15					
GOD.	5.6	5.7	5.4	5.6	-	-	-	-	-	-	818	040.2	0LIX	10	15	79	69	14	.	-	-	65	103	127	99	30	102	34	03	02	.	03	-	48				
BR. ST. 227 VLASINA																																						
I	6.8	6.0	5.3	6.1	046.7	-	-	-	-	-	060	012.6	01	13	14	31	.	.	.	03	11	14	10	03	32	14	02	.	.	.	08	31						
II	6.9	7.0	6.4	6.8	088.9	-	-	-	-	-	052	011.9	21	07	09	23	.	.	.	02	14	16	12	02	04	12	03	24					
III	6.6	6.2	5.2	6.0	129.6	-	-	-	-	-	170	033.4	19	01	03	24	.	.	.	03	10	18	13	06	08	14	05	.	.	.	06	19						
IV	6.6	7.8	6.8	7.1	113.7	-	-	-	-	-	063	018.8	29	.	15	.	.	.	01	24	12	01	21	08	04	.	.	.	02	02	07	03						
V	6.8	7.1	5.3	6.4	140.4	-	-	-	-	-	097	019.0	15	.	02	.	.	.	01	09	21	14	04	21	02	02	.	.	.	02	05	01						
VI	4.0	5.9	4.5	4.8	146.5	-	-	-	-	-	168	037.4	12	.	.	06	.	.	.	01	04	20	17	05	20	.	.	.	02	12	01							
VII	2.9	3.9	2.2	3.0	247.5	-	-	-	-	-	026	021.2	16	.	.	06	.	.	.	07	05	03	01	05	.	.	.	01	.	.	01							
VIII	3.9	4.3	4.0	4.1	238.4	-	-	-	-	-	025	008.0	05	.	02	.	.	.	05	04	08	06	08	08	.	.	.	03	01	.	01							
IX	5.7	6.7	5.8	6.1	151.6	-	-	-	-	-	148	046.5	01	.	02	.	.	.	04	08	19	13	04	19	01	.	.	.	03	04	01							
X	5.7	5.0	4.7	5.1	155.2	-	-	-	-	-	016	003.9	20	.	01	11	.	.	.	04	07	07	07	05	05	01	.	.	.	08	04							
XI	4.1	5.3	3.6	3.7	152.4	-	-	-	-	-	024	019.7	30	.	01	28	.	.	.	14	05	03	02	01	03	03	.	.	.	05	02							
XII	7.4	8.0	7.0	7.5	-	-	-	-	-	-	099	025.7	15	04	10	23	.	.	.	01	14	20	13	04	09	14	03	.	.	.	12	22						
GOD.	5.6	5.9	5.1	5.7	-	-	-	-	-	-	948	046.5	0LIX	25	38	159	08	.	.	.	48	96	175	122	31	128	73	20	.	.	.	06	27	58	100			
BR. ST. 228 BOSILJGRAD																																						
I	7.5	6.8	7.4	7.2	-	-	-	-	-	-	027	-	08	03	29	.	.	.	04	17	-	-	-	-	-	-	.	.	.	06								
II	7.3	6.9	6.8	7.0	-	-	-	-	-	-	044	007.5	27	.	21	.	.	.	06	16	08	08	03	05	04								
III	6.0	6.1	4.2	5.8	-	-	-	-	-	-	048	011.0	17	.	01	.	.	.	06	11	11	11	01	11	03								
IV	7.0	7.9	7.5	7.7	-	-	-	-	-	-	048	011.0	17	.	01	.	.	.	01	14	11	11	01	11	03								
V	6.4	7.6	5.5	6.5	-	-	-	-	-	-	099	020.0	21	.	01	.	.	.	02	12	13	11	05	13	01								
VI	3.7	6.0	5.9	5.2	-	-	-	-	-	-	073	023.0	22	.	11	.	.	.	02	07	08	08	03	08	06								
VII	2.6	5.1	1.8	3.2	-	-	-	-	-	-	018	014.5	16	.	18	05	.	.	07	02	02	01	02	02	01								
VIII	2.5	4.9	2.5	3.6	-	-	-	-	-	-	027	013.5	12	.	19	02	.	.	05	04	04	01	04	04	01								
IX	5.4	5.7	4.3	5.1	-	-	-	-	-	-	106	024.5	13	.	02	02	.	.	08	09	09	05	05	05	03								
X	4.1	4.9	4.7	5.2	-	-	-	-	-	-	015	005.3	29	.	10	02	.	.	07	07	05	03	02	01	02	01	.	.	.	02								
XI	5.3	2.8	3.0	3.7	-	-	-	-	-	-	021	012.0	30	.	27	.	.	.	13	07	03	03	01	32	02	04							
XII	8.3	7.6	8.3	8.0	-	-	-	-	-	-	011	005.0	05	.	24	.	.	.	01	19	03							
GOD.	5.4	6.0	4.8	5.4	-	-	-	-	-	-	076	7.88	81	91	86	17	1963	090.0	23V	04	09	-	16	.	04	54	41	77	124	127	119	66	148	32	02	.	05	68
BR. ST. 230 ZABLJAK																																						

Mjesec	Vrijeme godine i minuti	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta m/s, Fm (0-12)												
		Sm					Hm					Cestina pravaca i srednja jačina veta m/s, Fm (0-12)						Cestina pravaca i srednja jačina veta m/s, Fm (0-12)						
		7	14	21	Sred. sata	Det.	Hm	Hm	Hm	Hm	Hm	Det.	N	NE	E	SE	S	SW	W	NW	C			
$\varphi = 42^{\circ}21' N \lambda = 19^{\circ}21' E$ Gr., AG = + 1h 17 min.																								
I	692.7 -04.4	01.6 -02.6	02.0	02.6 -06.5	11.8	13 -22.8	09	04	02.0	01	01	01.0	09	02.6	05	03.2	01	02	01.5	06	01.8	66		
II	692.7 -01.8	03.3 00.5	00.6	05.0 -03.4	15.6	25 -16.6	16	07	01.9	01	01.0	02.3	01	05.0	02	03.5	06	02.0	02	02.0	02	02.0	53	
III	691.8 00.7	09.1 04.4	04.7	10.5 -00.1	19.0	04 -08.4	23	13	02.5	03	02.7	04	03.0	08	02.8	06	03.2	05	02.6	03	02.0	06	02.2	45
IV	691.2 05.2	10.6 06.9	07.4	12.0 03.6	20.2	30 -01.4	03	04	02.2	05	02.2	04	02.2	05	03.0	13	03.0	05	04.2	05	02.4	03	01.7	46
V	692.9 08.1	15.1 10.4	11.0	16.6 06.1	23.6	01 -03.7	18	06	02.5	03	02.3	03	02.0	01	07	04.1	05	J3.2	06	02.5	01	01.0	62	
VI	693.9 12.0	21.1 14.4	15.5	22.3 09.8	28.2	11 05.6	26	07	02.0	01	03.0	04	02.2	01	03.3	09	04.1	05	03.0	04	02.5	57		
VII	693.9 11.8	23.2 16.5	17.8	24.6 09.4	30.6	12 04.0	24	09	01.8	05	02.4	01	04.0	01	05	04.2	06	03.3	06	02.0	02	02.0	59	
VIII	693.7 11.2	23.2 15.9	16.5	24.5 09.3	31.6	07 04.6	31	04	02.2	02	02.0	03	02.0	01	08	02.5	05	03.0	06	02.3	07	01.0	58	
IX	693.2 07.5	16.5 10.2	11.1	17.8 05.9	26.2	26 -00.2	22	02	02.0	01	02.0	01	02.0	01	03	05.0	04	01.5	08	02.0	04	01.8	68	
X	697.0 06.9	12.8 07.1	08.0	13.8 03.6	25.2	03 -03.8	25	07	02.0	01	02.0	03	02.3	01	02.0	02	03.5	02	02.0	01	02.0	01	76	
XI	700.4 -02.7	05.7 -00.5	00.5	07.0 -03.8	16.6	16.03 -09.6	16	03	01.7	01	02.0	01	02.0	02	02.5	01	03.0	04	01.5	01	02.0	78		
XII	691.3 -00.2	03.9 00.5	01.1	05.2 -03.0	13.6	17 -11.2	08	02	02.0	01	02.0	03	02.0	02	02.0	04	03.5	05	02.6	03	02.3	01	69	
GOD.	693.7 04.4	12.2 07.0	07.6	13.5 02.6	31.6	07VM -22.8	09.1	08	02.1	22	02.3	34	02.3	26	02.7	64	03.4	53	03.2	55	02.2	36	01.9	737
$\varphi = 42^{\circ}02' N \lambda = 19^{\circ}45' E$ Gr., AG = + 1h 19 min.																								
BIJELO POLJE																								
$\varphi = 42^{\circ}02' N \lambda = 19^{\circ}45' E$ Gr., AG = + 1h 19 min.																								
I	-04.6	02.0 -02.4	01.7	03.0 -03.3	12.6	29 -17.9	09	01	01.5	01	01.0	08	01.1	01	01.0	35	01.4	05	01.0	06	01.0	35		
II	-0.6	0.6 02.0	02.2	07.1 -01.9	19.9	25 -09.6	16	01	01.6	01	01.0	02	01.3	01	01.3	01	02.0	05	01.8	01	02.0	01	28	
III	01.8 11.1	05.4 05.9	05.9	12.5 01.0	22.0	06 -03.7	23	01	01.7	02	01.5	14	01.3	01	01.3	07	02.7	01	02.1	19				
IV	05.9 12.6	07.9 08.3	14.1	22.7	12 -00.2	03	01	01.9	01	01.5	02	01.5	39	01.5	01	01.5	07	01.1	23					
V	06.8 17.3	16.9 12.0	18.8 06.8	27.0	01 -02.1	18	01	02.0	12	01.4	01	02.0	13	01.3	02	02.5	34	01.6	01	02.0	02	01.0	27	
VI	13.1 21.2	14.4 16.2	24.3 10.2	30.3	10.5	04.4	01	01.3	01.5	01.5	04	01.2	33	01.3	01	01.3	04	02.0	26					
VII	12.3 25.2	15.6 17.2	26.1 09.5	32.4	12 04.3	24	01	01.5	01	01.0	13	02.0	15	01.5	04	01.2	38	01.4	02	01.5	06	01.0	22	
VIII	11.7 25.1	15.0 16.7	26.5 09.7	32.9	07 05.9	22	01	01.9	01	01.0	18	01.3	03	01.0	27	01.5	01	04	02.0	31				
IX	08.5 17.4	16.5 11.7	18.7 07.2	26.1	26 -00.4	22	01	01.0	01	01.0	12	01.2	01	01.0	27	01.2	01	01.0	19	01.6	35			
X	05.4 14.0	10.7 07.2	08.5 15.4	22.2	03 -04.6	29	01	02	02.5	03	01.0	18	01.2	01	01.0	07	02.3	35						
XI	-01.7 04.2	-00.7 00.3	05.2 -02.6	18.4	03 -07.2	17	01	01.0	03	01.3	14	01.0	08	01.0	01	01.0	01	01.0	01	01.0	01	43		
XII	-00.6 05.4	01.8 02.4	04.4 -01.0	15.9	17 -09.2	06	01	02.0	03	01.7	01	01.0	12	01.0	03	01.0	41	01.8	03	01.7	03	01.3	27	
GOD.	-05.1 13.6	07.3 08.3	14.8 03.6	32.9	07VM -17.9	09.1	02	02.0	03	01.5	14	01.3	162	31.2	20	01.3	387	01.4	14	01.3	62	01.6	351	
HERCEGNOVI-IGALO																								
$\varphi = 42^{\circ}28' N \lambda = 19^{\circ}30' E$ Gr., AG = + 1h 14 min.																								
I	757.1 06.5	10.7 07.3	07.9	11.8 04.7	17.6	14 -01.4	07	07	05.0	09	05.1	16	03.3	09	03.0	02	02.5	02	02.5	05	02.0	06	02.3	37
II	753.1 07.1	11.1 08.3	08.8	12.4 03.9	16.4	25 08.8	16	04	02.0	07	03.3	16	02.8	05	02.6	03	02.0	02	03.5	09	02.0	05	01.8	33
III	754.3 08.6	14.5 10.3	10.9	19.6 07.0	22.4	03 01.9	23	05	04.0	07	03.9	14	02.9	10	02.9	04	02.8	09	02.7	10	02.9	06	02.0	28
IV	753.6 11.7	15.8 12.1	12.9	17.3 09.5	21.7	13 04.0	19	01	02.5	25	02.9	10	03.7	03	02.0	06	02.8	12	02.6	04	02.0	04	24	
V	754.5 14.6	18.8 14.8	15.7	20.6 11.6	25.3	01 05.3	18	02	01.5	03.3	15	03.3	36	02.2	03	02.0	03	04.0	14	02.2	08	01.9	39	
VI	756.8 19.9	24.8 19.7	21.0	26.1 16.2	30.6	12 11.8	28	01	02.0	01	02.4	01	02.4	07	02.2	06	01.8	07	03.4	12	03.2	07	02.0	36
VII	757.2 21.9	26.0 22.0	23.5	29.0 18.1	33.2	13 18.6	18	02	03.5	02	04.0	11	02.7	05	03.0	04	02.5	12	03.2	14	02.6	05	02.2	38
VIII	757.7 21.0	24.4 21.4	23.6	29.5 17.7	32.4	06 05.0	31.0	01	02.5	08	02.9	08	02.5	02	03.5	15	03.4	12	03.0	06	02.2	45		
IX	757.2 16.5	22.2 17.2	18.3	23.7 19.6	26.7	18 08.6	22	06	03.2	04	03.0	16	02.3	06	01.5	06	02.2	05	03.2	11	02.5	31		
X	759.7 13.3	19.8 14.5	20.8	11.6 17.5	27.5	03 04.6	29	06	04.0	08	03.5	12	02.8	05	02.4	04	02.0	07	02.6	14	02.1	03	02.0	34
XI	760.7 08.7	10.1 11.2	11.2	17.0 07.3	19.8	17.0 02.6	29	01	04															

G D N E S H	Oblačnost Nm (0-10)			Insekticid: kg/ha	Vlažnost vazduha			Padavine R mm			Broj dana na:																								
	Tn	Tx	Tn		Tx	Tn	Tx	Tn	P(0-12)	Nm(0-10)	R mm	•	*	*	Δ	Δ	Δ	Δ	R	T	≡														
	7	14	21		7	14	21	7	14	21	7	14	21	7	14	21	7	14	21	7	14	21													
PLJEVLJA																																			
BR. ST. 231																																			
I	7.6	5.7	5.1	6.2	071.7	03.6	09	71	87	82	57	042	023.0	30	08	11	25	•	•	•	07	02	01	09	10	07	01	03	08	•	•	•	•	11	19
II	8.6	8.1	6.6	7.6	044.4	04.1	08	73	86	82	31	098	037.5	14	03	04	21	•	•	•	08	02	01	14	14	12	03	05	11	•	•	05	21		
III	6.7	6.5	5.7	6.3	132.5	04.7	09	57	78	75	32	044	009.3	22	•	17	•	•	•	08	01	04	13	15	12	03	05	11	•	•	02	06			
IV	9.0	8.5	7.0	8.1	085.1	05.9	09	43	81	78	35	076	017.8	14	•	2	•	•	09	04	01	19	21	17	01	14	04	01	•	•	01	01	03	03	
V	7.9	8.0	6.0	7.3	106.2	07.5	91	59	82	77	32	131	015.1	21	•	•	02	•	•	•	08	04	•	12	22	19	05	21	02	•	•	•	02	04	
VI	7.3	6.4	3.7	5.8	175.9	09.7	92	32	81	75	34	078	029.3	16	•	•	04	•	•	•	08	01	05	09	02	07	09	01	05	02	09				
VII	2.9	4.2	2.6	3.7	269.2	09.5	91	42	73	69	30	026	014.2	16	•	•	16	01	•	•	04	01	11	01	05	03	01	05	03	03	03				
VIII	5.1	5.0	3.5	4.0	203.3	09.5	93	44	76	71	25	028	008.9	31	•	•	15	03	01	04	01	07	03	08	04	08	03	03	03	03	03				
GUD.	7.4	6.4	5.0	6.3	1442.3	06.5	91	60	83	78	20	817	043.1	43.IX	19	23	118	39	04	01	72	23	31	119	147	111	24	115	44	03	•	02	20	03	02
BIJELO POLJE																										$H = 540 \text{ m } H_b = - \text{ m } h = 2.0 \text{ m } h = 1.8 \text{ m}$									
BR. ST. 232																										$H = 540 \text{ m } H_b = - \text{ m } h = 2.0 \text{ m } h = 1.8 \text{ m}$									
I	7.6	5.7	6.0	6.5	072.6	03.6	90	73	90	84	43	063	038.7	30	08	09	27	•	•	•	01	•	03	10	10	07	01	03	08	•	•	•	01	04	21
II	8.5	7.5	7.8	8.0	051.0	04.0	91	68	85	81	16	140	049.4	14	•	20	•	•	•	02	14	11	07	02	07	04	•	•	02	13					
III	7.4	6.2	6.0	6.5	138.7	04.7	88	45	74	69	13	058	024.6	18	•	07	•	•	•	02	14	11	07	02	07	04	•	•	04	01					
IV	9.1	8.2	7.1	8.1	385.7	03.6	90	53	80	74	20	066	010.4	29	•	01	•	•	•	01	16	16	14	01	16	04	•	•	01	03					
V	7.9	7.7	7.2	7.6	131.1	07.9	92	53	85	77	22	134	026.0	09	•	•	01	02	•	•	02	01	•	14	20	17	05	19	01	•	•	01	03	03	
VI	7.3	6.1	4.4	5.9	207.1	10.1	89	49	87	75	25	066	016.0	28	•	•	15	02	•	•	03	13	09	03	13	05	02	07	07	04	07				
VII	2.9	3.5	2.5	3.7	279.5	09.5	92	37	82	70	22	024	011.9	16	•	•	23	04	•	•	02	04	01	07	05	01	07	•	•	06	07				
VIII	6.3	4.6	3.5	4.6	230.3	09.2	91	34	81	73	20	025	007.1	12	•	•	21	06	•	•	03	04	04	05	05	05	08	•	•	02	07				
IX	9.7	6.1	5.6	7.1	102.5	08.4	94	56	92	80	33	167	058.9	13	•	•	03	•	•	•	14	12	10	04	12	•	•	•	02	02	10				
X	9.2	5.3	5.1	6.6	101.4	04.8	93	56	87	78	21	041	013.2	22	•	•	05	•	•	•	12	06	07	01	06	•	•	•	•	•	13				
XI	9.8	6.2	6.1	7.4	052.4	04.0	93	70	91	85	36	023	013.1	20	•	01	25	•	•	•	13	04	03	01	03	01	•	•	16	01					
XII	9.2	7.6	7.5	8.1	351.9	13.3	88	61	82	77	33	115	032.7	19	•	03	14	•	•	•	01	20	19	14	03	16	05	•	•	01	03	13	10		
GUD.	8.1	6.2	5.7	6.7	1504.3	04.6	90	54	84	76	13	922	058.9	43.IX	08	13	100	64	12	•	07	01	19	143	145	113	29	121	32	02	•	04	14	98	46
HERCEGOVINA-IGALO																										$H = 40 \text{ m } H_b = 41.7 \text{ m } h = 2.0 \text{ m } h = 1.1 \text{ m}$									
BR. ST. 233																										$H = 40 \text{ m } H_b = 41.7 \text{ m } h = 2.0 \text{ m } h = 1.1 \text{ m}$									
I	6.5	7.1	6.1	6.6	085.4	26.3	77	69	80	75	32	276	059.9	30	•	•	03	•	•	•	13	06	05	12	16	13	09	16	•	•	04				
II	7.2	8.5	6.4	7.6	062.7	07.2	75	85	82	83	39	283	041.9	13	•	•	02	•	19	•	•	08	•	13	20	17	10	20	•	•	02	02			
III	5.4	5.5	5.1	5.3	186.7	07.2	82	62	75	73	33	289	052.3	22	•	•	07	•	•	•	11	08	07	09	17	12	10	17	•	•	02				
IV	8.0	7.7	6.8	7.5	120.9	09.0	85	69	85	80	35	279	119.1	26	•	•	05	•	•	•	12	01	•	16	21	18	08	21	•	•	03				
V	6.8	6.5	5.6	6.5	183.8	10.8	85	67	88	80	33	298	092.8	23	•	•	01	01	02	•	08	03	03	11	19	14	09	19	01	01	01				
VI	7.7	8.6	4.6	5.6	271.1	14.3	83	63	82	75	34	307	037.7	16	•	•	24	01	01	01	10	02	06	02	06	05	02	06	04	•	•	02			
VII	1.5	2.8	2.6	2.9	371.0	13.6	65	52	67	62	34	317	007.8	16	•	•	31	12	07	08	02	19	01	03	03	03	03	03	03	03	03	02			
VIII	2.2	3.5	1.6	2.6	310.2	14.4	71	54	75	67	32	001	001.1	30	•	•	31	18	02	09	01	19	01	02	01	02	02	02	02	02	02	02			
IX	4.5	5.2	3.5	4.4	208.1	11.4	75	61	79	72	37	271	080.1	07	•	•	11	•	•	•	13	05	10	05	10	08	07	10	•	•	06				
X	4.6	4.7	3.8	4.6	193.9	09.8	75	60	79	71	33	216	041.6	02	•	•	03	•	•	•	11	08	10	10	10	08	04</								

Broj	Vreme od početka m	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta m/s, Fm (0-12)																				
		M					NE					E			SE			S			SW			W			NW					
		7	14	21	24	00	M	NE	E	SE	S	SW	W	NW	C	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.	8.	9.					
$\varphi = 42^{\circ}17' N \lambda = 18^{\circ}51' E$ Gr., AG = + 1h 15 min.															BUDVA												BR. ST. 236					
I	761.0	06.2	10.5	06.7	07.5	11.6	06.3	17.0	14	-06.7	09	10	04.3	01	03.0	09	02.9	10	02.2	22	02.5	.	.	01	03.0	.	.	40				
II	757.1	07.7	11.2	08.6	09.1	12.6	05.8	16.5	27	00.2	16	4	05.2	02.2	11	02.7	29	02.3	01	03.0	.	.	41			
III	760.1	10.4	15.2	10.7	11.8	16.1	07.9	20.8	06	08.7	25	04	03.5	09	02.7	07	02.4	02	01.5	28	02.9	01	03.0	.	.	01	03.0	.	.	43		
IV	757.7	13.4	16.6	12.9	13.9	17.7	10.5	23.2	13	06.7	18	02	03.0	01	01.0	.	.	08	03.8	31	02.9	03	02.0	02	02.0	.	.	01	03.0	.	.	43
V	760.7	16.8	19.4	15.3	16.7	21.1	12.5	24.1	01	07.6	13	01	02.0	31	02.6	02	01.5	39			
VI	760.7	22.2	25.2	20.4	22.1	26.4	17.7	22.3	19	12.7	02	27	01.8	08	02.8	55			
VII	761.0	24.1	27.9	22.6	24.3	29.3	14.1	24.2	14	12.7	10	08	02.2	24	01.8	15	01.9	05	01.8	41			
VIII	761.7	22.5	27.5	21.9	23.4	26.8	16.6	23.4	06	16.2	12	03	02.7	32	02.2	04	02.0	01	02.0	53			
IX	761.2	17.9	22.2	17.4	18.7	23.3	14.7	27.1	17	18.8	22	06	02.2	.	.	.	07	02.4	40	02.1	02	03.5	08	02.6	36			
X	761.6	14.2	20.5	14.9	16.1	21.5	12.4	29.1	03	08.8	27	01	03.0	07	04.3	02	03.0	07	02.4	31	01.7	01	02.0	44				
XI	767.8	09.4	16.9	10.6	11.9	17.6	06.2	20.0	03	06.7	13	02	02.0	23	01.8	.	.	02	02.0	.	.	63					
XII	760.0	10.9	14.6	11.1	11.9	19.2	06.3	20.8	19	03.2	07	.	.	05	03.4	02	02.0	14	02.7	39	02.4	02	03.0	31				
GOD.	761.1	14.6	19.0	14.4	15.6	20.1	11.7	24.2	44.VII	-06.7	09.1	34	03.1	23	03.3	24	02.6	55	02.7	357	02.3	37	02.3	11	02.0	10	02.6	544				
$\varphi = 42^{\circ}24' N \lambda = 18^{\circ}46' E$ Gr., AG = + 1h 16 min.															CETINJE												BR. ST. 237					
I	-	-02.3	04.6	-01.6	06.6	05.6	-04.1	12.6	14	-12.0	10.06	16	.	.	01	02.0	04	04.0	02	04.5	.	.	.	03	04.3	02	03.5	81				
II	-	-00.2	05.6	01.6	02.3	07.6	-02.3	15.6	23	-12.4	16	01	03.0	.	.	06	03.7	04	03.8	04	03.2	.	.	03	04.3	02	03.5	66				
III	-	-02.0	10.1	04.6	05.3	11.5	06.2	20.0	03	-05.1	13	04	02.2	09	02.4	03	02.7	03	06.3	01	03.0	06	03.0	04	03.5	63						
IV	-	06.5	11.3	07.2	08.1	13.1	05.6	18.4	30	-01.2	18	01	02.0	.	.	08	02.5	08	02.5	06	03.0	03	02.5	02	03.0	56						
V	-	11.0	15.0	09.9	11.5	16.9	09.9	23.0	01	-01.2	13	.	.	03	02.7	11	02.3	04	03.8	01	05.0	02	02.5	04	03.2	02	03.5	66				
VI	-	16.4	21.9	14.0	16.6	23.4	09.6	27.6	20	03.8	20	.	.	02	02.0	08	02.6	04	02.2	03	02.3	02	03.0	06	02.5	03	02.5	63				
VII	-	17.3	24.6	15.8	18.4	26.1	09.1	31.4	12	04.0	23	.	.	03	02.3	10	02.4	05	02.4	02	03.0	.	.	04	02.8	03	02.5	63				
VIII	-	15.8	24.6	15.0	17.6	26.7	09.4	31.3	03	05.6	22	.	.	04	02.2	06	02.7	07	02.3	04	02.8	02	03.0	04	02.5	04	02.5	64				
IX	-	09.8	17.9	10.6	12.2	14.6	06.0	26.2	11	-06.6	22	.	.	03	02.0	04	02.7	03	02.7	02	04.0	01	02.0	04	02.5	02	03.0	69				
X	-	05.3	15.7	07.1	08.8	16.7	03.0	25.2	03	-03.2	31	03	05.0	08	02.4	05	01.8	06	02.0	01	01.0	.	.	03	03.0	01	01.0	66				
XI	-	-02.9	11.7	06.3	02.4	12.8	-04.0	17.6	14	-07.2	17.16	03	01.0	08	02.0	09	02.1	02	02.5	.	.	03	02.3	01	02.0	66						
XII	-	01.6	07.6	03.0	03.6	06.8	-01.1	12.7	18	-06.6	07	.	.	01	02.0	03	03.7	05	05.2	01	04.0	02	03.0	01	03.0	75						
GOD.	-	06.7	14.2	07.4	08.9	15.7	02.9	31.5	02.VII	-12.4	16.11	08	02.9	33	02.2	05	02.6	52	02.8	34	03.5	14	02.9	46	02.8	'24	03.0	799				
$\varphi = 42^{\circ}46' N \lambda = 18^{\circ}37' E$ Gr., AG = + 1h 16 min.															NIKŠIĆ												BR. ST. 238					
I	704.6	-00.3	03.9	01.2	01.5	04.9	-01.4	11.8	14	-07.0	10	19	02.2	25	02.7	06	01.7	35	02.2	24	02.7	01	01.0	02	01.5	04	01.0	07				
II	700.7	01.1	05.2	02.7	02.9	06.2	-00.1	14.4	25	-09.4	16	26	02.5	18	02.4	03	02.7	06	01.8	21	03.3	01	03.0	04	01.2	01	01.0	06				
III	703.8	03.5	09.5	06.1	06.4	10.8	02.3	20.4	03	-01.4	13	22	02.4	20	03.1	01	03.0	06	02.8	20	03.0	04	01.5	02	03.0	03	02.0	03				
IV	701.4	07.1	11.4	08.1	08.6	12.5	05.3	17.8	30	00.6	19	12	02.2	13	02.1	04	02.2	10	02.1	38	03.4	05	03.2	02	01.5	03	02.0	03				
V	704.7	10.5	15.3	11.4	12.1	16.4	07.7	22.8	01	00.8	13	18	02.2	12	02.5	02	02.5	06	02.7	37	03.7	05	03.2	05	02.6	04	02.0	04				
VI	705.8	15.6	21.4	16.7	22.7	11.5	26.0	10	01.1	16	19	01.8	14	01.6	02.5	06	01.3	33	03.5	04	04.0	03	02.0	04	01.5	05	01.0	06				
VII	706.7	17.1	24.6	18.7	19.8	25.8	13.2	31.5	13	00.6	16	25	02.3	15	02.5	02	04.5	05	01.6	19	03.6	07	03.1	08	01.9	36	01.2	07				
VIII	707.2	16.1	23.2	18.9	20.5	27.0	12.8	32.6	03	04.6	21	23	01.7	18	01.6	05	02.4	05	02.2	22	03.4	06	03.2	04	02.2	04	02.3	04				
IX	-	11.3	17.9	12.8	13.7	19.2	08.6	26.2	11	02.8	20	27	02.4	25	02.6	09	02.8	01	02.0	30	03.7	05	02.0	05	01.6	02	01.6	02				
X	708.3	07.9	15.6	10.6	14.7	20.5	05.2	25.5	12	00.6	30	30	08.0	23	02.8	06	02.5	06	02.6	35	02.7	19	03.7	07	02.0	05	01.6	02				
XI	711.2	00.9	11.8	04.2	05.3	12.8	-00.3	17.3	16	-03.6	09	21	02.2	26	01.8	.	02.3	07	03.0	21	02.5	02	01.5	01	01.0	03	01.7	09				
XII	703.5	02.6	06.7	03.8	04.3	07.7	01.4	12.8	16	-07.2	07	17	01.2	20	01.8	02	01.0	05	01.4	31	01.4	21	02.9	06	02.3	07	01.7	09				
GOD.	-	11.3	17.6	12.1	13.3	18.7	07.7	25.0	40.1	54	03.0	228	02.5	91	02.1	68	02.8	288	02.6	103	03.1	35	02.0	11	02.2	215						
$\varphi = 42^{\circ}14' N \lambda = 19^{\circ}03' E$ Gr., AG = + 1h 16 min.															VIRPAZAK												BR. ST. 239					
I	-	02.2	07.6	03.3	04.1	06.0	06.8	15.0	29	-06.0	18	.	.	32	03.0	06	01.6	16	02.1	02	01.3	19	01.9	10	01.3	04	01.8	02				
II	-	04.8	09.7	06.4	08.8	10.8	02.9	18.0	11	-03.4	19	05	02.4	19	02.4	06	05.2	05	05.0	03	04.0	01	03.0	03	02.0	36		
III	-	08.1	13.8	10.1	10.5	15.1	04.2	20.3	05	01.0	13	15	04.0	21	03.0	10	02.1	20	03.0	09	03.8	06	03.0	04	02.5	04	01.0	13				
IV	-	11.1	15.8	12.0	12.7	17.0	08.6	22.5	30	02.0	19	02	02.5	09	02.8	06	03.5	40	02.6	10	02.0	03	01.7	01	01.0	11	01.1	11				
V	-	14.9	19.3	14.5	15.8	20.5	11.3</																									

Meseč.	Oblačnost Nm (0-10)				Inzolačijski broj (Nm)	Vlažnost vazduha			Padavine R mm			Broj dana u sati																							
	7	14	21	30		Tn	Tx	Tn	Tx	Tx	Tn	P(0-12)	Nm(0-10)	R mm	≤	<	<	≥	≥	≥	≤	≤	<	>	≥	≥	•	*	*	Δ	▲	▲	□	T	≡
						7	14	21	30	30	30	30	30	30	30.00.0	0.0	25.0	30.0	20.0	0.6	6	6	2.0	8.0	0.1	1.0	0.0	•	Δ	▲	▲	□	T	≡	
BRO. ST. 236																																			
SUDVA																																			
I	6.1	6.6	6.0	6.2	095.6	05.8	74	62	77	71	22	166	068.3	30	.	.	82	.	.	.	03	01	07	14	21	15	04	21	.	.	.	01	03	.	
II	7.9	7.9	6.0	7.2	073.8	07.1	67	71	82	60	32	198	035.7	14	01	03	14	20	15	07	20	.	.	.	03	03	.		
III	5.5	4.8	3.4	4.6	191.2	07.3	76	63	73	69	18	198	032.7	16	04	01	09	05	14	16	04	14	.	.	.	02	01	.	
IV	6.0	7.5	6.7	7.4	117.0	09.7	81	74	85	60	40	146	052.8	24	04	02	18	22	14	04	22	.	.	.	04	04	.		
V	6.8	6.5	5.2	6.2	190.1	11.8	81	72	90	81	42	291	055.8	23	.	.	.	83	.	.	02	05	14	19	15	07	19	.	.	.	03	03	.		
VI	4.7	4.6	2.0	3.8	273.1	14.2	79	81	79	73	38	046	016.3	28	.	.	.	22	02	04	.	09	03	04	02	06	.	.	.	03	03	.			
VII	1.6	1.8	0.2	1.1	343.0	15.3	66	56	76	66	27	006	002.9	16	.	.	.	31	11	07	.	24	03	02	03	03	.	.	.	03	03	.			
VIII	2.4	3.4	0.9	2.2	295.0	15.7	76	62	77	71	29	006	004.6	12	.	.	.	31	07	04	.	17	01	03	01	03	.	.	.	02	02	.			
IX	3.8	5.4	3.3	4.2	196.5	11.6	72	63	76	70	25	170	039.5	13	.	.	.	87	.	.	02	10	09	09	08	08	09	.	.	.	04	04	.		
X	4.3	4.4	2.4	3.7	186.2	10.4	77	62	79	72	24	067	018.6	21	.	.	.	04	.	.	02	15	08	09	07	03	09	.	.	.	02	02	.		
XI	3.0	3.7	2.1	3.0	193.4	08.0	62	61	83	75	36	082	037.4	20	.	.	.	05	14	04	04	03	03	04	.	.	.	03	03	.					
XII	7.1	7.4	6.0	6.8	086.1	07.9	77	63	79	73	29	163	035.5	15	.	.	.	05	01	02	10	20	16	05	20	.	.	.	03	03	.				
GOD.	5.1	5.3	3.7	4.7	2247.0	10.6	77	64	80	73	18	1539	068.3	.	.	.	82	98	20	17	23	03	117	100	150	114	49	150	.	.	.	01	34	01	
CETINJE																																			
BR. ST. 237																																			
I	6.4	6.7	5.0	6.1	-	04.2	92	74	93	86	30	507	158.1	30	05	.	28	.	.	03	02	04	12	18	17	13	17	04	03	.	03	05	05		
II	8.1	8.0	6.0	7.5	-	05.9	95	75	93	87	31	567	109.9	13	01	.	20	.	.	02	01	01	14	20	19	13	09	01	.	03	01	03	05		
III	5.7	6.2	4.7	5.5	-	05.0	89	56	80	75	25	503	118.8	18	.	.	14	.	.	02	01	06	09	17	12	10	14	04	01	.	02	01	03	04	
IV	7.7	8.2	7.0	7.6	-	04.5	88	66	86	80	40	433	139.0	28	.	.	03	.	.	01	01	01	13	20	20	11	20	01	.	03	01	03	03		
V	6.8	7.6	5.8	6.7	-	08.4	68	90	81	40	458	114.5	23	.	.	01	.	.	02	.	01	08	19	18	11	19	.	.	.	04	08	02			
VI	5.2	5.4	3.5	4.7	-	11.1	78	59	89	75	38	091	045.0	16	.	.	08	.	.	02	03	08	05	02	08	.	.	.	03	03	.				
VII	2.4	4.3	1.9	2.9	-	10.9	71	49	81	67	26	006	052.9	16	.	.	18	03	.	01	12	01	01	01	01	.	.	.	01	01	.				
VIII	2.2	4.5	1.7	2.8	-	11.0	70	51	86	71	31	032	011.7	30	.	.	22	03	.	01	13	07	07	01	07	.	.	.	01	03	01				
IX	4.9	5.8	4.1	4.9	-	09.1	90	66	94	83	28	405	093.3	28	.	.	01	01	.	01	07	08	09	08	09	.	.	.	04	04	.				
X	4.3	4.6	3.0	3.9	-	07.2	90	60	92	81	27	198	064.3	02	.	.	08	01	.	03	02	13	07	10	10	05	10	.	.	.	02	01	.		
XI	3.1	3.6	2.2	2.9	-	04.6	95	58	93	82	20	181	069.9	28	.	.	27	.	.	05	15	06	05	04	03	05	01	.	.	01	03	.			
XII	7.5	7.6	6.7	7.3	-	05.7	97	76	96	90	36	498	108.9	17	.	.	16	.	.	05	04	02	20	12	18	06	03	.	05	03	02				
GOD.	5.4	6.0	4.3	5.2	-	07.4	87	63	89	79	20	3839	158.1	36	.	.	118	50	06	.	20	11	77	96	154	142	86	161	31	08	.	10	19	24	
NIKSIĆ																																			
BR. ST. 238																																			
I	6.5	6.5	5.7	6.2	095.3	04.1	83	70	82	78	21	273	103.8	30	.	01	20	.	.	11	06	07	13	15	07	12	08	04	.	.	.	04	06	11	
II	7.6	8.1	6.7	7.5	065.5	04.7	86	71	83	80	32	283	064.8	14	.	01	15	.	.	13	01	01	16	14	05	13	05	01	.	.	.	01	03	12	
III	5.6	5.8	5.9	5.8	166.9	04.8	79	54	76	68	18	220	063.1	18	.	.	04	09	04	.	15	19	05	08	16	14	07	15	03	03	.				
IV	8.0	8.5	7.7	8.1	091.1	06.5	84	65	82	77	34	321	061.1	14	.	.	04	09	03	.	13	13	07	07	13	11	08	13	.	01	03	.			
V	6.9	7.8	6.6	6.8	142.2	08.0	81	75	81	75	29	338	110.5	23	.	.	05	05	03	.	19	04	04	10	15	08	15	.	.	.	03	03	.		
VI	5.5	5.9	3.9	5.1	231.5	10.7	78	58	76	71	35	065	047.6	16	.	.	05	17	01	02	32	03	09	07	22	09	02	.	.	03	03	.			
VII	1.9	3.7	2.0	2.5	340.5	09.9	67																												

Mesec	Vremenski interval sat	Temperatura vazduha °C										Cestina pravaca i srednja jačina veta m/s, fm (0-12)																							
		TM			RH				Dat.			RH			Dat.			N		NE		E		SE		S		SW		W		NW		C	
		7	14	21	Sred. Giles)	RH1	RH2	RH3	Dat.1	Dat.2	Dat.3	RH4	Dat.4	Dat.5	Dat.6	N1	N2	E1	E2	S1	S2	SE1	SE2	S3	SW1	SW2	W3	W4	W5	NW6	C7				
$\varphi = 42^{\circ}22' N \lambda = 19^{\circ}15' E$ Gr., AG = + 1h 17 min.																									TITOGRAD-GOLUBOVCI		BR. ST. 241								
I	759.3	02.8	07.8	04.0	04.6	08.5	01.3	14.0	29	-05.6	09	16	03.9	04	02.8	04	02.2	10	02.3	07	01.9	01	02.0	01	02.0	03	03.0	47							
II	754.8	05.0	10.0	06.7	07.1	11.1	03.6	17.0	25	-06.9	16	15	02.5	05	01.8	04	02.5	09	02.6	07	02.3	04	02.5	05	02.5	34									
III	754.8	07.8	14.2	10.0	10.5	15.1	06.5	21.3	04	02.4	14	27	03.4	06	02.8	01	01.0	20	02.8	11	02.1	03	02.3	01	02.4	05	02.8	19							
IV	754.8	11.1	16.4	12.4	12.7	17.7	09.2	23.6	30	05.0	19	07	02.6	04	01.8	10	02.8	23	02.8	19	02.4	04	02.4	01	02.0	05	02.2	17							
V	757.5	14.8	20.0	15.4	16.4	21.3	11.8	27.7	01	04.8	13	22	02.0	04	02.3	14	02.7	17	02.1	05	02.6	01	01.0	05	01.6	22									
VI	757.5	20.8	24.5	21.1	22.4	28.0	17.1	31.5	20	11.6	29	17	01.8	03	02.0	02	04.0	21	02.6	20	02.2	05	02.4	06	02.5	16									
VII	757.5	23.2	29.7	24.1	25.3	31.2	19.6	35.0	13	14.8	01	32	02.4	09	02.7	01	02.0	10	02.4	21	02.2	07	02.0	06	02.2	07									
VIII	758.4	22.3	30.5	23.3	24.0	31.7	18.7	35.9	07	15.4	31	25	02.2	04	02.5	01	03.0	15	02.6	20	02.1	07	02.3	02	02.0	04	02.2	15							
IX	758.5	15.9	22.4	17.2	18.2	23.0	13.3	28.3	11	08.8	23	25	03.2	08	03.6	01	03.0	05	02.6	12	02.0	01	02.0	04	02.8	33									
X	761.2	11.8	19.1	13.6	14.5	20.1	10.2	25.6	03	03.8	30	24	03.2	08	02.5	05	02.6	09	02.0	07	02.1	06	01.8	04	02.5	33									
XI	765.4	03.3	13.9	06.4	07.5	14.8	02.1	19.0	02	-01.3	17	25	01.9	12	02.1	06	02.0	12	02.5	10	01.7	01	J2.0	06	02.8	20									
XII	757.5	05.9	16.8	07.0	07.7	12.0	04.2	16.9	30	-01.3	07	19	J2.3	09	02.6	05	01.6	06	02.5	03	01.7	03	02.0	05	01.8	40									
GOD.	758.4	12.1	19.4	13.4	14.3	19.6	09.8	35.9	07VII	-09.5	09.1	256	02.6	76	02.5	43	02.3	154	02.6	154	02.1	41	02.4	11	01.8	57	02.4	303							
$\varphi = 42^{\circ}26' N \lambda = 19^{\circ}17' E$ Gr., AG = + 1h 17 min.																									TITOGRAD		BR. ST. 242								
I	757.4	03.4	08.2	04.6	05.1	07.0	01.9	14.4	14	-05.5	09	19	04.6	04	05.0	01	01.0	06	03.8	04	02.2	01	02.0	02	01.5	08	01.4	48							
II	752.6	05.3	10.2	06.8	07.3	11.3	04.3	15.4	25	06.0	16	16	03.7	03	05.3	02	03.0	04	03.5	10	03.2	05	02.4	06	01.9	05	02.4	36							
III	755.7	08.1	14.4	09.9	10.6	15.5	06.9	22.6	04	03.0	14	19	04.2	06	05.0	03	03.3	06	02.5	14	03.2	05	01.8	05	02.4	35									
IV	752.9	11.0	16.1	12.2	12.9	17.7	09.4	23.6	12	05.4	20	13	02.6	02	03.5	03	03.0	18	03.4	13	02.8	01	02.0	07	02.4	35									
V	759.7	15.1	19.7	15.2	16.3	21.4	12.2	28.2	01	04.5	12	13	03.0	01	05.0	02	01.5	12	04.1	12	03.8	05	01.8	08	02.6	40									
VI	755.9	21.2	26.8	21.4	22.7	28.1	17.3	32.4	12	11.0	29	08	04.5	01	01.0	02	04.5	14	03.4	20	03.4	05	01.6	16	02.1	28									
VII	756.3	23.3	29.9	23.9	25.3	31.1	20.2	36.5	13	15.8	10	23	03.7	05	05.0	02	03.0	14	03.4	19	03.1	07	01.9	12	02.4	11									
VIII	756.6	22.7	30.8	23.7	25.1	31.3	19.8	35.6	07	15.0	31	21	03.1	02	04.5	02	05.5	18	03.3	21	03.0	01	01.0	06	02.2	11									
IX	756.7	16.2	22.4	17.2	18.2	24.0	13.7	28.6	11	09.5	12	29	04.6	05	02.0	07	03.3	12	02.8	05	01.8	08	02.6	26											
X	756.5	12.2	16.6	14.2	15.0	20.6	10.8	26.7	11	03.5	23	33	03.8	06	03.5	01	01.0	13	03.1	09	02.3	01	02.0	32	J1.5	11	03.1	17							
XI	763.8	03.1	14.6	06.4	07.7	15.2	02.2	19.6	16	02.0	16	20	02.8	04	01.5	01	01.0	18	01.8	13	02.1	03	01.7	08	02.2	23									
XII	755.6	06.0	11.0	07.4	08.0	12.0	04.8	17.6	30.14	-00.3	07	17	03.0	10	02.6	05	15	02.5	11	02.3	01	J3.0	04	01.5	18	02.2	17								
GOD.	756.6	12.3	18.6	13.6	14.5	19.8	10.3	36.5	13VII	-09.5	09.1	228	03.6	44	03.8	20	02.7	147	03.1	158	02.9	05	02.0	46	01.9	120	02.6	327							
$\varphi = 42^{\circ}30' N \lambda = 19^{\circ}32' E$ Gr., AG = + 1h 18 min.																									KLAŠIN		BR. ST. 243								
I	679.4	-04.0	01.7	-02.2	-01.7	02.6	-05.4	09.9	14	-17.0	10	22	03.1	05	02.0	04	02.2	06	02.3	01	01.0	01	01.0	01	01.0	01	01.0	50							
II	675.6	-01.8	01.0	00.0	00.3	04.3	-03.4	15.4	25	-10.6	16	25	02.2	05	02.0	04	02.0	06	02.8	14	02.1	01	04.0	05	01.0	31									
III	678.7	00.1	07.7	02.1	03.0	09.0	-00.7	16.0	04	-03.4	23	23	02.0	02	02.0	02	01.0	05	02.4	10	02.0	02	01.5	29											
IV	676.6	04.0	08.7	05.2	05.8	10.1	02.5	17.4	30	-01.8	21	18	02.1	01	01.0	01	01.0	05	02.6	22	02.0	07	01.0	01.0	03	05	35								
V	680.1	16.9	13.3	08.3	09.2	14.8	04.7	22.2	01	-03.4	13	19	01.9	05	02.0	04	02.7	05	02.4	06	02.0	08	01.0	03.0	30										
VI	681.6	11.5	19.2	12.2	13.9	21.2	08.3	25.2	25	11.10	04.6	04	01.4	04	01.0	01	01.0	05	02.5	06	02.0	08	01.4	03	04	39									
VII	683.0	11.4	22.2	13.1	15.0	23.6	07.2	29.6	12	03.8	26	23	02.4	05	02.0	04	02.9	06	02.0	16	02.2	07	01.0	10	01.7	28									
VIII	683.3	09.8	22.7	12.9	14.6	24.1	07.3	30.0	02	03.0	22	02	02.0	05	01.2	05	01.6	12	03.2	04	01.0	06	01.0	06	01.8	51									
IX	-	07.1	15.0	08.6	09.8	16.4	05.1	25.2	11	06.0	23	32	02.5	05	02.0	04	01.0	18	J1.3	04	01.0	03	01.0	03	01.0	32									
X	684.3	04.0	12.3	05.8	07.0	13.1	02.6	23.2	03	-04.1	23																								

Mjesec	Dnevni periodi u min.	Temperatura vjetračna °C										Gostina pravaca i srednja jedinica vjetra m/s, Pm (0-12)																						
		7	14	21	28	1	8	15	22	29	1	8	15	22	29	1	8	15	22	29	1	8	15	22	29	1	8	15	22	29	C			
$\varphi = 41^{\circ}31'N \lambda = 20^{\circ}32'E \text{ Crn. AG} = + 1h 22 \text{ min.}$																																		
I	-	-01.7	02.1	04.7	06.8	04.3	-02.1	00.8	29.15	-19.8	09	09	02.0	-	-	23	05.4	-	-	30	02.4	-	-	18	02.1	-	-	06	-	-				
II	-	-02.8	02.6	04.6	07.7	01.6	-02.8	01.6	24	-02.8	21	47	01.9	-	-	19	03.5	-	-	19	01.9	-	-	16	01.9	-	-	07	-	-				
III	-	-04.6	10.8	07.5	07.6	11.5	02.3	21.0	05.00	-02.8	14.19	27	01.2	-	-	21	03.0	-	-	35	02.0	-	-	17	02.2	-	-	07	-	-				
IV	-	-06.8	13.0	10.2	10.4	04.0	25.0	30	02.0	21.19	10	02.3	-	-	21	03.0	-	-	11	02.5	-	-	07	-	-	-	-	-	-	-	-	-		
V	-	10.8	16.7	12.3	12.4	18.2	07.2	25.0	21	02.0	14	13	02.0	-	-	12	03.1	-	-	26	02.7	-	-	32	02.0	-	-	10	-	-				
VI	-	14.6	22.5	18.3	18.7	24.8	11.0	30.3	12	02.0	28	22	02.0	-	-	05	04.0	-	-	25	04.1	-	-	26	02.2	-	-	12	-	-				
VII	-	15.9	26.8	21.2	21.7	27.8	11.0	30.3	19	02.0	10	22	02.0	-	-	04	04.0	-	-	24	01.8	-	-	26	01.9	-	-	23	-	-				
VIII	-	14.3	26.6	26.6	26.6	26.6	11.7	31.0	06	02.0	31	14	01.0	-	-	04	01.8	-	-	25	01.9	-	-	14	-	-	-	-	-	-				
IX	-	16.1	16.7	14.6	14.9	20.2	07.7	25.0	19	02.0	22	29	02.6	-	-	04	02.9	-	-	29	02.9	-	-	20	02.6	-	-	12	-	-				
X	-	04.7	16.1	11.4	11.5	16.9	04.5	26.0	07	-02.0	20.23	25	02.4	-	-	06	04.3	-	-	27	01.8	-	-	26	02.0	-	-	09	-	-				
XI	-	-06.7	02.2	02.2	02.2	02.2	-02.0	12.5	02	-02.0	22.21	50	02.0	-	-	15	01.9	-	-	16	02.1	-	-	16	02.1	-	-	09	-	-				
XII	-	02.2	07.5	04.6	04.6	04.3	02.0	15.0	22	-02.0	00.07	29	02.0	-	-	04	02.0	-	-	31	02.0	-	-	29	02.0	-	-	06	-	-				
GOD.	-	07.3	14.6	10.7	10.8	19.6	04.0	24.0	49.0	-13.0	09.1	203	02.1	-	-	04	03.0	-	-	340	02.0	-	-	250	02.0	-	-	122	-	-				
$\varphi = 41^{\circ}31'N \lambda = 20^{\circ}32'E \text{ Crn. AG} = + 1h 22 \text{ min.}$																																		
$\varphi = 41^{\circ}31'N \lambda = 20^{\circ}32'E \text{ Crn. AG} = + 1h 22 \text{ min.}$																																		
I	-	-01.3	09.1	-06.6	06.7	01.0	-02.0	10.0	20	-11.0	00.07	36	02.4	07	02.0	-	03	02.3	11	02.3	01	02.0	02	02.5	33	02.6	-	-	-	-	-	-		
II	-	-02.3	10.4	02.7	04.1	00.1	-02.3	10.0	12	-02.0	00	37	02.0	06	02.0	01	02.0	07	02.0	02	02.0	04	02.0	32	02.0	-	-	-	-	-	-			
III	-	-02.8	10.4	02.8	02.8	11.1	00.7	17.0	00	-02.0	16	26	02.1	06	02.0	31	03.0	-	18	01.9	07	02.1	03	02.0	31	02.0	-	01	-	-	-	-	-	
IV	-	-07.4	11.0	06.4	06.8	10.3	05.1	22.3	30	02.0	24	07	01.3	04	01.5	36	01.8	13	01.9	13	02.1	10	02.1	04	02.5	33	01.5	28	-	-	-	-	-	
V	-	11.4	12.1	12.1	12.7	20.6	07.0	24.0	20	04.0	11.05	05	01.6	04	02.0	05	02.0	07	02.4	10	02.1	02	02.0	04	02.0	34	01.5	-	-	-	-	-	-	
VI	-	22.7	17.7	17.8	17.8	20.8	04.0	28.0	12	02.0	29	37	01.7	02	04.5	04	01.5	06	02.0	13	01.8	13	02.3	09	02.1	32	01.5	41	-	-	-	-	-	-
VII	-	25.0	16.0	16.0	16.0	20.0	11.0	30.0	16	02.0	23.10	03	02.0	12	02.9	07	02.1	06	01.7	14	02.0	03	02.0	14	01.5	25	-	-	-	-	-	-		
VIII	-	15.6	20.6	17.0	17.0	21.4	06.0	30.0	11	02.0	05.00	05	01.6	05	02.4	06	02.0	36	02.7	17	02.7	03	02.7	02	04.5	33	01.5	18	-	-	-	-	-	-
IX	-	10.3	10.0	12.2	12.9	21.0	06.0	29.0	12	02.0	23	07	02.3	10	04.6	01	02.0	08	02.6	04	02.2	03	02.3	05	01.7	29	02.1	-	-	-	-	-	-	
X	-	05.3	10.0	09.3	10.2	16.4	05.2	26.0	03	-02.0	20	27	01.7	14	03.0	03	02.7	02	01.5	07	01.7	04	02.0	06	01.5	32	01.5	16	-	-	-	-	-	-
XI	-	00.5	07.2	07.2	07.2	10.5	02.0	22.0	02	-02.0	21.13	07	02.0	05	02.4	05	02.0	06	02.0	16	01.5	02	01.5	04	01.5	37	01.7	25	-	-	-	-	-	-
XII	-	03.0	07.7	04.0	04.7	09.0	02.0	19.0	19	-02.0	07	04	02.5	05	03.0	02	04.0	31	04.0	16	04.0	06	03.0	12	02.7	28	01.7	25	-	-	-	-	-	-
GOD.	-	07.5	14.6	09.0	10.0	16.0	04.7	24.0	46.0	-11.0	00.07	171	02.0	00	02.9	34	02.4	58	02.1	143	02.4	58	02.0	45	02.1	260	02.0	246	-	-	-	-	-	-
$\varphi = 41^{\circ}31'N \lambda = 20^{\circ}32'E \text{ Crn. AG} = + 1h 22 \text{ min.}$																																		
$\varphi = 41^{\circ}31'N \lambda = 20^{\circ}32'E \text{ Crn. AG} = + 1h 22 \text{ min.}$																																		
I	-02.7	-02.3	-02.1	-02.6	01.4	-05.0	10.0	19	-12.0	00	16	02.6	16	03.1	11	02.5	01	02.0	09	02.4	12	02.2	07	02.1	07	02.3	14	-	-	-	-	-	-	
II	-00.0	02.2	02.6	02.6	02.6	02.2	14.4	25	-02.0	00	12	02.6	11	03.0	11	02.3	06	01.8	08	01.8	07	02.0	05	01.8	06	02.3	16	-	-	-	-	-	-	
III	-00.1	02.7	03.1	03.0	03.0	02.1	-02.7	00.5	00	-02.0	19	25	02.2	12	02.5	18	02.4	11	01.8	04	02.0	14	01.7	04	01.8	16	-	-	-	-	-	-		
IV	-04.5	03.0	04.7	04.3	04.3	03.0	07.7	02.0	00	-02.0	16	24	03.0	04	02.7	05	03.0	19	02.2	02	02.5	07	02.3	16	02.1	12	-	-	-	-	-	-		
V	-09.2	11.6	10.3	10.3	12.7	06.0	17.0	06	-02.0	07	07	04	01.8	15	01.8	05	02.6	14	01.5	04	01.6	06	01.5	07	01.5	07	-	-	-	-	-	-		
VI	-19.6	17.0	17.5	17.5	19.5	12.2	20.6	25	-02.0	02	00	02.0	05	02.0	05	02.0	06	02.0	08	02.0	06	02.0	08	02.0	06	02.0	05	02.0	05	02.0	05			

Mes	Običajnost Hm (0-10)				Ispečenje broj	Vrijnost vrednosti				Podatkovne H m			Broj dana u Hm (0-10)												R T							
						U m				H m			Tn		Tn		Tn		Tn		Tn		P(0-12) Hm (0-10)		R m		R T					
	7	14	21	Skup (Dnev)		7	14	21	Skup (Dnev)	H m	Skup (Dnev)	Skup (Dnev)	<	<	<	<	<	<	<	<	<	<	<	<	<	<	<	<	<			
DEBAR																																
BR. ST. 251																																
I	6.9	6.5	7.2	6.9	-	34.6	34	75	78	79	49	128	035.0	31	03	04	17	.	.	.	03	04	03	17	03	05	06	03	01	.		
II	6.4	6.1	6.3	6.3	-	05.6	05	79	84	85	43	112	025.0	13	.	.	03	.	.	.	01	.	02	21	03	06	07	02	01	.		
III	6.2	6.2	6.9	6.5	-	05.6	01	62	70	72	28	109	055.0	22	.	.	04	.	.	.	01	.	03	13	03	07	07	02	02	.		
IV	6.2	7.9	6.3	6.1	-	06.6	78	88	75	73	46	113	018.0	16	.	.	01	.	.	.	01	21	13	07	13		
V	7.3	7.6	7.7	7.5	-	38.1	34	61	73	71	39	134	028.0	33	.	.	01	.	.	.	03	04	19	13	13	04	13	.	.	.		
VI	2.7	4.7	5.1	4.2	-	10.8	02	56	68	34	36	037	013.0	20	.	.	15	01	.	.	07	02	10	09	03	10		
VII	1.9	2.1	2.4	2.0	-	11.6	76	48	64	52	32	032	018.0	27	.	.	27	07	.	.	10	.	03	16	03	03	03	.	.	.		
VIII	2.5	2.9	7.7	2.7	-	11.5	78	55	62	65	43	063	003.0	12	.	.	23	04	.	.	14	02	01	01	01			
IX	5.9	5.8	5.9	5.6	-	09.1	08	63	72	74	47	137	026.0	14	.	.	01	.	.	.	04	10	07	07	07	05	.	.	01	.		
X	4.5	4.7	4.5	4.5	-	07.6	04	63	72	73	44	039	013.0	21	.	.	03	01	.	.	14	08	06	02	06	03		
XI	7.0	5.6	6.5	6.4	-	34.5	08	75	64	63	34	031	004.0	29	.	01	21	.	.	04	16	03	03	03	03			
XII	7.8	7.6	7.3	7.1	-	35.4	08	77	83	81	63	164	038.0	19	.	.	12	.	.	.	01	03	17	16	13	07	13	04	01	.		
GOD.	5.6	5.8	6.1	5.6	-	07.6	02	64	74	73	28	1100	055.0	22.0	03	05	71	71	12	.	07	07	78	140	90	94	90	13	04	.		
STRUGA																																
BR. ST. 253																																
I	5.2	5.7	5.6	5.8	-	03.9	75	63	81	73	24	000	024.0	30	02	.	10	.	.	.	11	16	11	03	08	04	01	.	.	01		
II	5.1	6.3	7.7	3.4	-	05.3	07	75	87	71	36	000	014.0	13	.	.	11	.	.	.	01	18	14	11	03	06	04	.	.	01		
III	5.6	5.3	5.3	5.3	-	05.2	03	64	81	76	39	161	028.0	20	.	.	09	.	.	.	07	09	11	11	07	11	01	.	.	01		
IV	6.4	6.2	6.1	6.2	-	36.3	03	62	76	74	31	078	013.0	06	.	.	03	.	.	.	03	08	17	15	01	17		
V	4.9	5.9	5.6	5.4	-	07.9	79	57	75	71	29	122	026.0	02	.	.	01	.	.	.	04	06	12	10	04	02	.	.	.	01		
VI	1.9	3.9	2.9	2.8	-	05.7	70	47	67	64	27	021	005.0	02	.	.	19	01	.	.	12	04	07	07	02	01	.	.	.	01		
VII	1.1	2.3	3.3	1.2	-	07.6	64	61	59	52	24	002	022.0	15	.	.	29	12	.	.	02	01	01	02	02	01		
VIII	1.0	3.9	1.3	2.0	-	07.7	71	43	67	60	25	030	027.0	12	.	.	29	06	.	.	02	19	03	01	01	01	.	.	.	03		
IX	2.6	4.7	3.6	3.4	-	06.7	85	56	76	73	28	104	029.0	21	.	.	06	01	.	.	03	02	12	12	09	04	05	.	.	01		
X	4.0	4.6	3.6	3.9	-	07.3	06	59	52	76	37	040	011.0	03	.	.	06	01	.	.	02	10	06	06	07	01	06	02	.	.		
XI	2.6	2.6	2.9	2.6	-	04.5	04	59	53	75	38	031	010.0	20	.	.	20	01	.	.	06	07	17	04	05	01	01	.	.	04		
XII	6.0	6.2	5.9	6.0	-	35.4	07	73	88	83	33	118	027.0	15	.	01	12	12	.	.	06	07	17	16	03	13	03	.	.	04		
GOD.	5.2	6.1	4.6	5.4	-	06.3	05	65	82	77	10	1264	049.2	22.0	06	04	23	134	08	.	.	04	05	100	150	128	47	102	77	09	.	.
NAVRVJ ANOV																																
BR. ST. 254																																
I	5.4	5.6	6.5	6.3	-	23.1	00	92	96	90	27	362	014.0	31	03	18	31	.	.	.	06	06	03	01	02	01	.	.	.	01		
II	6.6	6.2	6.2	6.4	-	25.6	07	91	82	86	87	32	029	015.0	27	12	12	27	.	.	.	06	19	20	16	09	09	13	.	.	01	
III	7.0	6.9	5.9	6.4	-	16.5	04	64	66	70	23	168	049.0	22	.	01	21	01	.	.	07	03	11	16	13	03	03	11	01	01		
IV	7.9	8.2	7.6	7.6	-	104.4	05	81	82	81	34	140	052.0	04	.	.	04	.	.	.	07	01	14	21	20	04	17	11	03	02		
V	4.9	5.7	7.3	5.3	-	09.1	94	95	95	92	32	135	037.0	03	.	.	01	.	.	.	03	15	15	05	13	06		
VI	2.0	2.6	7.4	6.6	-	14.6	95	95	95	93	33	045	046.0	04	.	.	02	.	.	.	02	14	09	04	10	01		
VII	1.9	2.2	2.2	2.6	-	19.3	83	82	67	66	28	044	032.0	23	.	.	07	.	.	.	04	10	01	02	01	02	01	.	.	01		
VIII	1.3	3.3	6.6	5.6	-	35.3	07	63	67	66	40	125	030.0	14	.	.	02	.	.	.	02	10	10	06	38	03	02	.	.	02		
IX	3.3	4.6	7.6	5.2	-	35.6	07	63	67	66	40	125	030.0	14	.	.	03	.	.	.	02	32	11	09	04	39	13	.	.	03		
X	4.3	4.2	2.6	5.4	-	04.8	71	26	71	71	37	045	022.0	28	01	03	10	.	.	.	02	34	03	03								

M	D	M	M	Temperatura vrednost °C								Cestina pravaca i srednja jedinica vetrov u m/s, Pm (0-12)																
				7	14	21	28	35	42	50	57	64	71	78	85	92	100	107	114	121	128	135	142	150				
$\varphi = 41^{\circ}50' N \lambda = 22^{\circ}02' E$ Grc, AG = + 1h 20 min.																												
I	-	-91.1	64.2	29.5	61.5	68.4	-93.0	12.6	20	-94.0	11	10	62.0	-	-	-	64	62.2	66	61.1	-	-	-	63	61.7			
II	-	-82.0	67.7	34.2	65.0	66.7	-93.0	11.2	27.1	-93.0	22	23	62.1	-	-	-	61	62.0	61	62.1	-	-	-	62	62.0			
III	-	-62.0	16.7	37.5	66.0	15.1	61.4	21.6	94	-93.0	14	24	62.5	61	61.0	-	62	62.0	10	61.9	62	62.5	-	62	62.0			
IV	-	-66.3	16.5	39.8	11.2	17.0	65.3	-	28	-93.0	20	20	61.9	-	-	-	62	62.0	-	-	-	-	-	62	62.0			
V	-	15.3	22.1	12.5	15.6	22.4	69.2	29.2	20	-92.0	13	20	62.2	-	-	-	62	62.3	-	-	64	61.8	-	-	74			
VI	-	17.0	26.4	16.1	20.9	28.7	12.5	34.2	25	67.4	61	10	61.9	-	-	-	64	61.5	62	61.3	63	62.3	-	-	71			
VII	-	19.4	31.6	20.1	22.0	31.8	14.1	36.2	67	69.6	21	20	61.6	-	-	-	62	61.3	-	-	-	-	-	62	61.6			
VIII	-	16.1	29.3	16.6	20.7	26.2	12.4	36.4	66	66.6	14	14	62.1	-	-	-	63	61.3	-	-	-	-	-	62	61.6			
IX	-	11.8	22.1	14.8	16.1	23.4	67.3	20.6	12	62.4	20.2	20	61.6	-	-	-	61	61.6	-	-	-	-	-	62	61.6			
X	-	66.7	19.7	22.3	11.2	17.0	67.6	21.6	64	-93.0	23	23	62.2	-	-	-	61	61.6	-	-	-	-	-	62	61.6			
XI	-	-66.4	64.1	31.9	62.4	77.1	-92.1	14.4	61	-97.2	24	24	62.2	-	-	-	61	61.6	-	-	-	-	-	62	61.6			
XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
SOB.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
$\varphi = 41^{\circ}54' N \lambda = 22^{\circ}02' E$ Grc, AG = + 1h 20 min.																												
I	-	66.2	65.7	22.9	62.9	62.2	-91.0	14.2	20	-92.0	11	21	61.7	62	61.6	61	62.0	-	-	62	62.0	-	-	63	61.7			
II	-	62.9	66.8	34.1	66.1	62.3	16.3	62.2	15.2	64	-93.0	21	20	61.6	63	61.0	-	63	61.3	-	64	62.2	-	63	61.2			
III	-	66.2	14.5	39.7	69.5	62.0	14.3	62.6	21.2	64	-93.0	14	23	61.4	64	61.3	-	61	62.0	61	61.0	64	61.4	63	61.2			
IV	-	16.4	16.5	12.3	15.4	17.0	67.5	62.2	20	62.3	20	20	61.2	61	64.0	-	60	62.0	-	60	62.0	61	61.0	60	60.9			
V	-	15.0	21.8	16.2	16.3	22.6	11.4	27.9	61	64.6	7.9	20	61.1	61	61.0	-	64	61.3	-	67	61.8	-	63	61.7				
VI	-	26.0	31.6	25.7	26.0	28.6	15.3	36.1	65	69.4	61	29	61.1	-	-	-	61	61.0	-	-	63	61.0	-	61	61.0			
VII	-	16.1	30.1	26.2	26.1	26.1	14.6	34.8	66	12.2	22	19	61.1	-	-	-	-	-	-	-	-	-	-	63	61.0			
VIII	-	15.7	27.9	22.5	22.6	22.6	15.3	34.4	66	12.2	22	19	61.1	-	-	-	-	-	-	-	-	-	-	63	61.0			
IX	-	15.7	22.3	17.8	17.7	22.7	16.7	26.2	12	64.6	26	19	61.1	-	-	-	-	-	-	-	-	-	-	62	61.0			
X	-	66.4	17.9	12.5	12.6	16.4	67.6	21.6	64	-93.0	22	22	61.0	61	62.0	-	61	61.0	-	62	61.0	-	62	61.0				
XI	-	-61.4	66.5	32.6	65.0	66.7	-93.0	15.6	26	-93.0	22	19	61.0	-	-	-	61	61.0	-	-	62	61.0	-	62	61.0			
XII	-	66.3	64.3	64.2	64.3	66.7	66.6	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
SOB.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-				
$\varphi = 41^{\circ}54' N \lambda = 22^{\circ}02' E$ Grc, AG = + 1h 20 min.																												
I	-	720.2	-91.7	64.5	61.6	61.7	65.5	-91.4	14.6	20	-91.0	11	21	64.3	65	62.0	61	62.0	15	64.7	67	69.1	66	62.2	13	64.1		
II	720.3	62.6	66.3	64.9	65.2	66.2	61.3	62.2	17.6	27	-93.0	21	21	61.0	62	62.0	-	15	63.3	15	65.1	-	62	62.3	19	63.0		
III	720.1	66.7	12.7	66.8	66.3	66.3	14.3	62.6	21.2	64	-93.0	14	23	63.4	61	62.0	61	62.0	12	64.5	13	64.6	62	62.0	27	64.1		
IV	720.2	66.3	16.7	11.6	11.7	11.7	16.3	67.3	21.6	20	61.0	19	20	61.6	63	61.0	64	64.5	14	64.0	15	64.1	62	62.1	31	63.1		
V	720.3	12.0	26.2	15.3	19.7	21.9	11.4	16.7	26.2	25	61.6	19	20	61.5	62	61.5	61	61.5	20	64.7	66	63.0	66	62.3	11	63.9		
VI	720.1	12.0	23.3	21.3	21.7	26.1	14.4	34.2	13	16.0	68	11	23.4	61	64.0	61	61.0	11	63.6	13	65.0	62	62.3	14	63.0			
VII	720.2	19.6	27.0	24.0	24.6	26.0	16.4	26.0	66	16.0	23	27	62.7	69	63.2	62	62.7	13	64.2	62	65.0	64	62.3	22	64.0			
VIII	720.4	17.4	27.9	22.5	22.6	26.3	15.3	34.4	66	16.4	20	61.6	62	62.0	62	61.5	14	64.6	63	62.0	62	61.5	31	63.5				
IX	720.2	12.8	21.1	16.3	16.3	22.6	11.1	20.5	12	64.5	23	13	61.6	61	62.0	-	12	64.2	61	62.0	62	62.0	01	61.6	25	62.7		
X	720.3	67.6	11.1	11.9	12.1	12.1	17.9	66.7	27.4	63	-93.0	20	23	60.6	65	61.6	61	61.0	16	63.7	62	64.0	61	62.0	17	63.0		
XI	720.1	-66.3	64.9	61.6	61.7	61.7	-64.5	15.6	61	-93.0	21	21	60.6	61	61.5	-	60	65.6	61	61.0	61	61.5	04	62.5	57	62.5		
XII	720.2	62.6	67.6	64.6	64.7	64.7	61.7	65.7	27.4	60	-93.0	21	21	60.6	61	61.5	-	61	65.6	61	61.0	61	61.5	19	63.5			
SOB.	720.0	66.0	16.2	11.9	12.2	17.4	67.2	26.0	64.6	63.6	-12.0	41	00	62.0	61	62.0	20	63.9	160	63.7	35	62.0	13	61.5	61	62.5	21	62.0
$\varphi = 41^{\circ}54' N \lambda = 22^{\circ}02' E$ Grc, AG = + 1h 20 min.																												
I	-	-66.4	65.3	21.9	62.2	62.7	64.7	-91.6	12.0	27	-94.0	11.9	27	62.5	-	-	-	14	63.1	-	-	66	62.1	-	-	75		
II	-	62.7	66.8	26.8	66.6	65.3	16.3	62.5	62.6	26	16	-93.0	23	23	62.1	-	-	-	12	62.9	-	-	66	62.1	-	-	56	
III	-	66.8	13.7	66.8	66.6	64.4	62.6	62.6	21.0	63.3	-93.0	14	23	62.4	-	-	-	11	62.5	62	62.0	63	62.5	-	66			
IV	-	16.4	12.3	12.3	17.0	16.0	66.3	23.4	30.6	66	19	20	62.3	-	-	-	13	62.7	62	62.5	62	62.5	01	62.5				
V	-	12.7	21.3	16.6	22.1	16.5	20.5	61.2	61.2	13	61	62.0	61	62.0	-	-	-	11	63.3	03	63.3	18	62.3	-	56			
VI	-	16.9	26.8	21.3	21.7	27.3	13.8	35.0	25	16.0	68	01	27	62.6	-	-	-	13	62.3	-	-	56	62.0	-	56			
VII	-	16.3	26.4	21.3	21.7	30.7	14.9	36.0	12.0	67	69.2	26	30	61.1	-	-	-	23	62.4	01	62.0	-	61	-	61			
VIII	-	16.1	26.6	21.0	26.3	29.7	12.0	34.0	67	16.0	16.14	04	62.5	61	62.0	-	-	21	62.5	-	-	-	62.5	-	57			
IX	-	11.5	21.0	16.4	16.4	22.9	67.0	30.6	66	66.6	23.82	35	28.6	61	62.0	-	-	19	62.5	-	-	33	62.3	-	71			
X	-	67.6	17.9	11.5	12.1	16.3	65.4	35.0	61	-93.0	21.0	20	61.9	-	-	-	67	62.9	-	-	65	62.2	-	61				
XI	-	66.3	65.6	61.9	62.6	64.6	-91.3	14.9	61	-94.0	23	24	63.0	-	-	-	63	62.0	-	-	63	62.0	-	63				
XII	-	62.3	65.8	65.8	65.2	67.0	61.1	15.0	17	-94.0	62	04	62.4	-	-	-	63	62.0	-	-	63	62.0	-	75				
SOB.	-	66.4	17.1	12.8	12.9	17.0	64.4	36.0	65.0	65.0	-																	

GOD.	Mjesec	Oblačnost mm (0-10)	Srednji jedinstveni sustav precip. mm/dan	Vlažnost vodonosnika			Podzemne vode mm	Broj dana u mjesecu																
				U g				Ta	Tz	Ts	Tz	Ts	Ta	P (0-12)	mm (0-10)	R mm	•	+	•	Δ	▲	▲		
				7	14	21	28	7	14	21	28	7	14	21	28	7	14	21	28	7	14	21		
ERODIJA																								
BR. ST. 266																								
I	6-3	5-6	5-2	5-7	-	04-5	02	02	02	02	02	02	02	02	02	02	02	02	02	02	02	02		
II	6-6	7-0	6-7	6-8	-	05-5	02	02	02	02	02	02	02	02	02	02	02	02	02	02	02	02	02	
III	6-6	6-5	3-9	6-2	-	06-2	03	03	03	03	03	03	03	03	03	03	03	03	03	03	03	03	03	
IV	5-4	6-9	6-1	6-1	-	06-3	07	07	06	06	06	06	06	06	06	06	06	06	06	06	06	06		
V	4-7	6-7	5-7	5-7	-	11-4	05	02	02	02	02	02	02	02	02	02	02	02	02	02	02	02	02	
VI	2-0	4-3	4-6	3-6	-	12-9	07	03	03	03	03	03	03	03	03	03	03	03	03	03	03	03		
VII	1-2	1-6	1-6	1-5	-	12-5	07	02	02	02	02	02	02	02	02	02	02	02	02	02	02	02		
VIII	1-2	1-2	2-2	1-5	-	12-1	07	04	06	06	06	06	06	06	06	06	06	06	06	06	06	06		
IX	4-7	5-0	5-1	5-2	-	10-8	06	06	03	03	03	03	03	03	03	03	03	03	03	03	03	03		
X	3-4	2-9	2-6	3-0	-	06-3	07	03	03	03	03	03	03	03	03	03	03	03	03	03	03	03		
XI	5-7	5-6	4-3	5-2	-	04-3	04	03	03	03	03	03	03	03	03	03	03	03	03	03	03	03		
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
KAVADARCI																								
BR. ST. 267																								
I	7-0	6-6	6-6	6-8	-	04-5	03	04	07	07	07	07	07	07	07	07	07	07	07	07	07	07		
II	7-4	7-0	6-7	6-3	-	05-4	02	06	06	06	06	06	06	06	06	06	06	06	06	06	06	06		
III	6-6	5-2	5-1	5-6	-	05-8	03	04	05	05	05	05	05	05	05	05	05	05	05	05	05	05		
IV	6-5	6-1	5-0	5-9	-	06-2	07	02	02	02	02	02	02	02	02	02	02	02	02	02	02	02		
V	5-4	6-8	4-9	5-7	-	06-9	02	03	04	04	04	04	04	04	04	04	04	04	04	04	04	04		
VI	-	-	-	-	-	17-3	08	09	08	08	08	08	08	08	08	08	08	08	08	08	08			
VII	1-3	1-3	0-9	1-2	-	16-1	05	07	07	07	07	07	07	07	07	07	07	07	07	07	07			
VIII	1-1	1-6	1-1	1-3	-	16-1	05	07	07	07	07	07	07	07	07	07	07	07	07	07	07			
IX	5-2	5-0	4-6	4-9	-	11-2	09	09	04	04	04	04	04	04	04	04	04	04	04	04	04			
X	4-6	5-3	3-7	6-3	-	10-2	06	06	02	02	02	02	02	02	02	02	02	02	02	02	02			
XI	9-5	7-7	7-7	6-3	-	02-2	09	02	02	02	02	02	02	02	02	02	02	02	02	02	02			
XII	7-0	7-6	6-6	7-0	-	03-6	07	04	04	04	04	04	04	04	04	04	04	04	04	04	04			
GOD.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-			
STIP																								
BR. ST. 268																								
I	6-8	6-9	5-3	6-3	-	102-8	04-8	03	04	04	04	04	04	04	04	04	04	04	04	04	04	04		
II	7-3	7-3	6-4	7-1	-	391-2	05-0	04	03	03	03	03	03	03	03	03	03	03	03	03	03	03		
III	6-3	6-4	4-1	5-6	-	05-4	02	03	04	02	02	02	02	02	02	02	02	02	02	02	02			
IV	6-9	7-0	6-8	7-0	-	159-8	07-0	05	05	05	05	05	05	05	05	05	05	05	05	05	05			
V	5-7	7-2	5-0	6-0	-	230-5	04-8	07	05	05	05	05	05	05	05	05	05	05	05	05	05			
VI	2-7	3-6	3-6	4-0	-	308-0	06-4	06	06	06	06	06	06	06	06	06	06	06	06	06	06			
VII	2-3	2-8	2-0	2-4	-	376-3	05-4	06	20	02	04	04	17	01	01	01	01	01	01	01	01			
VIII	2-0	2-9	2-0	2-7	-	325-0	09-7	04	35	07	50	25	01	01	01	01	01	01	01	01	01			
IX	5-6	5-0	4-5	5-0	-	201-0	08-9	03	47	05	05	31	01	01	01	01	01	01	01	01	01			
X	4-0	3-1	3-6	4-6	-	137-7	07-4	01	51	71	05	05	02	02	02	02	02	02	02	02	02			
XI	8-1	6-8	6-1	7-0	-	04-6	02	06	06	05	05	05	05	05	05	05	05	05	05	05	05			
XII	7-0	7-6	6-7	7-1	-	077-9	03-4	05	73	05	05	19	01	01	01	01	01	01	01	01	01			
GOD.	5-3	5-9	4-7	5-6	-	07-2	00	52	06	06	15	365	01-8	02	02	04	04	04	04	04	04			
DENIR KAPIJA																								
BR. ST. 269																								
I	6-9	6-9	4-8	6-2	-	04-3	02	02	03	03	03	03	03	03	03	03	03	03	03	03	03	03		
II	7-6	7-1	6-2	6-9	-	05-4	03	04	05	05	05	05	05	05	05	05	05	05	05	05	05	05		
III	5-9	5-7	3-8	5-1	-	05-4	02	03	03	03	03	03	03	03	03	03	03	03	03	03	03	03		
IV	7-0	6-8	5-8	6-6	-	07-3	05	04	04	04	04	04	04	04	04	04	04	04	04	04	04			
V	5-3	6-0	4-8	5-7	-	06-1	02	03	04	04	04	04	04	04	04	04	04	04	04	04	04			
VI	2-9	4-7	2-7	3-6	-	112-2	05	20	05	05	05	05	05	05	05	05	05	05	05	05	05			
VII	2-0	3-2	3-0	2-2	-	10-8	01	01	04	04	04	04	04	04	04	04	04	04	04	04	04			
VIII	2-0	2-9	1-9	2-3	-	10-6	08	33	02	01	01	01	01	01	01	01	01	01	01	01	01			
IX	4-7	5-2	3-6	4-5	-	06-8	02	06	06	07	31	01	01	01	01	01	01	01	01	01	01			
X	3-0	3-2	2-8	4-3	-	06-8	05	55	03	03	03	03	03	03	03	03	03	03	03	03				
XI	8-5	7-7	6-6	7-6	-	04-8	07	73	03	04	04	04	04	04	04	04	04	04	04	04				
XII	7-4	7-6	5-9	7-0	-	03-5	06	72	05	05	04	04	04	04	04	04	04	04	04	04				
GOD.	5-3	5-8	4-2	5-2	-	07-7	77	52	67	65	20	340	037-3	26-X	02	02	04	04	04	04	04			
ROCANI																								
BR. ST. 270																								
I	7-0	6-9	6-3	6-7	-	04-5	03	07	06	01	52	02	02	02	02	02	02	02	02	02	02	02		
II	7-0	7-0	7-7	7-6	-	05-6	02	06	06	06	36	03	03	03	03	03	03	03	03	03	03	03		
III	6-2	5-8	5-9	6-0	-	04-3	02	06	05	73	42	02	02	02	02	02	02	02	02	02	02	02		
IV	6-0	6-7	7-2	6-7	-	07-2	75	58	69	67	28	04	04	04	04	04	04	04	04	04	04	04		
V	5-3	6-2	7-5	6-3	-	06-8	05	48	68	64	20	04	04</td											

M	D	M	Temperatura vrednost °C								Gostina pravaca i srednje jedinice vetrova m/s, Pa (0-12)																							
			S				W				N			NE			E			SE			S			SW			W			NW		
			7	14	21	28	8	15	22	29	3	10	17	24	8	15	22	29	3	10	17	24	8	15	22	29	3	10	17	24	8	15	22	29
$\varphi = 41^{\circ}38' N \lambda = 22^{\circ}27' E$ Gr. AG = + 1h 30 min.																																		
I	-	-88.4	84.2	81.0	81.5	85.3	-83.1	11.5	20	-18.6	00	17	04.5	-	-	10	02.5	-	-	06	04.6	-	-	09	03.2	-	-	51						
II	-	-82.4	87.9	88.6	84.9	88.5	-82.3	14.5	13	-20.5	22.10	12	03.5	-	-	11	02.2	-	-	09	03.3	-	-	15	03.3	-	-	37						
III	-	-84.8	82.8	87.9	88.3	82.7	-80.2	10.5	04	-04.5	20.14	24	04.6	-	-	10	02.0	03	04.0	05	02.4	-	-	12	03.8	02	03.8	36						
IV	-	-10.0	10.2	10.2	11.2	16.1	83.3	23.6	28	-02.5	19	11	02.6	-	-	22	03.1	01	02.0	05	03.6	-	-	11	03.3	02	03.5	30						
V	-	-12.4	19.9	14.1	15.1	21.5	84.7	25.5	29.15	08.2	13	14	03.0	-	-	10	03.2	-	-	13	03.7	-	-	19	03.3	03	03.0	31						
VI	-	-17.4	23.6	20.6	21.1	26.9	18.2	31.0	23.13	06.0	01	13	04.0	-	-	06	02.0	-	-	06	03.8	01	03.0	10	04.3	06	04.7	44						
VII	-	-19.2	26.7	23.3	23.7	26.4	12.3	34.0	04	-04.5	23.23	16	03.4	-	-	06	03.7	-	-	06	03.6	-	-	13	04.1	04	03.5	44						
VIII	-	-17.1	27.7	26.6	21.9	26.7	16.6	33.5	05.04	04.5	14	14	04.4	02	03.0	07	02.7	-	-	07	03.3	-	-	11	04.4	04	03.5	46						
IX	-	-13.6	21.0	16.3	16.8	23.8	07.1	29.9	04	01.5	20.22	12	03.5	-	-	06	02.8	01	02.0	01	03.0	21	04.1	04	03.8	42								
X	-	-9.2	16.2	11.7	17.9	23.5	12.3	26.0	04.02	-02.0	20	01	04.2	-	-	07	01.9	02	03.0	06	02.0	01	04.0	13	03.7	01	03.8	31						
XI	-	-01.5	05.8	02.6	02.6	07.2	-04.6	17.8	29	-09.0	16	16	04.9	-	-	01	02.0	01	02.0	01	02.0	27	04.3	14	04.6	31								
XII	-	-02.6	06.6	03.9	04.4	07.6	-02.5	17.6	26	-09.5	07	07	03.7	-	-	04	02.2	01	02.0	02	03.0	-	-	17	04.1	-	-	42						
ODS.	-	-9.2	15.9	11.4	12.0	17.2	03.4	34.6	06.00	-15.0	09.1	17.3	04.0	02	03.0	104	02.6	07	03.2	45	03.4	03	03.3	178	03.9	01	04.9	317						
$\varphi = 41^{\circ}38' N \lambda = 22^{\circ}27' E$ Gr. AG = + 1h 30 min.																																		
$\varphi = 41^{\circ}38' N \lambda = 22^{\circ}27' E$ Gr. AG = + 1h 30 min.																																		
I	-	81.2	87.8	82.8	82.6	87.8	-80.2	15.8	20	-11.8	11	02	03.8	-	-	01	01.0	13	01.1	04	01.8	04	01.0	-	-	22	03.6	47						
II	-	82.5	10.8	88.3	86.2	10.6	82.4	12.6	14	-04.0	23	11	03.1	-	-	02	01.5	12	01.2	03	01.0	02	01.5	-	-	23	03.3	31						
III	-	86.7	15.3	86.8	87.7	15.2	87.8	25.0	04	-02.6	17	04	03.2	02	01.5	-	-	21	01.3	02	01.0	03	01.5	-	-	21	03.6	36						
IV	-	86.7	16.4	12.2	12.6	17.5	87.9	23.5	28	02.0	20	01	02.6	06	01.4	05	01.8	03	01.7	01	01.0	-	-	11	03.6	34								
V	-	15.6	22.3	19.3	17.1	23.0	11.0	27.8	24	03.8	13	03	03.2	02	02.0	01	01.0	26	01.7	05	01.8	01	02.0	-	-	23	02.9	32						
VI	-	20.7	26.7	21.4	21.6	23.0	19.8	32.9	19	03.4	01	13	02.3	02	01.5	02	01.0	19	01.7	01	04.0	01	02.0	29	02.8	36								
VII	-	21.7	26.3	23.6	24.9	21.7	18.0	30.8	06	01.8	21	04	02.0	02	01.5	02	01.0	12	01.8	02	02.0	04	01.5	-	-	26	03.2	39						
VIII	-	19.9	20.0	21.2	22.7	20.3	19.3	34.1	09	01.7	24	02	02.0	06	02.0	01	01.0	14	01.8	03	01.0	-	-	01	04.0	22	02.6	44						
IX	-	15.0	23.6	16.4	17.7	24.2	12.5	27.5	07	03.8	20	01	04.0	01	03.0	01	01.0	12	01.3	-	-	-	-	-	-	-	29	03.1	36					
X	-	86.6	19.4	11.6	12.8	20.7	07.1	24.6	08	00.0	20	01	04.0	-	-	01	04.0	-	-	01	03.8	-	-	-	28	04.1	36							
XI	-	82.3	16.5	9.6	9.6	11.0	00.4	-	-	-	-	-	-	-	-	-	-	02	01.5	-	-	02	01.5	-	-	-	27	03.1	45					
XII	-	82.5	16.0	9.7	9.8	11.1	02.6	19.0	18	-05.2	04	04	-	-	-	-	02	01.7	21	02.0	08	01.6	19	02.2	-	-	28	02.6	45					
ODS.	-	11.4	18.9	12.4	13.5	19.3	00.0	37.6	06.01	-08.2	01.1	14	02.8	122	01.9	20	02.0	04	02.1	02	02.3	04	02.1	03	03.0	246	03.2	349						
$\varphi = 41^{\circ}38' N \lambda = 22^{\circ}27' E$ Gr. AG = + 1h 31 min.																																		
$\varphi = 41^{\circ}38' N \lambda = 22^{\circ}27' E$ Gr. AG = + 1h 31 min.																																		
I	-	-31.5	93.1	97.7	91.2	96.3	-82.3	14.6	20	-12.0	00	15	02.4	02	01.5	07	01.1	07	01.7	11	02.1	01	01.0	03	01.3	10	02.7	37						
II	-	-9.1	9.5	9.5	9.5	10.3	91.2	12.6	14	-04.0	23	14	01.6	03	01.7	08	01.2	05	01.8	08	02.6	04	01.5	14	02.1	29	01.7	42						
III	-	-05.9	15.0	9.5	9.7	16.7	92.8	21.0	19	-05.0	14	03	04.6	03	03.0	03	02.3	05	02.0	09	02.4	10	02.3	04	01.8	24	02.9	22						
IV	-	-10.4	15.7	11.6	11.8	16.7	96.2	24.6	20	-06.4	21.17	1	-	-	-	13	03.4	04	01.8	07	01.9	12	02.6	04	02.3	13	02.3	20						
V	-	-13.2	21.5	15.5	16.4	22.6	09.6	27.0	25	06.8	13	05	01.6	03	01.3	04	02.0	03	02.4	16	02.4	11	02.5	08	01.9	17	02.1	26						
VI	-	-16.3	27.2	20.4	21.6	26.4																												

M	D	J	Temperatura vremena °C								Gostina pravaca i srednja jedinica vetrova m/s, fm (0-12)																
			7	14	21	28	9	16	23	30	9	16	23	30	9	16	23	30	9	16	23	30	9	c			
$\varphi = 41^{\circ}36' N \lambda = 22^{\circ}46' E$ Gr. $\Delta G = + 1h 31 min.$																											
DELČEVO																											
I	-	-01.7	03.8	-01.2	-00.3	00.1	-00.8	10.8	15.14	-14.5	10	14	02.6	03	04.0	06	01.7	04	03.0	13	01.5	03	01.7	09	01.7	08	02.3 30
II	-	01.9	07.7	02.2	02.9	00.1	-00.7	10.8	13	-07.0	22	08	01.9	06	01.8	06	01.3	07	04.3	09	02.1	05	02.4	12	02.3	04	02.8 27
III	-	02.9	11.5	05.0	04.4	12.3	00.2	21.0	00	-02.5	14	22	03.0	03	02.3	04	02.0	07	04.1	16	02.4	06	02.5	04	02.3	05	02.6 25
IV	-	02.5	12.9	05.0	04.7	12.7	03.8	21.3	00	-02.5	20	19	02.1	03	03.0	13	01.3	06	03.2	19	02.2	02	04.0	02	01.9	07	02.6 22
V	-	11.7	09.2	13.1	14.3	19.7	07.4	26.0	01	-01.0	13	06	01.6	02	02.0	12	01.4	04	02.5	14	03.5	05	02.8	17	02.3	02	02.5 20
VI	-	15.4	24.1	16.0	18.3	26.7	00.9	30.0	13	06.0	01	12	02.2	02	01.2	08	02.8	10	01.0	01	03.0	10	02.6	06	02.2	22	
VII	-	17.0	26.5	19.0	20.6	27.1	11.0	34.0	07	03.5	23	10	03.5	05	03.4	13	03.6	07	03.6	09	01.8	09	01.8	07	03.0	27	
VIII	-	14.3	25.8	18.0	18.9	26.5	10.0	31.3	00	06.0	17.14	15	01.9	04	02.2	07	01.1	04	03.2	18	02.3	03	03.7	00	01	02.0 39	
IX	-	09.0	19.5	12.5	13.6	20.7	00.9	26.5	12	00.0	23	15	02.5	05	02.2	03	01.0	03	02.3	16	01.8	02	02.0	07	01.9	05	02.0 36
X	-	04.3	14.0	06.1	09.1	16.7	02.2	27.0	02	-03.5	20	16	02.6	05	02.0	04	01.2	03	02.3	14	01.9	02	02.0	04	02.2	02	02.5 43
XI	-	-03.3	03.1	-00.3	01.0	08.5	-00.7	14.3	01	-1.0	21	15	02.5	03	01.0	01	01.0	03	02.3	02	02.5	01	01.5	06	02.2	23	
XII	-	00.1	04.7	02.5	03.0	07.6	-01.5	18.5	20.17	-0.5	09	05	02.0	02	01.3	07	01.1	02	03.5	12	02.2	01	02.0	01	02.0	02	04.0 41
ODS.	-	04.4	15.2	09.0	09.7	19.7	03.3	34.0	07AM	-14.5	40.1	160	02.4	43	02.6	02	01.3	58	01.2	152	02.2	36	02.9	02	02.1	30	02.0 432
$\varphi = 41^{\circ}43' N \lambda = 22^{\circ}51' E$ Gr. $\Delta G = + 1h 31 min.$																											
BERNOVO																											
I	009.8	-02.5	02.0	-02.2	-01.2	02.4	-02.4	09.9	14	-14.7	11	14	02.2	07	01.0	00	02.7	14	01.0	01	02.0	01	02.0	11	01.0	32	
II	009.1	-00.6	06.4	01.6	02.3	07.4	-02.0	14.0	20	-12.5	10	09	02.2	09	01.0	03	01.7	08	03.1	12	02.0	06	02.0	02	01.0	06	01.3 26
III	007.2	01.2	09.4	03.0	04.3	10.7	-00.6	16.9	04	-03.6	14	17	02.5	07	01.0	06	02.2	14	02.0	03	02.3	01	01.9	00	01.7	00	01.7 25
IV	005.0	05.1	11.5	07.0	07.7	12.0	02.7	16.0	20.12	-03.7	20	09	01.6	12	01.0	03	02.0	24	02.1	03	01.7	03	01.4	19			
V	008.6	09.9	17.1	11.0	12.2	18.2	04.4	24.7	01	-02.7	13	06	01.8	00	01.5	01	02.0	09	01.0	15	02.5	01	01.0	03	02.0	11	01.6 37
VI	009.6	15.0	21.6	14.9	16.3	23.0	00.7	27.0	12	04.6	01	06	02.0	06	01.1	04	01.2	04	02.0	09	03.1	01	01.0	02	02.0	17	01.8 39
VII	009.6	15.1	24.3	16.8	18.3	25.4	05.6	31.7	07	04.0	23	22	01.7	00	01.2	01	02.0	07	01.1	05	02.7	05	02.4	01	01.6	25	
VIII	001.5	12.4	25.6	15.4	16.7	24.7	00.6	30.0	00	04.0	14	14	01.5	05	01.0	00	01.2	06	01.0	03	01.7	03	01.6	09	01.6 47		
IX	009.8	00.0	17.4	10.6	11.9	18.6	04.3	24.2	07	00.0	23	20	02.5	03	01.0	00	02.0	02	01.0	06	02.3	04	02.2	01	01.5	46	
X	009.6	02.9	16.6	06.8	07.3	15.3	01.3	24.6	03	-11.0	20	16	02.6	11	01.0	03	01.3	04	02.0	02	01.0	01	01.6	07	01.3 44		
XI	009.6	-03.6	06.9	-01.0	00.8	00.7	-00.6	14.7	10	-06.7	23	06	01.3	12	01.0	01	01.0	06	02.7	04	02.2	02	01.5	01	01.6	06	
XII	007.0	-00.7	03.7	01.0	01.7	04.7	-02.1	14.5	17	-0.6	02	05	01.4	14	01.1	01	01.0	03	02.0	11	01.0	02	01.5	07	01.1 46		
ODS.	009.5	05.1	18.6	07.1	08.2	14.7	02.4	31.7	07VII	-16.7	41.1	162	02.0	100	01.1	23	01.3	02	02.2	126	02.2	31	01.8	18	01.8	114	01.6 439

Mjesec	Oblačnost mm (0-10)					Temperatura °C	Vlažnost vrednjava	Padavine mm			Broj dana u mjesecu																								
	7	14	21	28	50			7	14	21	28	50	Ta	Tn	Ts	Tx	Ts	Tn	F(0-12)	R(0-10)	R mm	•	*	+	Δ	W	▲	R	T	■					
													<	<	<	>	<	>	<	>	<	•	*	+	Δ	W	▲								
DELCEVO																																			
BR. ST. 276																																			
I 6.7	5.5	6.2	6.1	-	04.0	70	80	87	82	35	037	015.0	22	04	04	27	-	-	04	07	11	06	01	02	06	-	03	10							
II 7.6	6.5	6.7	6.5	-	04.8	84	69	81	73	41	058	015.0	21	-	-	18	-	-	03	02	12	10	08	03	05	07	01	-	01	05					
III 5.5	5.5	5.0	5.4	-	03.1	82	53	75	70	29	044	020.2	20	-	-	13	-	-	07	01	01	08	03	09	03	-	01	01	02						
IV 5.8	6.0	7.1	6.3	-	04.6	83	61	72	72	33	058	018.5	17	-	-	03	-	-	01	01	01	09	17	14	01	17	-	01	01	02					
V 5.2	6.5	5.8	5.8	-	08.2	77	51	73	67	29	084	026.0	26	-	-	01	01	-	04	02	06	14	12	13	14	-	01	05	-	-					
VI 2.4	3.3	4.1	3.9	-	10.3	76	48	72	65	31	046	013.3	18	-	-	15	01	-	01	08	01	10	01	10	-	-	-	-	-	-					
VII 2.3	3.1	1.7	2.6	-	09.2	65	26	55	52	18	018	018.5	16	-	-	22	09	01	04	01	19	01	01	01	01	01	-	01	01	-					
VIII 3.7	2.2	3.3	-	-	10.7	78	52	62	64	21	036	026.2	12	-	-	23	03	-	01	13	31	33	32	01	32	-	-	-	-						
IX 5.6	6.5	2.9	6.3	-	09.2	89	62	80	77	37	136	029.0	00	-	-	04	-	-	01	01	09	03	11	16	06	11	-	02	06	-					
X 4.1	4.4	5.1	3.5	-	07.0	90	61	61	77	13	021	011.0	22	-	-	07	02	-	01	01	13	06	04	06	01	35	02	01	-	06					
XI 6.4	2.7	3.8	6.3	-	34.1	85	63	84	78	34	027	020.2	30	01	01	27	-	-	01	08	04	02	01	32	01	-	14	01	-						
XII 7.5	6.2	6.5	6.7	-	04.9	84	74	84	82	43	076	023.0	15	01	01	16	-	-	01	01	12	38	35	03	06	02	-	-	09						
GOD.	5.2	5.0	4.4	4.9	-	07.0	81	59	70	72	13	651	029.0	08.IX	07	05	114	67	13	01	24	05	86	72	100	80	23	05	21	02	-				
BERGOV																											$H = 824 \text{ m } H_0 = 828.3 \text{ m } h = 2.0 \text{ m } h_0 = 1.3 \text{ m}$								
BR. ST. 277																											$H = 824 \text{ m } H_0 = 828.3 \text{ m } h = 2.0 \text{ m } h_0 = 1.3 \text{ m}$								
I 6.6	6.5	5.6	6.2	-	116.4	83.6	89	66	88	81	34	044	020.4	22	04	04	29	-	-	01	04	12	13	07	01	03	10	-	01	01	20				
II 6.9	7.6	6.6	7.0	-	084.6	04.5	90	66	87	81	33	062	010.2	06	01	-	23	-	-	01	01	13	11	11	01	39	06	-	01	01	11				
III 7.0	7.3	6.4	6.4	-	162.3	44.7	94	54	81	73	29	048	013.6	28	-	-	18	-	-	01	02	10	06	07	03	04	07	01	-	03					
IV 6.1	7.9	6.8	6.9	-	04.0	89	60	82	77	34	076	026.0	17	-	-	04	-	-	01	01	11	19	14	01	19	-	01	01	02						
V 5.2	7.7	6.0	6.3	-	220.0	07.9	86	54	82	74	25	163	023.5	12	-	-	01	-	-	01	09	15	12	03	14	-	-	02	01						
VI 2.6	6.2	2.1	4.0	-	284.8	05.6	81	49	78	69	30	061	020.6	02	-	-	10	-	-	01	08	32	06	02	39	-	-	02	11	-					
VII 1.9	3.4	1.2	2.2	-	255.0	07.0	71	38	64	58	26	069	006.9	16	-	-	15	06	-	01	09	02	02	02	03	-	-	02	-	-					
VIII 2.8	4.4	1.4	2.9	-	314.6	07.0	84	40	71	63	23	034	029.0	12	-	-	12	01	-	01	13	01	04	02	01	04	-	-	06						
IX 5.5	6.0	6.1	5.2	-	196.8	08.1	89	56	86	77	36	160	020.7	14	01	-	11	-	-	05	08	13	11	03	13	-	-	-	01						
X 4.5	5.2	2.3	4.0	-	195.0	04.2	91	54	83	78	36	040	024.1	29	01	-	11	-	-	09	04	07	04	02	06	03	-	-	01	04					
XI 5.3	3.8	3.0	4.1	-	03.9	93	52	90	78	21	028	020.9	30	-	-	27	-	-	01	10	37	03	03	01	33	01	-	-	09	02					
XII 7.0	7.1	6.3	6.8	-	04.5	91	71	90	84	47	073	022.8	06	02	02	21	-	-	01	03	12	10	08	03	03	06	-	-	03						
GOD.	5.1	6.1	4.2	5.2	-	06.4	87	55	82	74	21	686	029.0	42.VII	08	08	134	46	09	02	01	77	89	114	89	23	06	35	01	-	01	03	23	16	39

